

100

[1] $T = 650 \text{ K}$ $t = 300 \text{ d}$ $\delta_{\text{tot}} = 500 \text{ }\mu\text{m}$

a) $t^* = 6.62 \times 10^{-7} \exp \left[\frac{11949}{T} \right] = 63.757 \text{ d}$ $t > t^*$

$\delta^* = 5.1 \exp \left[-\frac{550}{T} \right] = 2.188 \text{ }\mu\text{m}$ ✓

$\frac{14}{16}$ $K = 7.48 \times 10^6 \exp \left[-\frac{12500}{T} \right] = 0.0333$ ✓

$\delta = \delta^* + K (t - t^*) = \boxed{10.049 \text{ }\mu\text{m}}$ ✓

b) $C_H = \frac{2f \delta_{\text{ox}} P_{\text{ZrO}_2} * \frac{32}{32+91} * \frac{1}{16}}{\left[\delta_{\text{tot}} - \frac{\delta_{\text{ox}}}{R_{\text{PB}}} \right] * P_{\text{Zr}}} * 10^6 + C_H^0 = \boxed{139.14 \text{ wt. ppm}}$ ✓

[2] $d = \frac{W}{14.7} = 0.005 \times 10^{-4} \text{ }\mu\text{m} = \frac{W (\text{mg/dm}^2)}{14.7}$ ✓

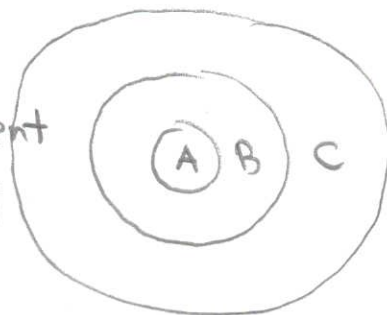
$\frac{14}{16}$ $W = 735 \text{ mg/dm}^2 = \frac{\Delta M}{(0.25)^2}$ ✓

$\Delta M = 735 \times (0.25)^2 = \boxed{45.9375 \text{ mg}}$ ✓

[3] In U-(Pu)-Zr fuel, Zr diffuses up the temp gradient via Soret effect and because it has different solubilities in different U phases we see:

u/o

- 1) A region: γ -U phase; rich Zr content
- 2) B region: β -U phase; Zr-depleted
- 3) C region: $\alpha+\delta$ phase: as-fabricated Zr content.



* lower Zr content = low melting temp.

[4] * Can achieve higher burn-up. ✓

* Higher centerline temperatures. ✓

* Higher fission gas release → larger gas plenum.

s/o

* Utilized in SFRs; sodium cooled; and have stainless steel cladding.

* MOX fuels restructure into three regions (inside-out): central void, columnar grains, as-fabricated grains.

* central void is the accumulation of bubbles that travel by a fuel evaporation-condensation mechanism due to the difference in vapor pressure.

* Fabricated hypostoichiometric; O travels up the temp grad; Pu is enriched in the columnar grain region. small

* Gap closes, fission product accumulate in the gap forming joint oxide gain (Cs_2MoO_4) which has higher thermal conductivity than the gap and is soft; works as a buffer for FCMI; and reduces fuel swelling.

[7] LOCA: a design basis accident; reduced or lost coolant flow due to e.g. coolant pipe break. ✓

- Power transient is less severe and takes longer time than the RIA transient. ✓
- The cladding deforms plastically (ballooning) due to decrease of coolant pressure → can lead to rupture. ✓
- Steam forms; clad reacts with steam; oxidation and brittle fracture ✓
-

[8] ① PCMI. ✓

② Cladding and assembly bow. ✓

③ The problem of Intergranular SCC of stainless steel clad in BWR has to be solved by control of the electrochemical potential by hydrogen injection which reduces IGSSC. ✓

Meaning: controlling water properties and its effect on clad internal by adjusting the concentration of hydrogen and consequently pH instead of e.g. Lithium-Boron chemistry. ✓

5 Three regions:

- 1) Central void: accumulation of pores and voids; have a lenticular shape and are normal to the thermal gradient; gas has low thermal conductivity and thus larger temp gradient. Voids move through a fuel evaporation-condensation mechanism due to difference in vapor pressure.
- 2) Columnar grains: destroyed microstructure due to the movement of the pores.
- 3) As-fabricated grains: appear when $T < 1800^\circ\text{C}$.

Reason: higher temperatures in the fuel $1800-2000^\circ\text{C}$ is required for movement and forming of central void.

6 Reactivity initiated accident: a design basis accident that is caused by a large and rapid insertion of reactivity caused by inadvertent ejection (PWR) or drop (BWR) of a control rod; mostly due to mechanical failure of the drive mechanism or change in void fraction or coolant/moderator T.

Effects of RIA: - DNB: isolation of fuel rod via coolant bubbles; partial melting of fuel.

- Rapid increase of temp and gas pressure inside fuel bubbles \rightarrow cracking of fuel.
- Rise in power and temp; significant accumulation of fission gases; grain boundary separation; PCMI; ballooning and rupture of fuel; fuel fragmentation; hydride formation in clad; oxidation in clad; brittle failure of clad.

⑩ - Pressure buildup: fission liberates O which forms CO with the C from the buffer; this gas increases the pressure on the carbon layer in TRISO pellets.

8/8 - Irradiation growth: Fuel kernel swells whereas the ^{pyrolytic} carbon layers initially shrink and then reach a turnaround point where they swell.
- SiC layer is compressed \rightarrow positive; delayed fracture.

10/10 ⑪ - Hydrides form because the hydrogen liberated during Zr oxidation/corrosion diffuses into the Zr clad; H has low solubility in Zr so it forms hydrides.

- Temp and stress gradient; H_2 moves up the stress gradient; Hydrides prefer areas with tensile stress. (embrittlement)
- Loss of ductility due to platelets or blisters
Hydrides move to stress concentrations at crack tips leading to delayed hydride cracking.

(12) 1) Oxygen diffusion through the oxide layer ✓

$\frac{4}{4}$ 2) Electron diffusion through the oxide layer.
- #2 isn't rate limiting, it's much faster than #1

(13) Pilling-Bedworth ratio: ratio of volume per atom of the metal oxide ✓ vs. volume per atom of the corresponding metal ✓

$\frac{4}{6}$ $R_{PB} < 1$: oxide layer is thin; breaks; no protective layer ✓

$R_{PB} > 2$: oxide layer flakes off; no protection ✓

$1 < R_{PB} < 2$: oxide layer is passivating; provides a protective layer. ✓