

Stress components in thick-walled cylinder

$$r_i = 0.5 \text{ cm} \quad r_o = 0.55 \text{ cm} \quad p = 15 \text{ MPa} \quad @ \quad r = 0.52 \text{ cm}$$

$$\sigma_\theta = \frac{\left(\frac{r_o}{r}\right)^2 + 1}{\left(\frac{r_o}{r_i}\right)^2 - 1} p \quad \sigma_r = -p \frac{\left(\frac{r_o}{r}\right)^2 - 1}{\left(\frac{r_o}{r_i}\right)^2 - 1}$$

$$\sigma_z = \frac{p}{\left(\frac{r_o}{r}\right)^2 - 1} \quad \frac{r_o}{r_i} = \frac{0.55}{0.5} = 1.1$$

$$\sigma_\theta = \frac{\left(\frac{0.55}{0.52}\right)^2 + 1}{1.1^2 - 1} (15) = 151.7 \text{ MPa}$$

$$\sigma_r = \frac{-15}{\left(\frac{0.55}{0.52}\right)^2 - 1} = -106 \text{ MPa}$$

$$\sigma_r = \frac{\left(\frac{0.55}{0.52}\right)^2 - 1}{1.1^2 - 1} (-15) = -8.5 \text{ MPa}$$

thin walled cylinder

$$r = \bar{r} = \frac{0.5 + 0.55}{2} = 0.525 \text{ cm}$$

$$\sigma_\theta = \frac{pR}{\delta} \quad \sigma_r = \frac{-p}{2} \quad \sigma_z = \frac{pR}{2\delta}$$

$$\sigma_\theta = \frac{(15)(0.525)}{0.05} = 157.5 \text{ MPa}$$

$$\sigma_r = \frac{-15}{2} = -7.5 \text{ MPa}$$

$$\sigma_z = \frac{(15)(0.525)}{2(0.05)} = 78.8 \text{ MPa}$$

max stress in fuel pellet from thermal expansion

$$\Delta T = T_0 - T_s = 425 \text{ K} \quad \alpha_F = 12 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$$

$$R_F = 0.5 \text{ cm} \quad E = 180 \text{ GPa} \quad \nu = 0.25$$

$$\sigma_r = -\sigma^* (1 - \eta^2)$$

$$\sigma_\theta = -\sigma^* (1 - 3\eta^2)$$

$$\sigma_z = -2\sigma^* (1 - 2\eta^2)$$

$$\sigma^* = \frac{\alpha E (T_0 - T_s)}{4(1 - \nu)}$$

$$\eta = \frac{r}{R_F}$$

max stress? $\rightarrow \sigma_\theta \rightarrow r = R_F \rightarrow \eta = 1$

$$\sigma^* = \frac{(12 \times 10^{-6})(180 \times 10^9 \text{ MPa})(425)}{4(1 - 0.25)} = 318.8 \text{ MPa}$$

$$\sigma_\theta = -318.8 (1 - 3(1^2)) = \underline{637.5 \text{ MPa}}$$

Cladding tube w/ thermal expansion

$$R_i = 0.6 \text{ cm} \quad t_c = 0.1 \text{ cm} \quad E = 250 \text{ GPa} \quad \nu = 0.3$$

$$\alpha_c = 15 \times 10^{-6} / ^\circ\text{K} \quad T_{ci} = 600 \text{ K} \quad T_{co} = 580 \text{ K}$$

$$\Delta T = 20 \text{ K}$$

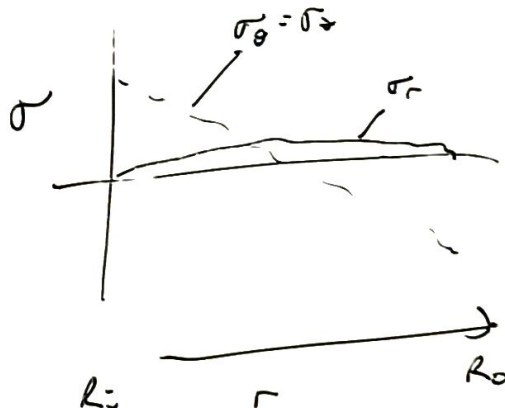
stress @ $r = 0.62 \text{ cm}$?

$$\begin{aligned} \sigma_r &= \frac{\Delta T}{2} \frac{\alpha E}{1-\nu} \left(\frac{r}{R_i} - 1 \right) \left(1 - \frac{R_i}{t_c} \left(\frac{r}{R_i} - 1 \right) \right) \\ &= \frac{20}{2} \frac{(15 \times 10^{-6})(250 \times 10^9 \text{ MPa})}{1-0.3} \left(\frac{0.62}{0.6} - 1 \right) \left(1 - \frac{0.6}{0.1} \left(\frac{0.62}{0.6} - 1 \right) \right) \end{aligned}$$

$$\sigma_r = 1.43 \text{ MPa}$$

$$\begin{aligned} \sigma_\theta = \sigma_z &= \frac{\Delta T}{2} \frac{\alpha E}{1-\nu} \left(1 - 2 \frac{R_i}{t_c} \left(\frac{r}{R_i} - 1 \right) \right) \\ &= \frac{20}{2} \frac{(15 \times 10^{-6})(250 \times 10^9 \text{ MPa})}{1-0.3} \left(1 - 2 \frac{0.6}{0.1} \left(\frac{0.62}{0.6} - 1 \right) \right) \end{aligned}$$

$$\sigma_\theta = \sigma_z = 32.1 \text{ MPa}$$



Gap thickness change

$$\alpha_F = 12 \times 10^{-6} \text{ } 1/K \quad \alpha_C = 15 \times 10^{-6} \text{ } 1/K$$

$$\bar{T}_F = 925 \text{ K}$$

$$\bar{T}_C = 550 \text{ K}$$

$$T_0^{C,F} = 300 \text{ K}$$

$$R_F = 0.5 \text{ cm}$$

$$\bar{R}_C = 0.58 \text{ cm}$$

$$t_j = 0.03 \text{ cm}$$

$$\Delta t_j = \bar{R}_C \alpha_C (\bar{T}_C - T_0^C) - R_F \alpha_F (\bar{T}_F - T_0^F)$$

$$= 0.58 (15 \times 10^{-6}) (250) - 0.5 (12 \times 10^{-6}) (625)$$

$$= 0.002175 - 0.00375 = -0.0016 \text{ cm}$$

$$t_j' = t_j + \Delta t_j = 0.03 - 0.0016 = \underline{\underline{0.0284 \text{ cm}}}$$

stress from displacement

$$-2D \quad r, \theta \quad @ r = 0.45 \text{ cm}$$

$$E = 200 \text{ GPa} \quad \nu = 0.3 \quad u_r(r) = 0.5r^2 - 0.2r$$

$$\epsilon = \begin{bmatrix} u_{r,r} & 0 \\ 0 & u_{r,r} \end{bmatrix} = \begin{bmatrix} r - 0.2 & 0 \\ 0 & 0.5r - 0.2 \end{bmatrix}$$
$$= \begin{bmatrix} 0.45 - 0.2 & 0 \\ 0 & 0.5(0.45) - 0.2 \end{bmatrix} = \begin{bmatrix} 0.25 & 0 \\ 0 & 0.025 \end{bmatrix}$$

$$\begin{bmatrix} \sigma_{rr} \\ \sigma_{\theta\theta} \end{bmatrix} = \frac{E}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1-\nu & \nu \\ \nu & 1-\nu \end{bmatrix} \begin{bmatrix} \epsilon_{rr} \\ \epsilon_{\theta\theta} \end{bmatrix}$$

$$C_{11} = \frac{E}{(1+\nu)(1-2\nu)} (1-\nu) = 269 \text{ GPa}$$

$$C_{12} = \frac{E}{(1+\nu)(1-2\nu)} \nu = 115 \text{ GPa}$$

$$\sigma_{rr} = C_{11} \epsilon_{rr} + C_{12} \epsilon_{\theta\theta} = (269)(0.25) + (115)(0.025)$$

$$\sigma_{\theta\theta} = C_{12} \epsilon_{rr} + C_{11} \epsilon_{\theta\theta} = (115)(0.25) + (269)(0.025)$$

$$\sigma_{rr} = 70 \text{ GPa}$$

$$\sigma_{\theta\theta} = 35.5 \text{ GPa}$$