- (5) Strán hortening is wherein plastic deformation from exposure to extrinsic load cases
 persent de strain, even after load is removed.
 - An increase in yield strain
- (6) Thermal Conductivity
 - Behaviour of Rssian products
 - Cherical reaction between products at inner dadly
 - . Meltig lemperature
- (7) @ Temperature profile and volume change of firel
 - (6) Temperature profile of dasting; stress profile of dasting
 - (c) Gap pressure estimation, heat tresport across gap, mechaical interraction between fuel and classing
- (8) (i) fission gas production and diffusion to grain boundary
 - @ Grain boundary bubble nucleation and growth, and increased interconnectiveness
 - (3) Gas transport to free surfaces through interconnected bubbles.
- (9) Instability of crystalline Structure secondary to accumulation of defects.
 - Reduction in material conductivity due to increase porosity value.
 - A retention of fission gas bubbles cours relact pressure of cladely the to
 - Increase in memoral consuctivity of firet
 - Increase in Essile desily of fuel de la increased philippin productives.

- (0)
- a)
 Point defects are OD defects: Example is vacancies; (b) 3D example = Precipitale
- 10 string force for green grain grown is reduction of grain boundary energy.
- Obers (6) Temperature gradient
 - @ classic energy gradical
 - @ Distocation energy greatient.
- 10 force for fuel densitionhum is reduction in auxilable free energy secondary to reduction in surface area?
- 12) Valence state of U.n 402 is +3
 - POSSIBLE udence states are +4, +5, and +6

$$\sigma_{r} = -\frac{P}{2} = \frac{50}{2} = -25 \, \text{Pira}$$

$$O_{\theta} = \frac{12}{6} = \frac{50 \times 5.4}{1.2} = 225 Mg$$

(6)
$$\delta r = -\frac{P(R_0/P)^2-1}{(R_0/R_i)^2-1}$$

$$= - \frac{50 \left(\frac{6.8}{5.6}\right)^{2} - 1}{\left(\frac{6.8}{5.6}\right)^{2} - 1}$$

$$= 50 \left(\frac{6.8}{5.6}\right)^{2} + 1 = 50 \times 2.47$$

$$\frac{\left(6.8/56\right)^{2} - 1}{\left(6.8/56\right)^{2} - 1} = 6.47$$

$$\delta_z = \frac{P}{(R_0/\rho_0)^2}$$

Since fuel is enclosed in zr cladbing.

323 MB

$$\frac{50}{(6.8/5.6)^{2}-1} = \frac{50}{0.47} = 106.38 PRay$$

Plascinum Strein =
$$E_{\theta} = \frac{1}{e} \left(O_{\theta} - V \left(O_{7} + O_{2} \right) \right)$$

$$= \mathcal{E}_0 = \frac{1}{160} \left(263 - 0.28 \left(106.38 - 50 \right) \right)$$

D gap Micliness = D Radius of Clabbing - D and is of fired.

D Radius of => 0.565 x 4.5 x 10-6 x (550-300) (550+

Ξ

and
$$O^* = \alpha \in (T_0 - T_S)$$

$$\frac{4(1-1)}{}$$

.:
$$\delta \phi = -\delta^{\frac{1}{2}} \left(1 - 3 \eta^{2}\right)$$
 where at made stress $\eta = 1$.

$$= \frac{D \times t}{q^2}$$

$$= 2 \times 10^{-15} \times 6.308 \times 10^7$$

$$= 8 \times 10^{-14}$$

7 = 1.577 × 10 4 6 is 1 71-2

$$f = 4\sqrt{\frac{2\times10^{-15}}{7.5}} - \frac{3}{2}\times(2\times10^{-15})\times\frac{6.308\times10^{7}}{(8\times10^{-11})^{2}}$$

$$-\frac{1.1652 \times 10^{-3}}{120} = -3x^{2}$$

$$\Rightarrow x^{2} = \left| \frac{1.1652 \times 10^{-3} + 1}{120} \right| \times \frac{1}{3} \Rightarrow 0.57735$$

