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奔跑的野兔

一、矢量分析

① 三种坐标系

直角 $\vec{r} = \vec{e}_x x + \vec{e}_y y + \vec{e}_z z$ $dS_x = dy dz$

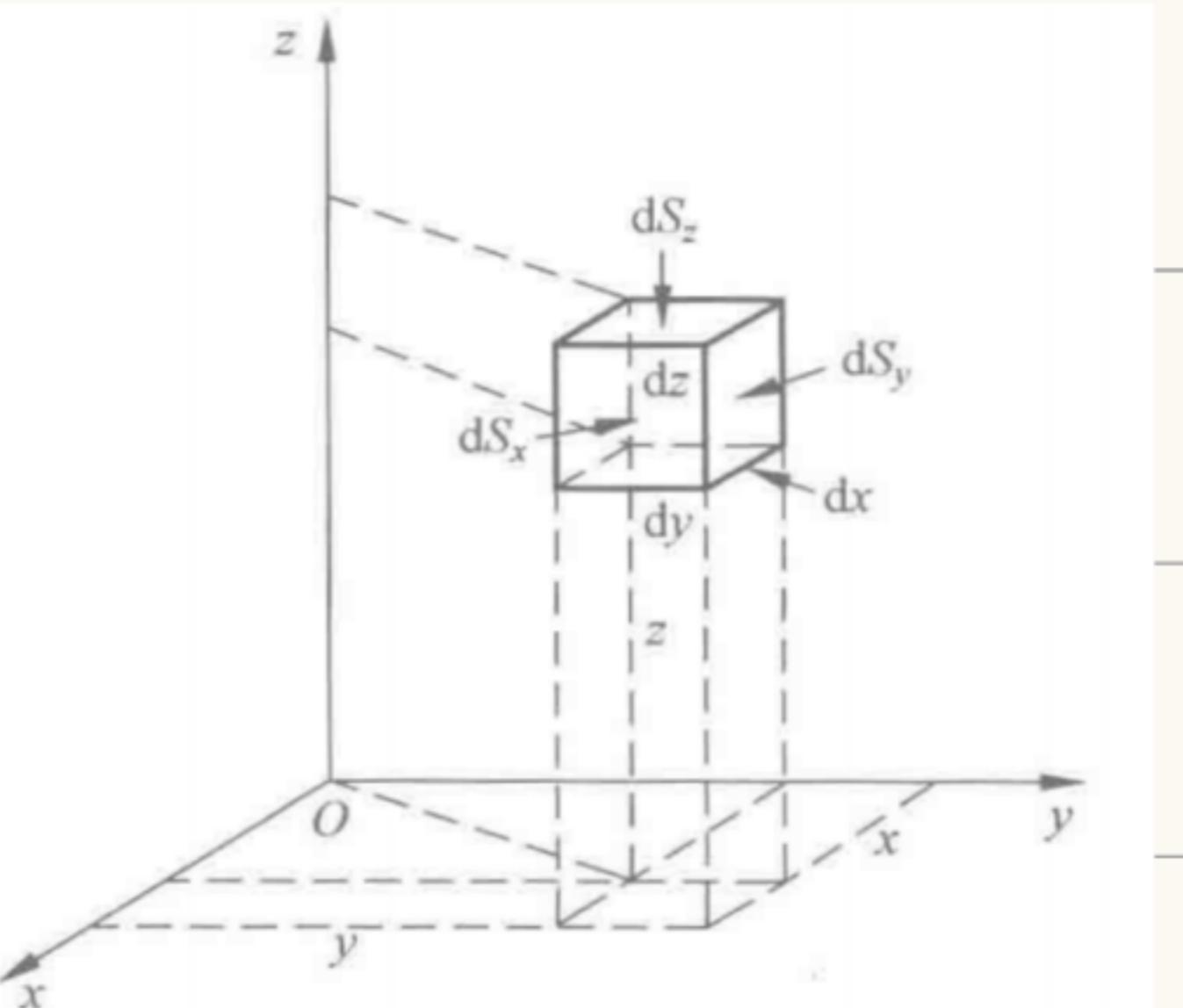


图 1.4 直角坐标系中长度元、面积元和体积元

圆柱 $r = \sqrt{x^2 + y^2}$, $\tan\varphi = \frac{y}{x}$, $z = z$

$$x = r \cos\varphi, y = r \sin\varphi, z = z \quad dS_r = r d\varphi dz$$

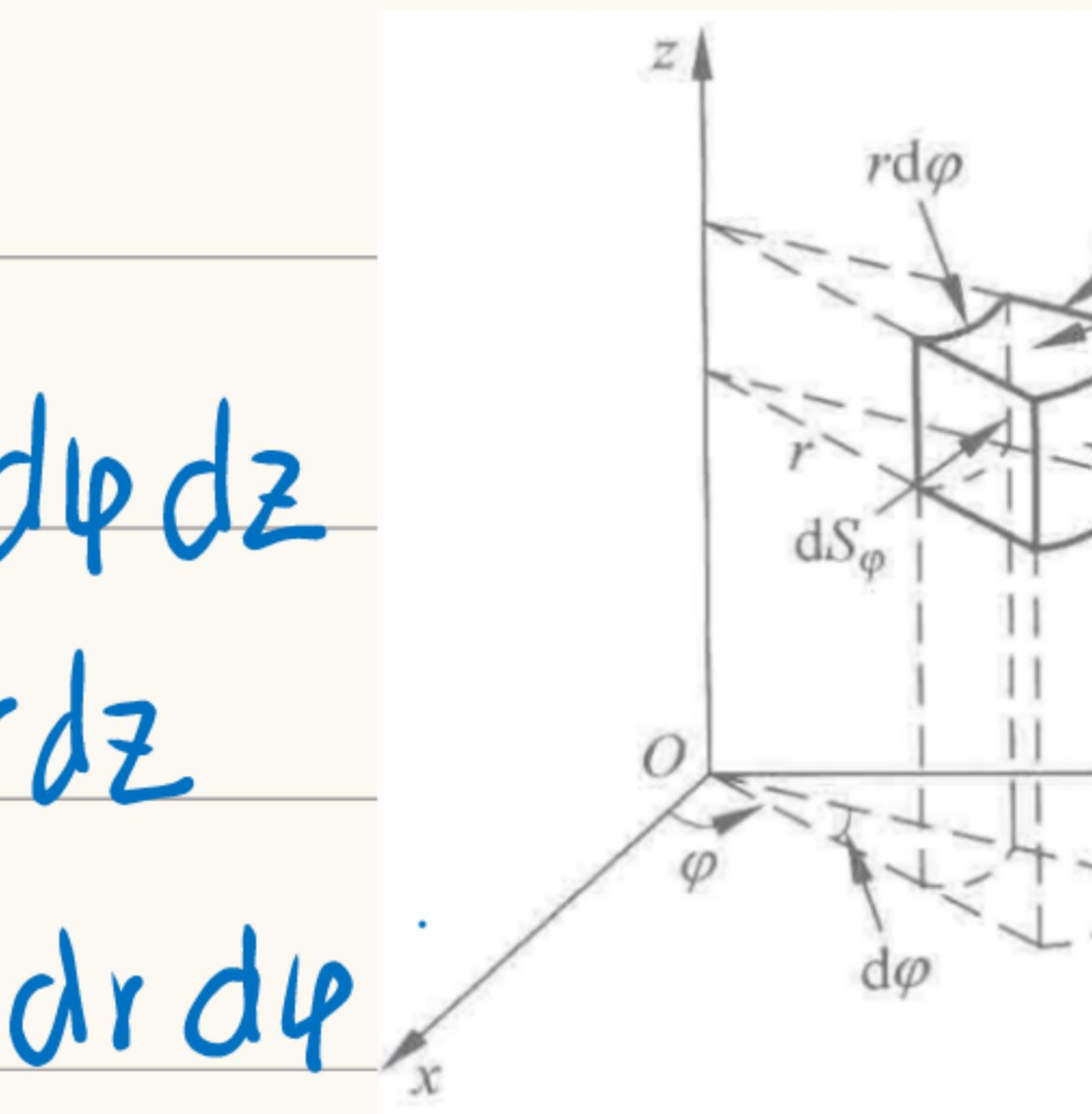


图 1.5 圆柱坐标系中长度元、面积元和体积元

$e_r \cdot e_r = e_\varphi \cdot e_\varphi = e_z \cdot e_z = 1 \quad dS_\varphi = dr dz$

$e_r \cdot e_\varphi = e_\varphi \cdot e_z = e_z \cdot e_r = 0 \quad dS_z = r dr d\varphi$

$e_r \times e_\varphi = e_z, e_\varphi \times e_z = e_r, e_z \times e_r = e_\varphi \quad dV = r dr d\varphi dz$

$$\begin{bmatrix} e_r \\ e_\varphi \\ e_z \end{bmatrix} = \begin{bmatrix} \frac{de_r}{d\varphi} = e_\varphi & \frac{de_\varphi}{d\varphi} = -e_r \\ \cos\varphi & \sin\varphi & 0 \\ -\sin\varphi & \cos\varphi & 0 \end{bmatrix} \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} \quad \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} = \begin{bmatrix} \cos\varphi & -\sin\varphi & 0 \\ \sin\varphi & \cos\varphi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} e_r \\ e_\varphi \\ e_z \end{bmatrix}$$

球 $r = \sqrt{x^2 + y^2 + z^2}$, $\tan\theta = \frac{\sqrt{x^2 + y^2}}{z}$, $\tan\varphi = \frac{y}{x}$

$$x = r \sin\theta \cos\varphi, y = r \sin\theta \sin\varphi, z = r \cos\theta$$

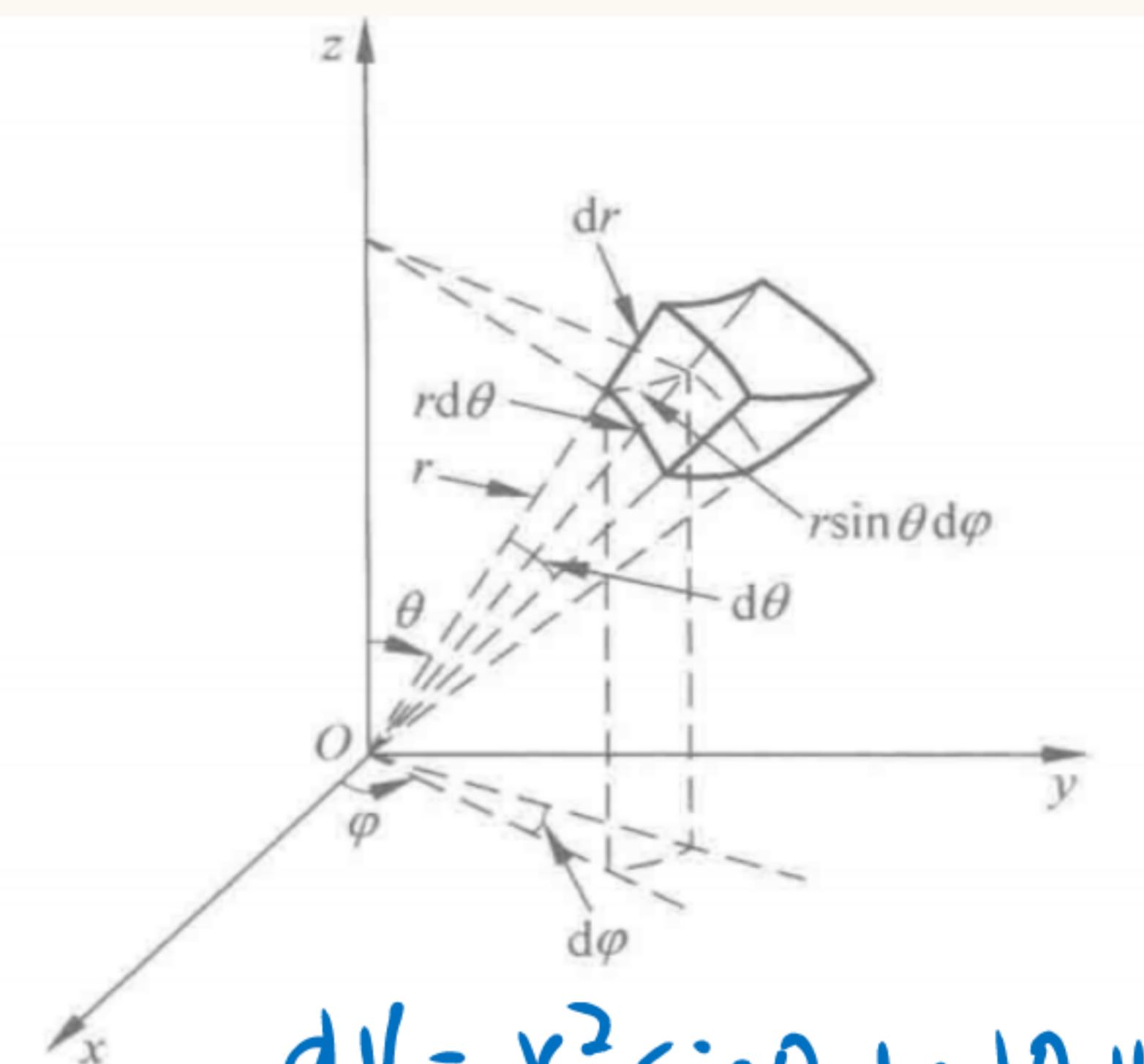


图 1.6 球坐标系中长度元、面积元和体积元

$e_r \cdot e_r = e_\theta \cdot e_\theta = e_\varphi \cdot e_\varphi = 1 \quad dS_r = r^2 \sin\theta d\theta d\varphi$

$e_r \cdot e_\theta = e_\theta \cdot e_\varphi = e_\varphi \cdot e_r = 0 \quad dS_\theta = r \sin\theta dr d\varphi$

$e_r \times e_\theta = e_\varphi, e_\theta \times e_\varphi = e_r, e_\varphi \times e_r = e_\theta \quad dS_\varphi = r dr d\theta$

$$\begin{bmatrix} e_r \\ e_\theta \\ e_\varphi \end{bmatrix} = \begin{bmatrix} \sin\theta \cos\varphi & \sin\theta \sin\varphi & \cos\theta \\ \cos\theta \cos\varphi & \cos\theta \sin\varphi & -\sin\theta \\ -\sin\varphi & \cos\varphi & 0 \end{bmatrix} \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} \quad \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} = \begin{bmatrix} \sin\theta \cos\varphi & \cos\theta \cos\varphi & -\sin\varphi \\ \sin\theta \sin\varphi & \cos\theta \sin\varphi & \cos\varphi \\ \cos\theta & -\sin\theta & 0 \end{bmatrix} \begin{bmatrix} e_r \\ e_\theta \\ e_\varphi \end{bmatrix}$$

$$\frac{\partial e_r}{\partial \theta} = e_\theta, \frac{\partial e_r}{\partial \varphi} = e_\varphi \sin\theta, \frac{\partial e_\theta}{\partial \theta} = -e_r, \frac{\partial e_\theta}{\partial \varphi} = e_\varphi \cos\theta, \frac{\partial e_\varphi}{\partial \theta} = 0, \frac{\partial e_\varphi}{\partial \varphi} = -e_r \sin\theta - e_\theta \cos\theta$$

② 矢量微分

0. 矢量场方程

$$\vec{F} \cdot d\vec{r} = 0$$

$$\frac{\partial A_x}{\partial x} = \frac{\partial A_y}{\partial y} = \frac{\partial A_z}{\partial z}$$

1. 散度 矢量 \rightarrow 标量

\vec{n} 为面元单位法线矢量

$$\text{面元矢量 } d\vec{s} = \vec{n} dS \text{ 或 } dS = \vec{n} \cdot d\vec{s}$$

$$\text{通量 } d\Phi = \vec{A} \cdot d\vec{s} = A \cos\theta dS$$

$$\text{e.g. 电通量 } d\Phi_E = \vec{E} \cdot d\vec{s} \quad \text{磁通量 } d\Phi_B = \vec{B} \cdot d\vec{s}$$

穿过闭合曲面的通量 $\Phi = \oint \vec{A} \cdot d\vec{s}$

$$\text{e.g. 对于静电场 } \Phi_E = \oint \vec{E} \cdot d\vec{s} = \frac{q}{\epsilon_0}, \text{ 对于磁场 } \oint \vec{B} \cdot d\vec{s} = 0$$

$$\text{散度 } \operatorname{div} \vec{A} = \lim_{\Delta V \rightarrow 0} \frac{\oint \vec{A} \cdot d\vec{s}}{\Delta V} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \nabla \cdot \vec{A}$$

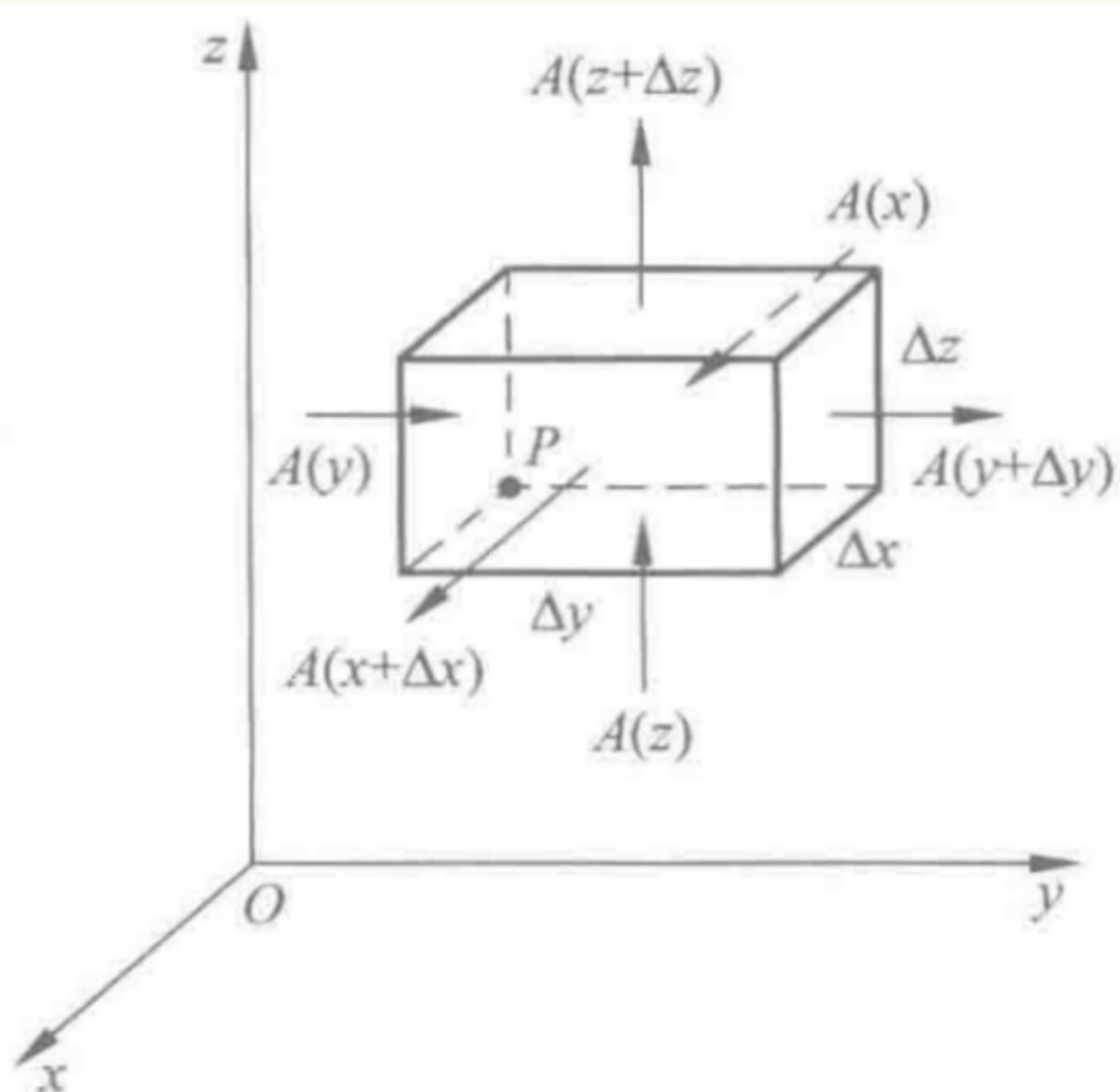


图 1.11 在直角坐标系内计算 $\nabla \cdot A$

$$\text{散度定理 (高斯定理)} \quad \oint \vec{A} \cdot d\vec{s} = \iiint_V \nabla \cdot \vec{A} dV \quad \text{闭合曲面的通量} = \text{散度的体积}$$

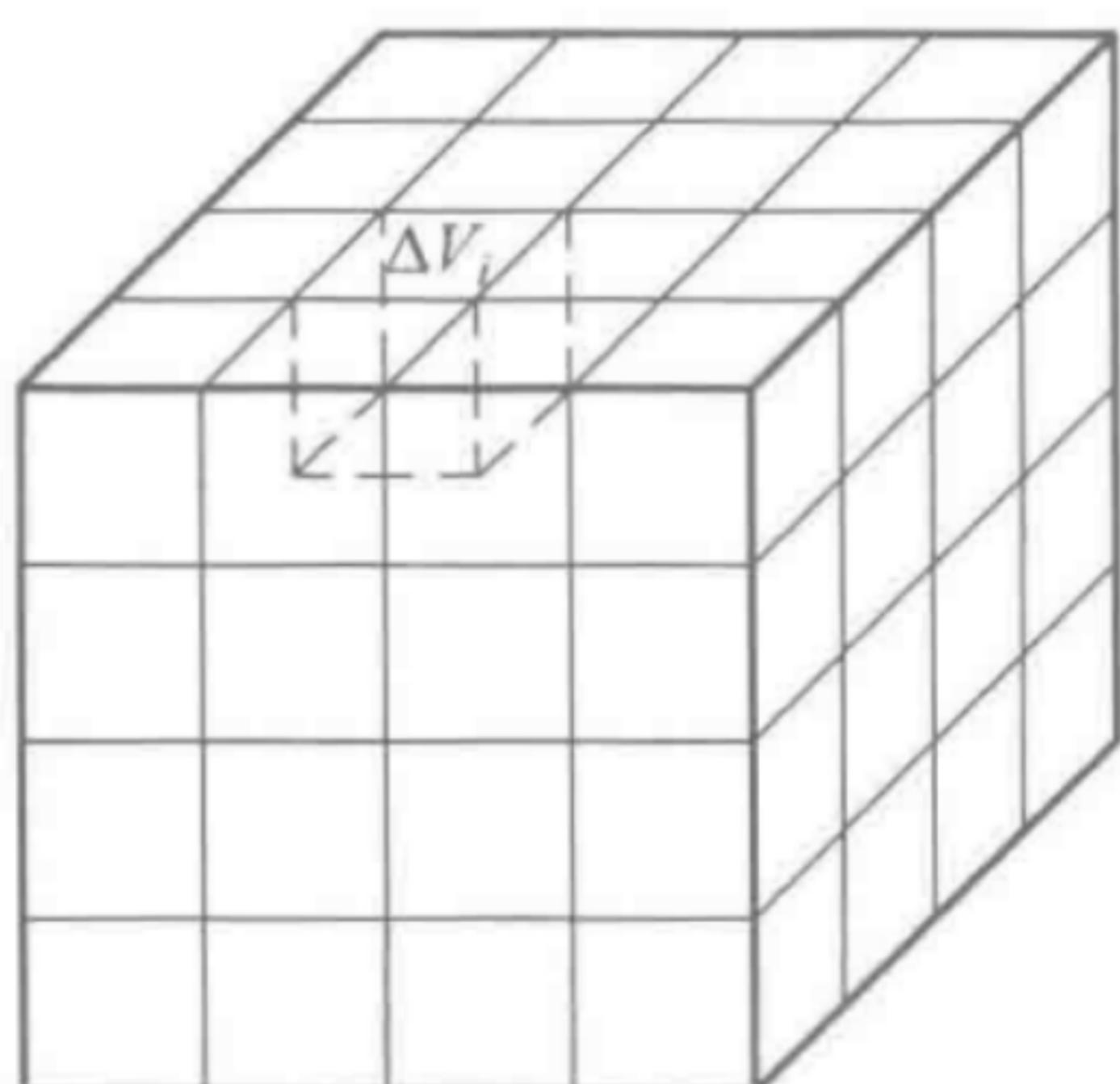


图 1.12 证明散度定理

$$\oint \vec{A} \cdot d\vec{s} = (\nabla \cdot \vec{A}) \Delta V_i$$

$$\oint \vec{A} \cdot d\vec{s} = \sum_i \vec{A} \cdot d\vec{s}_i + \sum_j \vec{A} \cdot d\vec{s}_j + \dots$$

$$= (\nabla \cdot \vec{A}) \Delta V_1 + (\nabla \cdot \vec{A}) \Delta V_2 + \dots$$

$$= \iiint_V \nabla \cdot \vec{A} dV$$

E.9. 电场高斯定理 $\oint \vec{D} \cdot d\vec{s} = \sum q_0 = \iiint_V \rho_0 dV$

$$\iint \vec{D} \cdot d\vec{s} = \iiint \nabla \cdot \vec{D} dV$$

2. 旋度 矢量→矢量

$$环流 I_A = \oint_L \vec{A} \cdot d\vec{l}$$

$$E.9. \oint_L \vec{H} \cdot d\vec{l} = I_0 + \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \neq 0 \quad \text{磁场为涡旋场}$$

$$\oint_L \vec{E} \cdot d\vec{l} = 0, \quad \text{电场为无旋场}$$

$$\text{平均涡旋量 } \frac{\oint_L \vec{A} \cdot d\vec{l}}{\Delta S}, \quad \text{涡旋量 } (\text{rot } \vec{A})_n \vec{A} = \lim_{\Delta S \rightarrow 0} \frac{\oint_L \vec{A} \cdot d\vec{l}}{\Delta S}$$

旋度 $\text{rot } \vec{A}$ 或 $\nabla \times \vec{A}$ 是矢量场 \vec{A} 在某点的最大涡旋量

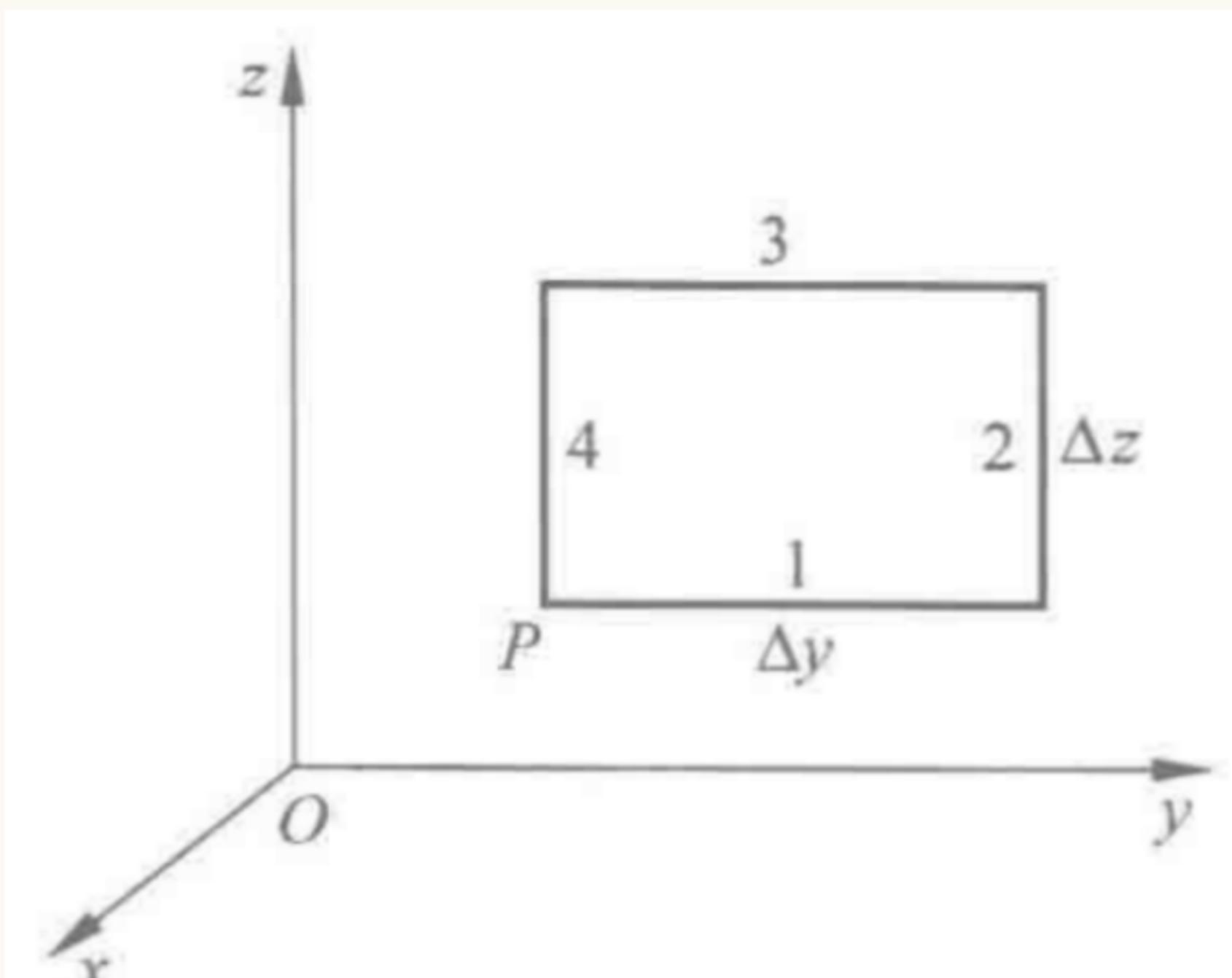


图 1.15 在直角坐标系内计算 $\nabla \times A$

$$\begin{aligned} \oint_L \vec{A} \cdot d\vec{l} &= \int_1 \vec{A} \cdot d\vec{l} + \int_2 \vec{A} \cdot d\vec{l} + \int_3 \vec{A} \cdot d\vec{l} + \int_4 \vec{A} \cdot d\vec{l} \\ &= A_y \Delta y + (A_z + \frac{\partial A_z}{\partial y} \Delta y) \Delta z - (A_y + \frac{\partial A_y}{\partial z} \Delta z) \Delta y - A_z \Delta z \\ &= (\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}) \Delta y \Delta z \\ (\text{rot } \vec{A})_x \vec{A} &= \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \\ (\text{rot } \vec{A})_y \vec{A} &= \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \\ (\text{rot } \vec{A})_z \vec{A} &= \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \end{aligned}$$

$$\text{rot } \vec{A} = \vec{e}_x (\text{rot } \vec{A})_x \vec{A} + \vec{e}_y (\text{rot } \vec{A})_y \vec{A} + \vec{e}_z (\text{rot } \vec{A})_z \vec{A}$$

$$= e_x \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + e_y \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + e_z \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

$$\text{旋度 } \text{rot } \vec{A} = e_x \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + e_y \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + e_z \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

$$\nabla \times \vec{A} = \begin{vmatrix} \vec{e}_x & \vec{e}_y & \vec{e}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$$

旋度的一个重要性质 $\nabla \cdot (\nabla \times \vec{A}) = 0$ 旋度的散度为 0

$$= (e_x \frac{\partial}{\partial x} + e_y \frac{\partial}{\partial y} + e_z \frac{\partial}{\partial z}) \left[e_x \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + e_y \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + e_z \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \right]$$

$$= \frac{\partial}{\partial x} \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + \frac{\partial}{\partial y} \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + \frac{\partial}{\partial z} \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) = 0$$

斯托克斯定理

$$\oint_C \vec{A} \cdot d\vec{l} = \iint_S (\nabla \times \vec{A}) \cdot d\vec{s}$$

环量等于旋度的面积分

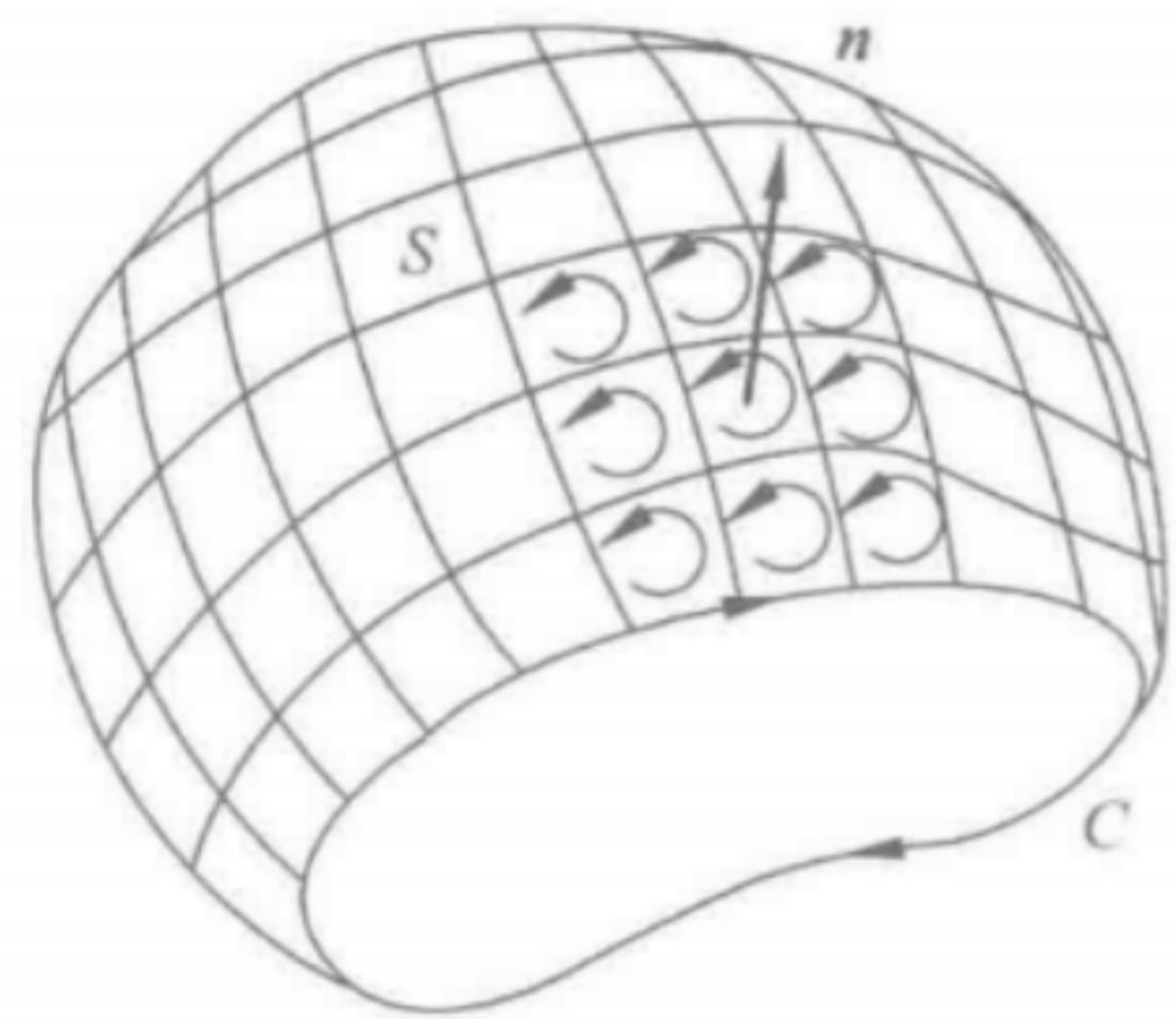


图 1.16 证明斯托克斯定理

$$\oint_{C_i} \vec{A} \cdot d\vec{l} = (\text{rot } \vec{A})_i \vec{n}_i \cdot d\vec{s}_i = \nabla \times \vec{A} \cdot d\vec{s}_i$$

$$\oint_C \vec{A} \cdot d\vec{l} = \oint_{C_1} \vec{A} \cdot d\vec{l} + \oint_{C_2} \vec{A} \cdot d\vec{l} + \dots$$

$$= \iint_S \nabla \times \vec{A} \cdot d\vec{s}_1 + \iint_S \nabla \times \vec{A} \cdot d\vec{s}_2 + \dots$$

$$= \iint_S \nabla \times \vec{A} \cdot d\vec{s}$$

e.g. 磁场环路定理 $\oint_C \vec{H} \cdot d\vec{l} = I_0 + \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} = \iint_S (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s}$

$$\oint_C \vec{H} \cdot d\vec{l} = \iint_S (\nabla \times \vec{H}) \cdot d\vec{s}$$

所以 $\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$

电场环路定理 $\oint_C \vec{E} \cdot d\vec{l} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$

$$\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

3. 梯度 标量 \rightarrow 矢量

$$\nabla u = \left(\vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z} \right) \vec{u} = \vec{e}_x \frac{\partial u}{\partial x} + \vec{e}_y \frac{\partial u}{\partial y} + \vec{e}_z \frac{\partial u}{\partial z}$$

梯度的一个重要性质: $\nabla \times \nabla u = 0$ 梯度的旋度等于0

$$\nabla \times \nabla u = \left(\vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z} \right) \times \left(\vec{e}_x \frac{\partial u}{\partial x} + \vec{e}_y \frac{\partial u}{\partial y} + \vec{e}_z \frac{\partial u}{\partial z} \right)$$

$$= \vec{e}_x \left(\frac{\partial}{\partial y} \frac{\partial u}{\partial z} - \frac{\partial}{\partial z} \frac{\partial u}{\partial y} \right) + \vec{e}_y \left(\frac{\partial}{\partial z} \frac{\partial u}{\partial x} - \frac{\partial}{\partial x} \frac{\partial u}{\partial z} \right) + \vec{e}_z \left(\frac{\partial}{\partial x} \frac{\partial u}{\partial y} - \frac{\partial}{\partial y} \frac{\partial u}{\partial x} \right) = 0$$

据此, 若 $\nabla \times \vec{A} = 0$, 则 $\vec{A} = -\nabla u$

e.g. 对于静电场 $\nabla \times \vec{E} = 0$, 引入电位 $\vec{E} = -\nabla \vec{u}$

4. 各种坐标系下的梯度、散度、旋度

常用拉梅系数

直角坐标系: $H_x = 1, H_y = 1, H_z = 1$

柱坐标系: $H_r = 1, H_\theta = r, H_z = 1$

球坐标系: $H_r = 1, H_\theta = r, H_\phi = r \sin\theta$

通用公式:

$$\text{梯度: } \nabla f = \frac{1}{H_1} \frac{\partial f}{\partial q_1} \vec{e}_1 + \frac{1}{H_2} \frac{\partial f}{\partial q_2} \vec{e}_2 + \frac{1}{H_3} \frac{\partial f}{\partial q_3} \vec{e}_3$$

$$\text{散度: } \nabla \cdot f = \frac{1}{H_1 H_2 H_3} \left(\frac{\partial (f_1 H_2 H_3)}{\partial q_1} + \frac{\partial (f_2 H_1 H_3)}{\partial q_2} + \frac{\partial (f_3 H_1 H_2)}{\partial q_3} \right)$$

$$\text{旋度: } \nabla \times f = \frac{1}{H_1 H_2 H_3} \begin{vmatrix} H_1 \vec{e}_1 & H_2 \vec{e}_2 & H_3 \vec{e}_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ H_1 f_1 & H_2 f_2 & H_3 f_3 \end{vmatrix}$$

③ 亥姆霍兹定理

若矢量场 $\vec{F}(\vec{r})$ 在无界空间中处处单值，且其导数连续有界。场源分布在有限区域 V' 中，则该矢量场唯一地由其散度和旋度确定，且可以表示为一个标量函数的梯度和一个矢量函数的旋度之和。

$$\vec{F}(\vec{r}) = -\nabla \phi(\vec{r}) + \nabla \times \vec{A}(\vec{r})$$

$$\phi(\vec{r}) = \frac{1}{4\pi} \int_{V'} \frac{\nabla' \cdot \vec{F}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV'$$

$$\vec{A}(\vec{r}) = \frac{1}{4\pi} \int_{V'} \frac{\nabla' \times \vec{F}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV'$$

④ 微分算符

1. nabla / Hamilton ∇

$$\nabla = \vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z}$$

2. Laplacian $\nabla^2 = \nabla \cdot \nabla$

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

⑤ 几个重要公式

矢量三重积， $\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A}) = \vec{C} \cdot (\vec{A} \times \vec{B})$

$$\vec{A} \times (\vec{B} \times \vec{C}) = (\vec{A} \cdot \vec{C}) \vec{B} - (\vec{A} \cdot \vec{B}) \vec{C}$$

$$\nabla \cdot (\vec{A} \times \vec{B}) = \vec{B} \cdot \nabla \times \vec{A} - \vec{A} \cdot \nabla \times \vec{B}$$

$$\nabla \times (u \vec{A}) = u \nabla \times \vec{A} + \nabla u \times \vec{A}$$

$$\nabla \times \nabla u = 0$$

$$\nabla \cdot \nabla \times \vec{A} = 0$$

$$\nabla \times \nabla \times \vec{A} = \nabla \cdot (\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$$

对于距离矢量 $\vec{R} = \vec{r} - \vec{r}'$, 有 $\nabla R = -\nabla' R = \frac{\vec{R}}{R} = \vec{e}_R$

$$\nabla \frac{1}{R} = -\nabla' \frac{1}{R} = -\frac{\vec{R}}{R^3} = -\frac{\vec{e}_R}{R^2}$$

$$\vec{r} = \vec{e}_x x + \vec{e}_y y + \vec{e}_z z$$

$$\vec{r}' = \vec{e}_x x' + \vec{e}_y y' + \vec{e}_z z'$$

$$R = |\vec{r} - \vec{r}'| = [(x-x')^2 + (y-y')^2 + (z-z')^2]^{\frac{1}{2}}$$

$$\nabla = \vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z}$$

$$\nabla' = \vec{e}_x \frac{\partial}{\partial x'} + \vec{e}_y \frac{\partial}{\partial y'} + \vec{e}_z \frac{\partial}{\partial z'}$$

$$\nabla R = \vec{e}_x \frac{\partial R}{\partial x} + \vec{e}_y \frac{\partial R}{\partial y} + \vec{e}_z \frac{\partial R}{\partial z}$$

$$= \vec{e}_x \frac{x-x'}{R} + \vec{e}_y \frac{y-y'}{R} + \vec{e}_z \frac{z-z'}{R}$$

$$= \frac{1}{R} (\vec{r} - \vec{r}')$$

$$= \frac{\vec{R}}{R}$$

$$= \vec{e}_R$$

同理 $\nabla' R = -\nabla R$

$$\nabla \frac{1}{R} = -\frac{1}{R^2} \nabla R = -\frac{\vec{R}}{R^3} = -\frac{\vec{e}_R}{R^2}$$

$$\nabla' \frac{1}{R} = -\nabla \frac{1}{R}$$

二、静电场分析

① 电荷与电荷分布

1. 体电荷密度

$$\rho(r) = \lim_{\Delta V \rightarrow 0} \frac{\Delta q}{\Delta V}$$

$$q = \iiint \rho(r) dV$$

2. 面电荷密度

$$\rho_s(r) = \lim_{\Delta s \rightarrow 0} \frac{\Delta q}{\Delta s}$$

$$q = \iint \rho_s(r) ds$$

3. 线电荷密度

$$\rho_v(r) = \frac{\Delta q}{\Delta l}$$

$$q = \int_L \rho_v(r) dl$$

4. 点电荷与δ函数表示法

$$\rho(r) = q \delta(r - r') = \begin{cases} 0, & r \neq r' \\ \infty, & r = r' \end{cases}$$

$$Q = \iiint_V \rho(r) dV = q \iiint_V \delta(r - r') dV = \begin{cases} 0, & r \text{ 不在 } V \text{ 内} \\ q, & r \text{ 在 } V \text{ 内} \end{cases}$$

5. 场强 E 和电位 V

$$\text{电场强度 } \vec{E}(r) = \frac{\vec{F}_0}{q_0} \text{ 电场力}$$

$$\text{电位 } \Phi(r) = \int_P^Q \vec{E} \cdot d\vec{l} , \quad \vec{E}(r) = -\nabla \Phi(r)$$

$$\text{电压 } \Phi_P - \Phi_Q = \int_{P_1}^{P_2} \vec{E} \cdot d\vec{l} = \int_{P_1}^{P_2} \vec{E} \cdot d\vec{l}$$

② 静电场基本方程

$$\left\{ \begin{array}{l} \oint \vec{E} \cdot d\vec{s} = \frac{1}{\epsilon_0} \sum_i q_i \quad \text{高斯定理} \\ \oint \vec{E} \cdot d\vec{l} = 0 \quad \text{环路定理} \end{array} \right.$$

$$\Rightarrow \left\{ \begin{array}{l} \oint \vec{D} \cdot d\vec{s} = \sum_i q_i \quad \text{有电介质时} \\ \oint \vec{E} \cdot d\vec{l} = 0 \end{array} \right.$$

高斯定理证明

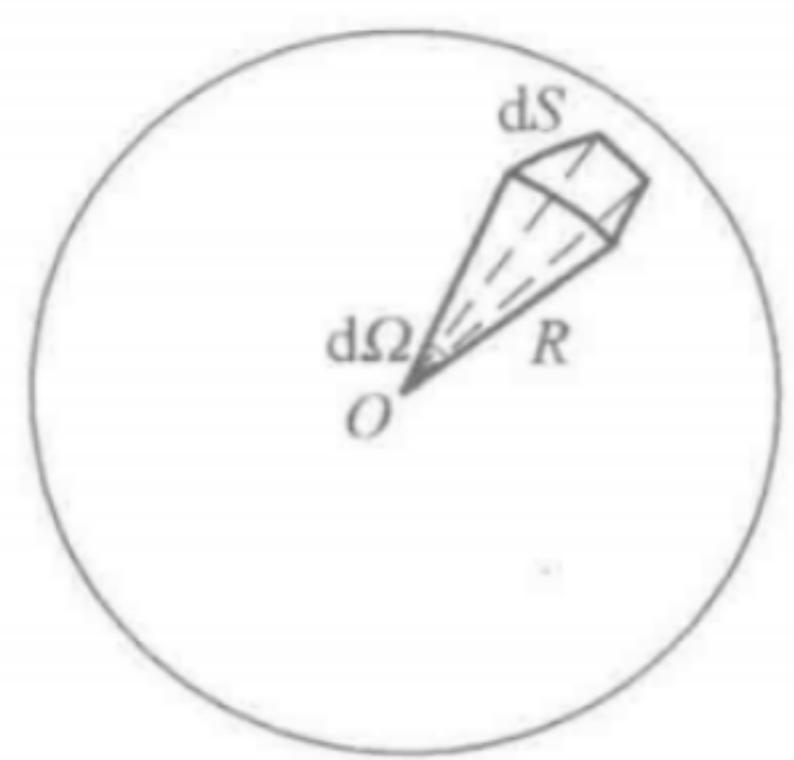


图 2.1 球面上的面元对球心的立体角

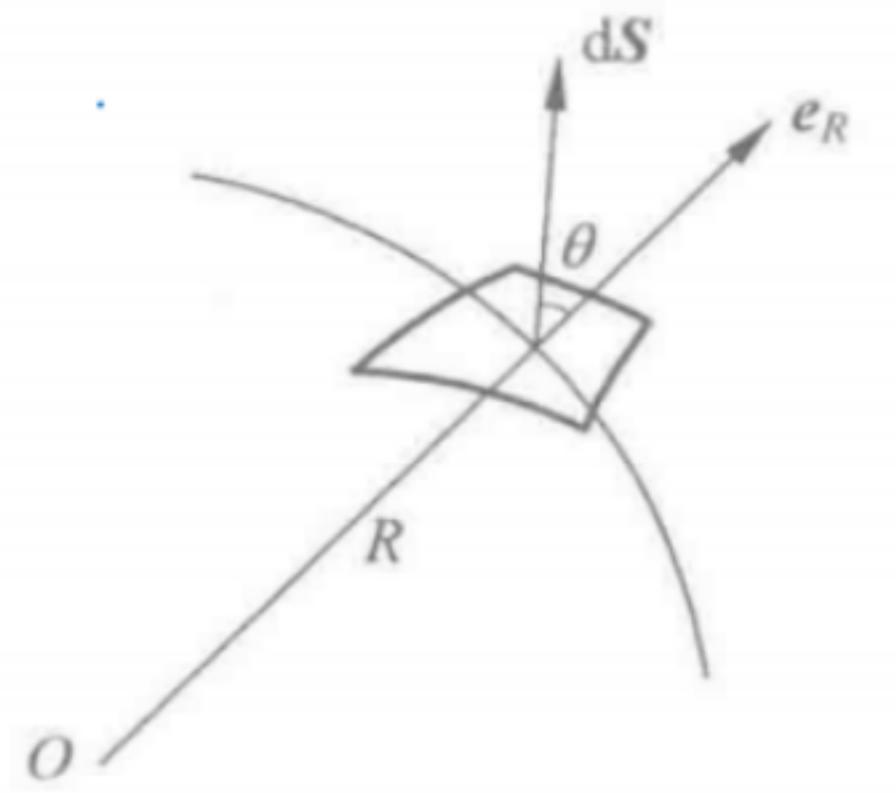


图 2.2 任一面元对一点的立体角

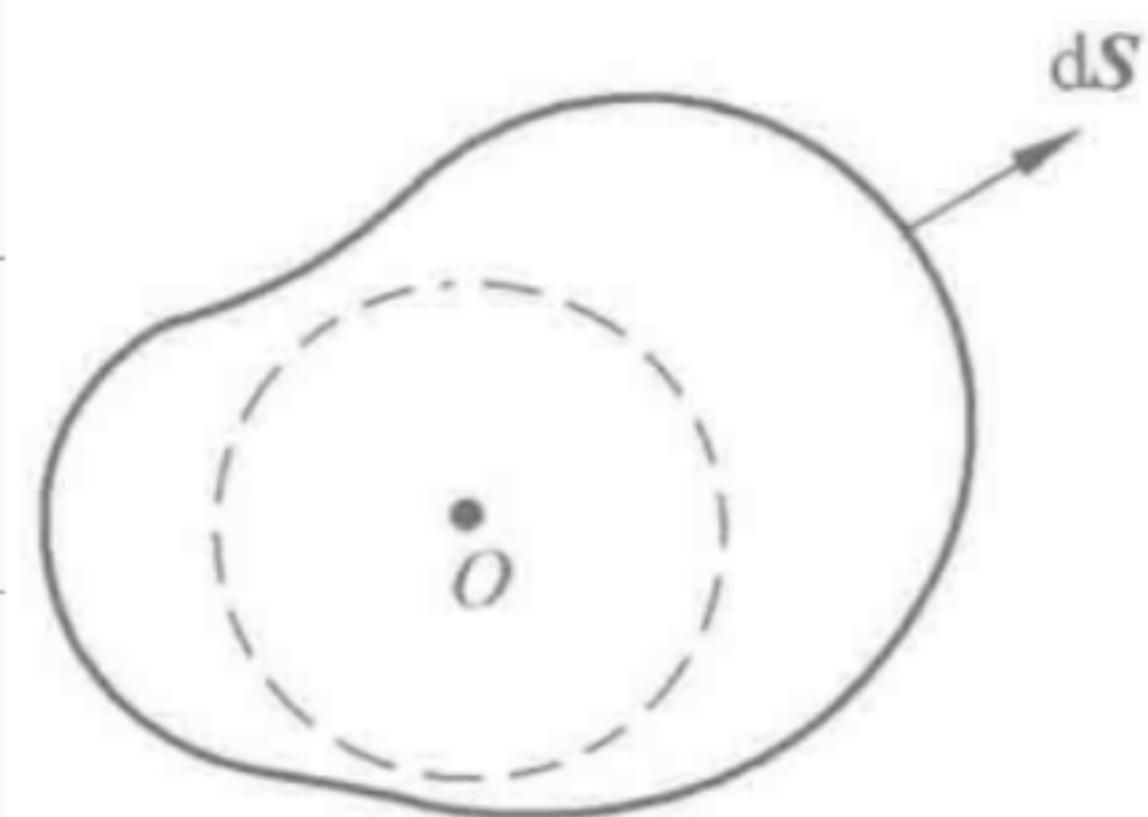
$$\text{立体角 } \Omega = \frac{dS}{R^2}$$

$$\text{整个球面的立体角 } \Omega = \frac{4\pi R^2}{R^2} = 4\pi$$

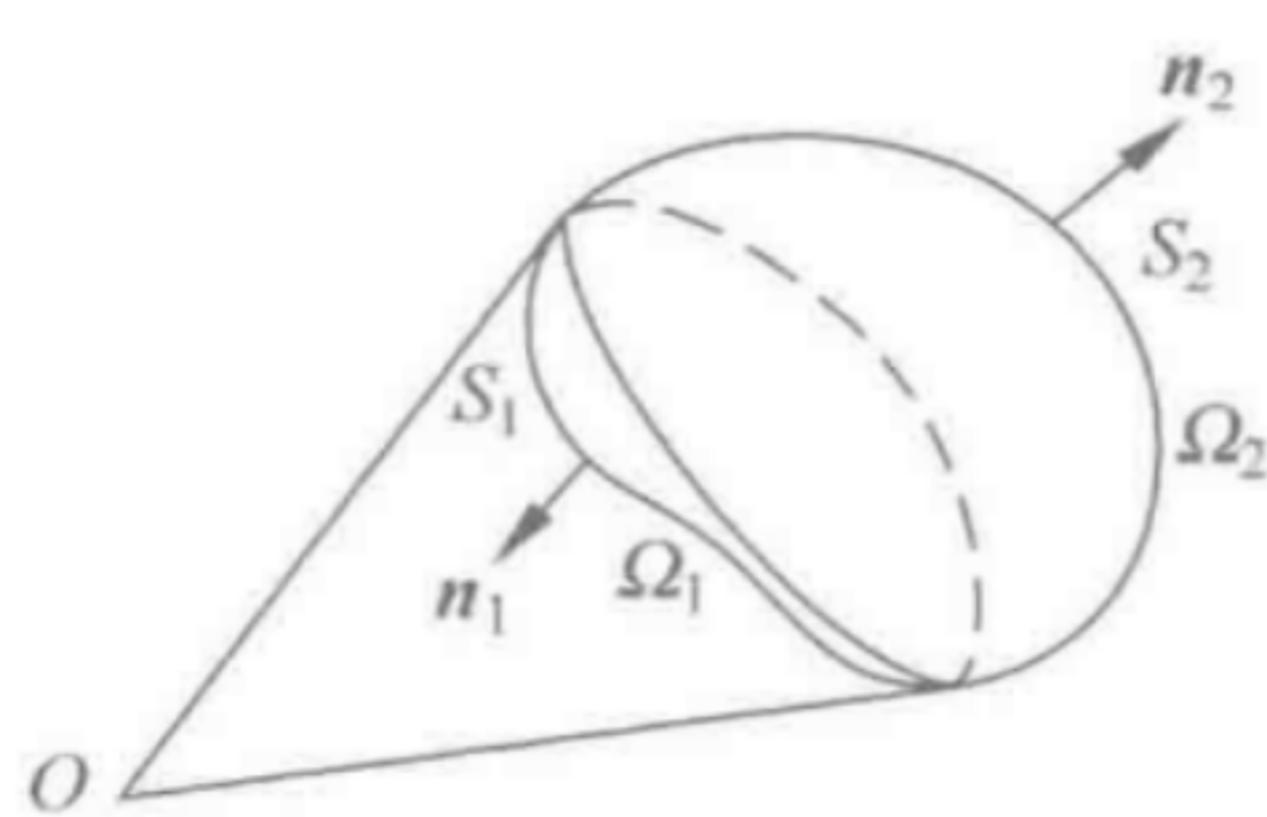
不在球面上的任一面元 $d\vec{s}$ 对一点 O 的立体角

以 O 到 $d\vec{s}$ 的距离 R 为半径做一个球面

$$d\Omega = \frac{d\vec{s} \cdot \vec{e}_R}{R^2} = \frac{dS \cos\theta}{R^2}$$



(a) O点在闭合曲面内



(b) O点位于闭合曲面外

任意形状的闭合曲面对一点 O 的立体角

O 在曲面内: $\Omega = 4\pi$

O 在曲面外: $\Omega = 0$

图 2.3 闭合面的立体角

立体角

$$\text{所以 } \oint \vec{D} \cdot d\vec{s} = \oint \frac{q \vec{e}_r}{4\pi R^2} \cdot d\vec{s} = \frac{q}{4\pi} \oint \frac{\vec{e}_r \cdot d\vec{s}}{R^2} = \begin{cases} q, & q \text{ 在曲面内} \\ 0, & q \text{ 在曲面外} \end{cases}$$

$$\oint \vec{D} \cdot d\vec{s} = \sum (\vec{D}_1 + \vec{D}_2 + \dots + \vec{D}_k) \cdot d\vec{s} = q_1 + q_2 + \dots + q_k = \sum_i q_i$$

$$\oint \vec{D} \cdot d\vec{s} = \iiint_V \nabla \cdot \vec{D} dV = \iiint_V \rho dV \xrightarrow{\text{体密度}}$$

$$\nabla \cdot \vec{D} = \rho$$

环路定理证明

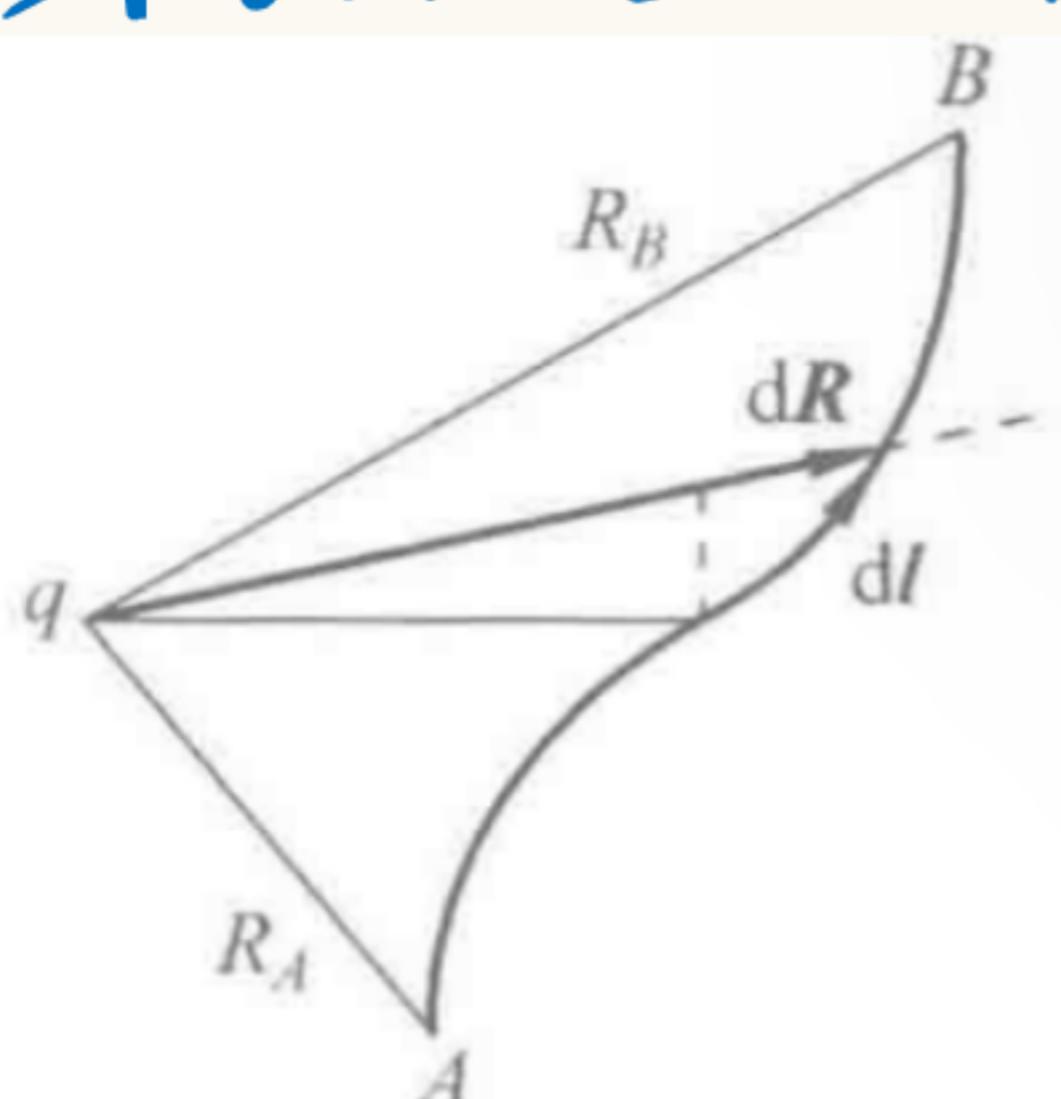


图 2.4 E 沿曲线的积分

$$\int_L \vec{E} \cdot d\vec{l} = \frac{q}{4\pi\epsilon_0} \int_L \frac{\vec{e}_r \cdot d\vec{l}}{R^2} = \frac{q}{4\pi\epsilon_0} \int_{R_A}^{R_B} \frac{dR}{R^2} = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{R_A} - \frac{1}{R_B} \right)$$

当 L 闭合时, $R_A = R_B$

可得 $\int_L \vec{E} \cdot d\vec{l} = 0$

$$\int_L \vec{E} \cdot d\vec{l} = \iint (\nabla \times \vec{E}) d\vec{s} = 0$$

$$\nabla \times \vec{E} = 0$$

③ 场强E和电位V的计算

1. 叠加原理

$$\text{点电荷的场强 } \vec{E}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{q(\vec{r}')}{R^2} \vec{e}_R$$

$$\text{点电荷组的场强 } \vec{E}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \sum_{i=1}^n \frac{q_i(\vec{r}'_i)}{R_i^2} \vec{e}_{R_i}$$

$$\text{电荷连续分布的场强 } \vec{E}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{dq(\vec{r}')}{R^2} \vec{e}_R$$

$$\text{电荷的线分布 } dq(\vec{r}') = \rho_l(\vec{r}') dl$$

$$\text{面分布 } dq(\vec{r}') = \rho_s(\vec{r}') dS$$

$$\text{体分布 } dq(\vec{r}') = \rho(\vec{r}') dV$$

$$\text{重}(\vec{r}) = \int_P^Q \vec{E} \cdot d\vec{l}$$

2. 对称性

利用高斯定理求 \vec{E}

$$\text{重}(\vec{r}) = \int_P^Q \vec{E} \cdot d\vec{l}$$

3. 利用点电荷电位的公式和电位的叠加原理求 Φ

第一步：利用点电荷电位的公式和电位的叠加原理求 Φ 。

点电荷的电位：

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \frac{q(r')}{R} \quad (2.47)$$

点电荷组的电位：

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \sum_{i=1}^n \frac{q_i(r'_i)}{R_i} \quad (2.48)$$

电荷连续分布的电位：

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \int \frac{dq(r')}{R} \quad (2.49)$$

线电荷元、面电荷元、体电荷元的表达式仍为式(2.32)~式(2.34)，代入式(2.49)，可以分别求出线电荷、面电荷、体电荷产生的电位的表达式

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \int_l \frac{\rho_l(r') dl}{R} \quad (2.50)$$

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \iint_S \frac{\rho_s(r') dS}{R} \quad (2.51)$$

$$\Phi(r) = \frac{1}{4\pi\epsilon_0} \iiint_V \frac{\rho(r') dV}{R} \quad (2.52)$$

第二步：利用电位梯度求场强

$$E = -\nabla \Phi \quad (2.53)$$

④ 静电场中的导体

下面列出静电平衡时导体的电特性，在分析一些问题时非常有用。

(1) 导体内电场强度处处为零。

(2) 导体是等位体，导体的表面是等位面。

(3) 导体内无电荷分布，电荷只分布在导体的表面。孤立导体表面的电荷分布与曲率有关，曲率比较大（凸出而尖锐）的地方，面电荷密度比较大；曲率比较小（比较平坦）的地方，面电荷密度也比较小；曲率为负值（凹进去）的地方，面电荷密度更小。

(4) 导体表面附近，电场强度的方向与表面垂直，电场强度的大小等于该点附近导体表面的面电荷密度除以 ϵ_0 ，所以导体表面附近的电场强度为

$$\vec{E} = \hat{n} \frac{\rho_s}{\epsilon_0} \quad (2.56)$$

其中 \hat{n} 是导体表面处的单位法线矢量，式(2.56)可以用高斯定理证明。

⑤ 静电场中的介质

1. 介质的分类

线性和非线性介质

极化强度 \vec{P} 是电场强度 \vec{E} 的函数， $\vec{P} = \vec{P}(\vec{E})$ 。 \vec{P} 的各分量可由电场强度 \vec{E} 的各分量的幂级数表示。

$$\left\{ \begin{array}{l} P_x = \alpha_1 E_x + \alpha_2 E_y + \alpha_3 E_z + \beta_1 E_x^2 + \beta_2 E_x E_y + \dots \\ P_y = \alpha'_1 E_x + \alpha'_2 E_y + \alpha'_3 E_z + \beta'_1 E_x^2 + \beta'_2 E_x E_y + \dots \\ P_z = \alpha''_1 E_x + \alpha''_2 E_y + \alpha''_3 E_z + \beta''_1 E_x^2 + \beta''_2 E_x E_y + \dots \end{array} \right.$$

若 \vec{P} 的各分量只与 \vec{E} 的各分量的一次项有关，与高次项无关，且 \vec{P} 的各分量与 \vec{E} 的各分量呈线性关系，这种介质称为线性介质。

$$\begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix} = \epsilon_0 \begin{bmatrix} \chi_{xx} & \chi_{xy} & \chi_{xz} \\ \chi_{yx} & \chi_{yy} & \chi_{yz} \\ \chi_{zx} & \chi_{zy} & \chi_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$$

χ_{ij} 称为介质的磁化率，与 \vec{E} 无关。

各向同性与各向异性介质

电介质内某点的物理特性在所有方向上都相同，与外加电场 \vec{E} 的方向无关，这种介质称为各向同性介质，否则为各向异性介质。

对于各向同性介质， $i \neq j$ 时 $\chi_{ij}=0$, $\chi_{xx}=\chi_{yy}=\chi_{zz}$, $\vec{P}=\epsilon_0 \chi_e \vec{E}$. χ_e 与 \vec{E} 无关

均匀介质和非均匀介质

电介质内的 ϵ 处处相同，与空间位置无关，即 $\nabla \epsilon = 0$ ，则称这种介质为均匀介质。

对于线性、各向同性的均匀电介质

$$\vec{P} = \epsilon_0 \chi_e \vec{E}, \quad \vec{D} = \epsilon_0 \epsilon_r \vec{E}, \quad \epsilon_r = 1 + \chi_e$$

2. 电介质极化的机理和电偶极子模型

无极分子 \rightarrow 位移极化

有极分子 \rightarrow 位移极化 + 取向极化

无论是无极分子电介质，还是有极分子电介质，在外电场中，分子中的正、负电荷的中心错开一定的距离，形成了一个电偶极子（分子电矩为 $p=ql$ ），所以可以用电偶极子模型研究电介质。外电场越强，一定体积中分子电矩的矢量和越大，极化强度矢量就定义为单位体积中分子电矩的矢量和

$$\vec{P} = \lim_{\Delta V \rightarrow 0} \frac{\sum \vec{p}}{\Delta V} \quad (2.60)$$

3. 计算电介质问题常用的公式

有电介质时静电场的高斯定理为 $\oint \vec{D} \cdot d\vec{s} = \sum q$

$$\oint_S \vec{E} \cdot d\vec{s} = \frac{q+q_p}{\epsilon_0} \quad (\text{Gauss})$$

电位移量的定义 $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$

$$q_p = \int_V \rho_p dv$$

对于线性、各向同性电介质 $\vec{D} = \epsilon_0 \epsilon_r \vec{E}$

$$\oint_S \vec{E} \cdot d\vec{s} = - \int_S \vec{P} \cdot d\vec{s}$$

$$\vec{P} = \epsilon_0 \chi_e \vec{E}$$

$$\oint_S (\epsilon_0 \vec{E} + \vec{P}) \cdot d\vec{s} = \int_V \rho dv$$

$$\rho_{sp} = \vec{P} \cdot \vec{n}$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} \Rightarrow \nabla \cdot \vec{D} = \rho$$

$$\rho_p = -\nabla \cdot \vec{P}$$

$$\vec{P} = \epsilon_0 \chi_e \vec{E}$$

$$\epsilon = \epsilon_0 \epsilon_r$$

$$\vec{D} = \epsilon_0 (1 + \chi_e) \vec{E}$$

$$\epsilon_r = 1 + \chi_e$$

$$= \epsilon_0 \epsilon_r \vec{E} = \epsilon \vec{E}$$

⑥ 电力线方程和等位面方程

1. 电力线方程

电力线上某一点处的切线方向表示该点电场强度的方向,若 dl 表示电力线上某一点处切线方向的线元,在该点处

$$\mathbf{E} = kdl \quad (2.71)$$

把式(2.71)在直角坐标系中展开

$$e_x E_x + e_y E_y + e_z E_z = e_x k dx + e_y k dy + e_z k dz$$

上式两端各分量分别相等,则

$$E_x = kdx, \quad E_y = kdy, \quad E_z = kdz$$

所以直角坐标系中的电力线方程为

$$\frac{dx}{E_x} = \frac{dy}{E_y} = \frac{dz}{E_z} \quad (2.72)$$

用相同的方法可以导出圆柱坐标系中的电力线方程

$$\frac{dr}{E_r} = \frac{rd\varphi}{E_\varphi} = \frac{dz}{E_z} \quad (2.73)$$

和球坐标系中的电力线方程

$$\frac{dr}{E_r} = \frac{rd\theta}{E_\theta} = \frac{r\sin\theta d\varphi}{E_\varphi} \quad (2.74)$$

2. 等位面方程

$$\Phi(x, y, z) = C$$

⑦ 静电场的边界条件

1. E 和 D 的边界条件

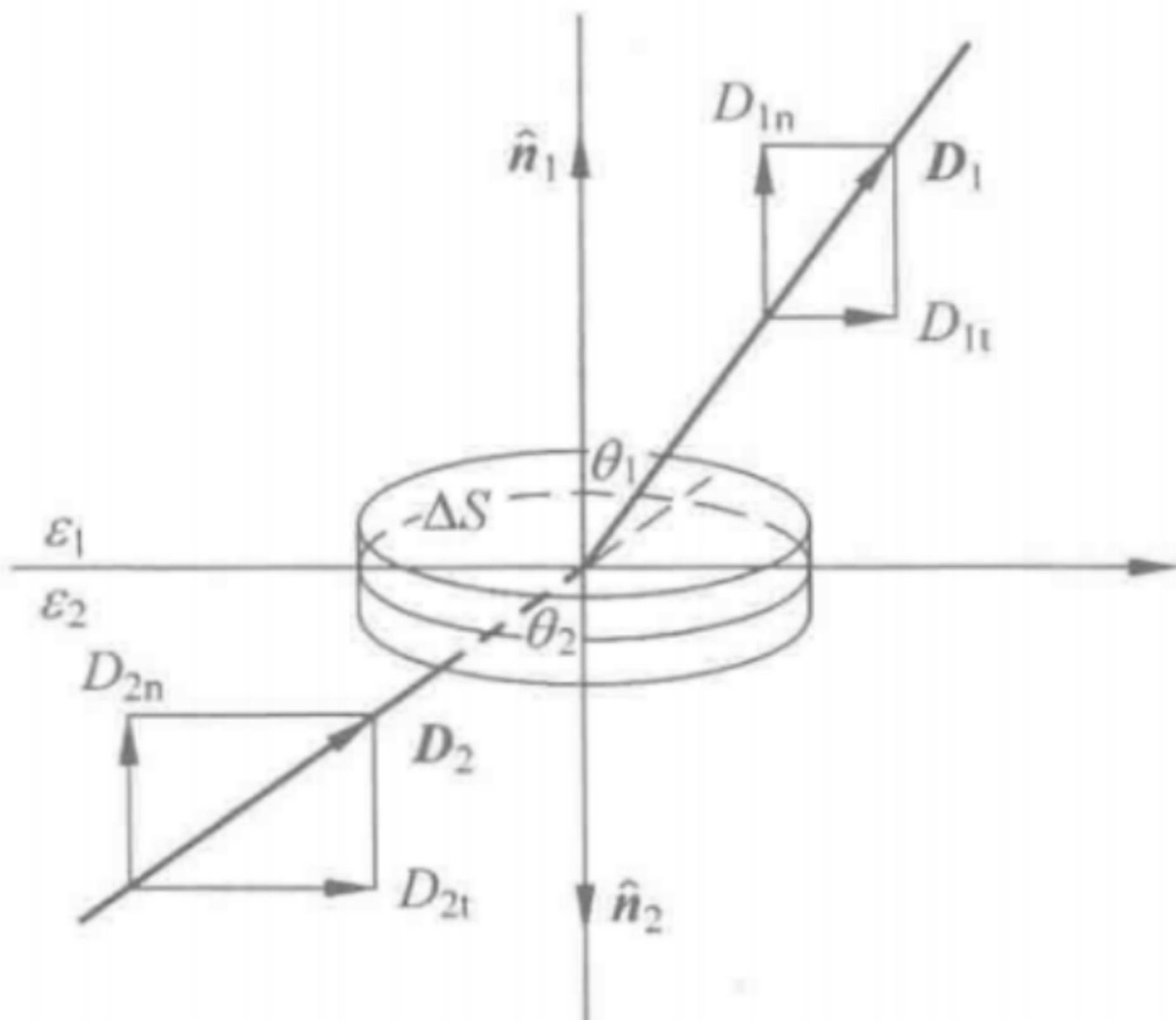


图 2.13 D 法向分量的边界条件

$$\oint \vec{D} \cdot d\vec{s} = \rho_s \Delta S$$

$$\iint_{\text{上}} \vec{D}_1 \cdot d\vec{s} + \iint_{\text{下}} \vec{D}_2 \cdot d\vec{s} + \iint_{\text{侧}} \vec{D} \cdot d\vec{s} = \rho_s \Delta S$$

$$\iint D_1 ds \cos\theta_1 + \iint D_2 ds \cos(\pi - \theta_2) = \rho_s \Delta S$$

$$D_{1n} \Delta S - D_{2n} \Delta S = \rho_s \Delta S$$

$$D_{1n} - D_{2n} = \rho_s$$

分界面上没有自由电荷时 $D_{1n} = D_{2n}$

$$\hat{n}_1 \cdot \vec{D}_1 = \hat{n}_2 \cdot \vec{D}_2$$

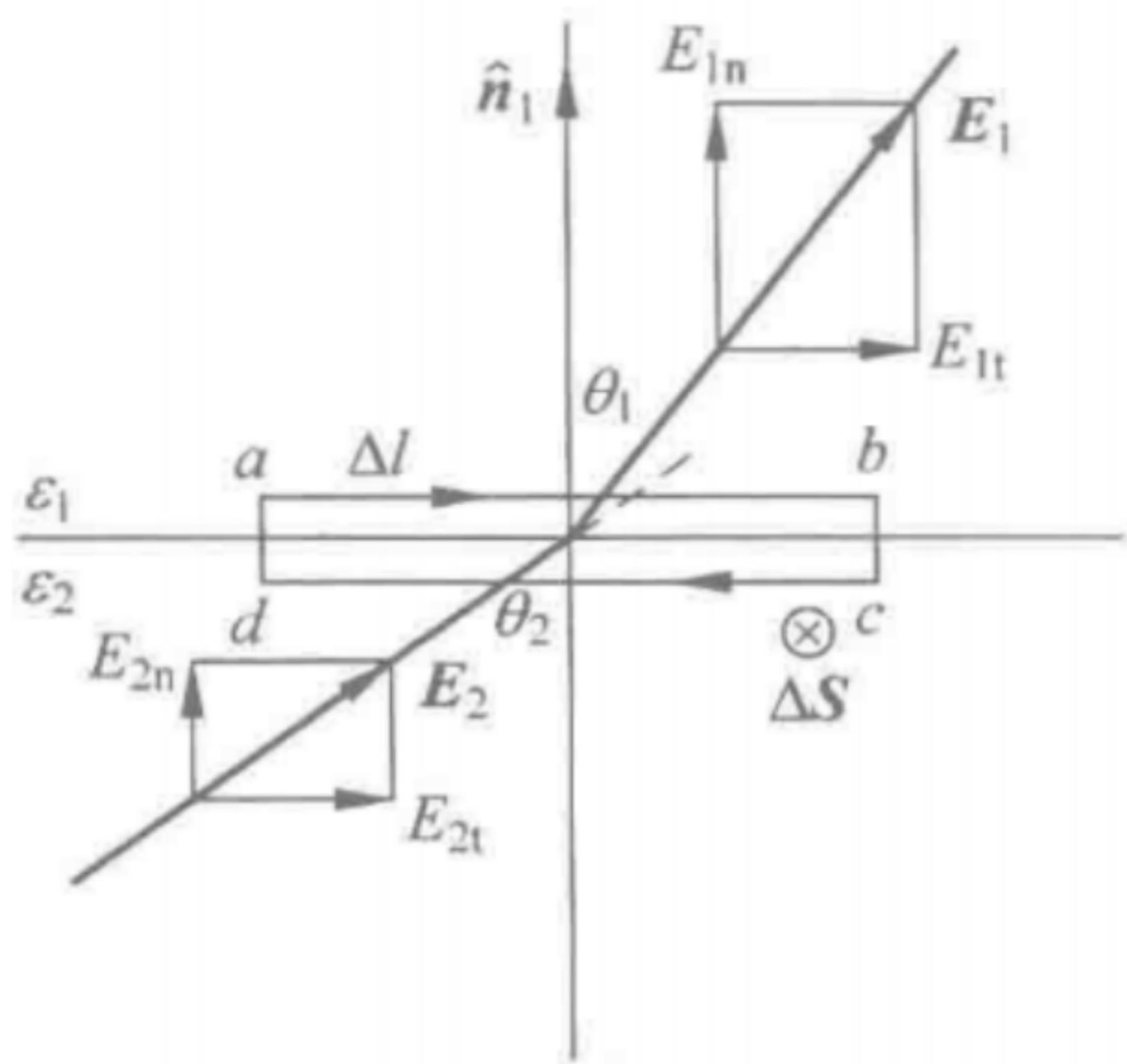


图 2.14 E 切向分量的边界条件

$$\oint_L \vec{E} \cdot d\vec{l} = 0$$

$$\int_{ab} \vec{E}_1 \cdot d\vec{l} + \int_{bc} \vec{E}_1 \cdot d\vec{l} + \int_{cd} \vec{E}_2 \cdot d\vec{l} + \int_{da} \vec{E}_2 \cdot d\vec{l} = 0$$

$$\vec{E}_1 \cdot \Delta \vec{l}_1 + \vec{E}_2 \cdot \Delta \vec{l}_2 = 0$$

$$\vec{E}_1 \cdot \Delta \vec{l}_1 - \vec{E}_2 \cdot \Delta \vec{l}_1 = 0$$

$$\vec{E}_1 \cdot (\vec{s} \times \hat{n}_1) \Delta l - \vec{E}_2 \cdot (\vec{s} \times \hat{n}_1) \Delta l = 0$$

$$\hat{n}_1 \times \vec{E}_1 = \hat{n}_1 \times \vec{E}_2$$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2$$

$$E_{1t} = E_{2t}$$

$$\tan \theta_1 = \frac{E_{1t}}{E_{1n}}, \tan \theta_2 = \frac{E_{2t}}{E_{2n}}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{E_{1t}}{E_{1n}} \cdot \frac{E_{2n}}{E_{2t}} = \frac{E_{2n}}{E_{1n}} = \frac{\frac{D_{2n}}{\epsilon_2}}{\frac{D_{1n}}{\epsilon_1}} = \frac{\epsilon_1}{\epsilon_2}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2}, \text{ 在 } \vec{E} \text{ 线上发生了折射}$$

2. 电位的边界条件

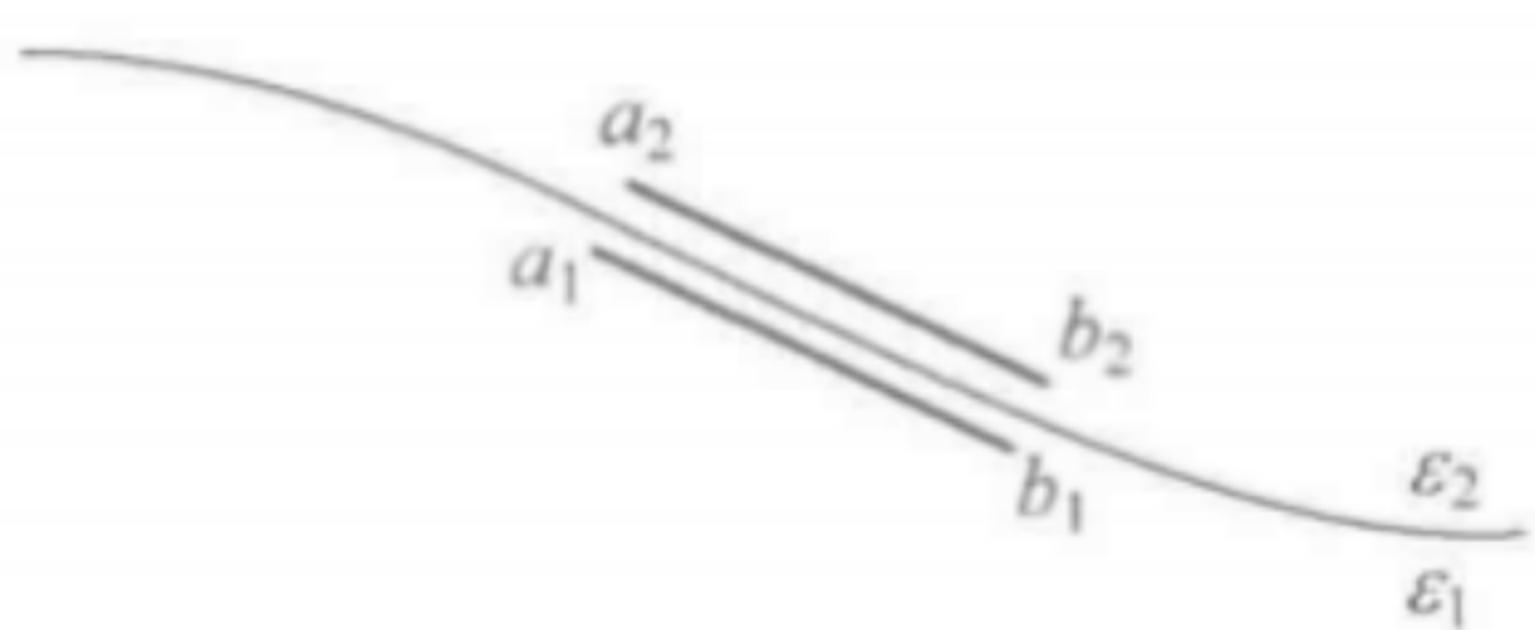


图 2.15 电位的边界条件

$$\Phi_1 - \Phi_2 = \int_{a_2}^{a_1} \vec{E} \cdot d\vec{l} = 0$$

$$\Phi_1 = \Phi_2$$

$$\Phi_{a_1} = \Phi_{a_2}, \Phi_{b_1} = \Phi_{b_2}$$

3. 导体与介质界面上的边界条件

\vec{E} 和 \vec{D}

$$\vec{E}_2 = 0, \vec{E}_{1t} = \vec{E}_{2t} = 0$$

$$D_{1n} = \rho_s, E_{1n} = \frac{\rho_s}{\epsilon}$$

主

$$\Phi_1 = \Phi_2$$

⑧ 没松方程和拉普拉斯方程

$$\nabla \cdot \vec{D} = \nabla \cdot \epsilon \vec{E} = \nabla \cdot \epsilon (-\nabla \Phi) = -\epsilon \nabla^2 \Phi = \rho$$

泊松方程 $\nabla^2 \Phi = -\frac{\rho}{\epsilon}$

拉普拉斯方程 $\nabla^2 \Phi = 0$ (没有电荷分布的区域)

⑨ 唯一性定理

1. 格林定理

$$\iiint_V \nabla \cdot \vec{A} dV = \oint_S \vec{A} \cdot d\vec{s}$$

全 $\vec{A} = \phi \nabla \psi$

$$\nabla \cdot \vec{A} = \nabla \cdot (\phi \nabla \psi) = \phi \nabla^2 \psi + \nabla \phi \cdot \nabla \psi$$

$$\vec{A} \cdot d\vec{s} = \vec{A} \cdot \vec{n} ds = \phi \nabla \psi \cdot \vec{n} = \phi \frac{\partial \psi}{\partial n}$$

$$\iiint_V (\phi \nabla^2 \psi + \nabla \phi \cdot \nabla \psi) dV = \oint_S \phi \frac{\partial \psi}{\partial n} ds \quad (\text{格林第一恒等式})$$

同理 $\iiint_V (\psi \nabla^2 \phi + \nabla \psi \cdot \nabla \phi) dV = \oint_S \psi \frac{\partial \phi}{\partial n} ds$

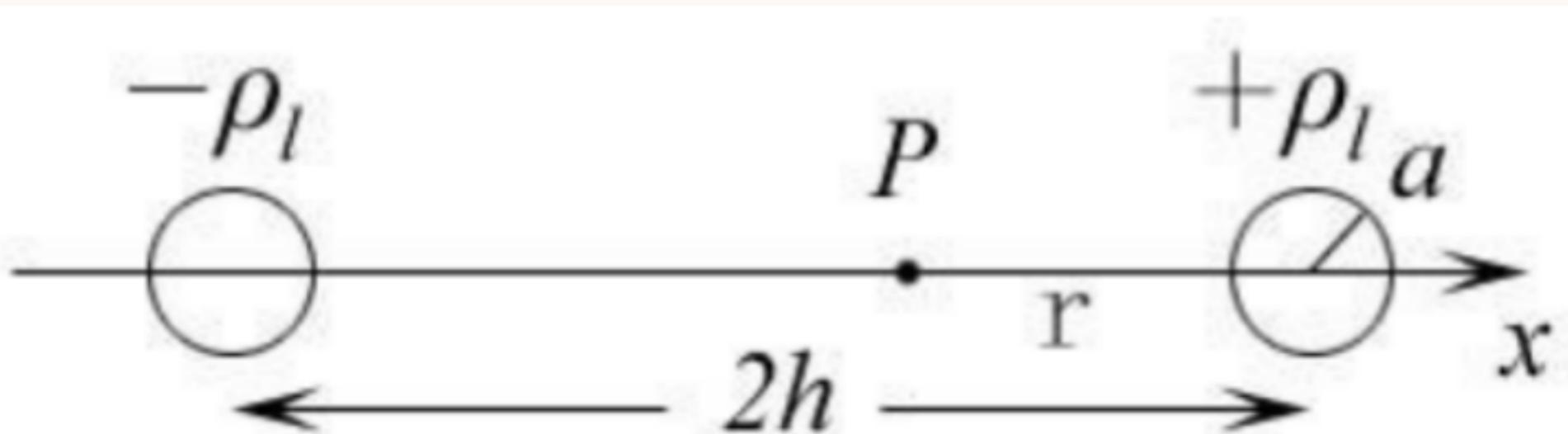
$$\iiint_V (\phi \nabla^2 \psi - \psi \nabla^2 \phi) dV = \oint_S (\phi \frac{\partial \psi}{\partial n} - \psi \frac{\partial \phi}{\partial n}) ds \quad (\text{格林第二恒等式})$$

2. 唯一性定理

对于同一个边值问题，用不同的方法求得的解都是相同的。

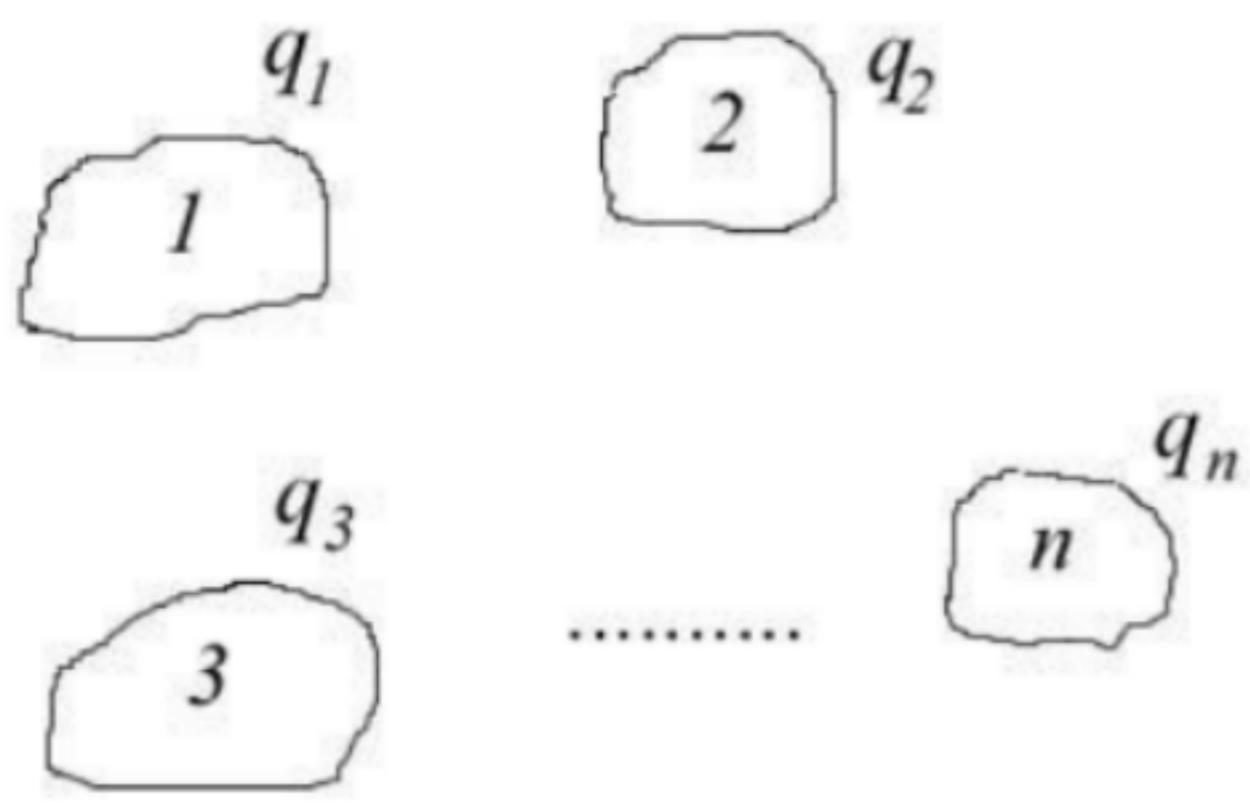
⑩ 导体系统的电容

1. 两导体间的电容



$$C = \frac{q_A}{\Phi_A - \Phi_B}$$

2. 系数



对于一个孤立的多导体系统，每个导体的电位不仅与该导体上所带的电量有关，而且受其它导体上所带电量的影响

$$\bar{\Psi}_1 = P_{11}q_1 + P_{12}q_2 + \dots + P_{1n}q_n$$

$$\vdots$$

$$\bar{\Psi}_i = P_{i1}q_1 + P_{i2}q_2 + \dots + P_{in}q_n$$

$$\vdots$$

$$\bar{\Psi}_n = P_{n1}q_1 + P_{n2}q_2 + \dots + P_{nn}q_n$$

$$\bar{\Psi}_i = \sum_{j=1}^n P_{ij}q_j, \quad P_{ij} \text{ 称为电位系数, } i=j \text{ 称为自电位系数, } i \neq j \text{ 称为互电位系数}$$

$$q_1 = P_{11}\bar{\Psi}_1 + P_{12}\bar{\Psi}_2 + \dots + P_{1n}\bar{\Psi}_n$$

$$\vdots$$

$$q_i = P_{i1}\bar{\Psi}_1 + P_{i2}\bar{\Psi}_2 + \dots + P_{in}\bar{\Psi}_n$$

$$\vdots$$

$$q_n = P_{n1}\bar{\Psi}_1 + P_{n2}\bar{\Psi}_2 + \dots + P_{nn}\bar{\Psi}_n$$

$$q_i = \sum_{j=1}^n \beta_{ij}\bar{\Psi}_j \quad \beta_{ij}, \quad i=j \text{ 称为电容系数, } i \neq j \text{ 称为感应系数}$$

$$\beta_{ij} = \frac{P_{ij}}{\Delta}, \quad \Delta \text{ 为电位系数行列式 } p_{ij}, \quad P_{ij} \text{ 是 } p_{ij} \text{ 的代数余子式}$$

3. 部分电容

$$q_i = \beta_{i1}(\bar{\Psi}_1 - \bar{\Psi}_i + \bar{\Psi}_i) + \beta_{i2}(\bar{\Psi}_2 - \bar{\Psi}_i + \bar{\Psi}_i) + \dots + \beta_{ii}(\bar{\Psi}_i - \bar{\Psi}_i + \bar{\Psi}_i) + \beta_{in}(\bar{\Psi}_n - \bar{\Psi}_i)$$

$$= \beta_{i1}(\bar{\Psi}_1 - \bar{\Psi}_i) + \beta_{i2}(\bar{\Psi}_2 - \bar{\Psi}_i) + \dots + (\beta_{i1} + \beta_{i2} + \dots + \beta_{in})\bar{\Psi}_i + \dots + \beta_{in}(\bar{\Psi}_n - \bar{\Psi}_i)$$

$$= C_{i1}(\bar{\Psi}_i - \bar{\Psi}_1) + C_{i2}(\bar{\Psi}_i - \bar{\Psi}_2) + \dots + C_{ii}\bar{\Psi}_i + \dots + C_{in}(\bar{\Psi}_i - \bar{\Psi}_n)$$

$$C_{ij} = -\beta_{ij}$$

$$C_{ii} = \beta_{i1} + \beta_{i2} + \dots + \beta_{in} = \sum_{j=1}^n \beta_{ij}$$

$$q_1 = C_{11}\Phi_1 + C_{12}(\Phi_2 - \Phi_1) + \dots + C_{1n}(\Phi_n - \Phi_1)$$

$$q_2 = C_{21}(\Phi_2 - \Phi_1) + C_{22}\Phi_2 + \dots + C_{2n}(\Phi_n - \Phi_2)$$

$$\vdots$$

$$q_n = C_{n1}(\Phi_n - \Phi_1) + C_{n2}(\Phi_n - \Phi_2) + \dots + C_{nn}\Phi_n$$

C_{ij} 称互有部分电容，表示第*i*个导体与第*j*个导体间的部分电容

$i=j$ 称自有部分电容，表示第*i*个导体与地间的部分电容

⑪ 静电场的能量与力

1. 静电场的能量

$$\text{能量密度 } W_e = \frac{1}{2} \vec{D} \cdot \vec{E}$$

$$\text{能量 } W_e = \iiint_V \frac{1}{2} \vec{D} \cdot \vec{E} dV$$

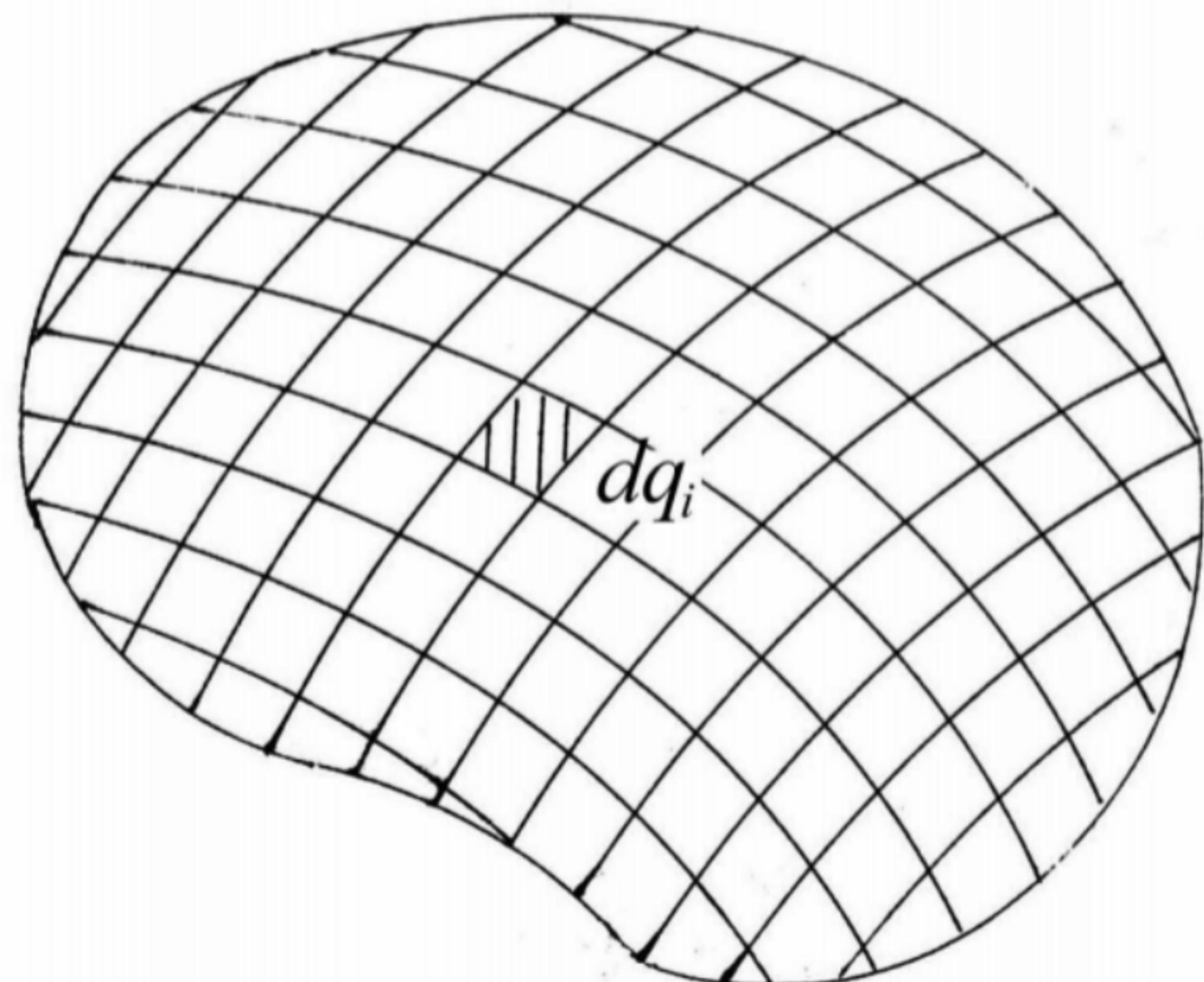


图2.22 建立电荷系统的过程

设在移动电荷过程中的某一时刻，场中某一点电位为 $\Phi_i(x, y, z)$

把电荷元 dq_i 移动到该点需要作的功为 $dA = \Phi_i dq_i$

在建立电荷系统的过程中， $0 \rightarrow l$, $0 \rightarrow \sigma$ 按比例增大

$$l' = \alpha l, \sigma' = \alpha \sigma, \alpha: 0 \rightarrow 1$$

$$dl' = \alpha dl, d\sigma' = \alpha d\sigma$$

$$dq_i = dl' dV + d\sigma' dS$$

$$\Phi_i = \alpha \Phi$$

$$dA = \Phi_i dq_i = \Phi_i dl' dV + \Phi_i d\sigma' dS$$

$$W_e = A = \iiint_V \Phi_i dl' dV + \iint_S \Phi_i d\sigma' dS$$

$$W_e = \int_0^l \alpha dl \iiint_V \rho \Phi dV + \int_0^\sigma \alpha d\sigma \iint_S \sigma \Phi dS$$

$$= \frac{1}{2} \iiint_V \rho \Phi dV + \frac{1}{2} \iint_S \sigma \Phi dS$$

对于多导体系统，电荷只分布在各导体表面 $W_e = \frac{1}{2} \iint_S \sigma \Phi dS = \sum_{i=1}^n \frac{1}{2} \iint_{S_i} \sigma_i \Phi_i dS$

$$= \sum_{i=1}^n \frac{1}{2} \Phi_i q_i$$

2. 静电场的能量分布

$$\rho = \nabla \cdot \vec{D}, \sigma = D_n = \vec{D} \cdot \vec{n}$$

$$We = \frac{1}{2} \iiint_V \Phi \nabla \cdot \vec{D} dV + \frac{1}{2} \iint_{S_1} \vec{D} \cdot \vec{n} ds$$

$$\text{由 } \nabla \cdot (\Psi \vec{A}) = \Psi \nabla \cdot \vec{A} + \vec{A} \cdot \nabla \Psi$$

$$\text{所以 } \nabla \cdot \vec{D} = \nabla \cdot (\Psi \vec{A}) - \vec{A} \cdot \nabla \Psi$$

$$\begin{aligned} We &= \frac{1}{2} \iiint_V \nabla \cdot (\Psi \vec{A}) dV + \frac{1}{2} \iiint_V \vec{D} \cdot \vec{E} dV + \frac{1}{2} \iint_{S_1} \Psi \vec{A} \cdot \vec{n} ds \\ &= \frac{1}{2} \iiint_{S_1 + S_2} \Psi \vec{A} \cdot \vec{n} ds + \frac{1}{2} \iiint_V \vec{D} \cdot \vec{E} dV + \frac{1}{2} \iint_{S_1} \Psi \vec{A} \cdot \vec{n} ds \end{aligned}$$

$$\text{静电场的能量 } We = \iiint_V \frac{1}{2} \vec{D} \cdot \vec{E} dV$$

$$\text{能量密度 } we = \frac{1}{2} \vec{D} \cdot \vec{E}$$

$$\text{对于各向同性介质 } we = \frac{1}{2} \epsilon E^2$$

3. 利用虚位移原理计算电场力

$$dW = dWe + \vec{f} \cdot d\vec{g}$$

$$\text{若各导体电荷不变 } dq = 0 \Rightarrow dW = 0, \vec{f} \cdot d\vec{g} = -dWe|_{q=c}, f = -\frac{dWe}{dg}|_{q=c}, \vec{f} = -\nabla We$$

$$\text{若各导体电量不变 } dW = \sum_i \Psi_i dq_i, dWe = \frac{1}{2} \sum_i \Psi_i d\vec{q}_i, f \cdot dg = dWe, f = \frac{dWe}{dg}|_{\Psi=c}, \vec{f} = \nabla We$$

⑫ 恒定电场

1. 电流与电流密度

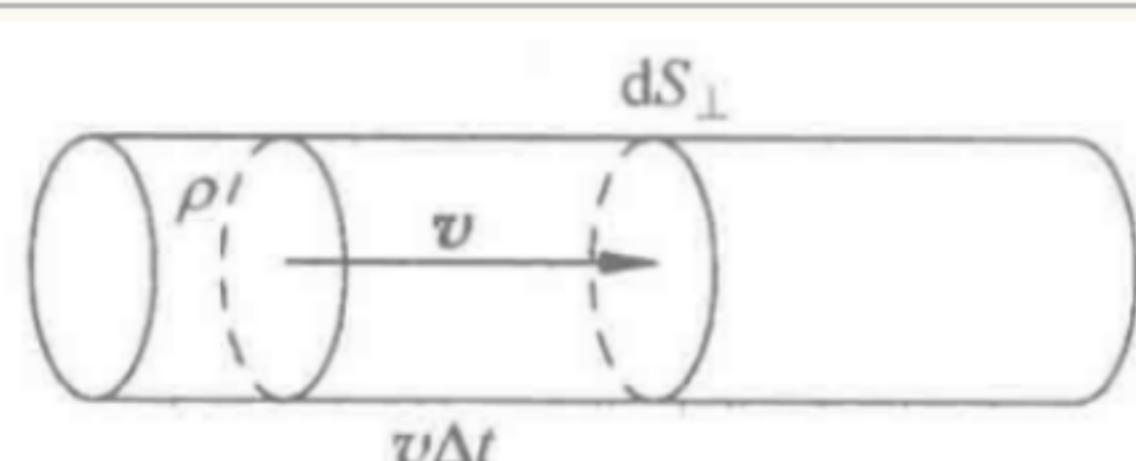


图 2.26 计算体电流密度

$$\text{体电流密度 } \vec{j} = \rho \vec{v}$$

$$J = \frac{dI}{dS_{\perp}}$$

$$\Delta q = \rho \cdot V \Delta t \cdot dS_{\perp}$$

$$I = \iint \vec{j} \cdot d\vec{s}$$

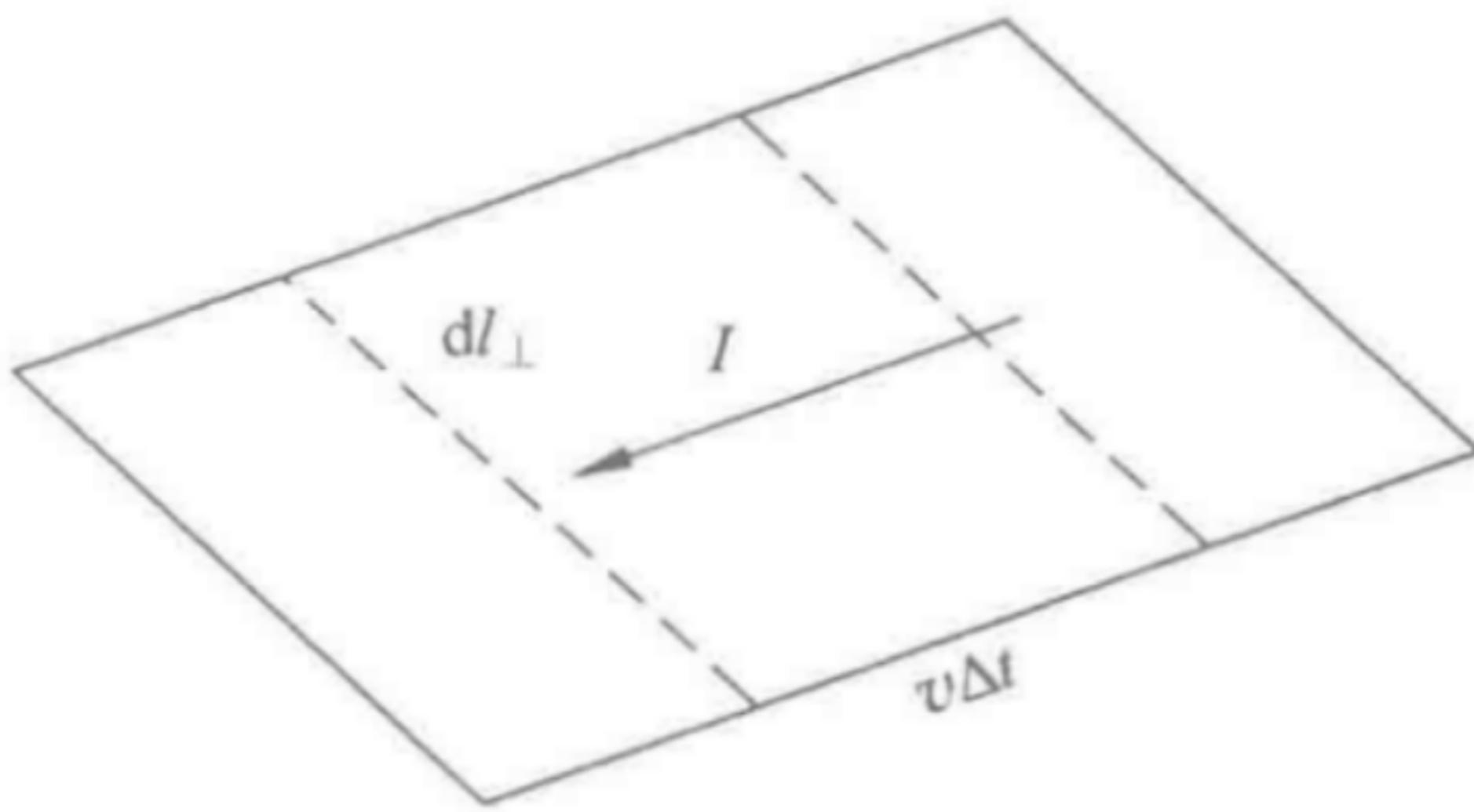
$$I = \frac{\Delta q}{\Delta t} = \rho \cdot V \Delta t$$

$$J = \frac{1}{dS_{\perp}} = \rho V$$

$$\vec{j} = \rho \vec{v}$$

$$\text{面电流密度 } \vec{J}_s = \frac{d\vec{I}}{dL_{\perp}}$$

$$I = \int_L \vec{J}_s \cdot (\vec{n} \times d\vec{l})$$



$$dq = \rho_s \cdot V \Delta t dL_{\perp}$$

$$I = \frac{\partial q}{\partial t} = \rho_s \cdot V dL_{\perp}$$

$$J_s = \frac{I}{dL_{\perp}} = \rho_s V$$

$$\vec{J}_s = \rho_s \vec{V}$$

图 2.27 计算面电流密度

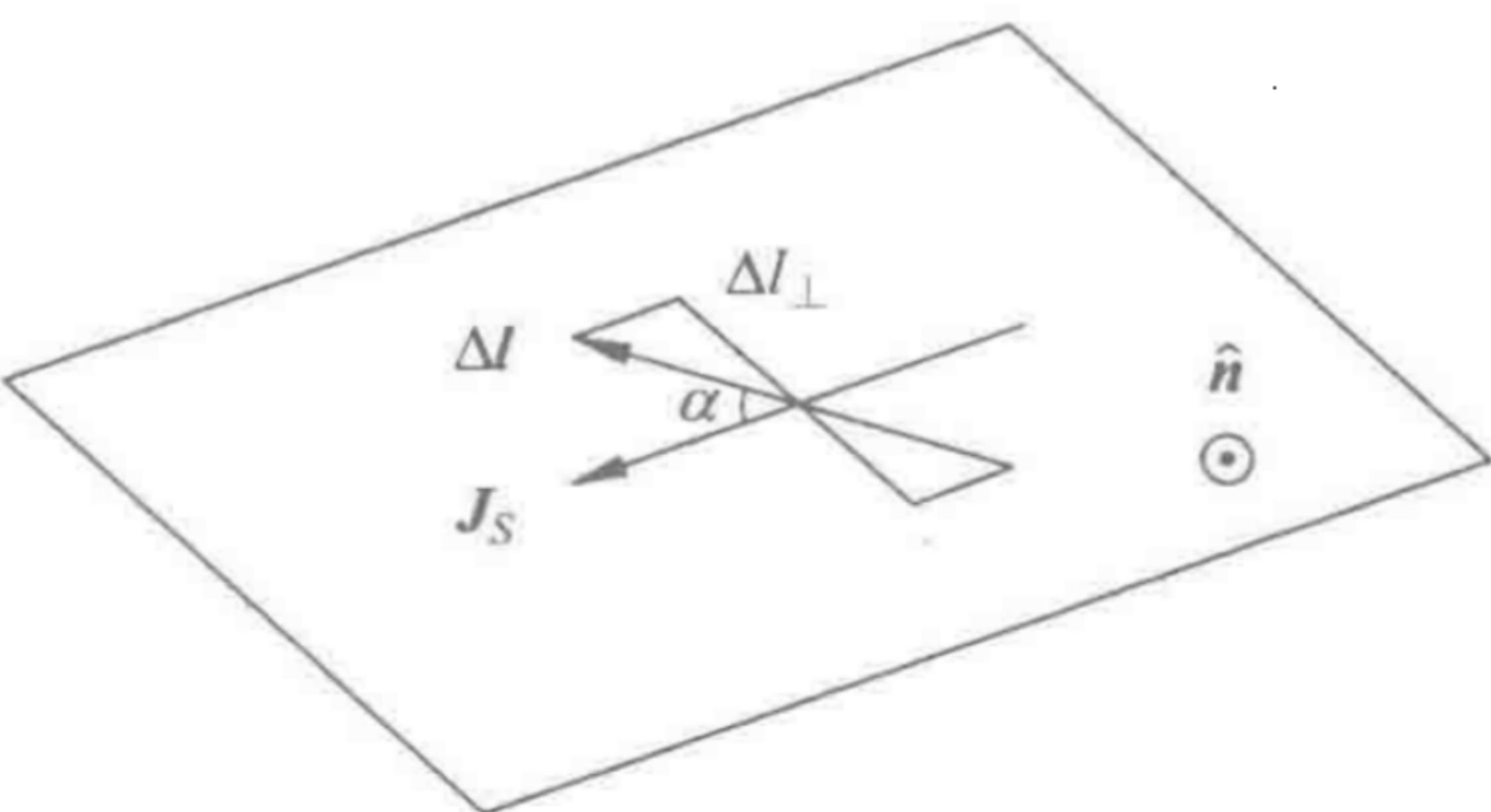


图 2.28 计算面电流

$$\text{线电流 } I = \frac{\partial q}{\partial t} = \rho_s V$$

电流元

$$\text{体电流元 } dq \vec{v} = \rho dV \vec{v} = \vec{J} dV$$

$$\text{面电流元 } dq \vec{v} = \rho dS \vec{v} = \vec{J}_s dS$$

$$\text{线电流元 } dq \vec{v} = \rho dl \vec{v} = I dl$$

2. 恒定电场的基本方程和边界条件

矢量场方程

$$\iiint_S \vec{J} \cdot d\vec{s} = - \frac{\partial q}{\partial t}$$

$$\iiint_V \nabla \cdot \vec{J} dV = - \iiint_V \frac{\partial \phi}{\partial t} dV$$

$$\nabla \cdot \vec{J} + \frac{\partial \phi}{\partial t} = 0$$

对于恒定电场，电荷的分布不变， $\frac{\partial q}{\partial t} = 0$

$$\iiint_S \vec{J} \cdot d\vec{s} = 0$$

$$\nabla \cdot \vec{J} = 0$$

$$\sum_k I_k = 0$$

$$\int_L \vec{E} \cdot d\vec{l} = 0$$

$$\nabla \times \vec{E} = 0$$

$$\nabla \times \nabla \Phi = 0$$

$$\vec{E} = -\nabla \Phi$$

位函数方程

$$\nabla \cdot \vec{J} = 0, \vec{J} = \sigma \vec{E}$$

$$\nabla \cdot \vec{J} = \nabla \cdot (\sigma \vec{E}) = \sigma \nabla \cdot (-\nabla \Phi) = -\sigma \nabla^2 \Phi = 0$$

$$\nabla^2 \Phi = 0$$

边界条件

$$J_{1n} = J_{2n}$$

$$\hat{n} \cdot (\vec{J}_1 - \vec{J}_2) = 0$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\sigma_1}{\sigma_2}$$

$$\Phi_1 = \Phi_2$$

$$\sigma_1 \frac{\partial \Phi_1}{\partial n} = \sigma_2 \frac{\partial \Phi_2}{\partial n}$$

3. 导电媒质中的传导电流

电源电动势 $E = \int_L \vec{E} \cdot d\vec{l}$

洛伦兹力 $\vec{f} = q \vec{v} \times \vec{B}$

非静电场强 $\vec{E}' = \frac{\vec{f}}{q} = \vec{v} \times \vec{B}$

动生电动势 $E = \int_L (\vec{v} \times \vec{B}) \cdot d\vec{l}$

均匀导体电阻 $R = \rho \frac{l}{S} = \frac{l}{\sigma S}$

不均匀导体电阻 $dR = \rho \frac{dl}{S} \quad R = \int_L \rho \frac{dl}{S} = \int_L \frac{dl}{\sigma S}$

电导 $G = \frac{1}{R}$

$$\text{欧姆定律 } I = \frac{V}{R}$$

$$I = \iint_S \vec{J} \cdot d\vec{s}, \quad V = \int_L \vec{E} \cdot d\vec{l}, \quad R = \int_L \rho \frac{dl}{s} \Rightarrow \vec{J} = \sigma \vec{E}$$

$$\text{焦耳定律 } P = I^2 R$$

$$\vec{J} = \rho \vec{v} = Nq \vec{v}$$

$$\text{每个电荷受的力 } \vec{F} = q \vec{E}$$

$$dt \text{ 内电场力对每个电荷做的功 } dA = \vec{F} \cdot d\vec{l} = q \vec{E} \cdot \vec{v} dt$$

$$dt \text{ 内电场力对 } dv \text{ 内所有电荷做的功 } dA = NdV \cdot q \vec{E} \cdot \vec{v} dt = \vec{J} \cdot \vec{E} dv dt$$

$$dt \text{ 内电场力对 } dv \text{ 内所有电荷做的功率为 } dp = \frac{dA}{dt} = \vec{J} \cdot \vec{E} dv$$

$$dt \text{ 内电场力对 } dv \text{ 内所有电荷做的功率密度为 } P = \frac{dp}{dv} = \vec{J} \cdot \vec{E}$$

导体内的净余电荷

$$\nabla \cdot \vec{J} = 0, \quad \vec{J} = \sigma \vec{E}$$

$$\sigma \nabla \cdot \vec{E} = 0, \quad \nabla \cdot \vec{E} = 0, \quad \nabla \cdot \vec{E} = \frac{\rho}{\epsilon}$$

$\rho = 0$, 恒定电场中导体内没有净余电荷

$$\text{给导体充电时 } \nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot \vec{J} = -\sigma \nabla \cdot \vec{E} = -\frac{\sigma}{\epsilon} \nabla \cdot \vec{D} = -\frac{\sigma}{\epsilon} \rho$$

$$\rho = \rho_0 e^{-\frac{\sigma}{\epsilon} t} = \rho_0 e^{-\frac{t}{T}}$$

$$T = \frac{\epsilon}{\sigma}, \text{ 驰豫时间}$$

	恒定电场	静电场
基本方程	$\nabla \times \vec{E} = 0 \quad (E = -\nabla \Phi)$ $\nabla \cdot \vec{J} = 0$ 导体内没有电荷分布 $\nabla^2 \Phi = 0$ 导体内没有电荷分布	$\nabla \times \vec{E} = 0 \quad (E = -\nabla \Phi)$ $\nabla \cdot \vec{D} = 0$ 没有电荷分布的区域 $\nabla^2 \Phi = 0$ 没有电荷分布的区域
边界条件	$J_{1n} = J_{2n}$ $E_{1t} = E_{2t}$ $\Phi_1 = \Phi_2$ $\sigma_1 \frac{\partial \Phi_1}{\partial n} = \sigma_2 \frac{\partial \Phi_2}{\partial n}$	$D_{1n} = D_{2n}$ $E_{1t} = E_{2t}$ $\Phi_1 = \Phi_2$ $\epsilon_1 \frac{\partial \Phi_1}{\partial n} = \epsilon_2 \frac{\partial \Phi_2}{\partial n}$
积分量	$I = \iint_S \vec{J} \cdot d\vec{S}$ $U = \int E \cdot d\vec{l}$ $G = I/U$	$q = \iint_S \vec{D} \cdot d\vec{S}$ $U = \int E \cdot d\vec{l}$ $C = q/U$
本构关系	$J = \sigma E$	$D = \epsilon E$

5. 接地

接地电阻 = 接地导线的电阻 + 接地体的电阻 + 接地体与大地之间的接触电阻 + 大地的电阻 ≈ 大地的电阻，一般要求接地电阻小于 2Ω 。

跨步电压

由 (2.179) 式，接地电极附近地面上任一点的电位可以写为

$$\Phi = \int_r^\infty \mathbf{E} \cdot d\mathbf{l} = \int_r^\infty \frac{Idr}{2\pi\sigma r^2} = \frac{I}{2\pi\sigma r} \quad (2.180)$$

由 (2.180) 式可以绘出沿地面电位 Φ 随距离 r 变化的曲线，如图 2.38 所示。可以看出，如果入地电流比较大（例如电力系统的接地电极和防雷系统的接地电极），在接地电极附近电位梯度很大，相隔一步之间的电位差可能超过人体的安全电压，称为跨步电压。

由 (2.179) 式可以计算图 2.38 中 A、B 两点之间的跨步电压

$$U_{AB} = \int_A^B \mathbf{E} \cdot d\mathbf{l} = - \int_A^B E dr = - \int_r^{r+b} \frac{Idr}{2\pi\sigma r^2} = \frac{I}{2\pi\sigma} \left(\frac{1}{r} - \frac{1}{r+b} \right) \approx \frac{Ib}{2\pi\sigma r^2} \quad (2.181)$$

设人体的安全电压为 U_0 （一般取为交流 30V，直流 50V），由 (2.181) 式可以求出危险区的半径为

$$r_0 = \sqrt{\frac{Ib}{2\pi\sigma U_0}} \quad (2.182)$$

三、恒定磁场场

① 恒定磁场的基本规律

1. 磁感应强度 B

$$\text{毕奥-萨伐尔定律} \quad d\vec{B} = \frac{\mu}{4\pi} \frac{I d\vec{l}' \times \hat{e}_r}{r^2}$$

$$\text{一个线电流回路产生的磁场} \quad \vec{B} = \frac{\mu}{4\pi} \oint_L \frac{I d\vec{l}' \times \hat{e}_r}{r^2}$$

$$\text{体电流产生的磁场} \quad \vec{B} = \frac{\mu}{4\pi} \iiint_V \frac{I dV' \times \hat{e}_r}{r^2}$$

$$\text{面电流产生的磁场} \quad \vec{B} = \frac{\mu}{4\pi} \iint_S \frac{I dS' \times \hat{e}_r}{r^2}$$

2. 磁感应线方程

$$\text{直角坐标系中} \quad \frac{dx}{B_x} = \frac{dy}{B_y} = \frac{dz}{B_z}$$

$$\text{柱坐标系中} \quad \frac{dr}{B_r} = \frac{rd\varphi}{B_\theta} = \frac{dz}{B_z}$$

$$\text{球坐标系中} \quad \frac{dr}{B_r} = \frac{r d\theta}{B_\theta} = \frac{rsin\theta d\varphi}{B_z}$$

3. 恒定磁场基本方程

$$\left\{ \begin{array}{l} \oint_S \vec{B} \cdot d\vec{s} = 0 \\ \oint_L \vec{B} \cdot d\vec{l} = \mu_0 \sum I_i \end{array} \right. \quad \begin{array}{l} \text{高斯定理} \\ \text{环路定理} \end{array}$$

后续内容实为复习材料，已无力做到一二章详细程度，下页省略不重要内容

$$\left\{ \begin{array}{l} \nabla \cdot \vec{B} = 0 \\ \nabla \times \vec{H} = \vec{J} \end{array} \right.$$

4. 磁介质的磁化

$$\text{磁化强度} \quad \vec{M} = \lim_{\Delta V \rightarrow 0} \frac{\sum \vec{m}}{\Delta V}$$

$$\vec{A} = \frac{\mu_0}{4\pi} \frac{\vec{m} \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$d\vec{A} = \frac{\mu_0}{4\pi} \frac{\vec{M}(\vec{r}') dV' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$\vec{A} = \frac{\mu_0}{4\pi} \int_V \vec{M}(\vec{r}') \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} dV'$$

$$= \frac{\mu_0}{4\pi} \int_V \vec{M}(\vec{r}') \times \nabla' \frac{1}{|\vec{r} - \vec{r}'|} dV'$$

$$= \frac{\mu_0}{4\pi} \int_V \frac{\nabla' \times \vec{M}'(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' - \frac{\mu_0}{4\pi} \int_V \nabla' \times \frac{\vec{M}'(\vec{r}')}{|\vec{r} - \vec{r}'|} dV'$$

$$= \frac{\mu_0}{4\pi} \int_V \frac{\nabla' \times \vec{M}'(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' + \frac{\mu_0}{4\pi} \oint_S \frac{\vec{M}'(\vec{r}')}{|\vec{r} - \vec{r}'|} \times d\vec{s}'$$

$$= \frac{\mu_0}{4\pi} \int_V \frac{\nabla' \times \vec{M}'(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' + \frac{\mu_0}{4\pi} \oint_S \frac{\vec{M}'(\vec{r}') \times \vec{n}}{|\vec{r} - \vec{r}'|} \times d\vec{s}'$$

$$\vec{B}' = \frac{\mu_0}{4\pi} \int_V \frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' + \frac{\mu_0}{4\pi} \oint_S \frac{\vec{J}_s(\vec{r}')}{|\vec{r} - \vec{r}'|} \times d\vec{s}'$$

$$\left\{ \begin{array}{l} \vec{J}_m(\vec{r}') = \nabla' \times \vec{M}'(\vec{r}') , \quad \vec{J}_{ms}(\vec{r}') = \vec{M}'(\vec{r}') \times \vec{n} \\ \vec{J}_{ms} = \vec{M}' \times \vec{n} , \quad \vec{J}_m = \nabla \times \vec{M}' \end{array} \right.$$

$$\left\{ \begin{array}{l} \nabla \times \vec{B}' = \mu_0 (\vec{J} + \vec{J}_m) = \mu_0 (\vec{J} + \nabla \times \vec{M}') \end{array} \right.$$

$$\nabla \times (\frac{\vec{B}}{\mu_0} - \vec{M}) = \vec{J}$$

$$\nabla \times \vec{H} = \vec{J}$$

$$\left\{ \begin{array}{l} \vec{H}' = \frac{\vec{B}'}{\mu_0} - \vec{M}' \end{array} \right.$$

$$\vec{M}' = \chi_m \vec{H}'$$

$$1 + \chi_m = \mu_r$$

$$\vec{B} = \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

5. 石蕊路

$$\Phi = \frac{L_m}{R_m}$$

$$E_m = Nl \text{ 称为石蕊电动势} , \quad R_m = \frac{l}{\mu s} \text{ 为石蕊阻}$$

② 恒定磁场的边界条件

$$\left\{ \begin{array}{l} \vec{n} \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s \\ \vec{n} \cdot (\vec{B}_1 - \vec{B}_2) = 0 \end{array} \right. \quad \left\{ \begin{array}{l} H_{1t} - H_{2t} = J_s \\ B_{1n} = B_{2n} \end{array} \right.$$

③ 矢量磁位

$$\vec{B} = \nabla \times \vec{A}$$

库仑规范 $\nabla \cdot \vec{A} = 0$

$$\nabla^2 \vec{A} = -\mu_0 \vec{J}$$

④ 标量的磁位

没有电流分布的区域 $\vec{H} = -\nabla \Phi_m$

$$\nabla^2 \Phi_m = 0$$

$$\Phi_{m1} = \Phi_{m2}$$

$$\mu_1 \frac{\partial \Phi_{m1}}{\partial n} = \mu_2 \frac{\partial \Phi_{m2}}{\partial n}$$

⑤ 互感

自感系数 L , $\Psi_L = L I = \sum_i \Phi_i$

互感系数 M , $\Psi_{12} = M_{12} I_1$, $\Psi_{21} = M_{21} I_2$

2. M 和 L 的计算

1) 利用定义式计算

计算自感系数

由

$$I \rightarrow \phi_L \rightarrow L = \frac{\phi_L}{I}$$

计算互感系数

$$I_1 \rightarrow \phi_{12} \rightarrow M = \frac{\phi_{12}}{I_1} \quad \text{或} \quad I_2 \rightarrow \phi_{21} \rightarrow M = \frac{\phi_{21}}{I_2}$$

计算 ϕ_{12} 还是计算 ϕ_{21} , 可以根据问题中的条件选择简便的方法。

2) 利用矢量磁位 A 计算 L 和 M

(1) 利用矢量磁位 A 计算磁通量

$$\Phi = \oint_l \vec{A} \cdot d\vec{l}$$

(2) 利用矢量磁位 A 计算 L 和 M

$$M = N_1 N_2 \frac{\mu_0}{4\pi} \oint_{l_1} \oint_{l_2} \frac{d\vec{l}_1 \cdot d\vec{l}_2}{r}$$

$$L = N^2 \frac{\mu_0}{4\pi} \oint_{l_2} \oint_{l_1} \frac{d\vec{l}_1 \cdot d\vec{l}_2}{r}$$

利用矢量磁位 A 计算 L 和 M 的公式形式上相同, l_1 、 l_2 表示的意义不同。

⑥ 磁场的能量

$$W_m = \frac{1}{2} \sum_{j=1}^N \sum_{k=1}^N M_k I_k L_j = \frac{1}{2} \sum_{j=1}^N I_j \Psi_j$$

$$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} dV$$

$$W_m = \frac{1}{2} \vec{H} \cdot \vec{B} = \frac{1}{2} \mu H^2$$

⑦ 磁场力

$$\left\{ \begin{array}{l} d\vec{f} = I d\vec{l} \times \vec{B} \\ \vec{f} = \int_V I d\vec{l} \times \vec{B} \end{array} \right.$$

$$\left\{ \begin{array}{l} \vec{F} = \int_V \vec{j} dV \times \vec{B} \\ \vec{f} = \int_S \vec{j}_s ds \times \vec{B} \end{array} \right.$$

$$\left\{ \begin{array}{l} d\vec{f}_{12} = I_2 d\vec{l}_2 \times \vec{B}_{12} = \frac{\mu_0}{4\pi} \frac{I_2 d\vec{l}_2 \times (I_1 d\vec{l}_1 \times \vec{e}_R)}{R^2} \\ f_{12} = \frac{\mu_0}{4\pi} \oint_L \oint_{L'} \frac{I_2 d\vec{l}_2 \times (I_1 d\vec{l}_1 \times \vec{e}_R)}{R^2} \end{array} \right.$$

$$\left\{ \begin{array}{l} \vec{F} = q \vec{v} \times \vec{B} \\ f = - \frac{\partial W_m}{\partial q} | \Psi_j = C \\ f = \frac{\partial W_m}{\partial q} | I_j = C \\ f = I_1 I_2 \frac{\partial M}{\partial q} \end{array} \right.$$

$$\text{洛伦兹力 } \vec{F} = q \vec{v} \times \vec{B}$$

四、静态场边值问题的解法

① 电磁场边值问题概述

1. 三类边值问题(以静电场为例)

(1) 第一类边值问题: 给定边界面上的电位 $\Phi|_S$ 。

(2) 第二类边值问题: 给定边界面上电位的法线导数 $\frac{\partial \Phi}{\partial n}|_S$, 对于导体就是给定导体表面电荷的分布。这是因为导体表面的面电荷密度 $\rho_s = \epsilon E_n = -\epsilon \frac{\partial \Phi}{\partial n}$ 。

(3) 第三类边值问题: 一部分边界上给定边界面上的电位 $\Phi|_S$, 另一部分边界上给定边界面上电位的法线导数 $\frac{\partial \Phi}{\partial n}|_S$ (对于导体就是给定导体表面电荷的分布)。

表 4.1 静电场、恒定电场、恒定磁场满足的微分方程

	泊松方程	拉普拉斯方程
静电场	$\nabla^2 \Phi = -\frac{\rho}{\epsilon}$	$\nabla^2 \Phi = 0 \quad (\rho = 0 \text{ 的区域})$
恒定电场		$\nabla^2 \Phi = 0$
恒定磁场	$\nabla^2 \mathbf{A} = -\mu \mathbf{J}$	$\nabla^2 \Phi_m = 0 \quad (\mathbf{J} = 0 \text{ 的区域})$

表 4.2 静电场、恒定电场、恒定磁场边界上的衔接条件

静电场	$\Phi_1 = \Phi_2$	$\epsilon_1 \frac{\partial \Phi_1}{\partial n} = \epsilon_2 \frac{\partial \Phi_2}{\partial n}$
恒定电场	$\Phi_1 = \Phi_2$	$\sigma_1 \frac{\partial \Phi_1}{\partial n} = \sigma_2 \frac{\partial \Phi_2}{\partial n}$
恒定磁场	$\Phi_{m1} = \Phi_{m2}$	$\mu_1 \frac{\partial \Phi_{m1}}{\partial n} = \mu_2 \frac{\partial \Phi_{m2}}{\partial n}$

② 直角坐标系中的分离变量法

$$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} + \frac{\partial^2 \Phi}{\partial z^2} = 0$$

$$\text{同阶 } f(x)g(y)h(z): \frac{1}{f(x)} \frac{d^2 f(x)}{dx^2} + \frac{1}{g(y)} \frac{d^2 g(y)}{dy^2} + \frac{1}{h(z)} \frac{d^2 h(z)}{dz^2} = 0$$

设每项分别为 $-k_x^2, -k_y^2, -k_z^2$

$$\text{有 } \frac{d^2 f(x)}{dx^2} + k_x^2 f(x) = 0, \quad k_x^2 + k_y^2 + k_z^2 = 0$$

若 k_x 为实数, $f(x) = A_1 \sin k_x x + A_2 \cos k_x x$ 周期函数

若 k_x 为虚数, $f(x) = B_1 \sinh d_x x + B_2 \cosh d_x x$ 或 $B'_1 e^{d_x x} + B'_2 e^{-d_x x}$ 单调函数

若 $x=0$ 时 $\Phi=0$, 为双曲函数, 若 $x=\infty$ 时, $\Phi=0$, 为指数函数

通解 $\Phi(x, y, z) = f(x)g(y)h(z)$

(3) 圆柱坐标系中的分离变量法

二维：

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \Psi}{\partial r} \right) + \frac{1}{r^2} \cdot \frac{\partial^2 \Psi}{\partial \varphi^2} = 0$$

$$\text{同乘 } \frac{r^2}{f(r)g(\varphi)} : \frac{r}{f(r)} \cdot \frac{\partial}{\partial r} \left(r \frac{\partial f(r)}{\partial r} \right) + \frac{1}{g(\varphi)} \frac{\partial^2 g(\varphi)}{\partial \varphi^2} = 0$$

设分别为 r^2 和 $-r^2$

$$\frac{d^2 g(\varphi)}{d \varphi^2} + r^2 g(\varphi) = 0$$

$$r^2 \frac{d^2 f(r)}{d r^2} + r \frac{d f(r)}{d r} - r^2 f(r) = 0$$

$$g(\varphi) = A_n \sin n\varphi + B_n \cos n\varphi$$

$$f(r) = C_n r^n + \frac{D_n}{r^n}$$

$$\text{通解 } \Psi(r, \varphi) = \sum_{n=1}^{\infty} (A_n \sin n\varphi + B_n \cos n\varphi) \left(C_n r^n + \frac{D_n}{r^n} \right)$$

(4) 球坐标系的分离变量法

轴对称场 (5个无关) :

$$\text{通解 } \Psi(r, \theta) = \sum_{m=0}^{\infty} \left(A_m r^m + \frac{B_m}{r^{m+1}} \right) P_m(\cos \theta)$$

$$P_m(x) = \frac{1}{2^m m!} \cdot \frac{d^m}{dx^m} (x^2 - 1)^m \text{ 勒让德多项式}$$

$$P_0(x) = 1, P_1(x) = x$$

⑤ 镜像法

1. 点电荷对无限大导体平面的镜像

$$q' = q$$

$$h' = h$$

2. 点电荷对介质平面的镜像

上半空间: $q' = -\frac{\epsilon_2 - \epsilon_1}{\epsilon_2 + \epsilon_1} q, z = -h$

下半空间: $q'' = \frac{\epsilon_2 - \epsilon_1}{\epsilon_2 + \epsilon_1} q, z = h$

3. 点电荷对导体球的镜像

$$q_2 = -\frac{a}{d_1} q_1, d_2 = \frac{a^2}{d_1}$$

五、时变电磁场

① 电磁感应定律

$$\text{动生电动势: } e_i = \int_L (\vec{v} \times \vec{B}) \cdot d\vec{l}$$

$$\text{感生电动势: } e_i = \oint_L \vec{E}_i \cdot d\vec{l}$$

$$\text{法拉第定律: } e_i = - \frac{d\psi}{dt} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

麦克斯韦关于感应电场(涡旋电场)的假说的基本根据:

变化的磁场在其周围空间激发涡旋电场

$$\left\{ \begin{array}{l} \oint_L \vec{E} \cdot d\vec{l} = \oint_L (\vec{E}_k + \vec{E}_i) \cdot d\vec{l} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} + \int_L (\vec{v} \times \vec{B}) \cdot d\vec{l} \\ \nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} + \nabla \times (\vec{v} \times \vec{B}) \end{array} \right.$$

$$\Rightarrow \left\{ \begin{array}{l} \oint_L \vec{E} \cdot d\vec{l} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \\ \nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} \end{array} \right.$$

② 位移电流

麦克斯韦关于位移电流的假说的基本根据:

变化的电场在其周围空间激发涡旋磁场

$$\left\{ \begin{array}{l} \oint_L \vec{H} \cdot d\vec{l} = I_L + I_d = \iint_S \vec{J} \cdot d\vec{s} + \iint_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s} \\ \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \end{array} \right.$$

③ 麦克斯韦方程组

$$\left\{ \begin{array}{l} \oint_L \vec{H} \cdot d\vec{l} = \iint_S (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s} \\ \oint_L \vec{E} \cdot d\vec{l} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \\ \iint_S \vec{B} \cdot d\vec{s} = 0 \\ \iint_S \vec{D} \cdot d\vec{s} = q \end{array} \right. \quad \left\{ \begin{array}{l} \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \\ \nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} \\ \nabla \cdot \vec{B} = 0 \\ \nabla \cdot \vec{D} = \rho \end{array} \right. \quad \left\{ \begin{array}{l} \vec{D} = \epsilon_0 \epsilon_r \vec{E} \\ \vec{B} = \mu_0 \mu_r \vec{H} \\ \vec{J} = \sigma \vec{E} \end{array} \right.$$

④ 时变电磁场的边界条件

$$\left\{ \begin{array}{l} \vec{n} \times (\vec{E}_1 - \vec{E}_2) = 0 \\ \vec{n} \times (\vec{H}_1 - \vec{H}_2) = \vec{j}_s \\ \vec{n} \cdot (\vec{B}_1 - \vec{B}_2) = 0 \\ \vec{n} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_s \end{array} \right. \quad \left\{ \begin{array}{l} E_{1t} = E_{2t} \\ H_{1t} - H_{2t} = j_s \\ B_{1n} = B_{2n} \\ D_{1n} - D_{2n} = \rho_s \end{array} \right. \quad \left\{ \begin{array}{l} E_{1t} = E_{2t} = 0 \\ H_{1t} = j_s \\ B_{1n} = B_{2n} = 0 \\ D_{1n} = \rho_s \end{array} \right.$$

⑤ 坡印廷定理和坡印廷矢量

$$\vec{S} = \vec{E} \times \vec{H}$$

$$\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

$$\nabla \times \vec{H} = \vec{j} + \frac{\partial \vec{D}}{\partial t}$$

$$\vec{H} \cdot (\nabla \times \vec{E}) - \vec{E} \cdot (\nabla \times \vec{H}) = - \vec{H} \cdot \frac{\partial \vec{B}}{\partial t} - \vec{E} \cdot \vec{j} - \vec{E} \cdot \frac{\partial \vec{D}}{\partial t}$$

$$\vec{j} \cdot (\vec{E} \times \vec{H}) = - \vec{B} \cdot \frac{\partial \vec{H}}{\partial t} - \vec{E} \cdot \vec{j} - \vec{D} \cdot \frac{\partial \vec{E}}{\partial t}$$

$$= - \frac{1}{2} (\vec{H} \cdot \frac{\partial \vec{B}}{\partial t} + \vec{B} \cdot \frac{\partial \vec{H}}{\partial t}) - \vec{E} \cdot \vec{j} - \frac{1}{2} (\vec{E} \cdot \frac{\partial \vec{D}}{\partial t} + \vec{D} \cdot \frac{\partial \vec{E}}{\partial t})$$

$$= - \frac{\partial}{\partial t} \left(\frac{1}{2} \vec{E} \cdot \vec{B} \right) - \vec{E} \cdot \vec{j} - \frac{\partial}{\partial t} \left(\frac{1}{2} \vec{H} \cdot \vec{B} \right)$$

$$\int_V \nabla \cdot (\vec{E} \times \vec{H}) dV = - \frac{\partial}{\partial t} \int_V W dV - \int_V P dV$$

$$\frac{\partial W}{\partial t} = - \oint (\vec{E} \times \vec{H}) \cdot d\vec{s} - \int_V \vec{E} \cdot \vec{j} dV$$

⑥ 时变电磁场的矢量位和标量位

$$\text{由 } \nabla \cdot \vec{B} = 0, \quad \vec{B} = \nabla \times \vec{A}$$

$$\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} = - \frac{\partial}{\partial t} (\nabla \times \vec{A}) = - \nabla \times \frac{\partial \vec{A}}{\partial t}, \quad E + \frac{\partial A}{\partial t} = - \nabla \Phi / \vec{E} = - \nabla \Phi - \frac{\partial \vec{A}}{\partial t}$$

$$\text{洛伦兹条件 } \nabla \cdot \vec{A} = - \mu \epsilon \frac{\partial \Phi}{\partial t}$$

达朗贝尔方程

$$\nabla \times (\nabla \times \vec{A}) = \nabla \times \vec{B} = \mu \nabla \times \vec{H}$$

将 $\nabla \times \vec{H} = \vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t}$ 和 $\vec{E} = -\nabla \Phi - \frac{\partial \vec{A}}{\partial t}$ 代入

$$\nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A} = \mu \vec{J} - \mu \epsilon \frac{\partial}{\partial t}(\nabla \Phi) - \mu \epsilon \frac{\partial^2 \vec{A}}{\partial t^2}$$

$$\nabla^2 A^2 - \mu \epsilon \frac{\partial^2 \vec{A}}{\partial t^2} = \nabla(\nabla \cdot \vec{A}) - \mu \vec{J} + \nabla(\mu \epsilon \frac{\partial \vec{A}}{\partial t}) = \nabla(\nabla \cdot \vec{A} + \mu \epsilon \frac{\partial \vec{A}}{\partial t}) - \mu \vec{J}$$

$$\nabla^2 \vec{A} - \mu \epsilon \frac{\partial^2 \vec{A}}{\partial t^2} = -\mu \vec{J}$$

$$\vec{E} = -\nabla \Phi - \frac{\partial \vec{A}}{\partial t}$$

$$\nabla \cdot \vec{E} = -\nabla \cdot (\nabla \Phi + \frac{\partial \vec{A}}{\partial t})$$

$$\epsilon(\nabla \cdot \vec{E}) = -\epsilon \nabla \cdot (\nabla \Phi + \frac{\partial \vec{A}}{\partial t}) = \rho$$

$$\nabla^2 \Phi + \nabla \cdot \frac{\partial \vec{A}}{\partial t} = -\frac{\rho}{\epsilon}$$

$$\nabla \cdot \frac{\partial \vec{A}}{\partial t} = \frac{\partial}{\partial t} \nabla \cdot \vec{A} = \frac{\partial}{\partial t} (-\mu \epsilon \frac{\partial \Phi}{\partial t})$$

$$\nabla^2 \Phi - \mu \epsilon \frac{\partial^2 \Phi}{\partial t^2} = -\frac{\rho}{\epsilon}$$

六、平面电磁波

① 正弦电磁场的复数表示方法

1. 电磁场量的复数形式

$$E(x, y, z, t) = E_m(x, y, z) \cos(\omega t + \psi) = \operatorname{Re} [E_m(x, y, z) e^{j(\omega t + \psi)}]$$

$$E = \operatorname{Re} [E_m e^{j(\omega t + \psi)}] = \operatorname{Re} [E_m e^{j\psi} \cdot e^{j\omega t}] = \operatorname{Re} [\dot{E}_m \cdot e^{j\omega t}]$$

略去 Re , $E = \dot{E}_m e^{j\omega t}$

2. 麦克斯韦方程组的复数形式

$$\nabla \cdot \vec{D} = \rho$$

$$\nabla \cdot \vec{j} + j\omega \rho = 0$$

$$\nabla \times \vec{E} = -j\omega \vec{B}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{B} = \vec{j} + j\omega \vec{D}$$

② 平均坡印廷矢量

$$S_{av} = \frac{1}{2} \operatorname{Re} (\vec{E} \times \vec{H}^*)$$

$$S_{av} = \frac{1}{T} \int_0^T S_n dt = \frac{1}{T} \int_0^T (E_y H_z - E_z H_y) dt = \frac{1}{T} \int_0^T [E_{ym} H_{zm} \cos(\omega t + \psi_{yE}) \cos(\omega t + \psi_{zH}) \\ - E_{zm} H_{ym} \cos(\omega t + \psi_{zE}) \cos(\omega t + \psi_{yH})] dt$$

$$S_{av} = \frac{1}{2} [E_{ym} H_{zm} \cos(\psi_{yE} - \psi_{zH}) - E_{zm} H_{ym} \cos(\psi_{zE} - \psi_{yH})] \\ = \frac{1}{2} \operatorname{Re} [\dot{E}_y H_z^* - \dot{E}_z H_y^*]$$

$$\text{同理, } S_{av} = \frac{1}{2} \operatorname{Re} (\dot{E} \times \dot{H}^*)$$

③ 理想介质中的均匀平面波

1. 电磁波传播的基本方程

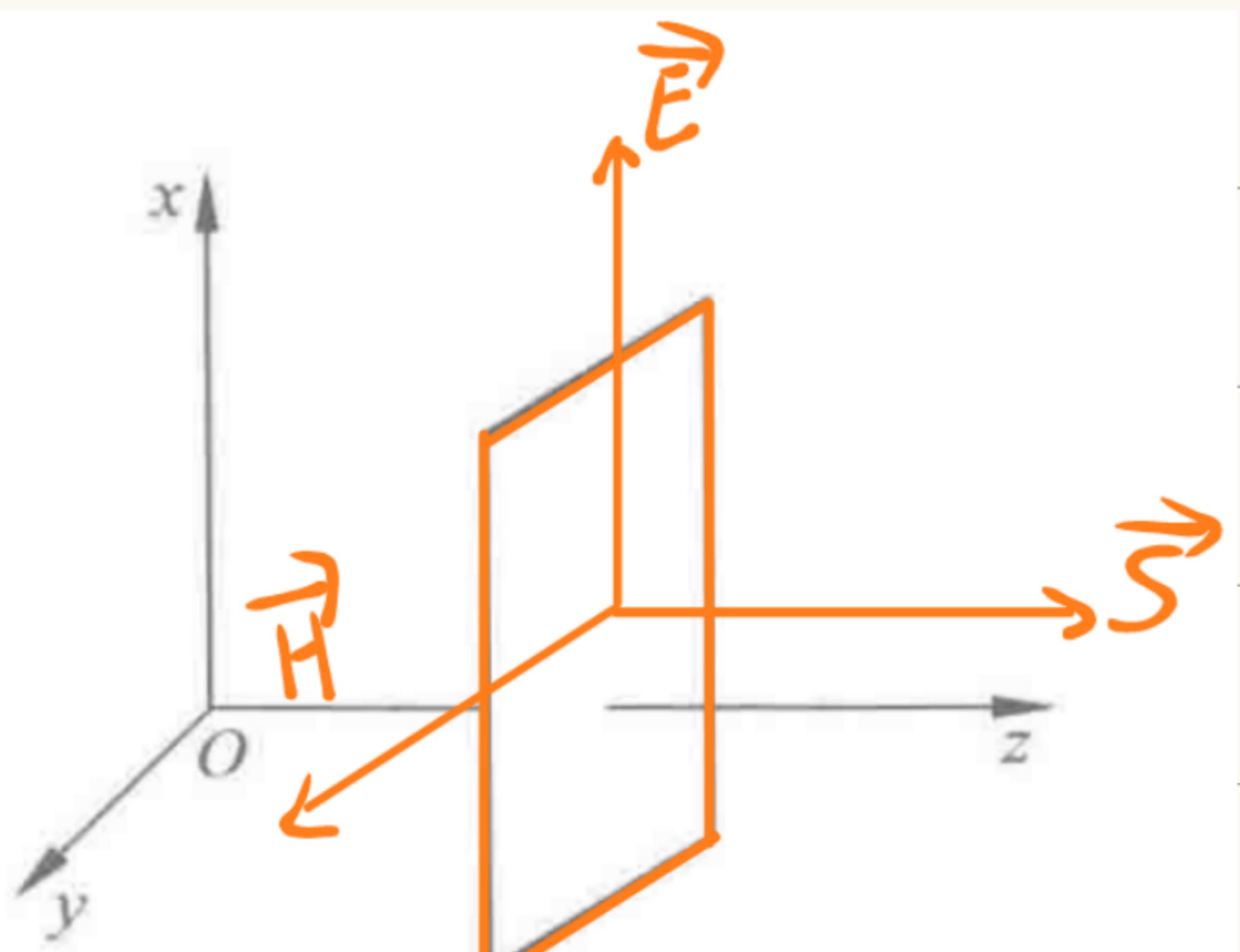
$$\left\{ \begin{array}{l} \nabla \times \vec{H} = j\omega \epsilon \vec{E} \\ \nabla \times \vec{E} = -j\omega \mu \vec{H} \\ \nabla \cdot \vec{H} = 0 \\ \nabla \cdot \vec{E} = 0 \end{array} \right. \quad \begin{array}{l} \nabla \times (\nabla \times \vec{E}) = -j\omega \mu (j\omega \epsilon \vec{E}) \\ \nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = \mu \epsilon \omega^2 \vec{E} \\ \nabla^2 \vec{E} + \mu \epsilon \omega^2 \vec{E} = 0 \end{array}$$

$$\mu \epsilon = \frac{1}{v^2}$$

$$k^2 = \frac{\omega^2}{v^2} = \omega^2 \mu \epsilon, k \text{ 称为波数}$$

$$\left\{ \begin{array}{l} \nabla^2 \vec{E} + k^2 \vec{E} = 0 \\ \nabla^2 \vec{H} + k^2 \vec{H} = 0 \end{array} \right.$$

2. 均匀平面电磁波



由波动方程可得

$$\frac{d^2 E_x}{dz^2} + k^2 E_x = 0$$

$$\frac{d^2 H_y}{dz^2} + k^2 H_y = 0$$

图 6.3 均匀平面电磁波

解得 $E_x = E_m^+ e^{-jkz} + E_m^- e^{jkz}$

$$H_y = -\frac{1}{j\omega \mu} (\nabla \times E_x) = \frac{k}{\omega \mu} (E_m^+ e^{-jkz} - E_m^- e^{jkz})$$

$$\text{取 } E_m^+ e^{jkz} e^{j\omega t} = E_m^+ e^{j(\omega t - kz + \psi^+)} \stackrel{\text{Re}}{=} E_m^+ \cos(\omega t - kz + \psi^+) = E_m^+ \cos[\omega t - \frac{z}{v}] + \psi^+$$

在无限大的介质中，没有反射波

$$\left\{ \begin{array}{l} \dot{E}_x = E_m e^{-jkz} \\ \dot{H}_y = \frac{k}{\omega \mu} E_m e^{-jkz} \end{array} \right. \quad \left\{ \begin{array}{l} E_x = E_m \cos(\omega t - kz + \psi^+) \\ H_y = \frac{k}{\omega \mu} \cos(\omega t - kz + \psi^+) \end{array} \right.$$

$$T = \frac{1}{f} = \frac{2\pi}{\omega}$$

$$V = \lambda f = \frac{1}{\sqrt{\mu \epsilon}}$$

$$k = \frac{\omega}{V} = \frac{2\pi}{\lambda} = \omega \sqrt{\mu \epsilon}$$

$$\eta = \frac{E_x}{H_y} = \frac{\omega \mu}{k} = \sqrt{\frac{\mu}{\epsilon}}$$

沿传播方向 \vec{e}_n 传播的均匀平面波

$$\vec{E} = \vec{E}_m e^{-jkz} \Rightarrow \vec{E} = \vec{E}_m e^{-jk(\vec{e}_n \cdot \vec{r})}$$

④ 波的极化特性

1. E_x, E_y 相位相同

$$\left\{ \begin{array}{l} E_x = E_{xm} \cos(\omega t - kz) \\ E_y = E_{ym} \cos(\omega t - kz) \end{array} \right.$$
$$E = \sqrt{E_x^2 + E_y^2} = \sqrt{E_{xm}^2 + E_{ym}^2} \cos(\omega t - kz)$$

$$\alpha = \arctan \frac{E_y}{E_x} = \arctan \frac{E_{ym}}{E_{xm}}$$

线极化波

2. E_x, E_y 相位相差 $\frac{\pi}{2}$ 且 $E_{xm} = E_{ym}$

$$\left\{ \begin{array}{l} E_x = E_{xm} \cos(\omega t - kz) \\ E_y = E_{ym} \cos(\omega t - kz - \frac{\pi}{2}) = E_{ym} \sin(\omega t - kz) \end{array} \right.$$

若 $E_{xm} = E_{ym} = E_m$

$$E = \sqrt{E_x^2 + E_y^2} = E_m, \quad \alpha = \arctan \frac{E_y}{E_x} = \omega t - kz$$

圆极化波

3. 其它

带有圆极化波

(3) 电矢量 \vec{E} 的旋转方向。

圆极化波和椭圆极化波根据电矢量 \vec{E} 的旋转方向, 又可以分为右旋极化波和左旋极化波。若 \vec{E} 的旋转方向与传播方向成右手关系, 称为右旋极化波; 若 \vec{E} 的旋转方向与传播方向成左手关系, 称为左旋极化波, 如图 6.11 所示。

⑤ 损耗媒质中的均匀平面波

1. 损耗媒质中电磁场的基本方程

$$\left\{ \begin{array}{l} \nabla \times \vec{H} = \sigma \vec{E} + j\omega \epsilon \vec{E} \\ \nabla \times \vec{E} = -j\omega \mu \vec{H} \\ \nabla \cdot \vec{H} = 0 \\ \nabla \cdot \vec{E} = 0 \end{array} \right. \quad \begin{array}{l} \nabla \times (\nabla \times \vec{E}) = -j\omega \mu (\sigma + j\omega \epsilon) \vec{E} \\ \nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = \omega^2 \mu \epsilon (1 - j\frac{\sigma}{\omega \epsilon}) \vec{E} \\ \nabla^2 \vec{E} + \mu \epsilon \omega^2 \vec{E} = 0 \end{array}$$

$$\epsilon_c = \epsilon (1 - j \frac{\sigma}{\omega \epsilon})$$

$$\gamma^2 = -\omega^2 \mu \epsilon_c, \quad Y = j\omega \sqrt{\mu \epsilon_c} = \alpha + j\beta$$

$$\left\{ \begin{array}{l} \nabla^2 \vec{E} - \gamma^2 \vec{E} = 0 \\ \nabla^2 \vec{H} - \gamma^2 \vec{H} = 0 \end{array} \right.$$

2. 损耗媒质中 \vec{E} 、 \vec{H} 的表达式

由波动方程可得

$$\frac{d^2 E_x}{dz^2} - \gamma^2 E_x = 0$$

$$\frac{d^2 H_y}{dz^2} - \gamma^2 H_y = 0$$

$$\dot{E}_x = \dot{E}_x^+ e^{-\gamma z} + \dot{E}_x^- e^{\gamma z}$$

不考虑反射波

$$\dot{E}_x = \dot{E}_x^+ e^{-\gamma z} = \dot{E}_x^+ e^{-\alpha z} e^{-j\beta z}$$

$$E_x = E_{xm}^+ e^{-\alpha z} \cos(\omega t - \beta z + \psi_m)$$

$$\dot{H}_y = -\frac{1}{j\omega\mu} -\gamma \dot{E}_x = \frac{\alpha + j\beta}{j\omega\mu} \dot{E}_x^+ e^{-\alpha z} e^{-j\beta z}$$

$$\therefore \frac{\alpha + j\beta}{j\omega\mu} E_{xm}^+ = H_{ym}^+ e^{j\psi_m}$$

$$H_y = H_{ym}^+ e^{-\alpha z} \cos(\omega t - \beta z + \psi_m)$$

3. 导电媒质中电磁波的传播特性

损耗角 δ_c

$$\tan |\delta_c| = \frac{\sigma}{\omega\epsilon} = \frac{\sigma E}{\omega\epsilon E} = \frac{|j|}{|\frac{\partial E}{\partial t}|} = \frac{\text{传导电流}}{\text{位移电流}}$$

传播常数 γ

$$\gamma = j\omega \sqrt{\mu\epsilon_r} = j\omega \sqrt{\mu(\epsilon - j\frac{\sigma}{\omega})} = \alpha + j\beta$$

$$\text{解得 } \alpha = \omega \sqrt{\frac{\mu\epsilon_r}{2} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon_r^2}} - 1 \right)}$$

$$\beta = \omega \sqrt{\frac{\mu\epsilon_r}{2} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon_r^2}} + 1 \right)}$$

波阻抗 η_c

$$\eta_c = \frac{\dot{E}_x}{\dot{H}_y} = \frac{j\omega\mu}{\alpha + j\beta} = \sqrt{\frac{\mu}{\epsilon_r}} = \sqrt{\frac{\mu}{\epsilon(1 - j\frac{\sigma}{\omega\epsilon})}} = \frac{\eta}{\sqrt{1 - j\frac{\sigma}{\omega\epsilon}}}$$

相速度和波长

$$v = \frac{\omega}{\beta} = \frac{1}{\sqrt{\frac{\mu\epsilon_r}{2} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon_r^2}} + 1 \right)}}$$

$$\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{\omega \sqrt{\frac{\mu\epsilon_r}{2} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2\epsilon_r^2}} + 1 \right)}}$$

4. 弱导电媒质中的均匀平面波

$$\frac{\sigma}{\omega\epsilon} \ll 1$$

$$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2}} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} - 1 \right) \approx \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$$

$$\beta = \omega \sqrt{\frac{\mu \epsilon}{2}} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} + 1 \right) \approx \omega \sqrt{\mu \epsilon}$$

$$\eta_c = \frac{\eta}{1 + j \frac{\sigma}{2\omega\epsilon}}$$

$$\lambda = \frac{2\pi}{\beta} = \frac{\nu}{f}$$

$$v = \frac{\nu}{\beta} = \frac{1}{\sqrt{\mu\epsilon}}$$

5. 强导电媒质中的均匀平面波

$$\frac{\sigma}{\omega\epsilon} \gg 1$$

$$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2}} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} - 1 \right) \approx \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma}$$

$$\beta = \omega \sqrt{\frac{\mu \epsilon}{2}} \left(\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} + 1 \right) \approx \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma}$$

$$\eta_c = \sqrt{\frac{\mu}{\epsilon(1 - j \frac{\sigma}{\omega\epsilon})}} \approx \sqrt{\frac{j\omega\epsilon}{\sigma}} = \sqrt{\frac{\nu\mu}{\sigma}} e^{j\frac{\pi}{4}} = \sqrt{\frac{\pi f \mu}{\sigma}} (1 + j)$$

$$\lambda = \frac{2\pi}{\beta} = 2\sqrt{\frac{\pi}{f \mu \sigma}}$$

$$v = \frac{\nu}{\beta} = 2\sqrt{\frac{\pi f}{\mu \sigma}}$$

⑥ 平面上的垂直入射

两种媒质分界面上的垂直入射

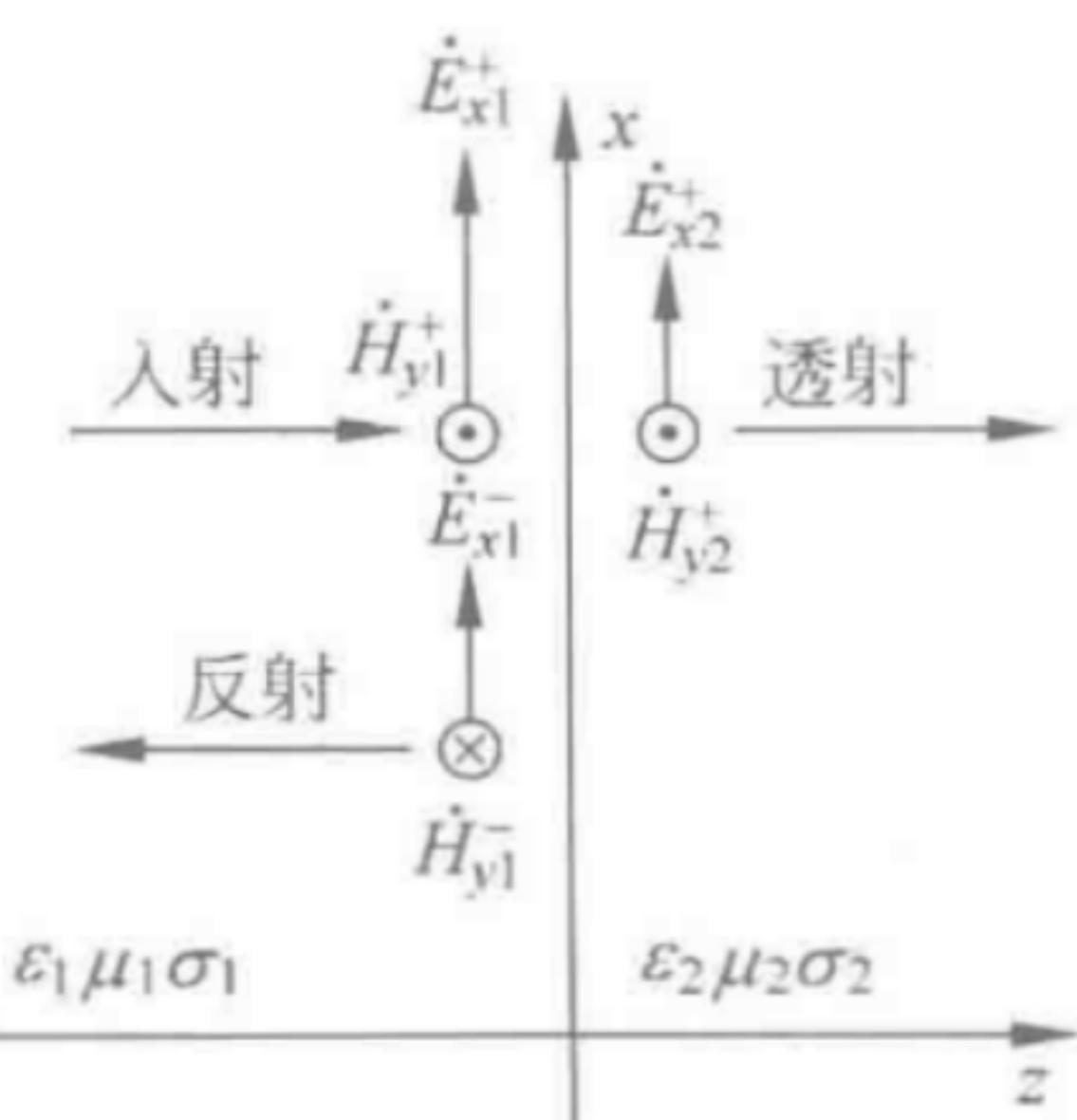


图 6.26 两媒质界面上的垂直入射

$$\text{入射波: } \dot{E}_{x1}^+ = \dot{E}_{m1}^+ e^{-\gamma_1 z}$$

$$\dot{H}_{y1}^+ = \frac{\dot{E}_{m1}^+}{\eta_1} e^{-\gamma_1 z}$$

$$\text{反射波: } \dot{E}_{x1}^- = \dot{E}_{m1}^- e^{\gamma_1 z}$$

$$\dot{H}_{y1}^- = \frac{\dot{E}_{m1}^-}{\eta_1} e^{\gamma_1 z}$$

$$\text{透射波: } \dot{E}_{x2}^+ = \dot{E}_{m2}^+ e^{-\gamma_2 z}$$

$$\dot{H}_{y2}^+ = \frac{\dot{E}_{m2}^+}{\eta_2} e^{-\gamma_2 z}$$

$$\left\{ \begin{array}{l} \dot{E}_{x1} = \dot{E}_{x1}^+ + \dot{E}_{x1}^- = \dot{E}_{m1}^+ e^{-\gamma_1 z} + \dot{E}_{m1}^- e^{\gamma_1 z} \end{array} \right.$$

$$\text{同理 } \dot{H}_{y1} = \frac{\dot{E}_{m1}^+}{\eta_1} e^{-\gamma_1 z} - \frac{\dot{E}_{m1}^-}{\eta_1} e^{\gamma_1 z}$$

由边界条件

$$\left\{ \begin{array}{l} \dot{E}_{m1}^+ + \dot{E}_{m1}^- = \dot{E}_{m2}^+ \\ \frac{\dot{E}_{m1}^+}{\eta_1} - \frac{\dot{E}_{m1}^-}{\eta_1} = \frac{\dot{E}_{m1}^+}{\eta_2} \end{array} \right. \Rightarrow \left\{ \begin{array}{l} \dot{E}_{m1}^- = \frac{\eta_2 - \eta_1}{\eta_1 + \eta_2} \dot{E}_{m1}^+ \\ \dot{E}_{m2}^+ = \frac{2\eta_2}{\eta_1 + \eta_2} \dot{E}_{m1}^+ \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{反射系数 } T = \frac{\dot{E}_{m1}^-}{\dot{E}_{m1}^+} = \frac{\eta_2 - \eta_1}{\eta_1 + \eta_2} \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{透射系数 } T = \frac{\dot{E}_{m2}^+}{\dot{E}_{m1}^+} = \frac{2\eta_2}{\eta_1 + \eta_2} \end{array} \right. \Rightarrow T = T + 1$$

$$\begin{aligned} S_{av} &= \operatorname{Re} \left(\frac{1}{2} \dot{E}_{m2}^+ \cdot \frac{\dot{E}_{m2}^{+*}}{\eta_2} \right) = \operatorname{Re} \left[\frac{1}{2} (\dot{E}_{m1}^+ + \dot{E}_{m1}^-) \left(\frac{\dot{E}_{m1}^{+*}}{\eta_1} - \frac{\dot{E}_{m1}^{-*}}{\eta_1} \right) \right] \\ &= \operatorname{Re} \left[\frac{1}{2} \frac{\dot{E}_{m1}^{+2}}{\eta_1} - \frac{1}{2} \frac{\dot{E}_{m1}^{-2}}{\eta_1} \right] \end{aligned}$$

2 理想导体表面的反射、驻波

设均匀平面波由理想介质垂直入射到理想导体表面

$$\gamma_1 = j\beta_1, \quad E_2 = 0$$

$$\text{所以 } \dot{E}_{1m}^+ = -\dot{E}_{m1}^- \quad T = -1$$

$$\dot{E}_{x1}^+ = \dot{E}_{m1}^+ e^{-j\beta_1 z}, \quad \dot{E}_{x1}^- = -\dot{E}_{m1}^+ e^{j\beta_1 z}$$

$$\text{有 } \dot{E}_x = \dot{E}_{x1}^+ + \dot{E}_{x1}^- = \dot{E}_{m1}^+ (e^{-j\beta_1 z} - e^{j\beta_1 z}) = -2j\dot{E}_{m1}^+ \sin\beta_1 z$$

$$\text{所以 } E_{x1} = 2E_{m1}^+ \sin\beta_1 z \sin\omega t$$

$$\text{同理 } H_{y1} = 2 \frac{\dot{E}_{m1}^+}{\eta_1} \cos\beta_1 z \cos\omega t$$

相对于驻波，理想介质中的均匀平面波 $\dot{E}_x = \dot{E}_{xm} e^{-j\beta z}$ 称为等幅行波

导电媒质中的均匀平面波 $\dot{E}_x = \dot{E}_{xm} e^{-\alpha z} e^{-j\beta z}$ 称为衰减行波

$$\text{导体表面的面电流密度 } \vec{J}_s = \vec{n} \times \vec{H}_1 = -\vec{E}_z \times \vec{E}_y \vec{H}_{y1}$$

$$= \vec{E}_x \vec{H}_{y1} |_{z=0} = \vec{E}_x \frac{2\dot{E}_{m1}}{\eta_1}$$

驻波的能量和能流

$$W_e = \frac{1}{2} \epsilon_1 E_{x1}^2 = 2 \epsilon_1 E_{m1}^{+2} \sin^2 \beta_1 z \sin^2 \omega t$$

$$W_m = \frac{1}{2} \mu H_{y1}^2 = 2 \mu_1 \frac{E_{m1}^{+2}}{\eta_1^2} \cos^2 \beta_1 z \cos^2 \omega t = 2 \epsilon_1 E_{m1}^{+2} \cos^2 \beta_1 z \cos^2 \omega t$$

$$S_{av} = \operatorname{Re} [\frac{1}{2} \vec{E}_1 \times \vec{H}_1^*] = 0$$

趋肤深度 δ (透入深度)

$$e^{-\alpha \delta} = e^{-1} \text{ 则 } \delta = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega \mu \sigma}}$$

3. 两种理想介质界面的反射、驻波比

$$\gamma_1 = j\beta_1, \quad \gamma_2 = j\beta_2$$

$$\dot{E}_{x1} = \dot{E}_{x1}^+ + \dot{E}_{x1}^- = \dot{E}_{m1}^+ e^{-j\beta_1 z} + \dot{E}_{m1}^- e^{j\beta_1 z}$$

$$= \dot{E}_{m1}^+ e^{-j\beta_1 z} + I \dot{E}_{m1}^+ e^{j\beta_1 z} - I \dot{E}_{m1}^- e^{-j\beta_1 z} + I \dot{E}_{m1}^- e^{j\beta_1 z}$$

$$= (1+I) \dot{E}_{m1}^+ e^{-j\beta_1 z} + 2I \dot{E}_{m1}^+ \cos \beta_1 z$$

$$\text{同理 } \dot{H}_{y1} = \frac{1-I}{\eta_1} \dot{E}_{m1}^+ e^{-j\beta_1 z} - j \frac{2I}{\eta_1} \dot{E}_{m1}^+ \sin \beta_1 z$$

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$$\dot{E}_{x1} = \dot{E}_{m1}^+ e^{-j\beta_1 z} + I \dot{E}_{m1}^+ e^{j\beta_1 z} = \dot{E}_{m1}^+ e^{-j\beta_1 z} (1+I e^{j2\beta_1 z})$$

$$I(z) = I e^{j2\beta_1 z}$$

$$\dot{E}_{x1} = \dot{E}_{m1}^+ e^{-j\beta_1 z} [1+I(z)]$$

$$\text{同理 } \dot{H}_{y1} = \frac{\dot{E}_{m1}^+}{\eta_1} e^{-j\beta_1 z} [1-I(z)]$$

$$\eta(z) = \eta_1 \frac{1+I(z)}{1-I(z)}$$

驻波比

$$E_{x1, \max} = E_{m1}^+ + E_{m1}^-$$

$$E_{x1, \min} = E_{m1}^+ - E_{m1}^-$$

$$S = \frac{E_{x1, \max}}{E_{x1, \min}} = \frac{1 + \frac{E_{m1}^-}{E_{m1}^+}}{1 - \frac{E_{m1}^-}{E_{m1}^+}} = \frac{1+IT}{1-IT}$$

① 平面上的斜入射

折射定律

$$\frac{\sin \theta''}{\sin \theta} = \frac{v_1}{v_2} = \frac{n_1}{n_2} = \frac{\epsilon_1}{\epsilon_2}$$

全反射

$$\epsilon_1 > \epsilon_2$$

$$\sin \theta_c = \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\theta \geq \theta_c$$

全透射

$$平行极化波 \theta = \theta_B = \arctan \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

垂直极化波不可能发生全透射

第八章太混乱了，所以不写了

