
Fabrication of Uranium Oxide Fuels

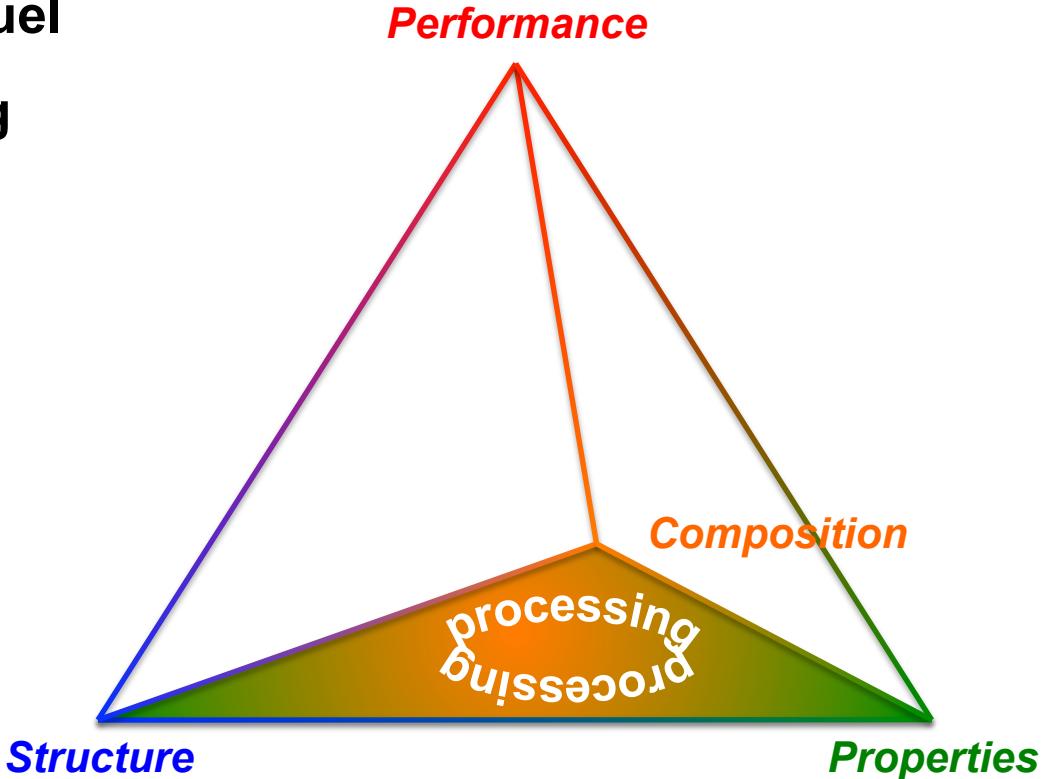
Erik Luther

ATR User Week 2012

LA-UR-12-21451

Outline

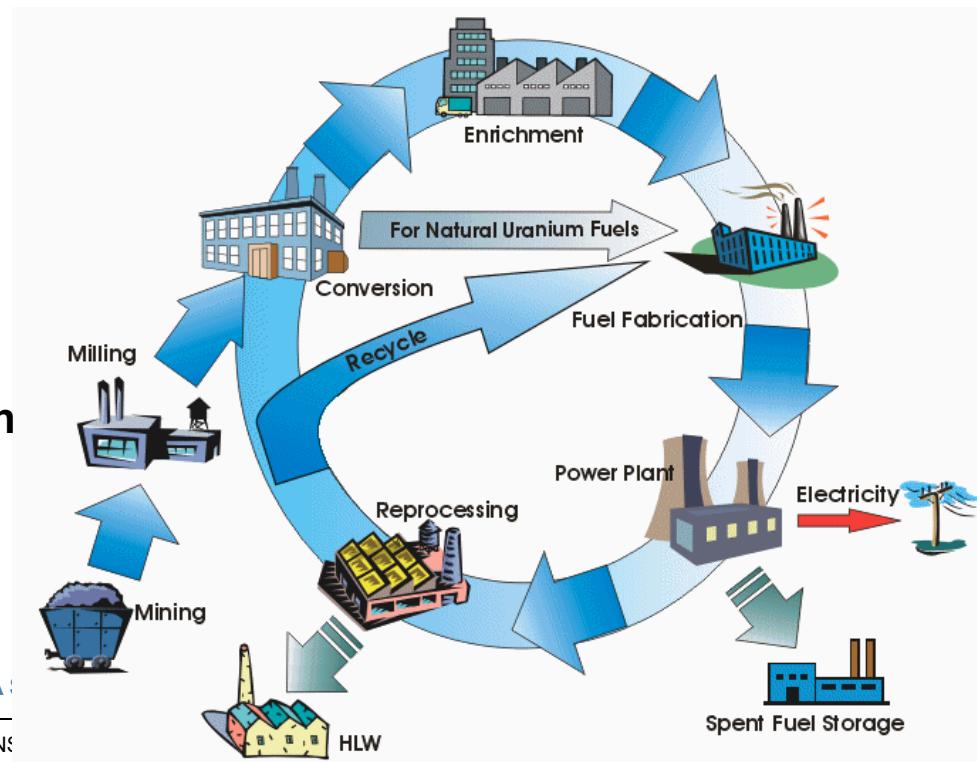
- Ceramic Nuclear Fuel
- Powder Processing Science
 - Powder feedstock
 - Compaction
 - Sintering
- Summary



**MICROSTRUCTURE; e.g., grain size and porosity, AFFECTS PROPERTIES;
e.g., thermal conductivity and creep**

Uranium Fuel Cycle

- Exploration for uranium
- Mining and milling of uranium ore to produce uranium concentrate known as 'yellow cake'
- Purification and conversion of yellow cake into gaseous uranium hexafluoride (UF_6) suitable for enrichment to increase the proportion of ^{235}U to 2-5%
- Conversion of enriched UF_6 to UO_2 powder suitable for making oxide fuel pellets
- **Fabrication of uranium dioxide fuel pellets**
- Fabrication of fuel pins made from stacks of UO_2 fuel pellets encapsulated in cladding, grouped in clusters, termed fuel assemblies
- Service
- Used fuel storage – recycle?



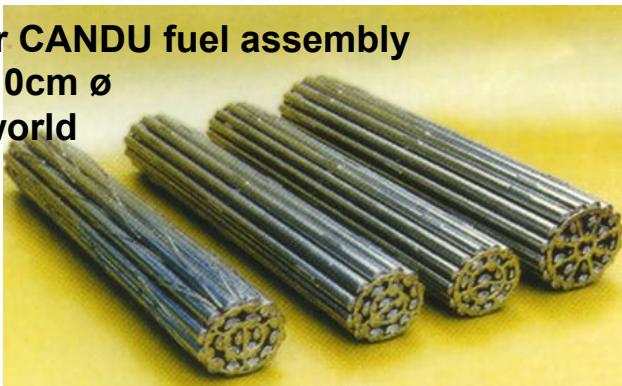
World LWR fuel fabrication capacity, metric tons/yr

Countries	Fabricator	Location	Conversion	Pelletizing	Rod/assembly
Belgium	AREVA NP-FBFC	Dessel	0	700	700
Brazil	INB	Resende	160	160	280
China	CNNC	Yibin	400	400	450
France	AREVA NP-FBFC	Romans	1800	1400	1400
Germany	AREVA NP-ANF	Lingen	800	650	650
India	DAE Nuclear Fuel Complex	Hyderabad	48	48	48
Japan	NFI (PWR)	Kumatori	0	360	284
	NFI (BWR)	Tokai-Mura	0	250	250
	Mitsubishi Nuclear Fuel	Tokai-Mura	475	440	440
	GNF-J	Kurihama	0	750	750
Kazakhstan	Ulba	Ust Kamenogorsk	2000	2000	0
Korea	KNFC	Daejeon	600	600	600
Russia	TVEL-MSZ*	Elektrostal	1450	1200	120
	TVEL-NCCP	Novosibirsk	250	200	400
Spain	ENUSA	Juzbado	0	300	300
Sweden	Westinghouse AB	Västeras	600	600	600
UK	Westinghouse**	Springfields	950	600	860
USA	AREVA Inc	Richland	1200	1200	1200
	Global NF	Wilmington	1200	1200	750
	Westinghouse	Columbia	1500	1500	1500
Total			13433	14558	12662

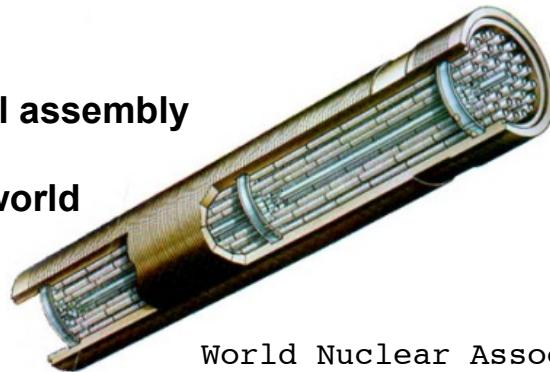
Types of Nuclear Fuel Assemblies

- Numerous fuel assembly types
- UO₂ pellets clad with zircalloy or stainless
- ~27 tons of fuel is required each year by a 1000 MWe reactor

PHWR or CANDU fuel assembly
50cm x 10cm ø
~6% of world capacity



AGR fuel assembly
36 pin
~2% of world capacity



BWR fuel assembly
6x6 to 10x10
~22% of world capacity



PWR fuel assembly
17x17
~4 meters
~66% of world capacity

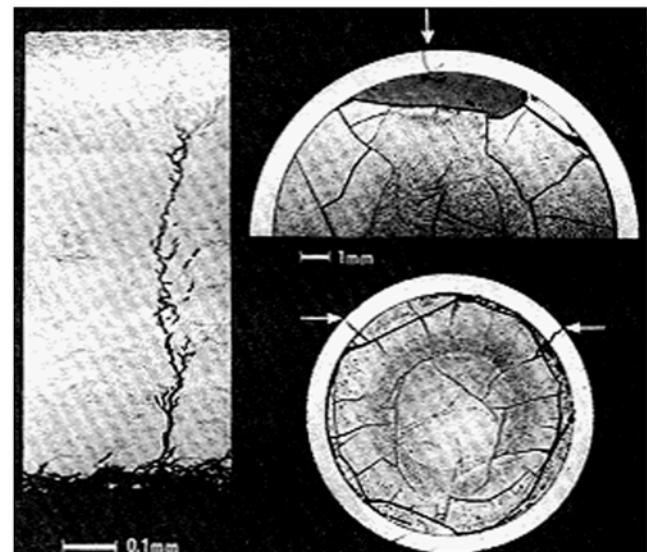


Ceramic Nuclear Fuel

- **Specifications based on 40+ years of experience**
 - Chemistry
 - Geometry
 - Microstructure
 - Physical
- **Fuel assemblies still fail due to pellet failure**
- **Science**
 - Separate effects of thermal gradients, radiation, microstructure etc. on thermal diffusivity, fission product distribution, pore generation and migration
 - Safer fuels – better scientific understanding
- **Other fuels**
 - Fast reactors
 - MOX, MA-MOX, thoria?
 - UN, UC, composites, targets?
 - Recycle?



Garzarolli et al., 1979



Fuel Failure – so what?

- High temperature, chemical corrosion, radiation damage, physical stresses
- Cladding is breached – radioactive material leaks into coolant water
- Not a significant plant safety risk
- “Very minor” leak – ignored leaking rod is removed at next refueling
- “Small” leak – allowable thermal transients are restricted
- “Significant” leak – reactor shutdown, faulty assembly removed
- Cost penalty to operating at reduced power or shutdown & replace failed fuel with matching remaining enrichment
- Balance economics and longer fuel burn

Bottom line: pellet failure affects the bottom line

Minimizing fuel failure

- Fuel failure rates improved ~ 60% from 1986 to 2006
- ~14 leaks per million rods loaded (IAEA 2010)
- Exclusion of foreign material from primary coolant water
 - Sophisticated debris filters
- Improved cleanliness in fuel assembly
- Pellet – Clad Interaction (PCI)
 - Power transients
 - PCMI: Pellet – Clad contact pressure
 - PCCI: Chemical reaction – build up of e.g. iodine, cesium, cadmium
 - Fragmented “relocated” fuel pellets
 - Localized heating

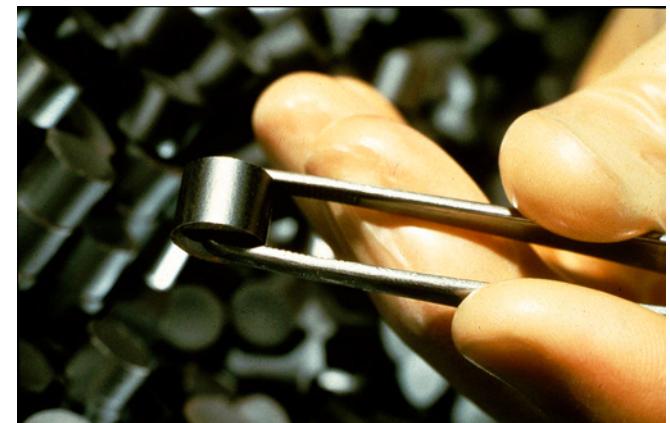


Suspect missing pellet surface

Slide 8

Fuel Pellet Specifications

- 87.7% uranium
- Total impurities 1500 $\mu\text{g/g}$
- O/M from 1.99 to 2.02
- Equivalent Boron Content (EBC) < 4.0 $\mu\text{g/g}$ (B, Gd, Eu, Dy, SM, Cd)
- Dimensions TBD (diameter, length, perpendicularity, surface finish)
 - ~1 cm x 1.2 cm (+/- ~0.001)
- Density TBD
 - 95% of theoretical – 10.96 g/cc
- Grain size and pore morphology TBD
 - ~30 μm
- Pellet integrity
 - Visually acceptable
- Cracks
 - ½ the pellet length, 1/3 the pellet circumference
- Chips
 - 1/3 of the pellet end
 - > 5% of cylindrical area



Fabrication of UO₂ Fuel Pellets

“Turning big rocks into little rocks then turning little rocks into big rocks”

■ Powder synthesis

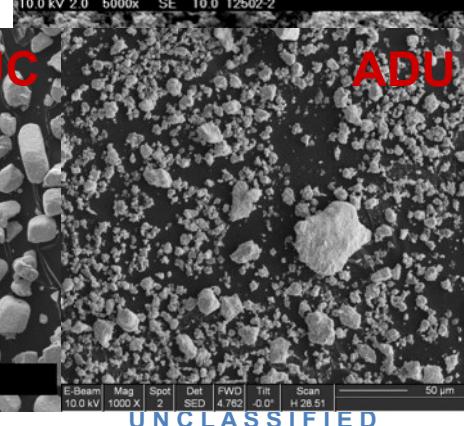
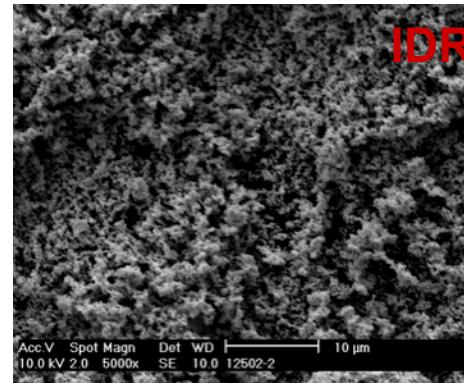
- IDR (Integrated Dry Route)
- ADU (Ammonium Diuranate)
- AUC (Ammonium Uranium Carbonate)

■ Powder conditioning

■ Compaction

■ Thermal treatment

Path Dependent



UO₂ Powder

Recycled Powder

Additives
– binder, lubricant, poisons

Milling

Sieving

Granulation

Pressing

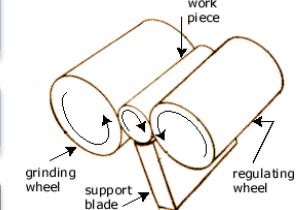
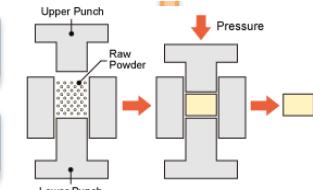
Burnout

Sintering

Grinding

Inspection

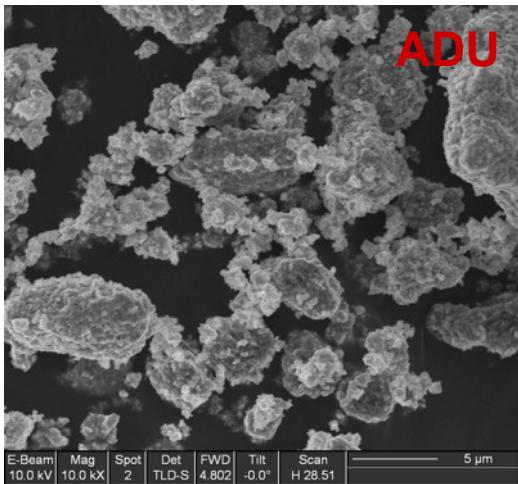
Service



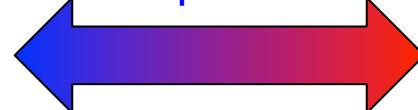
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Black Art or Science?

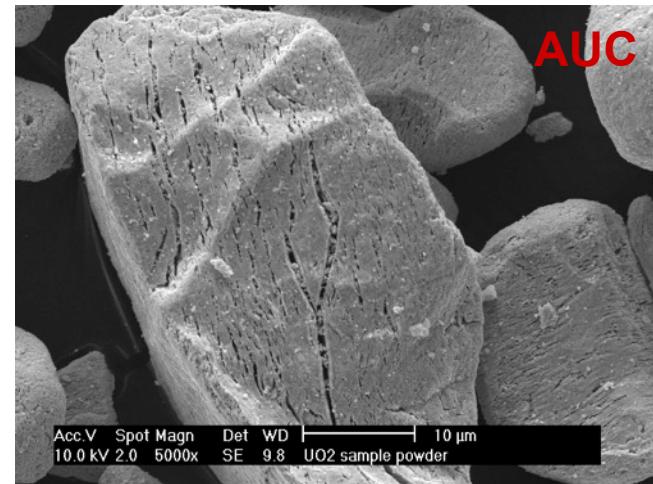
- Process knowledge is not directly transferrable
 - Specifications for powder feedstock has limitations
 - Feedstock will change
 - Small changes to feedstocks will affect processing parameters
 - How do you compensate for variations?
- Chemistry/powder additions for MOX, MA-MOX
- Material recycled from used fuel will come in many forms



Would you treat this powder the same as this powder?



What would you do differently to get the same pellet?



The crime...

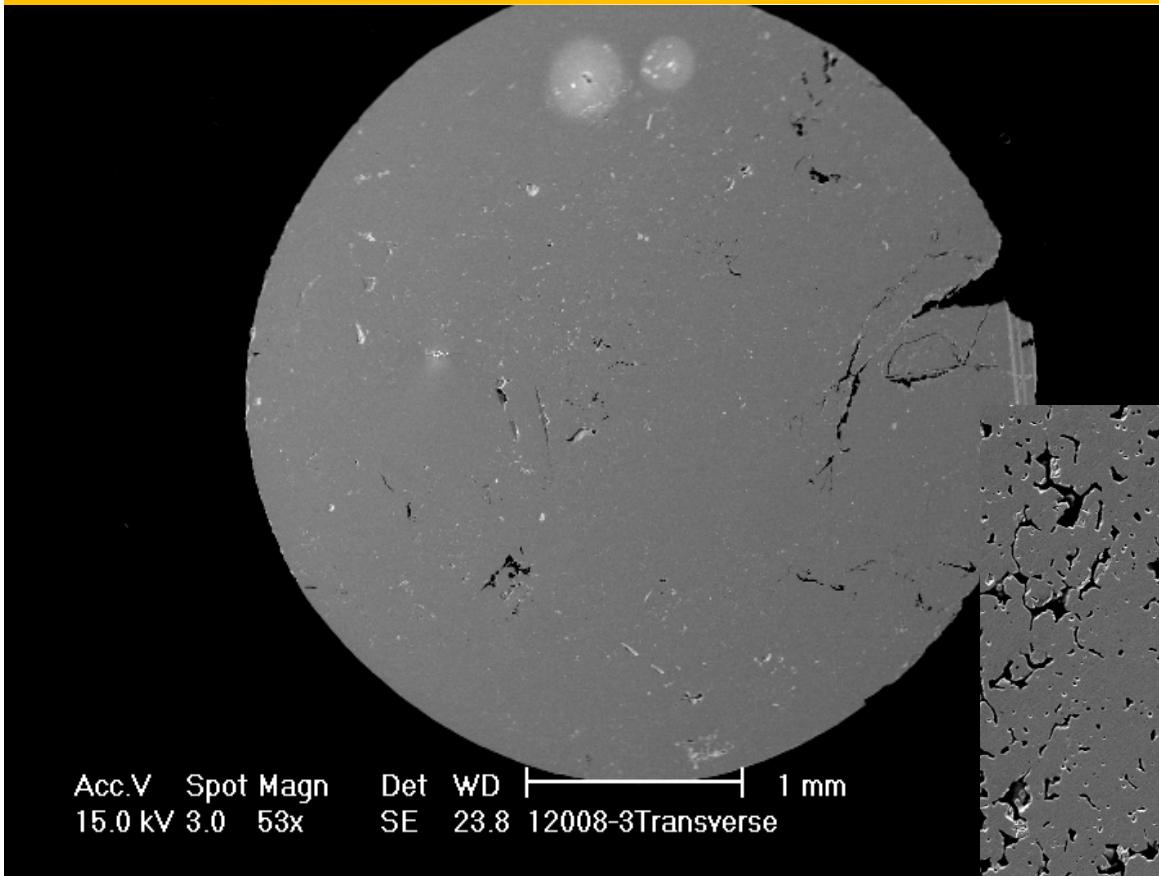
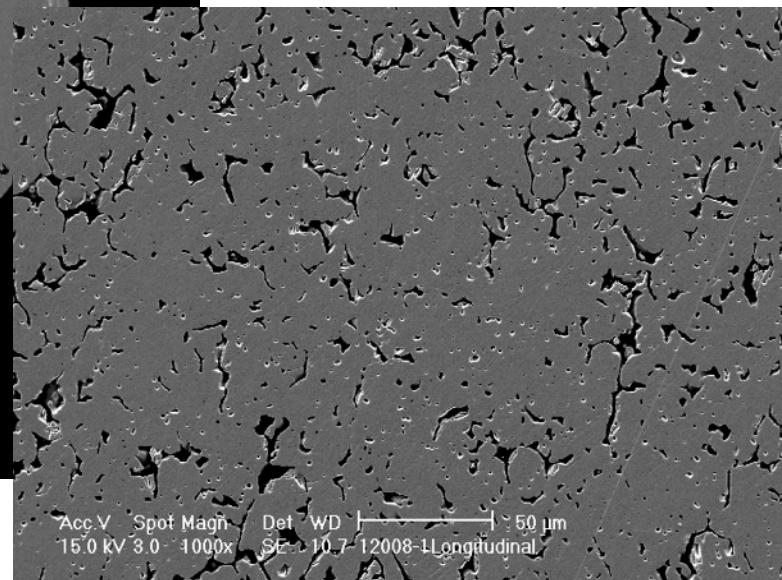


ABB DUO₂ sintered at 1750 °C

***Porosity that will alter
heat transfer and
fission gas transport
properties***



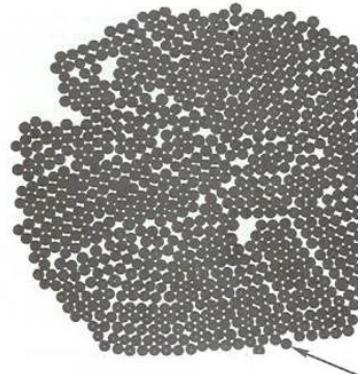
I suspect the powder...

■ **UO₂ powder particle variables**

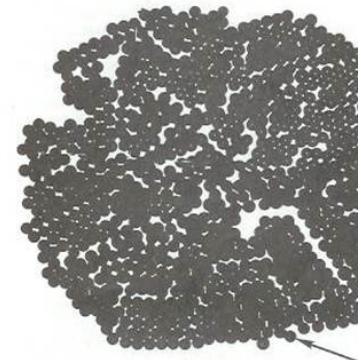
- Morphology
- Agglomeration
 - Hard
 - Soft
- Size distribution
- Powder flow into die
 - Uniformity



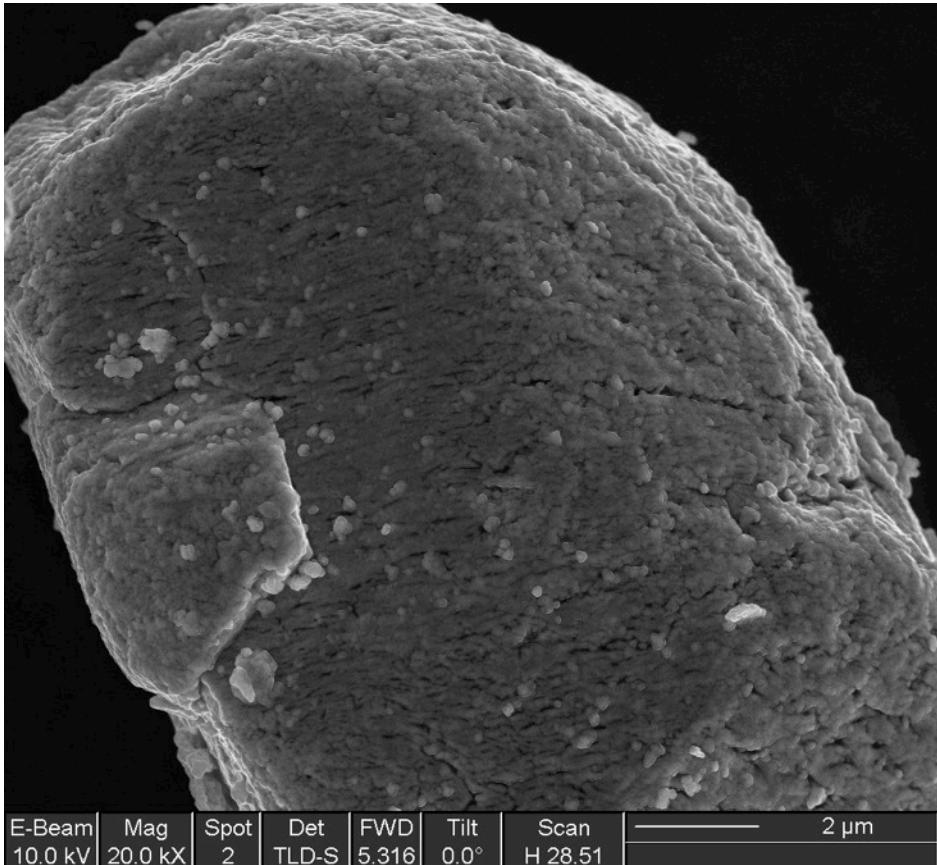
Seemingly uniform packing



Particle agglomerates



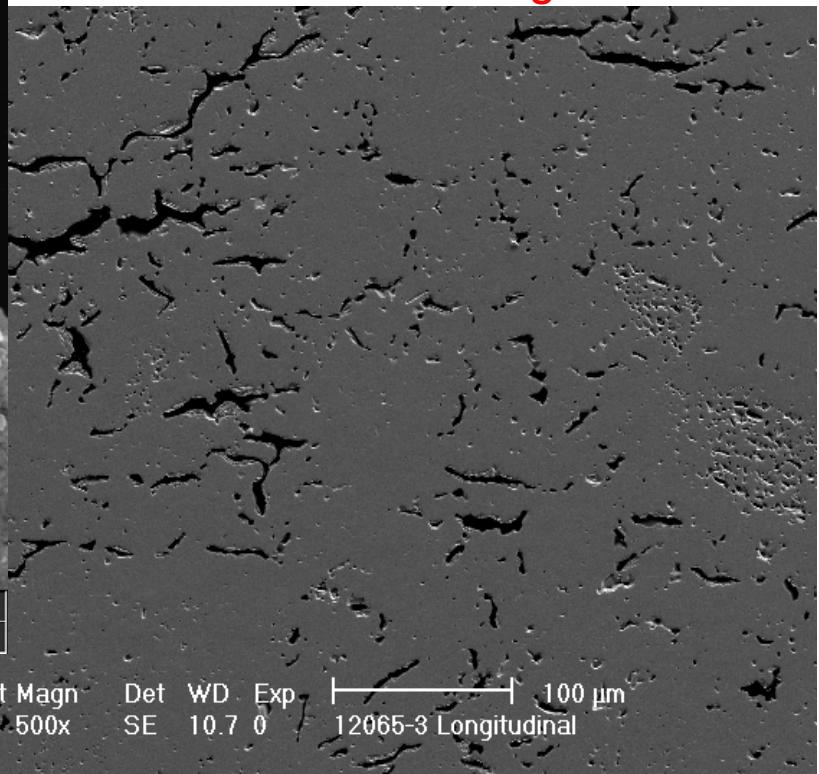
Guilty...



As-received powder

Poor Powder Flow &
Microporosity

Isolated “stranded” pores
affect sintering rate

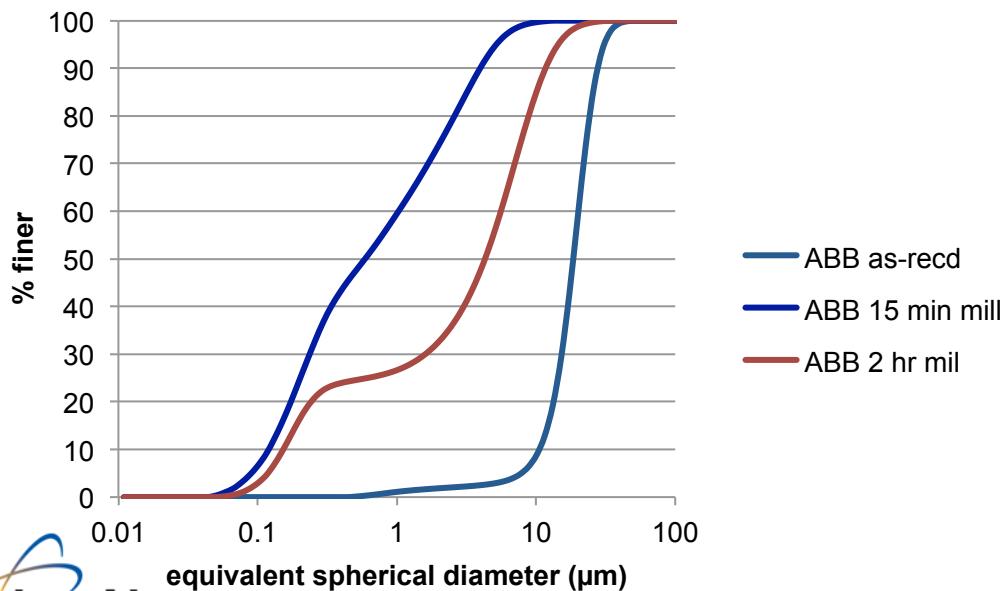
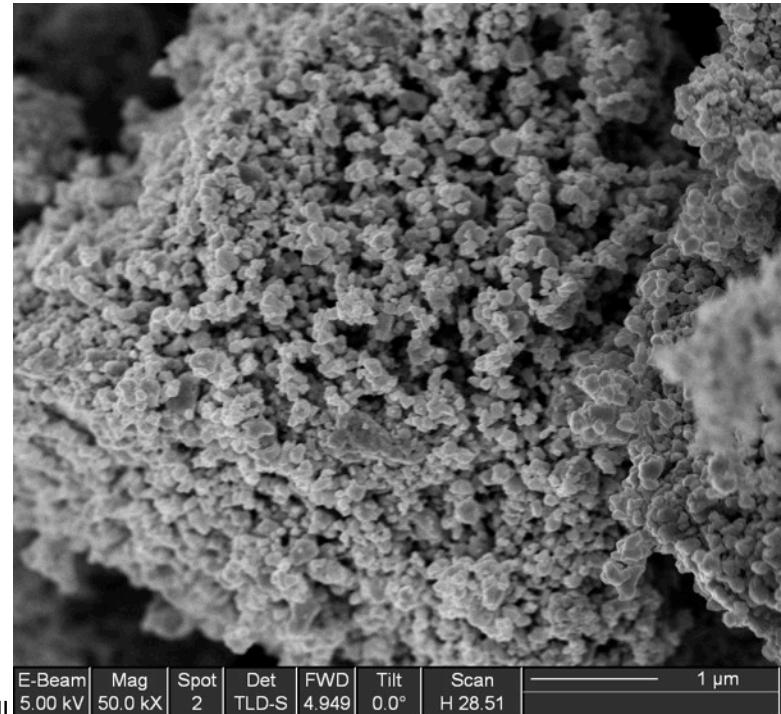
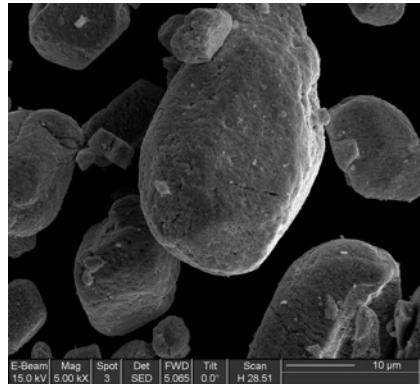


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Pellet sintered at 1750 °C

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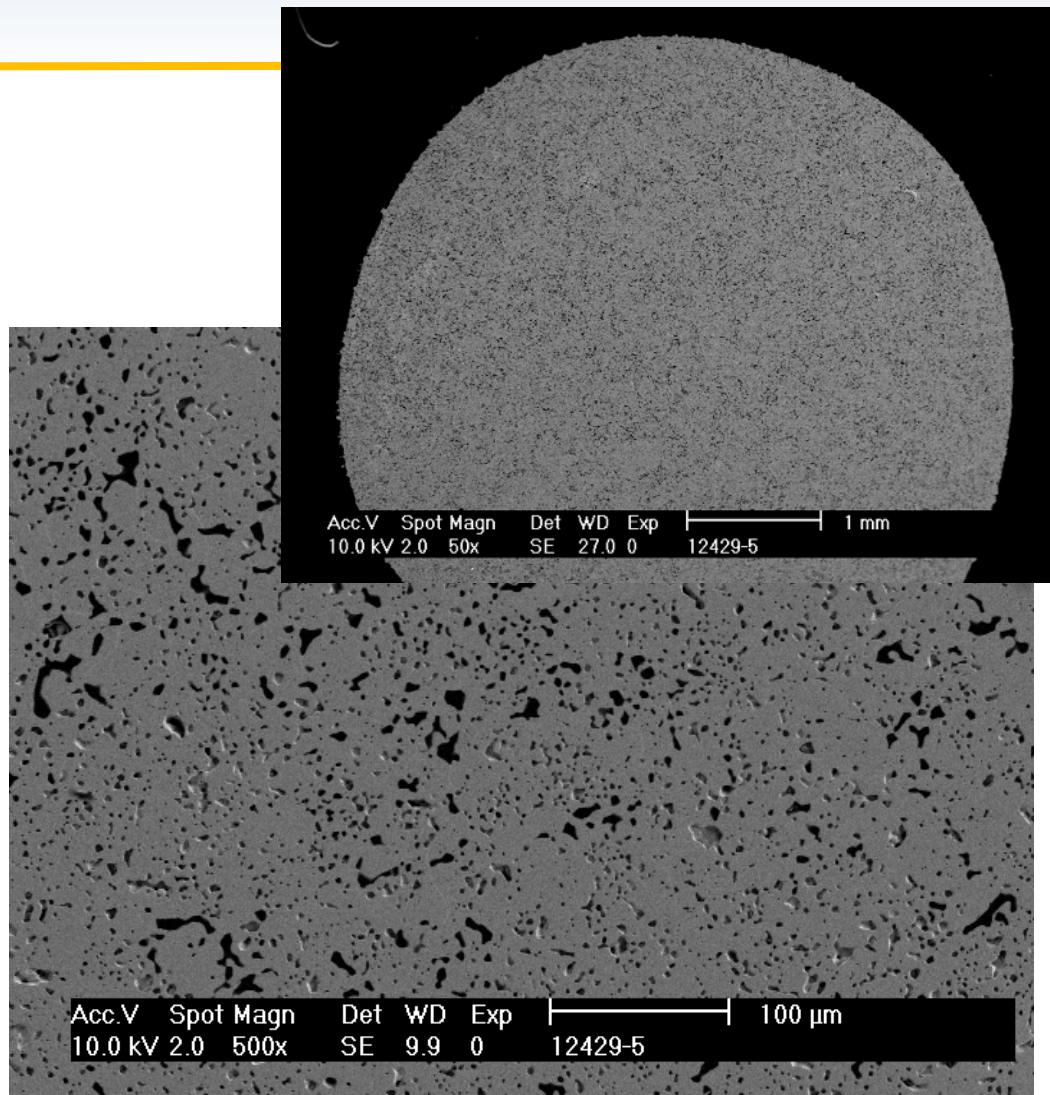
Reforming the powder...



Surface area ABB
as-received: $5.5 \text{ m}^2/\text{g}$
2 hr milled: $7.3 \text{ m}^2/\text{g}$

A repeat offender...

- **No cracking**
 - Die filling improved
 - Stresses reduced
- **Still porous**
 - Pore shape improved



Want higher density

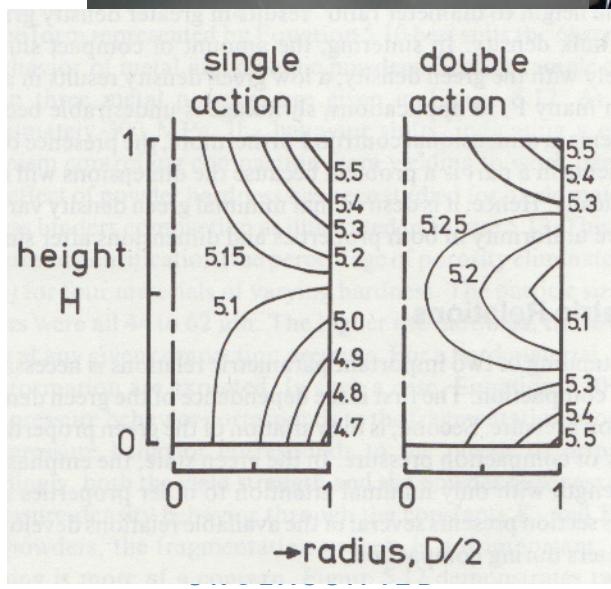
Digging deeper...

■ Compaction

- Air removal
- Friction
 - Die wall
 - Powder/powder

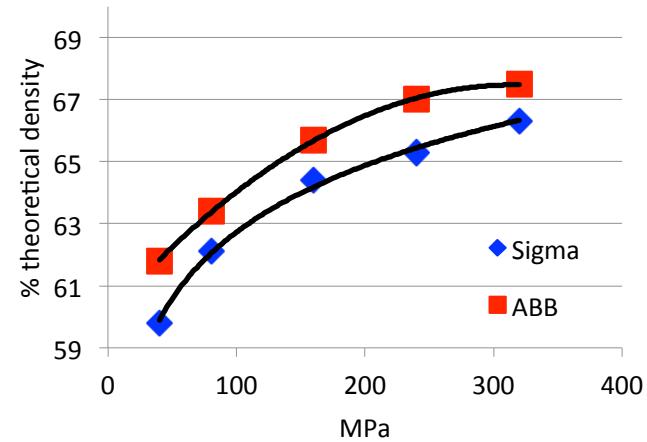
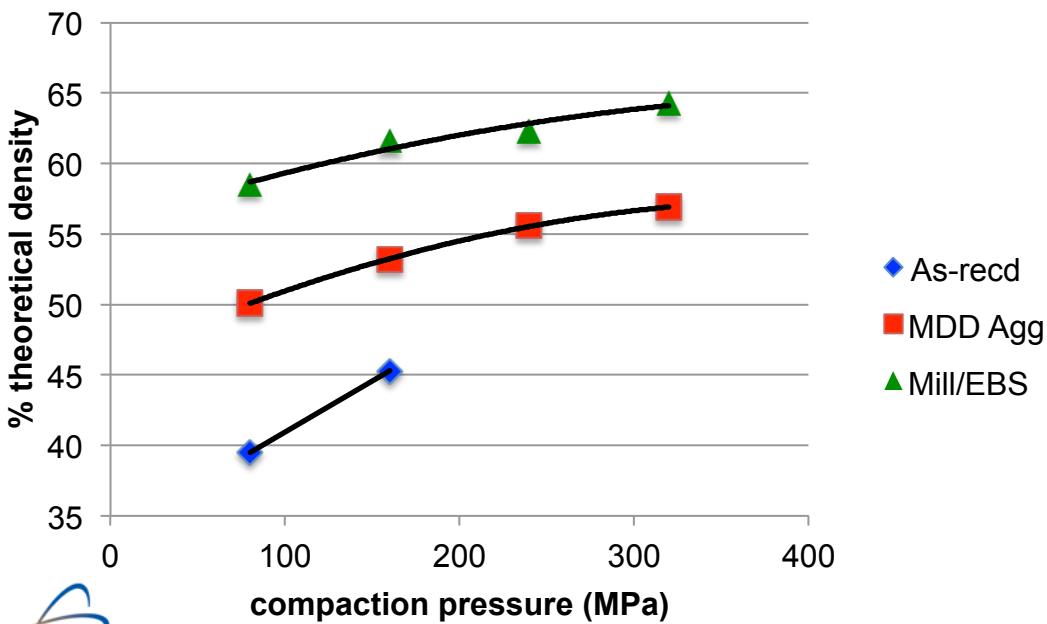
• Solutions

- Lubricants
 - Oil for tooling
 - Stearic acid
- Tooling
 - e.g., carbide liners



Green density

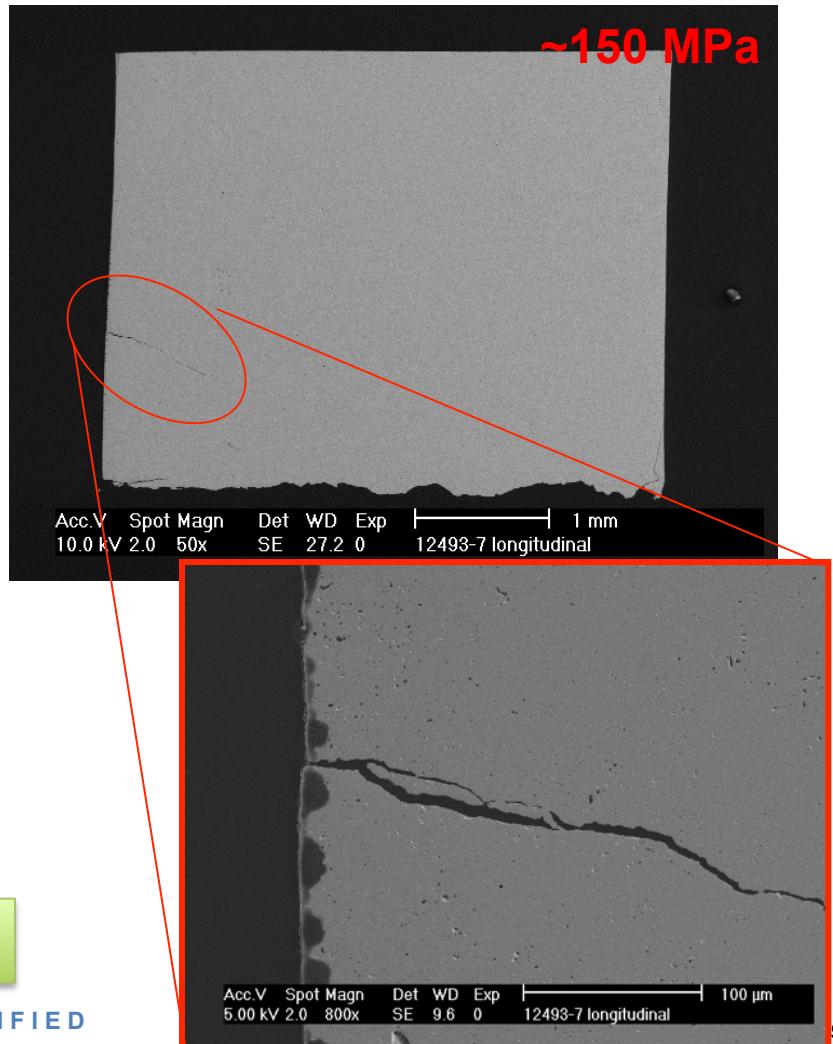
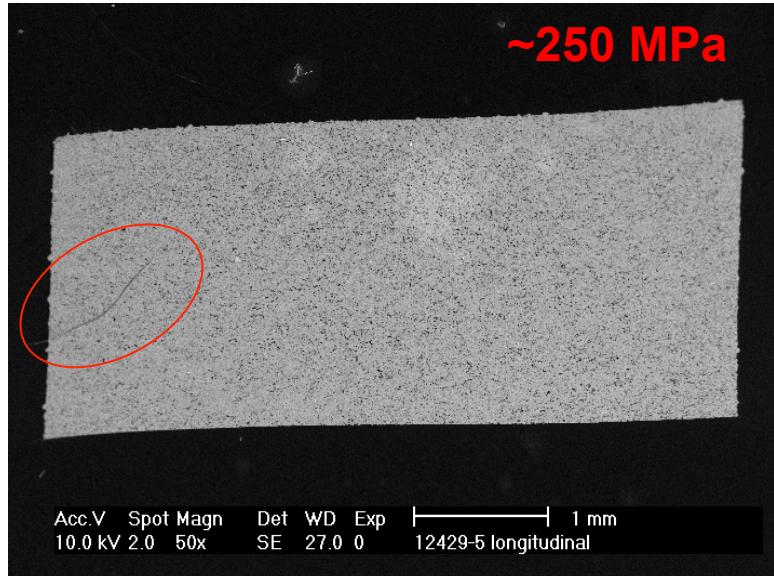
- **DUO₂ powder (various sources)**
 - As received
 - Milled
 - Milled for 15 min with EBS
- **Pellets pressed in dual action punch and die set**
 - Nominal 5.7 mm diameter by 5 mm thick



Volumetric densities sensitive to O/M ratio
Trend line added to aid eye

Pressure – enough is enough

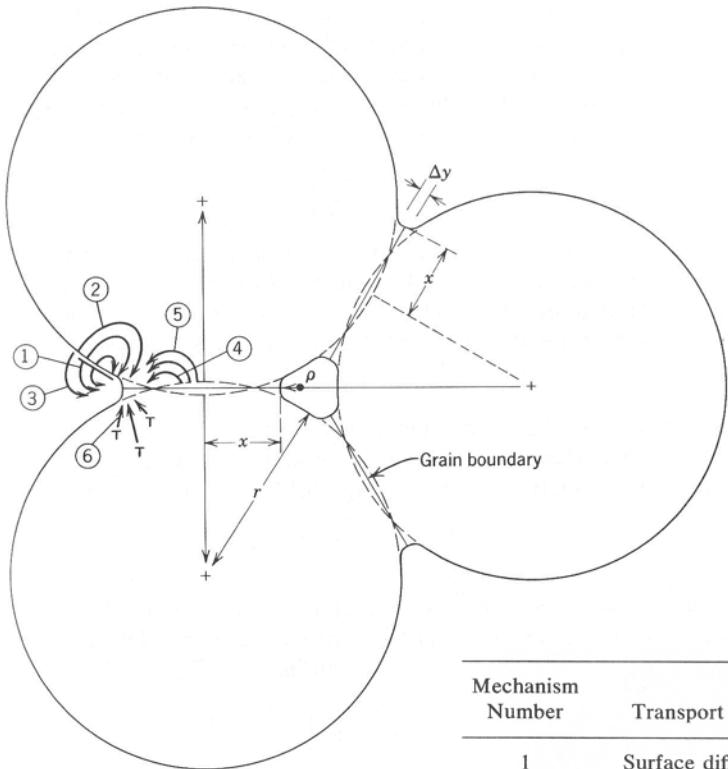
- Delamination
- Cracks follow density gradients
 - Higher gradient when thicker



Defects don't go away

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Sintering Theory



Introduction to Ceramics, W
Kingery, H Bowen, D
Uhlmann, John Wiley & Sons,
1976

Mechanism Number	Transport Path	Source of Matter	Sink of Matter
1	Surface diffusion	Surface	Neck
2	Lattice diffusion	Surface	Neck
3	Vapor transport	Surface	Neck
4	Boundary diffusion	Grain boundary	Neck
5	Lattice diffusion	Grain boundary	Neck
6	Lattice diffusion	Dislocations	Neck

Sintering requires mass diffusion

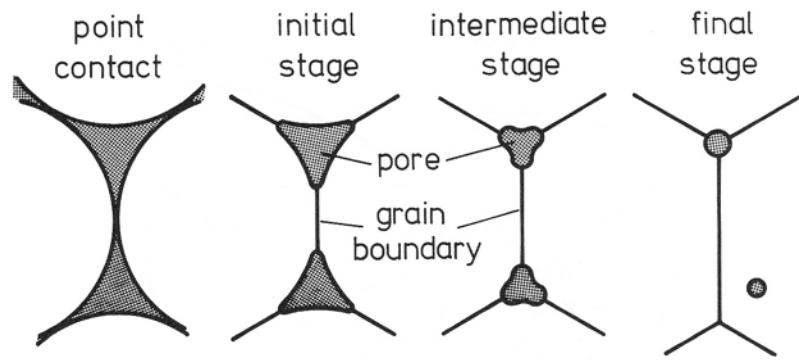
- Pore removal can be driven by chemical potential due to geometry
 - Surface area
 - Particle size
 - Chemical heterogeneity
 - Stoichiometry (O/M ratio)
 - Macroscopic heterogeneity
 - Microscopic heterogeneity
 - Heat transport

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Sintering Theory

- **Initial**
 - Surface smoothing
 - Grain boundaries/necks form
 - Rounding of open pores
- **Intermediate**
 - Pore shrinkage at boundaries
 - Mean porosity decreases
 - Slow grain growth
- **Final**
 - Closed pores
 - Pores at boundaries shrink or disappear
 - Large pores shrink slowly
 - Fast grain growth
 - Trapped pores shrink slowly



Powder Metallurgy Science, R. German, Metal Powder Industries Foundation, 1984

Decreasing Porosity

A: 800°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 10.1 12571-1

B: 900°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 9.9 12571-2

C: 1000°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 10.0 12571-3

D: 1100°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 10.1 12571-4

E: 1200°C

Acc.V Spot Magn Det WD | 20 µm
15.0 kV 3.0 2000x SE 10.5 12571-5

F: 1300°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 11.0 12571-6

F: 1400°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 10.1 12571-7

G: 1500°C

Acc.V Spot Magn Det WD | 20 µm
10.0 kV 2.0 2000x SE 10.9 12571-8

H: 1600°C

Acc.V Spot Magn Det WD | 100 µm
10.0 kV 2.0 500x SE 9.7 12571-9

Porosity Coarsens



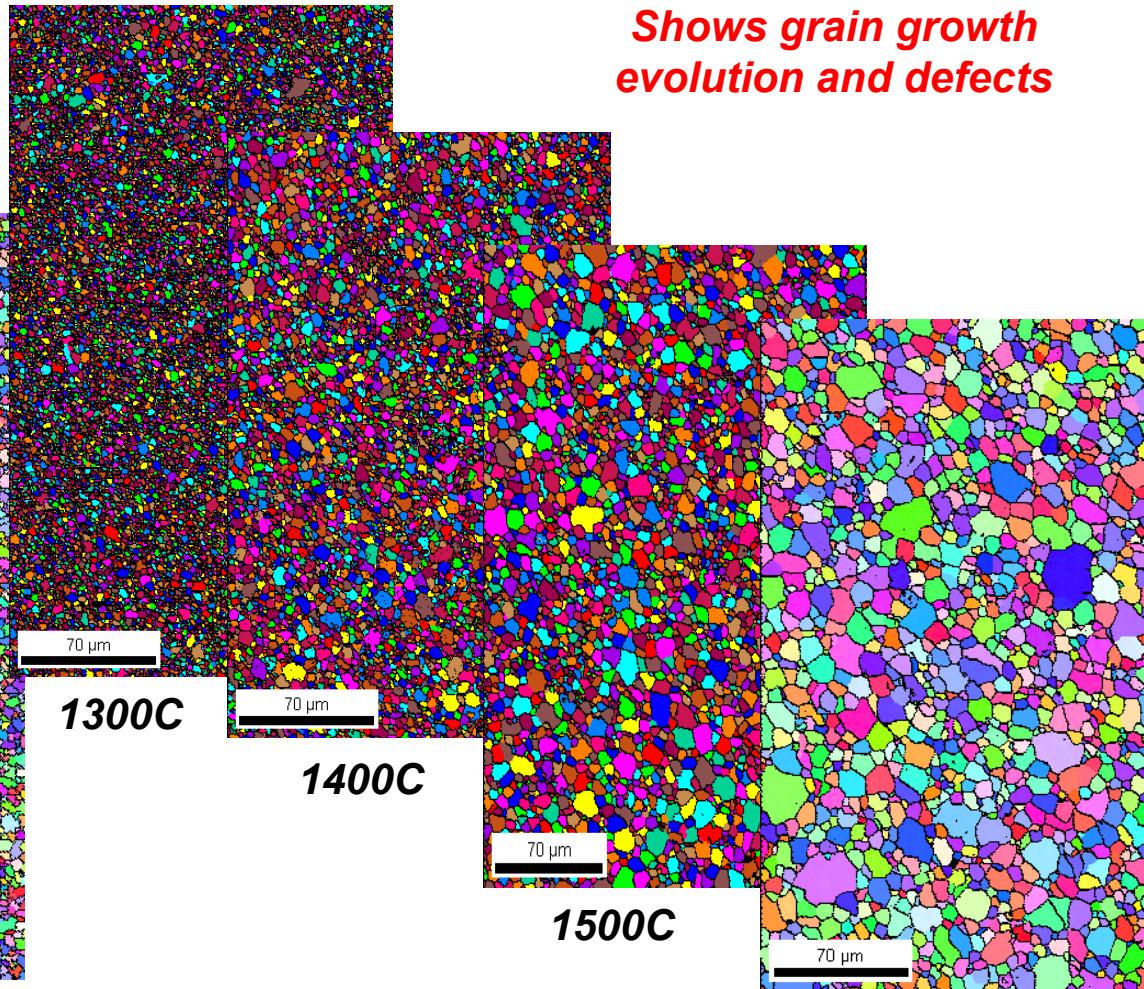
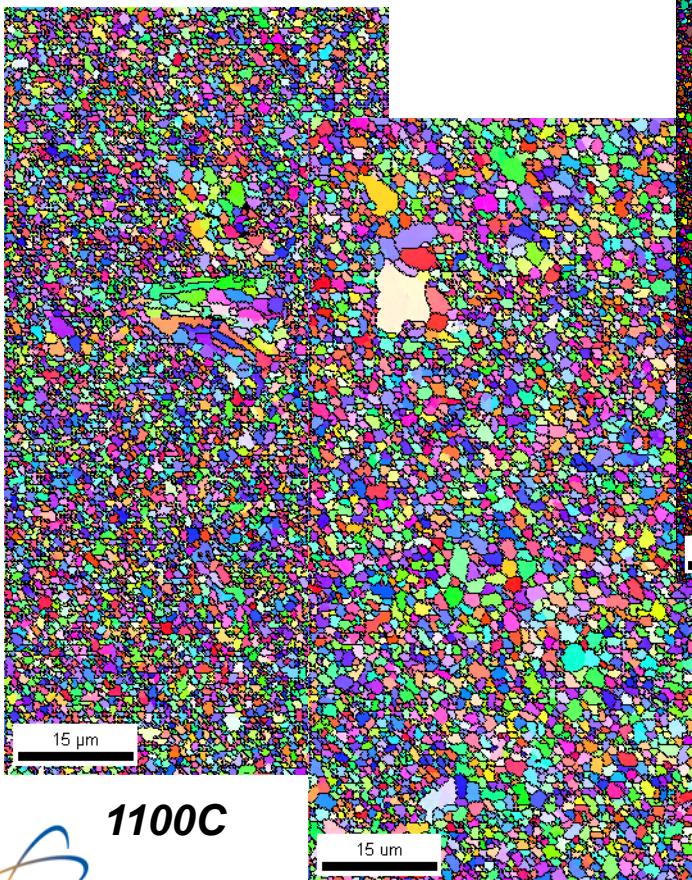
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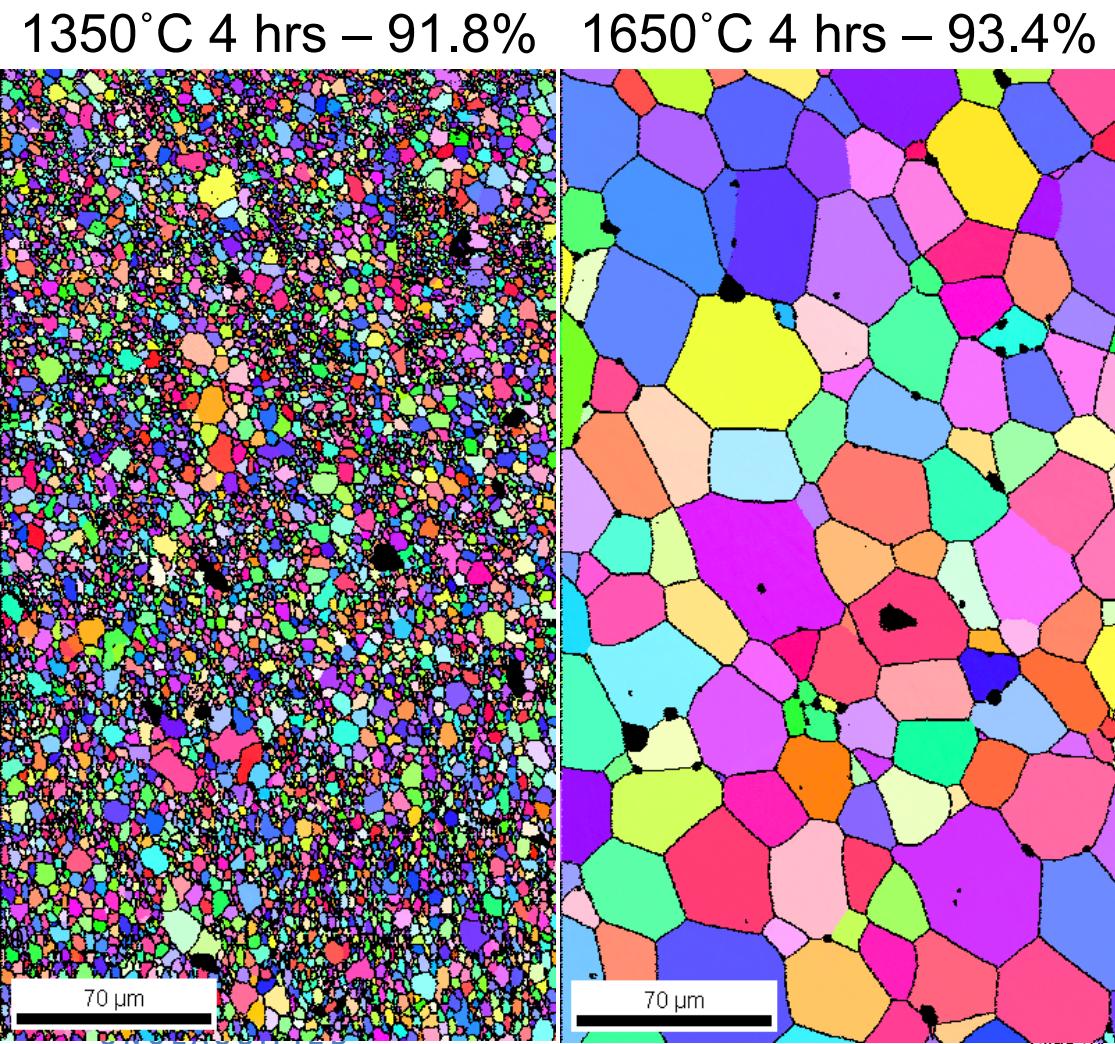
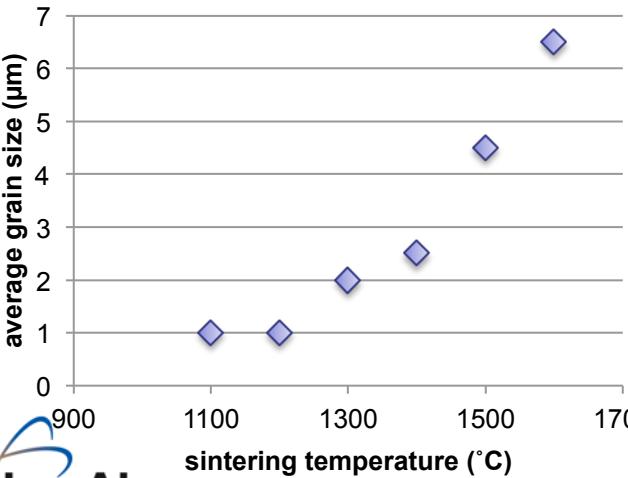
Grain Evolution During Sintering

Electron Backscatter Diffraction
of evolving microstructure



Grain size “control”

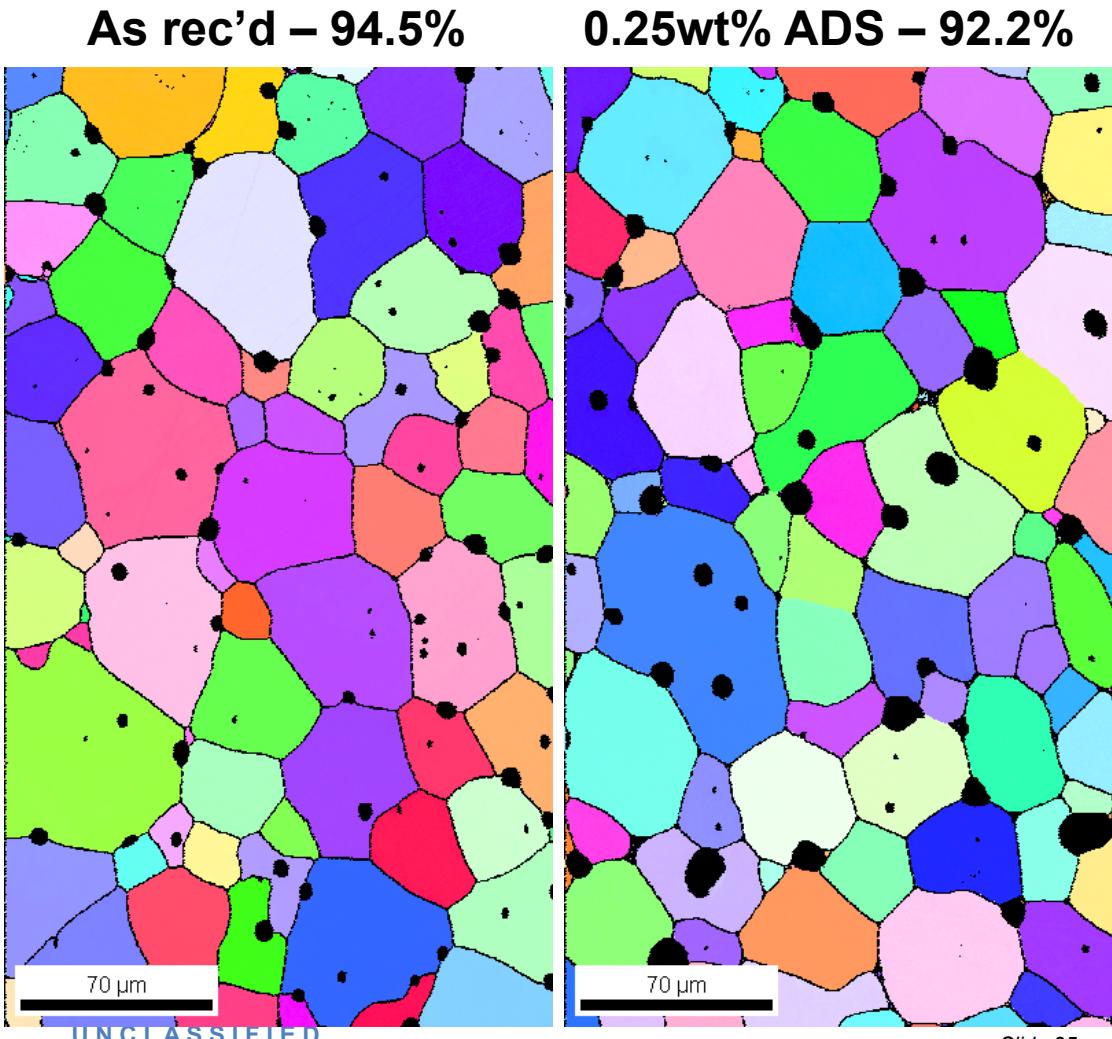
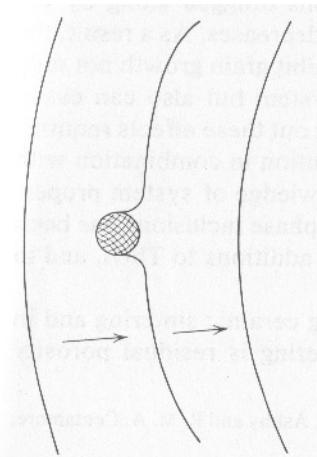
- EBSD images of pellets sintered under gettered argon
- Grains grown from 3 microns to 21 microns
- Density relatively constant 92% and 93% respectively
- No strong texture



Grain size control

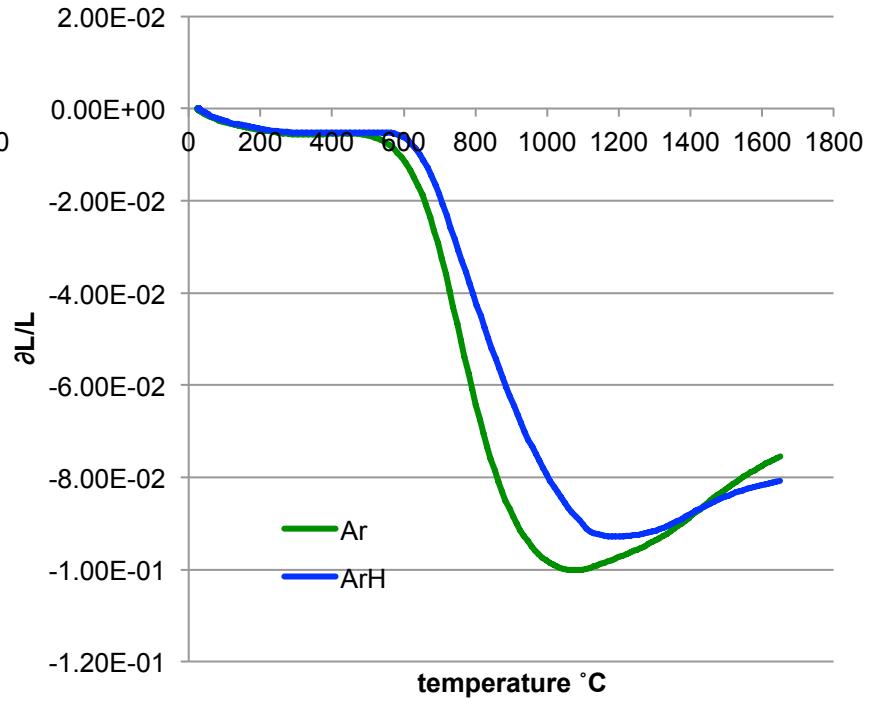
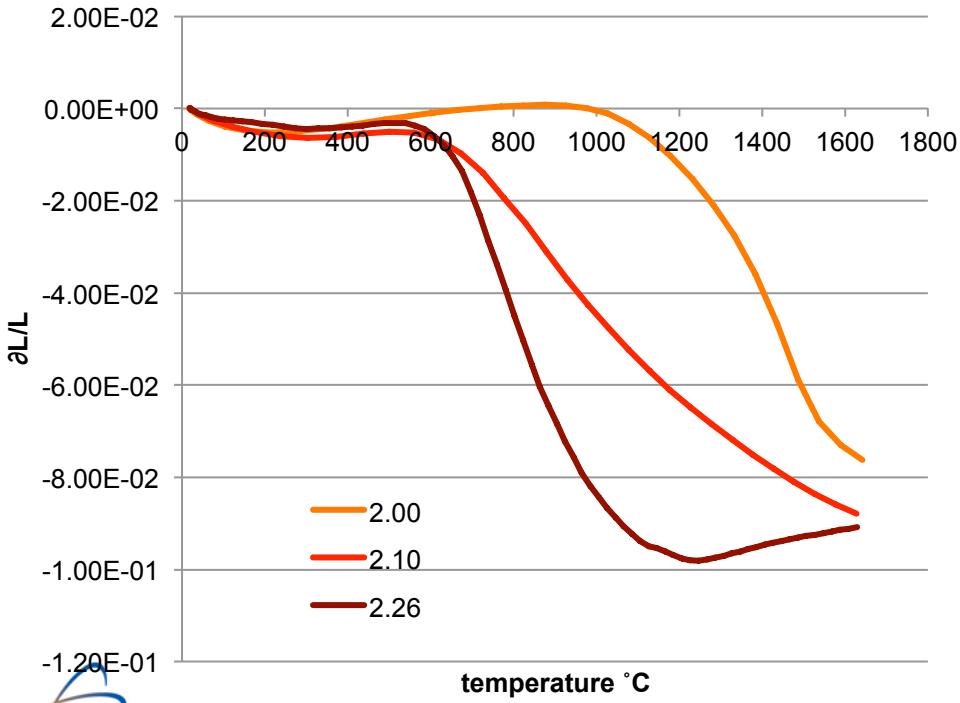
- Addition of aluminum from ADS (aluminum distearate) ~100 ppm
- Al_2O_3 is known to pin grain boundaries
- 1650°C for 4 hrs
- Grain size decreased from 21 μm to 11 μm

Minimizing
grain
boundary
energy



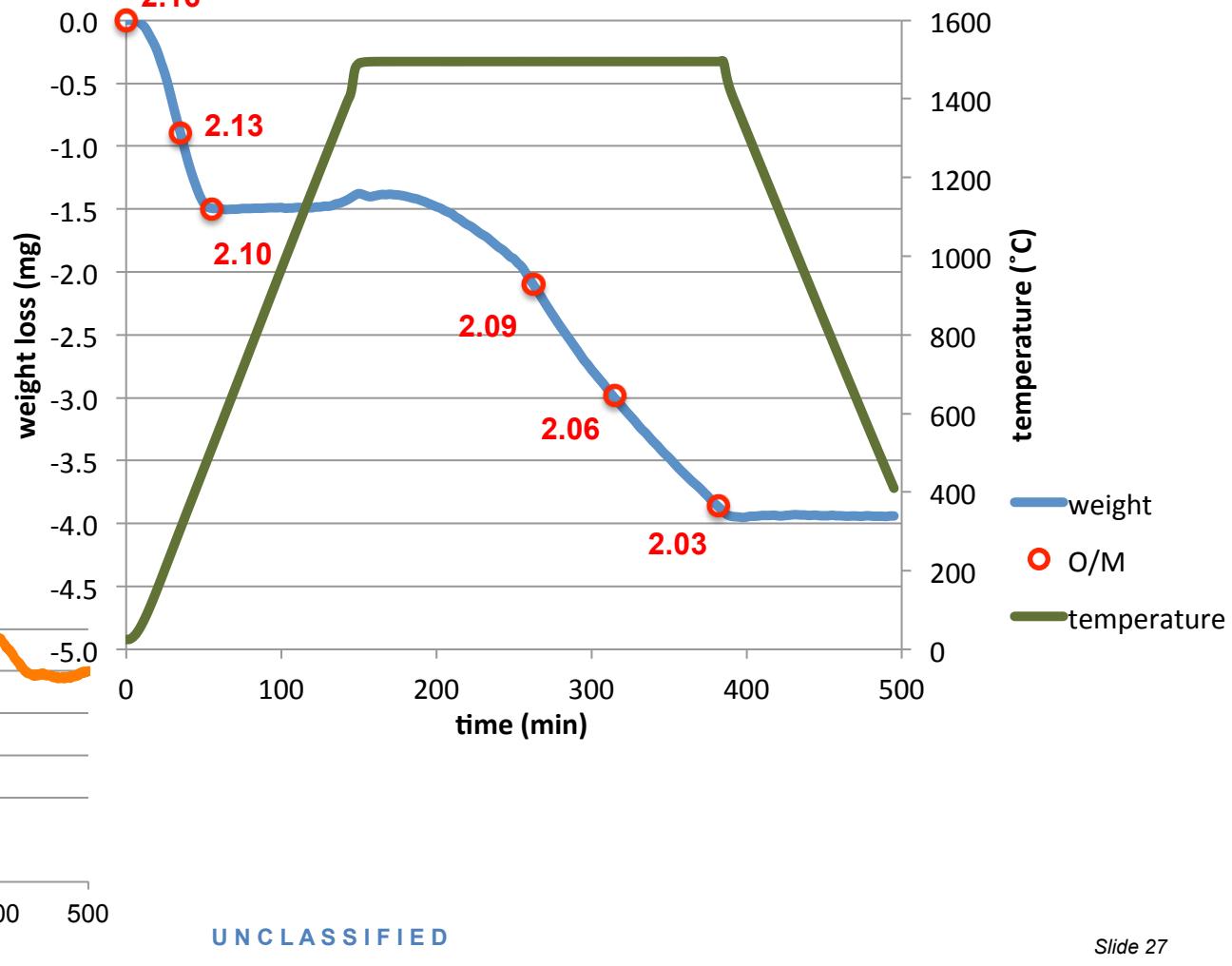
O/M effects on sintering

- UO_2 sintering is enhanced by hyperstoichiometry ($\text{O}/\text{U} > 2.00$)
- Can adjust O/M of powder prior to processing or adjust with atmosphere



O/M control

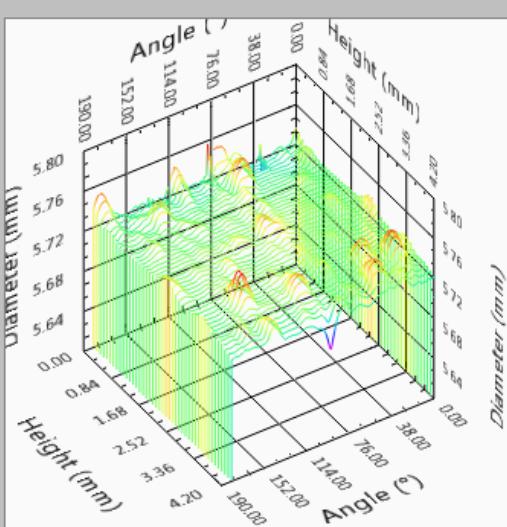
- Guided by thermodynamic modeling at ORNL
- Achieved with sophisticated gas control system
- Argon carrier with sub ppm hydrogen and oxygen control
- Allows precise sintering control



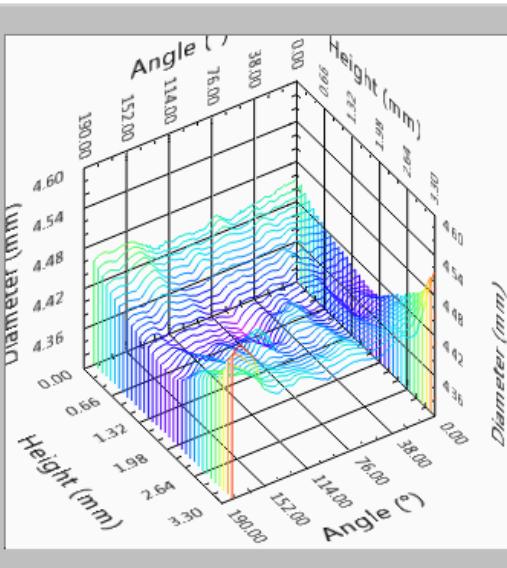
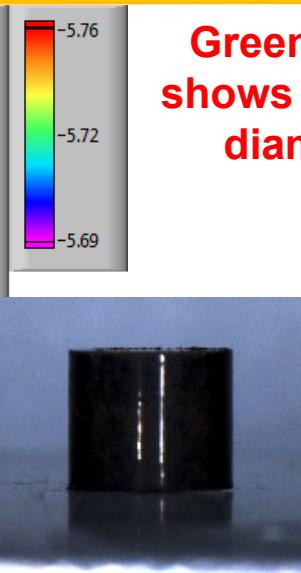
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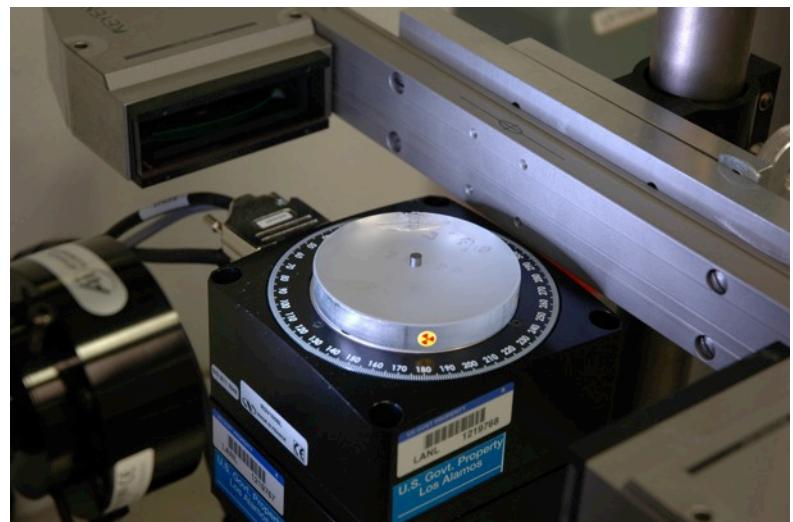
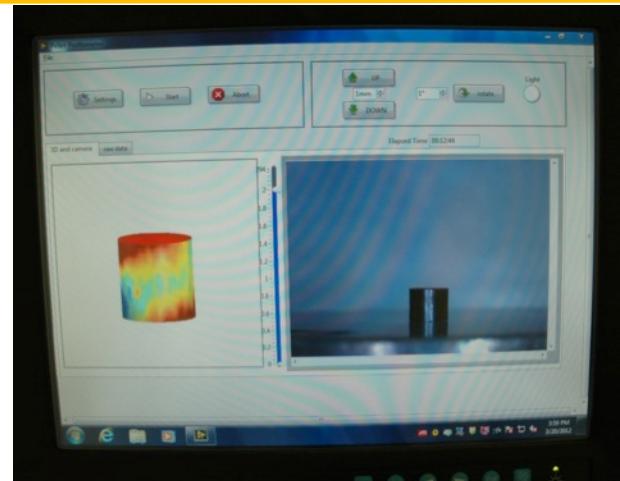
Dimensional changes due to sintering



Green pellet
shows uniform
diameter



Sintered pellet
shows
“hourgassing”

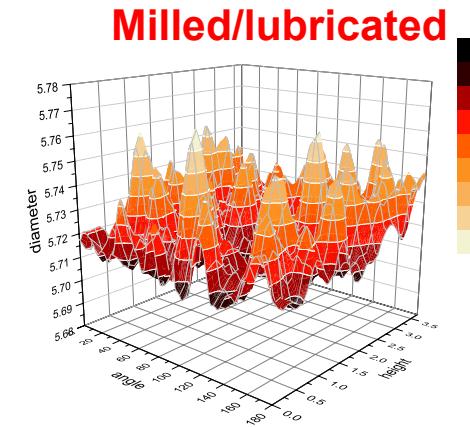
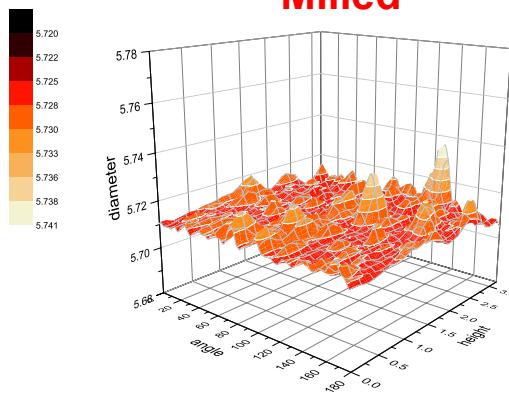
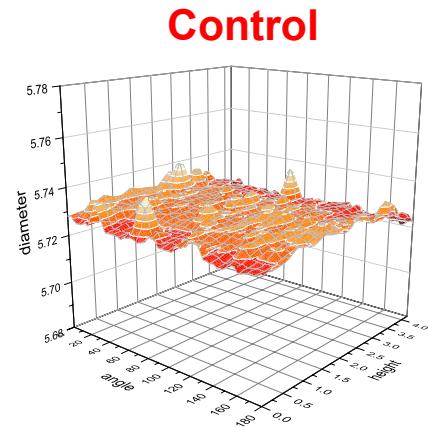


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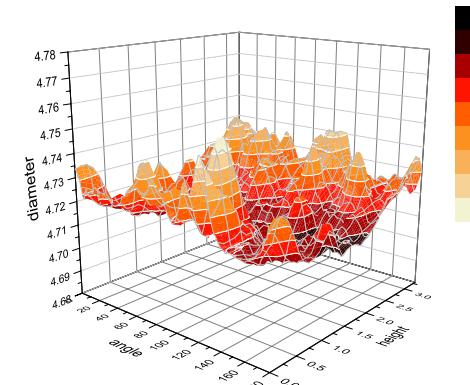
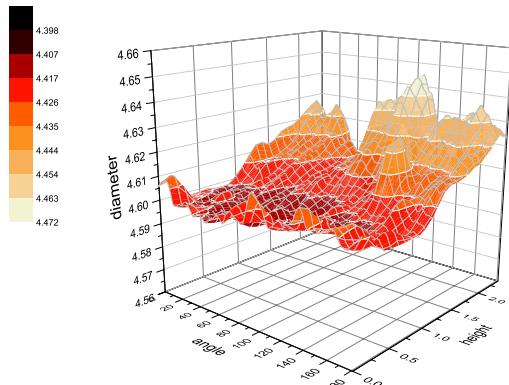
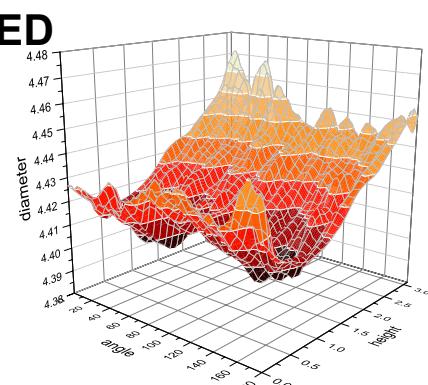
SA

Processing modifications to minimize hourgassing

**GREEN
pellets:**



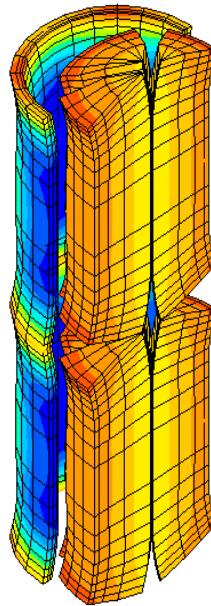
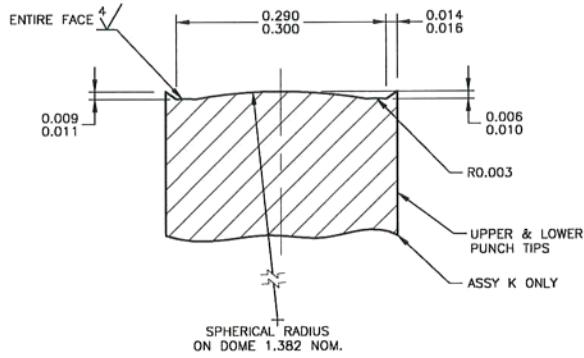
**SINTERED
Pellets:**



Less Hourgassing
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Pellet Geometry

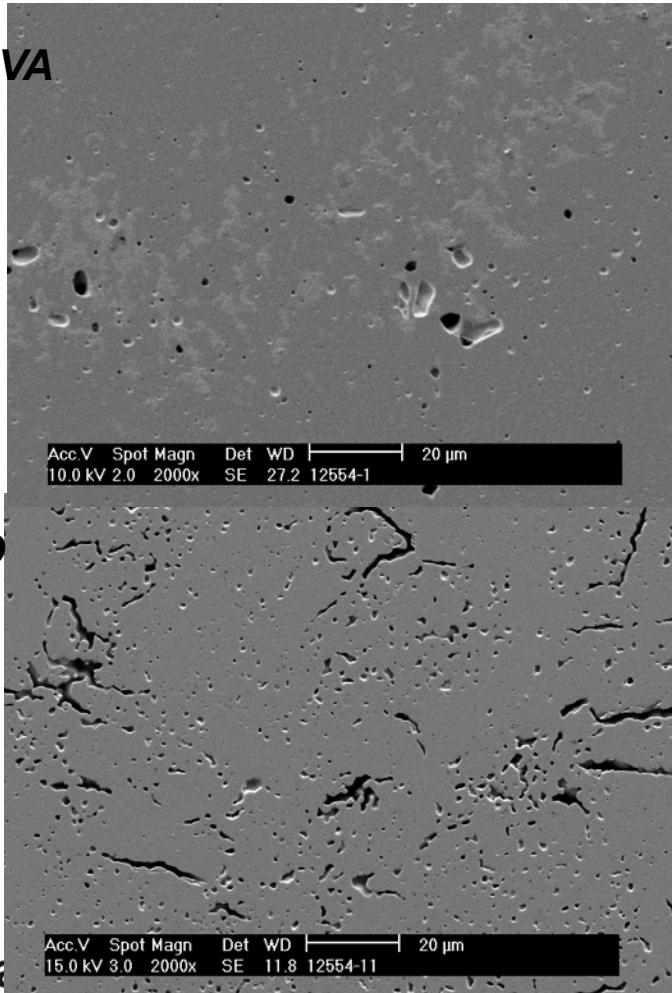
- **Dished and chamfered**
 - Dish to accommodate thermal expansion
 - Chamfer to minimize chipping
- **Why not barreled?**
- **Controlled porosity?**



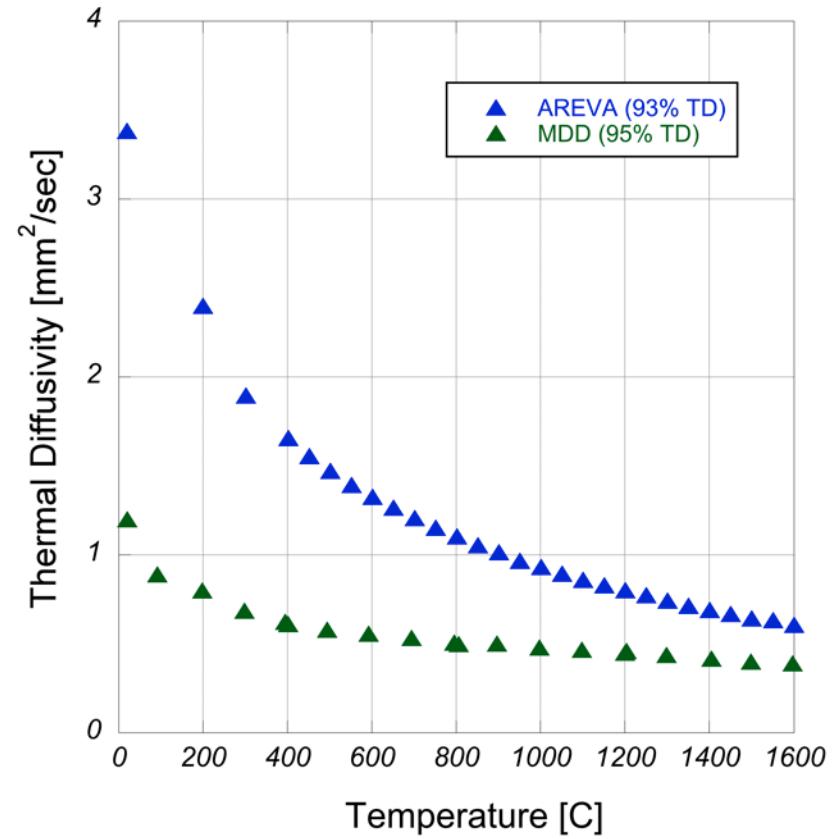
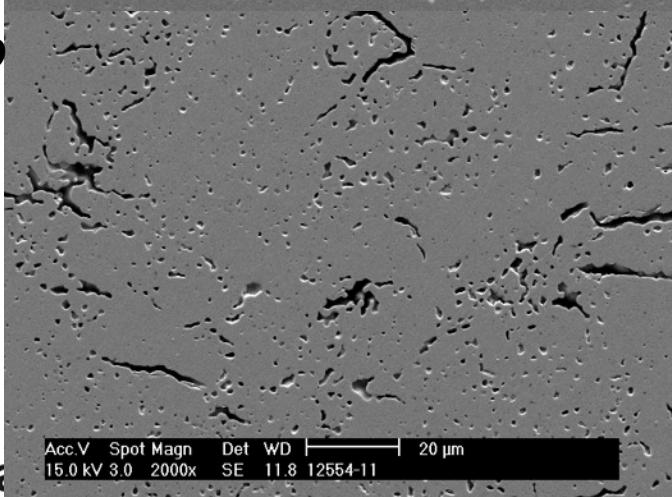
Microstructure Affects Properties

- Pore structure

AREVA



MDD



Diffusivity of MDD Pellet Compared to Typical Curve

Alternative Fabrication Methods

There's more than one way to skin a cat...

■ Spark Plasma Sintering (SPS)

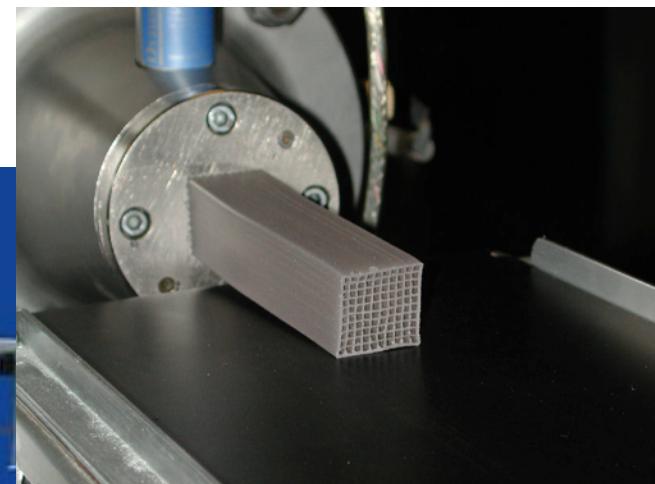
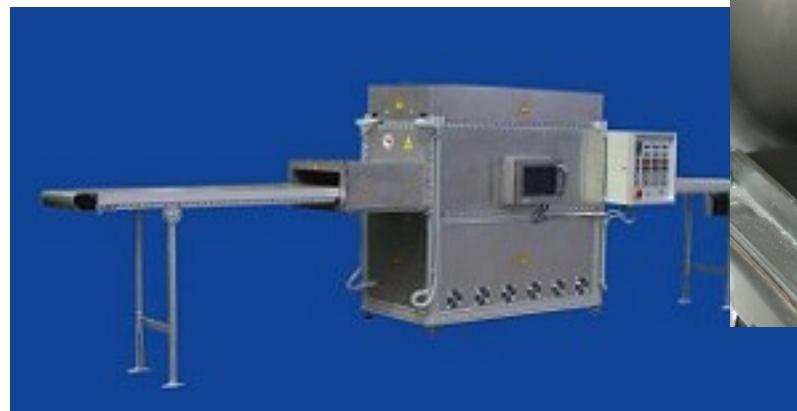
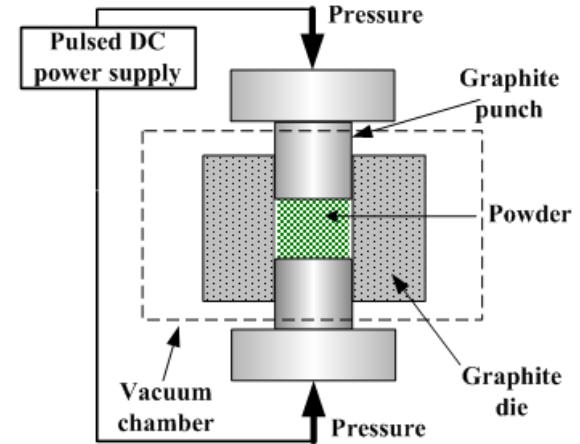
- Rapid, near net shaping
- Large volume production, microstructure

■ Extrusion

- Homogeneous microstructure, continuous, complex shapes
- Liquid processing

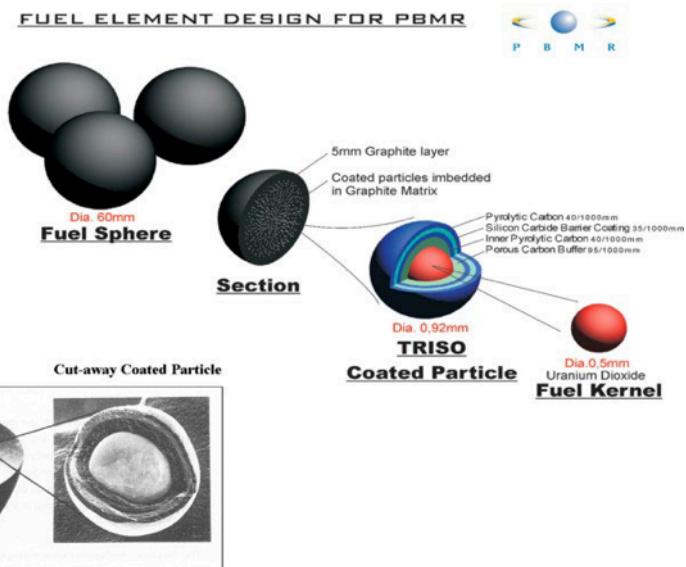
■ Microwave sintering

- Rapid, remote equipment
- Microstructure

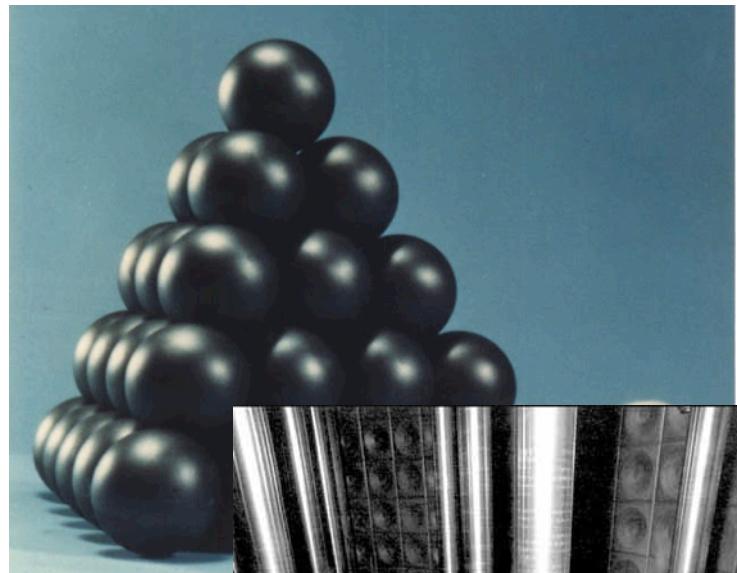


“Safer” designs

- High temp – crack steam to generate hydrogen
- 1/30th powder density
- Helium coolant
- Negative feedback stabilizes core around 1600C



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Summary

- Uranium oxide fuel pellets widely used in PWR, BWR, PHWR, AGR
- Fabrication by traditional cold press and sinter
 - Powder conditioning
 - Compaction
 - Sintering
- Properties of pellet are path dependent
- Most failure attributed to “missing pellet surface”
- Specifications, QC and process control
- Advanced characterization (EBSD, laser flash, 3D SEM)
- Alternative fabrication methods

Acknowledgments

LANL

Ken McClellan

Darrin Byler

Andrew Nelson

Bogdan Mihaila

Pallas Papin

Denny Guidry

Anna Llobet

John Dunwoody

Steve Willson

ORNL

Stewart Voit

Ray Vedder

Claudia Rawn

Chinthaka Silva

Dixie Barker

ASU

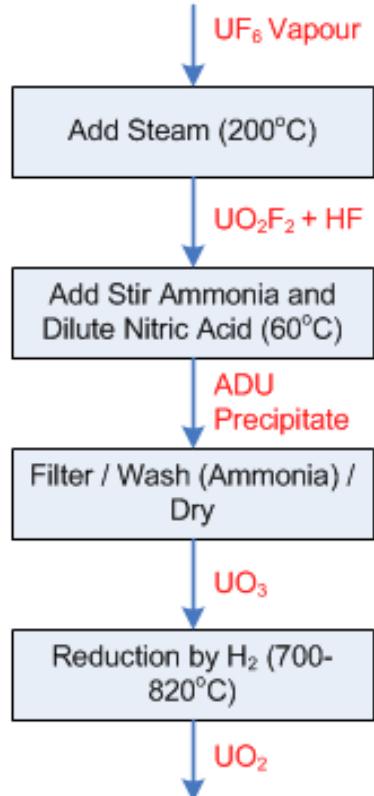
Pedro Peralta

Perspective

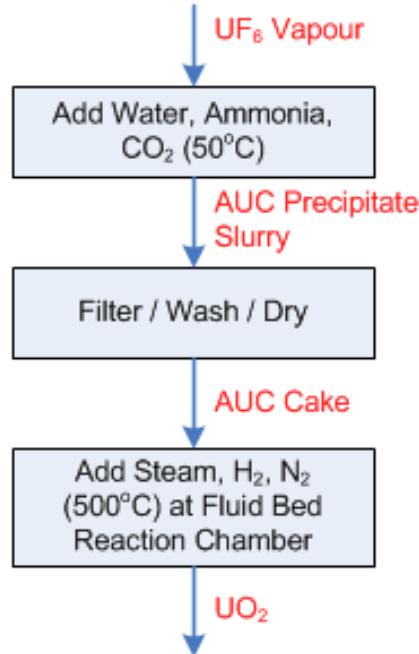
- All the used nuclear fuel produced by the U.S. in 50 years of operation—approximately 62,500 metric tons—would only cover a football field to a depth of about 7 yards. – Nuclear Energy Institute 2010
- A 1000 MW(e) nuclear power station – produces ~ 30 tons of high level waste per year. In comparison, a 1000 MW(e) coal plant produces 300,000 tons of ash per year. – International Atomic Energy Agency
- Some coal deposits contain uranium at concentrations greater than 100 ppm. Burning coal concentrates this by a factor of ten.
- The fly ash emitted by a coal power plant carries into the surrounding environment 100 times more radiation than a nuclear power plant producing the same amount of energy. – Scientific American
- One fuel pellet provides as much energy as 1 ton of coal, 149 gallons of oil, 17,000 ft³ of natural gas – Ameren

UO_2 Reconversion Process

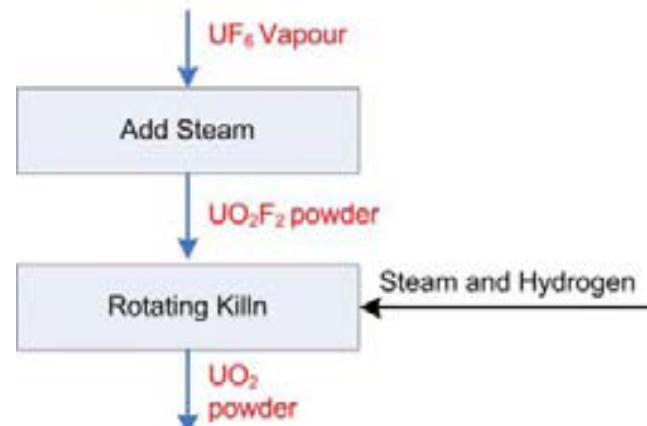
ADU Reconversion Process



AUC Reconversion Process



Integrated Dry Route (IDR)



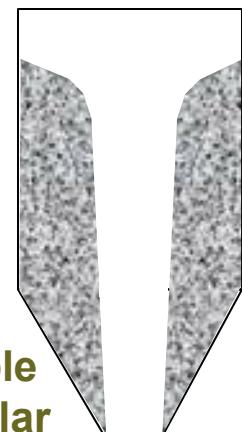
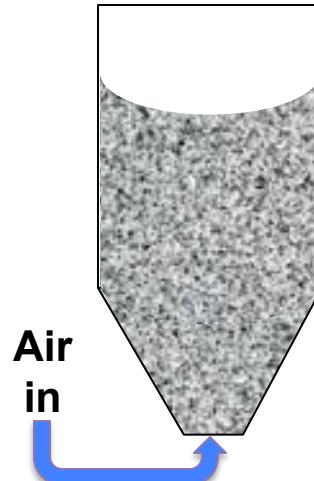
- Nuclear Fuel Cycle Information System, IAEA 2009
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Everything you ever wanted to know about hoppers...*

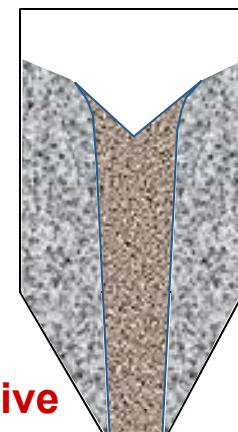
*but were afraid to ask



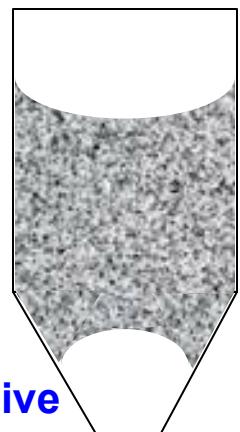
image from stellar manufacturing



Stable
annular
region
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Active
flowing
region



Cohesive
Arch plugs
hopper

Issues

- Ratholing/Piping
- Funnel Flow
- Arching/Doming
- Insufficient Flow
- Segregation
- Flushing

Sintering Reality

- **Sintering**
 - Elemental diffusion
 - Impurities and/or sintering aids
 - Heat transport
 - O/M ratio
- **Small, high surface area, uniformly packed, “active” particles**
- **Processing space**
 - Powder conditioning
 - Milling, sieving, O/M, etc.
 - Pressing conditions
 - Density, density variations, etc.
 - Atmosphere (O/M)
 - Hydrogen, oxygen, water
 - Initial reduction, post reduction, constant O/M
 - Temperature and time

How do you grow grains?

How do you prevent grains from growing?

O/M controlled sintering

- Sintering a pellet under controlled atmosphere
- Complex P_{O_2} profile to maintain constant O/M
- Guided by thermodynamic modeling at ORNL
- Achieved with sophisticated gas control system
- Argon carrier with sub ppm hydrogen and oxygen control

