

Question (1) Why different cladding/structural materials are required for advanced reactors

- \* Advanced reactor systems operate at much higher operating temperatures
- \* Higher fast neutron fluxes leading to more radiation damage in cladding and structural materials
- \* Need to be compatible to different types of coolants other than water (Na in SFRs and molten salts in MSR)

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Question (2) Considerations when optimizing the composition for F/M steels

- \* Precipitation behavior: favorable and/or unfavorable precipitation of phases must be taken into consideration when choosing the composition of a major alloy constituent and solute addition

~~Corrosion resistance~~

⇒ Precipitates may enhance or degrade the mechanical properties of steel

- \* Corrosion resistance: Minimum of composition of some elements such as Cr or Al may be required to achieve good corrosion resistance (by forming a protective passive film)

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Question (3) Why Ferrite steels swell less than Austenite steels?

- \* The relaxation volume for interstitial in ferrite is larger than in Austenite
  - Therefore, in ferrite, interstitials repel other interstitials & attract vacancies (recombination) ✓
- \* Vacancy migration barriers are lower in ferrite
  - more mobile vacancies in ferrite tend ~~more~~ to recombine more with interstitials ✓
- \* Interaction between solute & dislocations make them strong sinks for vacancies ✓
- \* Vacancies tend to bind more with carbon in ferrite than in Austenite (because C-vac binding energy in ferrite is about twice that in austenite) ✓  
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Question (4) Role of oxide particles in ODS steels

- \*  $Y_2O_3$  /  $Y_2Ti_2O_7$  stabilize ferrite ✓ at high temperatures during high T strength (prevents phase transformation from  $\alpha$  to  $\gamma$ ) 5/5
- \* The oxide particles also improve swelling resistance, and creep resistance ✓
  - defect sinks, dislocation obstacles

## Question(5)

### Advantages of Ni alloys

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- \* Compatible with water, molten salts and liquid Na ✓
- \* Excellent corrosion resistance ✓
- \* High Temperature stability ✓

### Disadvantages of Ni alloys

- \* Production of Helium under irradiation leads to He embrittlement  
(from the  $(n, \alpha)$  reaction with Ni-58) ✓
- \* High cost ✓

Improving strength of Ni alloys precipitation hardening ✓  
solution Annealing ✓

## Question(6) Unique features of continuous in research reactors compared to LWRs

- \* Operating temperatures are much lower in research reactors ✓  
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- \* Neutron flux is much higher in research reactors ✓
- \* More operation time under transient conditions in research reactors ✓  
- high density fuels, no plenum, plate type fuel, high burnups

Question (7) Why is amorphization a concern in research reactors?

\* Amorphization of  $U_3Si_2$  is beneficial to inhibit swelling

- nope

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Question (8) U-Si vs. U-Al

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\* U-Si has higher fissile density than U-Al ✓  
∴ This allows for going to lower  $U^{235}$  enrichment. ✓

\* Problems of U-Si: ~~interaction~~ with the matrix and formation of  
U-Al-Si phases ✓  
~~swelling~~ ✓

Push towards U-Mo

\* Higher fissile density (lower enrichment required) ✓  
\* Mo is very good in stabilizing the  $\gamma$  phase ✓

Question (9) Swelling in  $U_3Si$  vs  $U_3Si_2$  3/6

\*  $U_3Si$  swells more drastically ✓

\*  $U_3Si_2$  amorphizes which leads to suppressing <sup>X</sup> the swelling

- both amorphize and swell

the  $\Delta V$  crystal  $\rightarrow$  amorphous is believed to govern swelling

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Question (10) Why  $\gamma$  U-Mo is the dominant phase in-reactor?

\* fission gas bubbles formed in U-Mo resist the transformation of  $\gamma$  phase to the  $\alpha$ -phase (orthorhombic)

- nope

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### Question (11)

\* The fabrication of U-Mo fuel has to be performed (casted) above the liquidus line - obviously

\* Then quenched to temperature below solidus line  $\frac{3}{6}$   
- again, obviously

- Mo segregation, Mo solidifies first

### Question (12) Evolution of fission gas bubbles in U-Mo as function of burnup

\* In the beginning (at low burnup), gas bubbles of small size and high number density are formed ✓

\* The formed tiny gas bubbles form a superlattice that is ~~not~~ distinct and often observed in U-Mo fuels ✓

\* As the burnup increases  $\rightarrow$  recrystallization occurs ✓

\* Recrystallization results in grain refinement with more grain boundaries created ✓

\* At that point, breakaway of swelling occurs where swelling rate increases ✓

\* Fission gas bubbles are observed along grain boundaries at high burnup. ✓

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### Question (13) Role of Zr layer in U-Mo monolithic fuel

- \* Zr layer acts as an interdiffusion barrier between the fuel and the Al cladding ✓
- \* Typically, Zr layers have thickness of 25  $\mu\text{m}$  ✓  
(The ~~range of length~~ (The longest recoil range in the fuel  $\sim 9 \mu\text{m}$ )  
- prevent interaction layer growth  
✓/✓

### Question (14) Why is Al suited for research reactors & not in LWRs?

- \* At the low operating temperatures in research reactors, Al has excellent properties:
  - excellent corrosion resistance due to formation of protective passive layer of  $\text{Al}_2\text{O}_3$  ✓
  - Doesn't have a ductile to brittle transition at low temperature ✓
  - Good mechanical properties at low temp (ductile) ✓
  - swelling resistant & creep resistant ✓
- \* In addition, Aluminum is cheap, and also easily fabricated (machinable, castable, and weldable) ✓
- \* However at high temperatures (in the range of LWR operation):
  - ~~Very~~ Close to the melting point of Al ✓
  - creep and swelling behavior ~~degrades~~ degrades at high T ✓
  - becomes more susceptible to corrosion ✓  
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