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## AEROSPACE STRUCTURES

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1. The semi-momocoque wing of Figure 1 is loaded by triangular pressure distribution. Compute the rotation angle of the section located at distance  $l$  from the encastre (i.e. the location from which the pressure load starts. Refer to Table 1 for the problem data, and assume reasonable values for any missing constant.

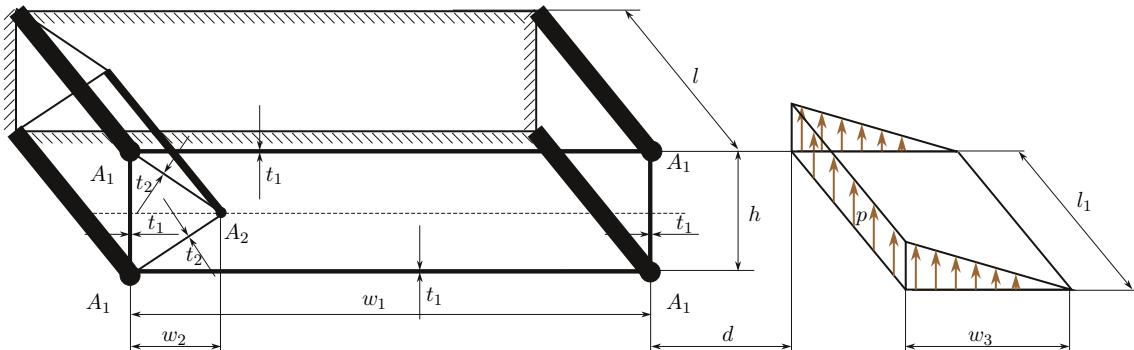


Figure 1: Loaded wing

$A_1$	$75 \text{ mm}^2$	$w_1$	$300 \text{ mm}$	$l_1$	$1100 \text{ mm}$	$E$	$72000 \text{ MPa}$
$A_2$	$100 \text{ mm}^2$	$w_2$	$40 \text{ mm}$	$w_3$	$60 \text{ mm}$	$\nu$	$0.3$
$t_1$	$1 \text{ mm}$	$l$	$3000 \text{ mm}$	$d$	$20 \text{ mm}$		
$t_2$	$0.5 \text{ mm}$	$h$	$60 \text{ mm}$	$p$	$2 \text{ MPa}$		

Table 1: Semi-monocoque wing data

2. The  $h \times w \times t$  solid of Figure 2 is joined to a beam with torsional stiffness  $GJ$ . The beam is loaded by a moment per unit of length  $m$ . Compute the vertical displacement and the rotation of the beam free extremity. Refer to Table 2 for the problem data, and assume reasonable values for any missing constant. Choose and justify a suitable structural model for the solid.

$t$	$5 \text{ mm}$	$GJ$	$22 \text{ Nm}^2$
$l$	$1000 \text{ mm}$	$E$	$72000 \text{ MPa}$
$h$	$700 \text{ mm}$	$\nu$	$0.3$
$w$	$30 \text{ mm}$	$m$	$4 \text{ N}$

Table 2: Semi-monocoque wing data

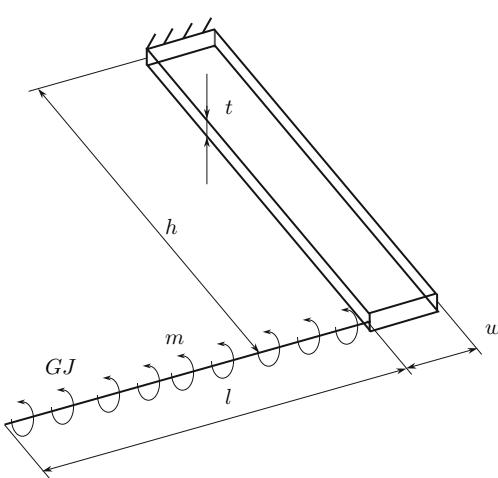


Figure 2: Cantilever bending

3. Define and derive the expression of the work-conjugated beam generalized deformation and internal actions starting from a kinematic beam model.