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# NUCK497

## HW-2 Solution

1- Given parameters:

$$R_f = 0.5 \text{ cm}$$

$$t_{\text{clad}} = 0.65 \text{ mm}$$

$$t_{\text{gap}} = 30 \text{ } \mu\text{m}$$

$$T_{\text{cool}} = 600 \text{ K}$$

$$y_{\text{xe}} = 10 \%$$

$$h_{\text{cool}} = 2.5 \text{ W/cm}^2 \text{ K}$$

$$k_{\text{cr}} = 0.17 \text{ W/cm K}$$

| Fuel Material                  | $k_{\text{fuel}} [\text{W/cm K}]^a$ | $\Theta [\text{W/cm}^3]^b$ | $T_{\text{melting}} [\text{K}]^a$ |
|--------------------------------|-------------------------------------|----------------------------|-----------------------------------|
| U <sub>metal</sub>             | 0.38                                | 395                        | 1405                              |
| UO <sub>2</sub>                | 0.03                                | 779                        | 3138                              |
| UC                             | 0.25                                | 531                        | 3123                              |
| UN                             | 0.2                                 | 553                        | 3133                              |
| U <sub>3</sub> Si <sub>2</sub> | 0.23                                | 463                        | 1938                              |

<sup>a</sup> Values taken from slide 18 of Lec 2.

<sup>b</sup> Calculated in HW-1

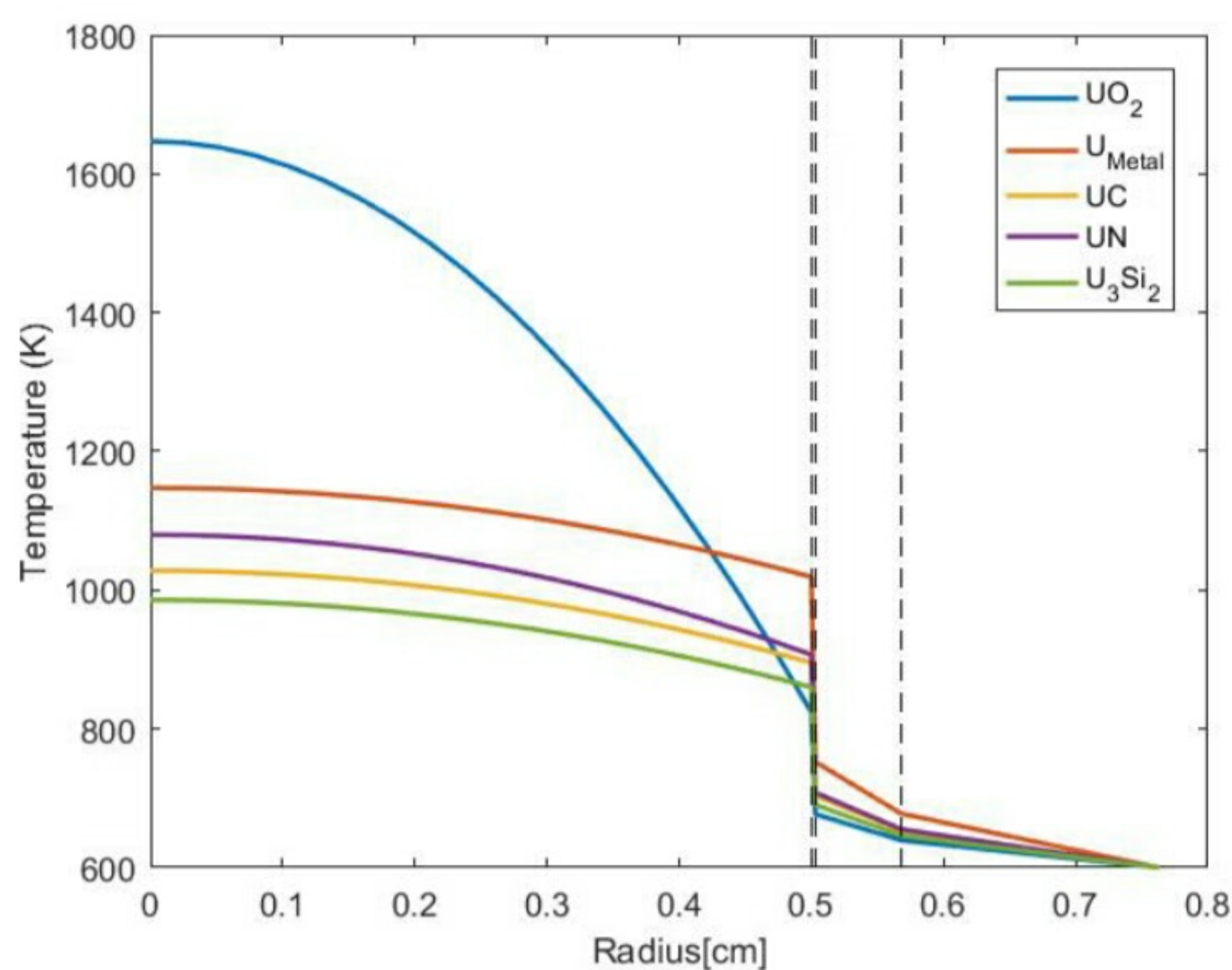
Relevant equations:

$$T_{\text{co}} - T_{\text{cool}} = \frac{\Theta}{2h_{\text{cool}}} R_f$$

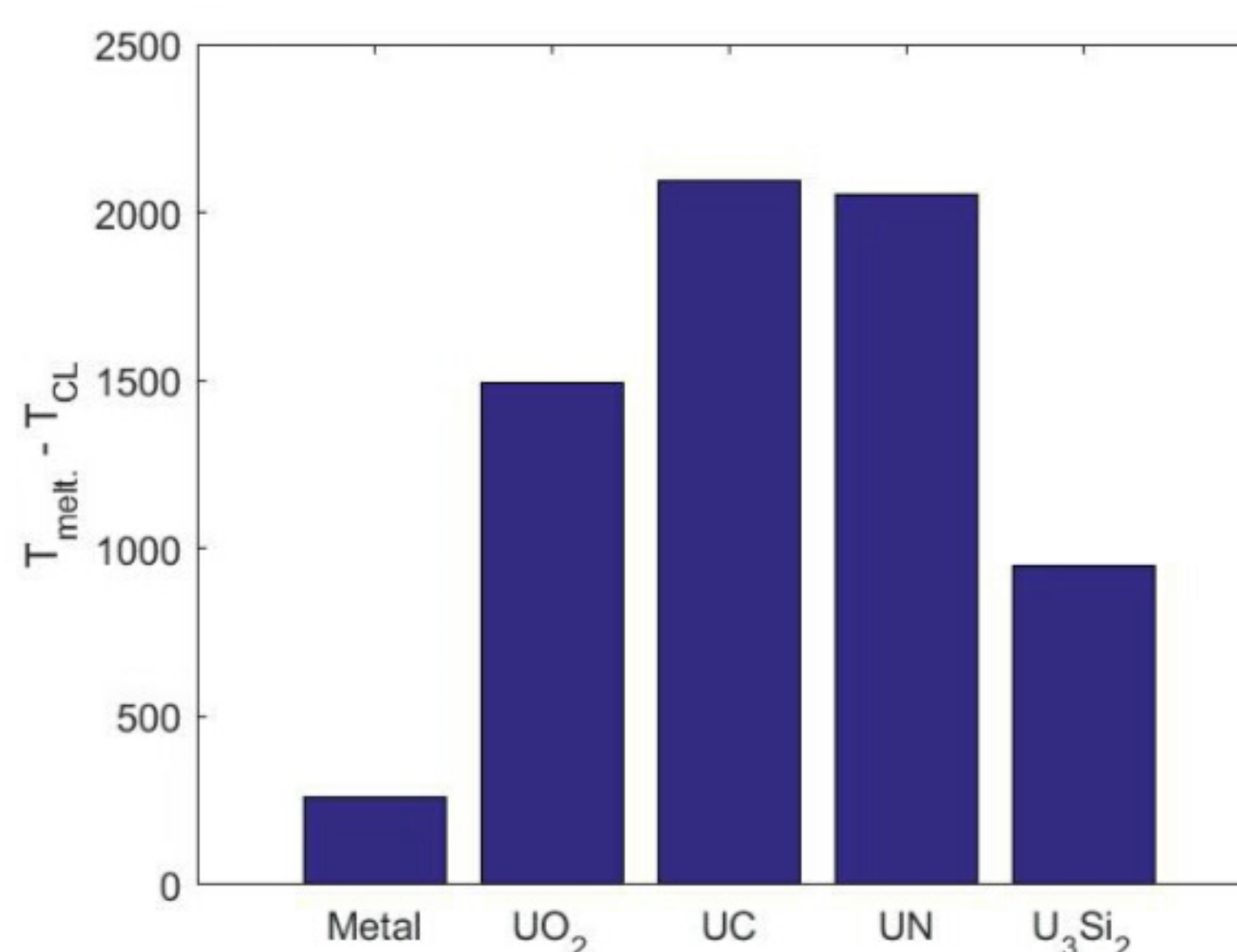
$$T_{\text{ci}} - T_{\text{co}} = \frac{\Theta}{2k_c} R_f t_{\text{clad}}$$

$$T_s - T_{\text{ci}} = \frac{\Theta}{2h_{\text{gap}}} R_f$$

$$T_m - T_s = \frac{\Theta}{4k_f} R_f^2$$

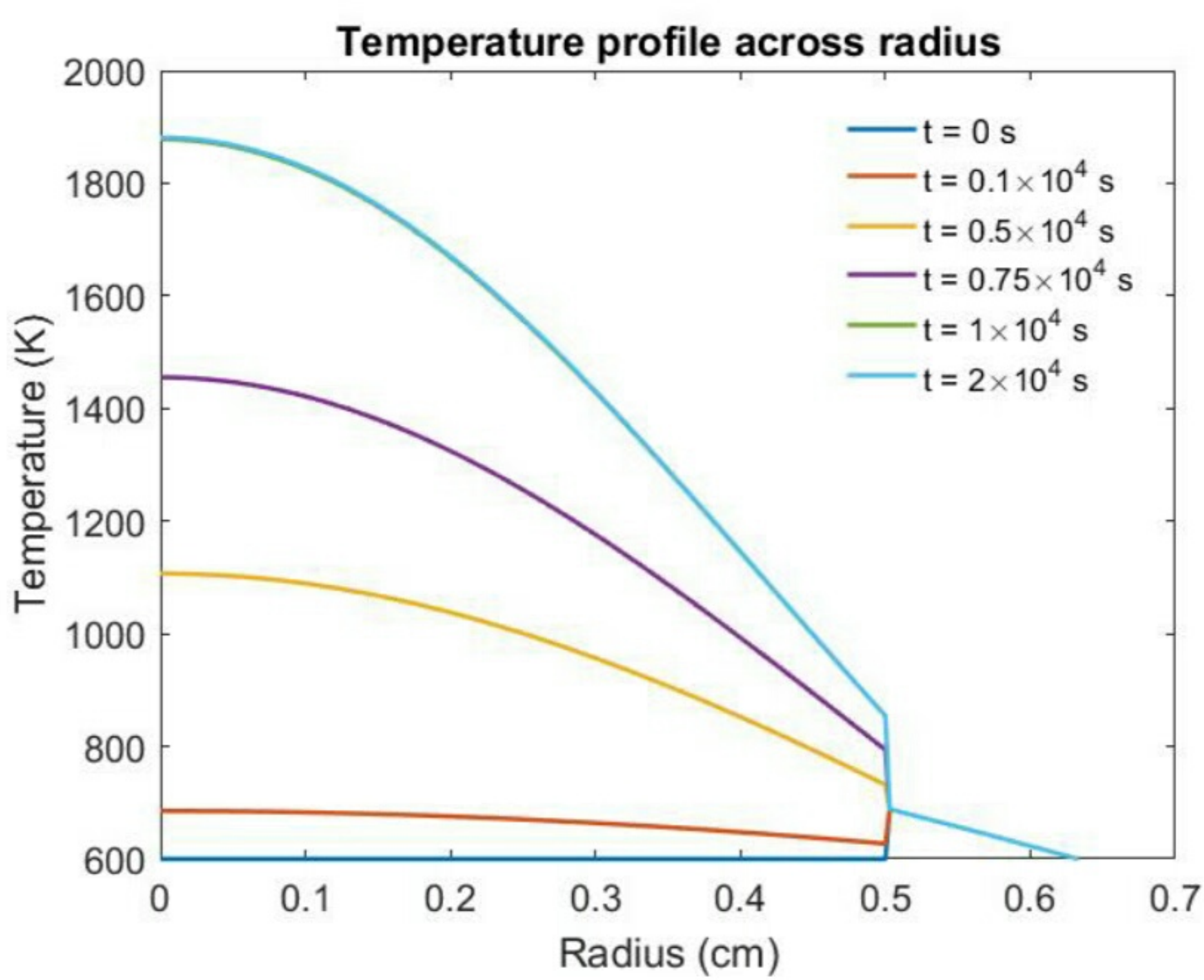
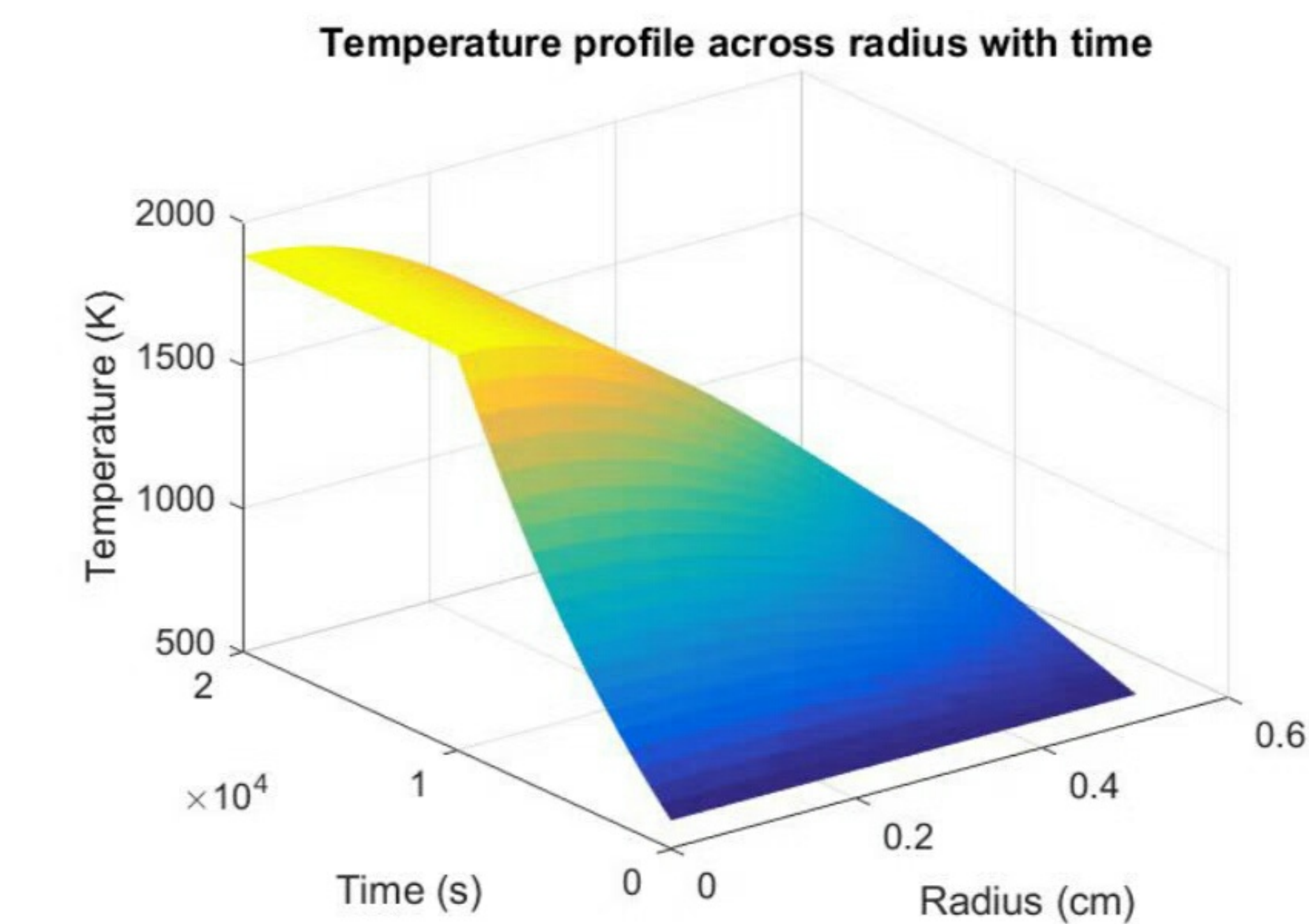


| Fuel Material                  | $T_{\text{melting}} [\text{K}]$ | $T_{\text{centerline}} [\text{K}]$ |
|--------------------------------|---------------------------------|------------------------------------|
| U <sub>metal</sub>             | 1405                            | 1147                               |
| UO <sub>2</sub>                | 3138                            | 1647                               |
| UC                             | 3123                            | 1028                               |
| UN                             | 3133                            | 1080                               |
| U <sub>3</sub> Si <sub>2</sub> | 1938                            | 986                                |

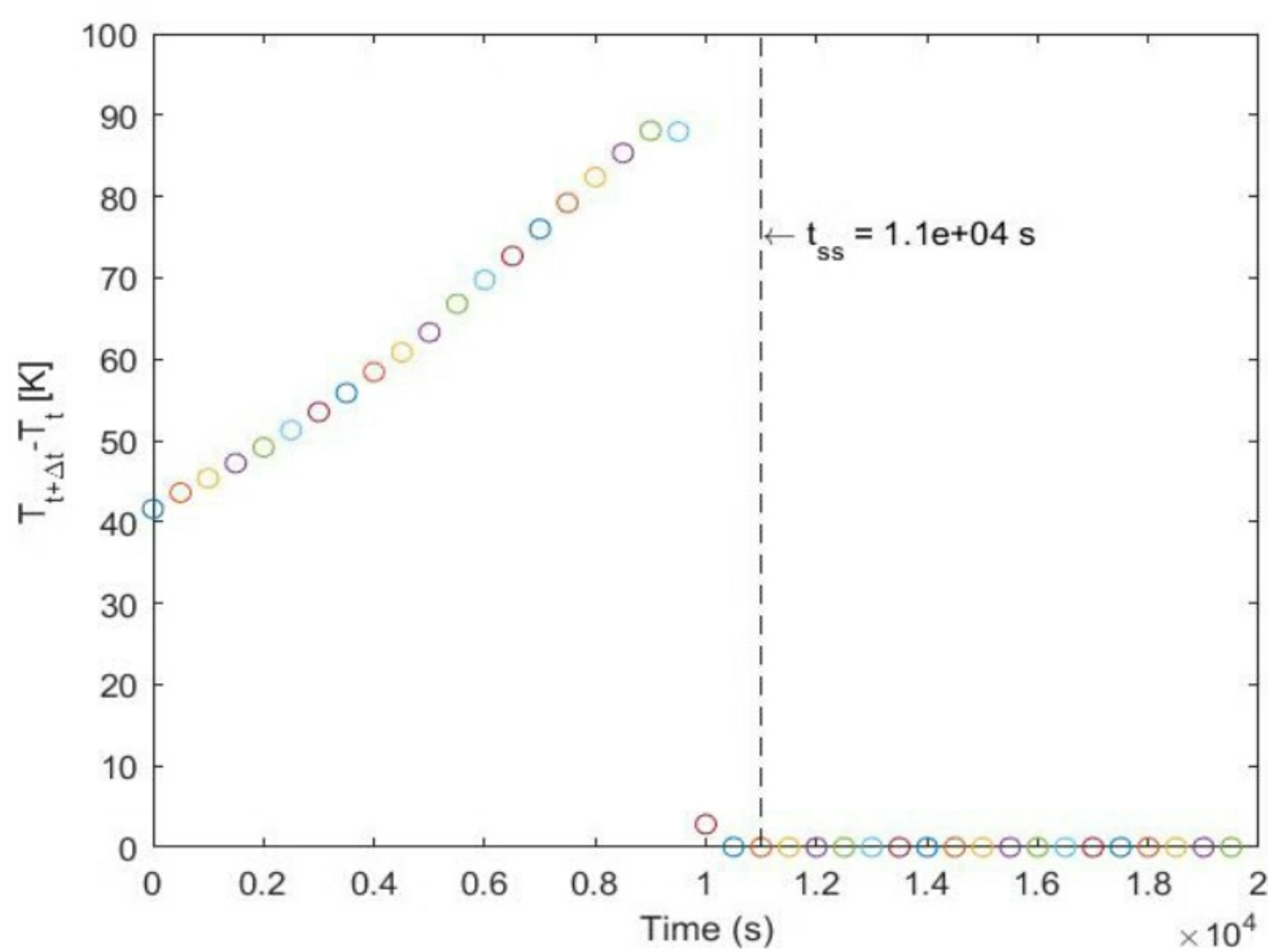




Q-2) a)

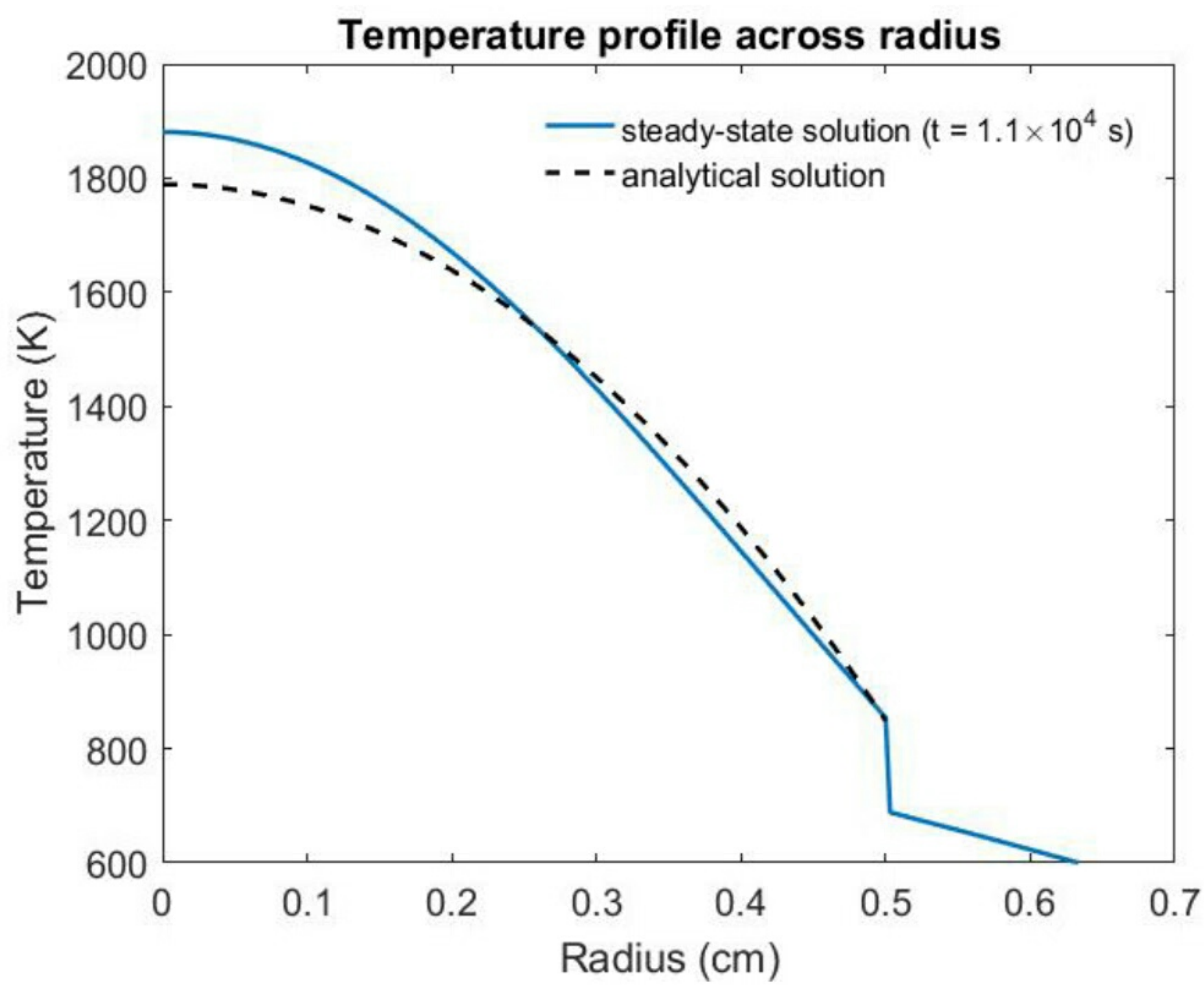


b) Max temperature difference was calculated for each time step. Steady-state solution was obtained if  $\Delta T_{\max} < \epsilon = 0.001$ .



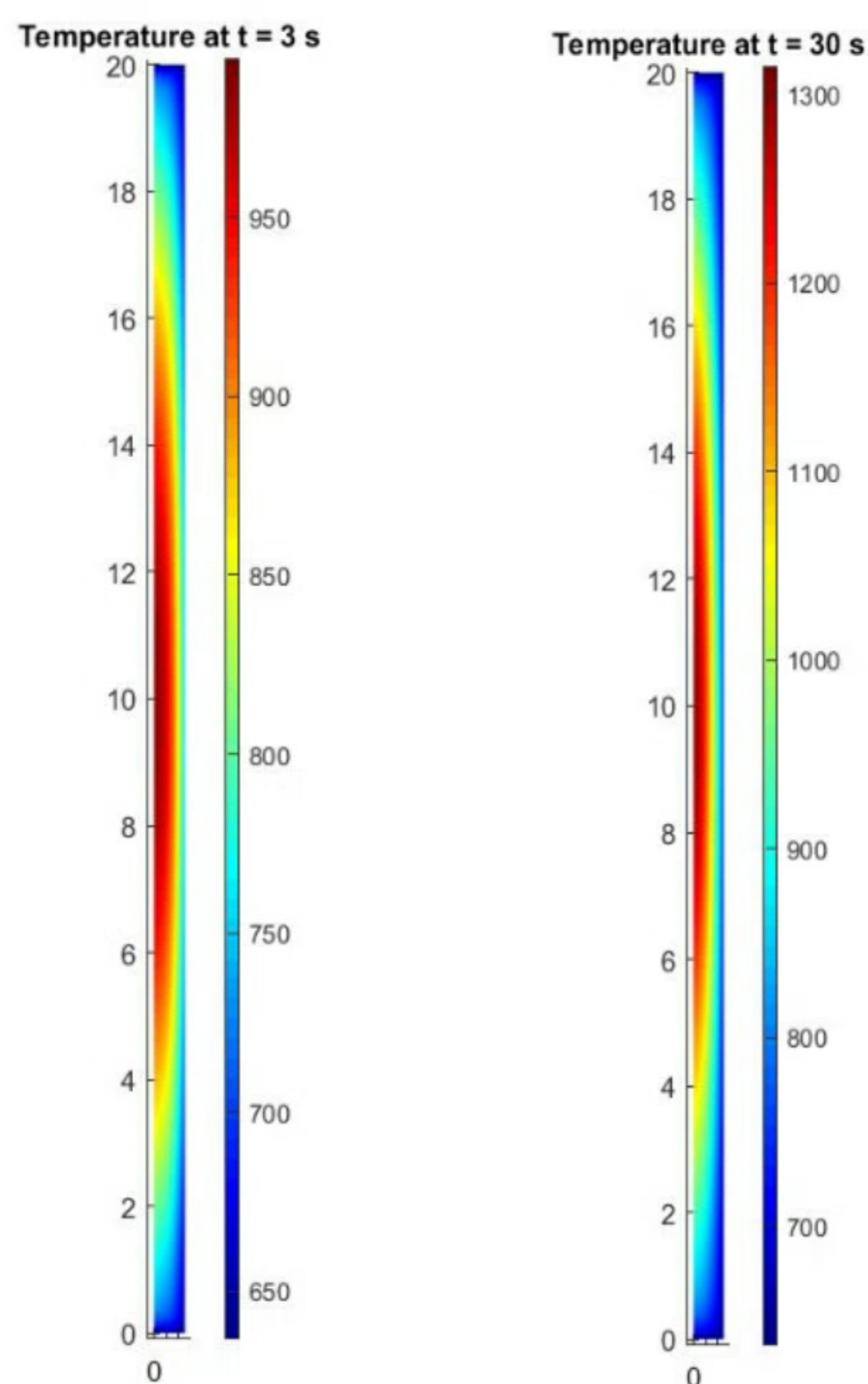


c)



Analytical solution and steady-state solution show slight variation. The main reason of this difference is the usage of constant  $k$  in analytical solution.

Q-3)



Θ-4)

$$\Delta T_{\max} = T_{\text{limit}} - \left( \Delta T_{\text{fuel}} + \Delta T_{\text{gap}} + \Delta T_{\text{clad}} + \Delta T_{\text{cool}} + T_{\text{in}} \right)$$

Maximum possible Temperature Difference

70% of Melting temperature  
 $0.7 T_{\text{melt}}$

Temperature drop across the fuel  
 $(T_o - T_s)$

Temperature drop across the gap  
 $(T_s - T_{ci})$

Temperature drop across the clad  
 $(T_{ci} - T_{co})$

Temperature drop across the coolant  
 $(T_{co} - T_{cool})$

Coolant inlet Temperature  
 $T_{in}$

We can rewrite this relation as follows:

$$\Delta T_{\max} = T_{\text{limit}} - [T_o - T_{\text{cool}} + T_{in}]$$

By using the results obtained in Θ-1, we can calculate  $\Delta T_{\max}$  for each fuel material:

