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(2) $K_{\text{coat}} = 5 \text{ W/mK} = 0.05 \text{ W/cmK}$
 $K_{\text{lead}} = 15 \text{ W/mK} = 0.15 \text{ W/cmK}$
 $K_F = 0.5 \text{ W/cmK}$
 $K_{\text{gap}} = 25 \text{ W/mK} = 0.25 \text{ W/cmK}$

$$h_{\text{cool}} = 5.5 \text{ W/cm}^2 \text{K}$$

$$T_{\text{cool}} = 200 \text{ K}$$

$$Q = 400 \text{ W/cm}^2$$

$$r_1 = 0.6 \text{ cm} = r_4$$

$$r_2 = 0.2 \text{ cm}$$

$$r_3 = 0.25 \text{ cm}$$

$$r_4 = 0.25 \text{ cm}$$

$$\text{LHR} = Q \pi R_F^2 = 400 \pi (0.6)^2 = 452.4 \text{ W/cm}$$

$$T_{\text{coat}} = T_{\text{cool}} + \frac{\text{LHR}}{2 \pi R_F h_{\text{cool}}} = 200 + \frac{452.4}{2 \pi (0.6) (5.5)} = 221.8 \text{ K} \quad \checkmark$$

$$T_{\text{lead}} = T_{\text{coat}} + \frac{\text{LHR}_{\text{coat}}}{2 \pi R_F K_{\text{coat}}} = 221.8 + \frac{452.4 (0.25 - 0.2)}{2 \pi (0.6) (0.05)} = 245.8 \text{ K} \quad \checkmark$$

$$T_{\text{gap}} = T_{\text{lead}} + \frac{\text{LHR}_{\text{lead}}}{2 \pi R_F K_{\text{lead}}} = \frac{452.4 (0.25 - 0.2)}{2 \pi (0.6) (0.15)} + 245.8 = 285.8 \text{ K} \quad \checkmark$$

$$T_{\text{fuel}} = T_{\text{gap}} + \frac{\text{LHR}_{\text{gap}}}{2 \pi R_F K_{\text{gap}}} = 285.8 + \frac{452.4 (0.2 - 0.6)}{2 \pi (0.6) (0.25)} = 281.8 \text{ K} \quad \checkmark$$

$$T_o = T_{\text{fuel}} + \frac{\text{LHR}}{4 \pi K_F} = 281.8 + \frac{452.4}{4 \pi 0.5} = \boxed{1053.8 \text{ K}} \quad \checkmark$$

@ $r = 0.4 \text{ cm}$,

$$T(r) = \frac{Q (R^2 - r^2)}{4K} + T_F \Rightarrow T(0.4) = \frac{400 (0.6^2 - 0.4^2)}{4(0.5)} + \quad -$$

③ $k = 145 \text{ W/mK}$

$\rho = 15.67 \text{ g/cm}^3$

$\sigma_f = 570 \text{ b}$

U_3Si_2
enrichment: 19.5%

14/14

a) $\phi = 2 \times 10^{12} \text{ n/cm}^2\text{s}$

mass U: $0.195(235) + 0.805(238) = 237.415 \text{ a.m.u.}$ ✓

mass Si: 28 a.m.u.

total mass: $3(237.415) + 2(28) = 768.245 \text{ a.m.u.}$ ✓

$N_f = 15.67 \frac{\text{g}}{\text{cm}^3} \cdot \frac{\text{mol}}{768.245} \cdot \frac{6.022 \times 10^{23} \text{ at.}}{\text{mol}} \cdot \frac{30}{103.84} \cdot 0.195 = 7.19 \times 10^{21} \frac{\text{at.}}{\text{g}}$ ✓

$Q = E_f N_f \phi \sigma_f$

$Q = (200 \times 10^6 \text{ eV}) \left(1.602 \times 10^{-19} \frac{\text{J}}{\text{eV}} \right) \left(7.19 \times 10^{21} \frac{\text{U}^{235}}{\text{g}} \right) \left(2 \times 10^{12} \frac{\text{n}}{\text{cm}^2\text{s}} \right) \left(510 \times 10^{-24} \text{ cm}^2 \right)$

$Q = 262.62 \text{ W/cm}^3$ ✓

b) $\rho_{\text{UO}_2} = 10.97 \text{ g/cc}$

$N_f = 7.19 \times 10^{21} = \left(10.97 \frac{\text{g}}{\text{cc}} \right) \frac{1}{M} \cdot \frac{6.022 \times 10^{23} \text{ at.}}{\text{mol}} \cdot 1x$

$\frac{x}{M} = 1.09 \times 10^{-3} \Rightarrow M = \frac{x}{1.09 \times 10^{-3}}$ ✓

262.62

$M = (x \cdot 235 + (1-x) \cdot 238) + 2 \cdot 16 = \frac{x}{1.09 \times 10^{-3}}$

$x = 0.2557x + 0.259 - 0.259x + 3.48 \times 10^{-2}$

$x = 29.3\% \text{ enrichment}$ ✓

④ $z_0 = 3 \text{ m}$; $LHR^0 = 150 \text{ W/cm}^2$; $\delta = 1$!

$9/12$

$z_0 = 1.5 = \frac{L}{2}$

a) $LHR @ z = 1.8 \text{ m}$

$$LHR\left(\frac{z}{z_0}\right) = 150 \cos\left[\frac{\pi}{2(1.1)}\left(\frac{1.8}{3} - 1\right)\right] = 46.66$$

-2

b) i) Water $c_p = 4200 \text{ J/kgK}$, $\dot{m} = 0.22 \text{ kg/s cool}$

$$T(z)_{\text{cool}} - T_{\text{cool}}^{\text{in}} = \frac{2 \cdot (1.1)}{\pi} \frac{3(150)}{0.22(4200)} \left[\sin\left(\frac{\pi}{2(1.1)}\right) - \sin\left(\frac{\pi}{2(1.1)}\left(\frac{1.8}{3} - 1\right)\right) \right]$$

-0.54

$$T(z)_{\text{cool}} - T_{\text{cool}}^{\text{in}} = 0.1532 \text{ K}$$

$$T_{\text{cool}}^{\text{out}} - T_{\text{cool}}^{\text{in}} = -1$$

$z = 3 \text{ m}$ $z_0 = 1.5 \text{ m}$

ii) sodium $c_p = 1404 \text{ J/kgK}$ $\dot{m} = 0.12 \text{ kg/s cool}$

$$T(z)_{\text{cool}} - T_{\text{cool}}^{\text{in}} = 0.1532 \times \frac{0.22(4200)}{0.12(1404)} = 0.8402 \text{ K}$$

only need $\dot{m} c_p$

⑤ Forward Euler: $f(t_{n+1}) = f(t_n) + dt f'(t_n)$

$t_0 = 1$

$t_1 = 0.33$ $f_1 = 6 + 0.33 [4(0) - 3(0)^2] = 6$

$t_2 = 0.66$ $f_2 = 6 + 0.33 [4(0.33) - 3(0.33)^2] = 6.33$

right process, but wrong I.C.

$t_3 = 0.99$ $f_3 = 6.33 + 0.33 [4(0.66) - 3(0.66)^2] = 6.77$

$t_4 = 1.32$ $f_4 = 6.77 + 0.33 [4(0.99) - 3(0.99)^2] = 7.11$

$t_5 = 1.65$ $f_5 = 7.11 + 0.33 [4(1.32) - 3(1.32)^2] = 7.13$

$t_6 = 1.98$ $f_6 = 7.13 + 0.33 [4(1.65) - 3(1.65)^2] = 6.61$

$12/16$

Backward Euler

$$f(t_{n+1}) = f(t_n) + \Delta t f'(t_{n+1}) \checkmark$$

Same thing

$$\begin{aligned} t_1 = 0.33 & \quad f_1 = 6 + 0.33 [4(0.33) - 3(0.33)^2] = 6.33 \\ t_2 = 0.66 & \quad f_2 = 6.33 + 0.33 [4(0.66) - 3(0.66)^2] = 6.78 \\ t_3 = 0.99 & \quad f_3 = 6.78 + 0.33 [4(0.99) - 3(0.99)^2] = 7.12 \\ t_4 = 1.32 & \quad f_4 = 7.12 + 0.33 [4(1.32) - 3(1.32)^2] = 7.14 \\ t_5 = 1.65 & \quad f_5 = 7.14 + 0.33 [4(1.65) - 3(1.65)^2] = 6.62 \\ t_6 = 1.98 & \quad f_6 = 6.62 + 0.33 [4(1.98) - 3(1.98)^2] = 5.35 \end{aligned}$$

⑧ → 3 phases in operation temperature cause swelling
→ low melting point (1400K) \checkmark u/y

⑨ Ratio of fuel volume per total volume in fuel cell.
Important due to fuel swelling during operation u/y

⑩ We enrich U to increase fissile quantity (U-235) in the fuel. Enrichment is possible due to mass difference between U-235 to U-238. → details of centrifuge process?
6/x

Blank Questions: 1, 6, 10, 11