1.
$$R_f = 0.45 \text{ cm}$$
 $CHR = 250 \text{ W/cm}$ $k_f = 0.1 \text{ W/cm} K$ $E = 290 \times 10^3 \text{ m/s}$

a) $\Delta T = \frac{CHR}{47 k_p} = \frac{250}{470(0.1)} = 198.949 K$

$$0 = \frac{250}{4100} = \frac{12 \times 10^6 (290 \times 10^3)(198.944)}{4100} = 230.775 \text{ m/s}$$

Max: Op > r= Rp

$$\frac{\sigma}{\sigma} = -\sigma^*(1-372^2) \qquad 7 = \frac{1}{R_F} \rightarrow 1$$

$$\frac{\sigma}{\sigma_{g,max}} = -230.775(1-3) = 461.55 \text{ MPa}$$

b) of = 120 mp.

$$-\frac{\sigma_{frae}}{\sigma^{+}} = 1 - 377$$

$$-\frac{1 + 170}{230.775}$$

$$= 0.418059$$

$$0.418059 = \frac{1}{0.45} \Rightarrow 0.1881 \text{ cm} \Rightarrow r$$

$$R_{\phi} = 0.1881 = 0.7618 \text{ cm} \Rightarrow r$$

(or to a pop of 0.1881 on)

```
3. Stg
              Rf = 0.52 cm Teo = 550K
                                                 kRel = 0.04 W/K
               tg = 0.005cm R: 0.525
tdad = 0.08cm Ro = 0.605
                                                keled = 0.15 Wank
                                                LHR =400 Wem
                                                K = 12x156/K
                              Rc = 0.525+0.605
Rc = 0.565 V
14/14
                                                04 = 81156 1/K
          Dtg = Ride (Ti-To)-Reaf (Ti-To)
                                               Trot = 300K = T'=TE
        ΔR<sub>c</sub> = 0.565(12x106)[587.647-300] = 0.001916 cm
      atchd = (HK+chd = 400(0.08) = 65.294K ~
      T = Teled = 587.647 K
       TS-TCT = LHR - 400(0.005) = 204.0498 K ~
       Ts = 819.3388K
       To-Ts = CHIK = 295.77
       Tc = 1217.716 K
        ORF = 0.52 (8x156) [1217.776 - 700) : 0.00381566
            t, = 0.005 + 0.001916 - 0.00381566 = 0.0031
           \Delta t_q = -0.0019 \text{ cm}
```

7.
$$P = 25 \text{ MPa}$$
 $R_{c} = 0.52 \text{ cm}$
 $t_{ded} = 0.08 \text{ cm}$
 $r = -\frac{P}{2} = -\frac{7}{2} = -12.5 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{25(0.52)}{0.08} = 162.5 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{7}{2} = \frac{7}{2} = 81.25 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{7}{2} = \frac{7}{2} = 81.25 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{7}{2} = \frac{7}{2} = 81.25 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{7}{2} = \frac{7}{2} = 81.25 \text{ MPa}$
 $r = -\frac{P}{2} = \frac{7}{2} = \frac{7}{2}$

(12 = (1+w)(1-20) = 48 = 92.307 GPa

- strain? (= = [(To - Y (Tr + TE))

4. Formed taler $dt = 0.25 \quad t_{0} = 0 \quad t_{0} = 1.0$ $y_{0} = y_{0} + dt y_{0}(0)$ $y_{1} = y_{0} + dt y_{0}(0)$ $y_{2} = y_{0} + dt y_{0}(0)$

- started on the right path, just y, correct

 $\frac{8}{10} \quad \Delta T_{c} = 250 \, \text{K} \quad \Delta_{c} = 8 \times 10^{6} \, \text{E} = 250 \times 13 \, \text{MPe} \quad U = 0.3$ $\frac{1}{10} \quad \Delta T_{c} = 0.1 \, \text{cm} \quad R_{c} = 0.55 \, \text{cm} \quad \text{Mox when } r = R_{0} \, \Delta R_{c}$ $\frac{1}{10} \quad \Delta T_{c} = 0.1 \, \text{cm} \quad R_{c} = R_{c} + L_{c} = 0.65 \, \text{cm}$ $\frac{1}{10} \quad \Delta T_{c} = 0.1 \, \text{cm} \quad R_{c} = R_{c} + L_{c} = 0.65 \, \text{cm}$ $\frac{1}{10} \quad \Delta T_{c} = 0.1 \, \text{cm} \quad R_{c} = 0.65 \, \text{cm}$ $\frac{1}{10} \quad \Delta T_{c} = 0.65 \, \text{cm}$ $\frac{1}{10} \quad$

1

÷.

6. i) Finite Pifference: Computationally cheap, but comot handle mechanics/hyth dimensional equations
i) Finite Volume: Great for fluid mech / Hernel hydroulic problems, but restricted to flux B.Cs
i) Finite Element: Can solve mechanics equations, but complex to implement/computationally expenses
(relatively)

7. Shain hardening is when a moteral is plasheolly deformed under a load and then the load is removed, so that the yield shreight is increased as well as hardness. The mechanism for this is dislocation pilop, where dislocations (lines of impurity/displaced alones) get "caypht" on barriers such as precipitates, such boundaries, ada.

8. All fel codes must be able to predict three groups of parenetes!

i) feel (Thermal profile, volume desperate)

2) Cled (Thrernel profile, etres: etc.)

3) Gap (Heat transport, preserve, etc.)

FRAPTRAN and FALLON are currently used by various bodies for helpert.

9. 0-D: Vaccney

Yy 3-D: Void (Cluster of vaccneres)

10. Microstrubre-bosed fiel modely ains to use strubed relationships to cornect microstrubre variebles to property values as a form of purincebouste modely. It hopes to provide more accurate modely with more fundamental physics retter then relying an empirical curve fits, being able to circular laters: fields and more complicated plenamene.

11. Which Burney Strubres (HES) have a longe amounts of voids the to fiscen products, which got stess on the sucrounding moderial. During a drawlest or LOCA, then additional themself stresses ladges released to this region fragmantage privarying spreading moderal around the full pin. Scientists are looking to better model the plenamenan using Phose-Tield Modeling, when stress fields are construbed by tracking vacancies from products with sinks/sources though the moderal. This provides a robust methodology to predict how bubbles repond to chapes in various promoters.

The microstructure is the orientation of species/phosos at the microscopic scale, such as with how grains in a metal are. The microstructure greatly affects how the meteral behaves at an approperty scale. It is generally tailored by shoichbreety and kind of heat treatment process, such as add-rolling to headen (in the case of steel). In the case of steel) in the case of steel of steel of steel of should only on example is how UDzi's microstructure significantly damped based on O/V roho, terming various species and lattice phases.

I this is from later fectures, but technically yes.

I to people were thought metal to be a