

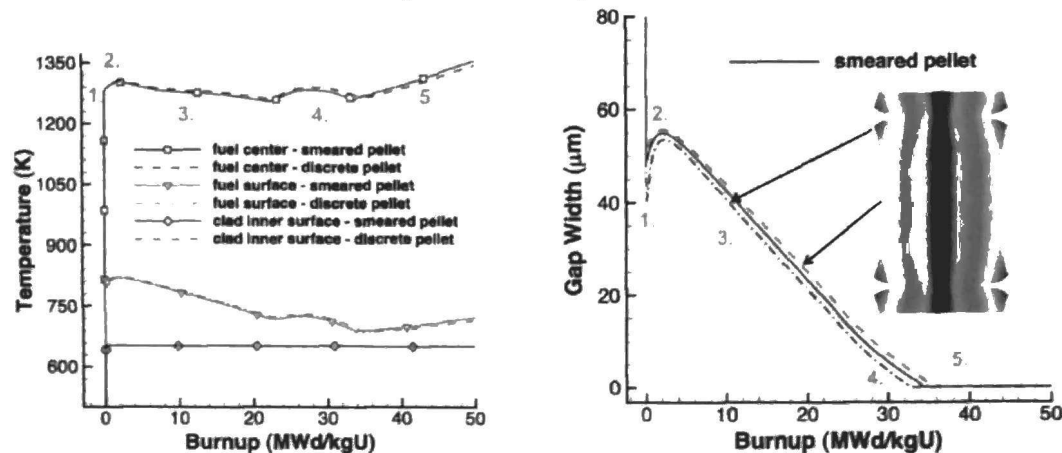
## NucE 497 Fuel Performance Exam 2 covering modules 4 - 6

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-6, 19/25

**Question 1 (25 points):**

The temperature and gap width of a fuel pellet, as predicted by a fuel performance code, is shown below. Using the plots as your guide, determine what is currently occurring within the cladding, gap, and pellet at each number. Note that the numbers are at the same burnups on the two plots.



For each number, describe what is occurring in the cladding, gap, and pellet. Also, describe what features in the plots indicated these behaviors.

-4, Describe how these changes impact on T

- Fuel:** initial thermal expansion  
**Gap:** decreased due to thermal expansion, creep  
**Cladding:** thermal creep
- Fuel:** densification due to elimination of initial porosity  
**Gap:** increasing in size as fuel shrinks  
**Cladding:** thermal & irradiation creep
- Fuel:** Swelling due to fission products  
**Gap:** decreasing as fuel swells, cladding creeps  
**Clad:** hydride formation, creep
- Fuel:** Creep due to temperature/irradiation, fission gas release, decreased  $k$   
**Gap:** decreasing as fuel  
**Clad:** same as 3
- Fuel:** Creep continues, swelling continues, more gas release  
**Gap:** vanishes, fuel in contact w/ cladding  
**Clad:** contacts fuel, fracture possible

-2, T increases because fuel  $k$  decreases with burnup

## Question 2 (30 points)

-4, 26/30

A fuel pellet with an average grain size of 8 microns is irradiated with a volumetric neutron flux of  $2.0 \times 10^{13}$  fissions/(cm<sup>3</sup> s). Assume the pellet is at a uniform temperature of 900 °C.

a) What is the fission gas diffusion coefficient at this temperature? (5 pts)

$$\dot{F} = g \sigma_f N \phi = 0.03 (1.0 \times 10^{28} \text{ cm}^{-2}) (5.50 \times 10^{-22}) (2.0 \times 10^{13})$$

$$= 3.3424 \times 10^{-11} \text{ cm}^3/\text{s}$$

-0,  $\dot{F}_{dot} = 2.0 \times 10^{13}$

$$D = D_1 + D_2 + D_3$$

$$D_1 = 7.6 \times 10^{-6} \exp \left[ \frac{-3.03}{k_b T} \right] = 7.6 \times 10^{-6} \exp \left[ \frac{-3.03}{8.617 \times 10^{-5} (1173)} \right]$$

$$= 7.28 \times 10^{-19} \text{ cm}^2/\text{s}$$

$$D_2 = 1.41 \times 10^{-18} \exp \left[ \frac{-1.19}{k_b T} \right] \sqrt{\dot{F}} = 1.41 \times 10^{-18} \exp \left[ \frac{-1.19}{8.617 \times 10^{-5} (1173)} \right] \sqrt{3.3424 \times 10^{-11}}$$

$$= 5.12 \times 10^{-18} \text{ cm}^2/\text{s}$$

$$D_3 = 2.0 \times 10^{-30} \dot{F} = 6.785 \times 10^{-19} \text{ cm}^2/\text{s}$$

b) How many gas atoms/cm<sup>3</sup> are released from the fuel after 2 years of irradiation? Assume the chain yield  $y = 0.3017$ . (10 pts)

$$N_{gas} = y \dot{F} t = 0.3017 (3.3424 \times 10^{-11}) (1.752 \times 10^8 \text{ s}) = 6.455 \times 10^{-18} \text{ cm}^{-3}$$

-0,  $\dot{F}_{dot} = 2 \times 10^{13}$

$$N_{release} = f N_{gas}$$

-1, Check tau to see which eqn to use

$$f = 4 \sqrt{\frac{D t}{\pi a^2}} - \frac{3}{2} \frac{D t}{a^2} = 4 \sqrt{\frac{6.5265 \times 10^{-18} (6.307 \times 10^7)}{\pi (8 \times 10^{-4})^2}} - \frac{3}{2} \left[ \frac{6.5265 \times 10^{-18} (6.307 \times 10^7)}{(8 \times 10^{-4})^2} \right]$$

$$f = 0.056268$$

$$N_r = (0.056268) (6.455 \times 10^{-18}) = 3.632 \times 10^{-17} \text{ cm}^{-3}$$

c) After 2 years of irradiation, the pellet is removed from the reactor and from its cladding, venting all released gas. It is then moved to a furnace and annealed at 2000 °C. Estimate how long before 10% of the gas trapped in the pellet is released. How many gas atoms/cm<sup>3</sup> will have been released during this time? (15 pts)

$$D_1 = 7.6 \times 10^{-6} \exp \left[ \frac{-3.03}{k_b T} \right] = 1.453 \times 10^{-12} \text{ cm}^2/\text{s}$$

$$D_2 = 1.41 \times 10^{-18} \exp \left[ \frac{-1.19}{k_b T} \right] \sqrt{3.3424 \times 10^{-11}} = 8.213 \times 10^{-13} \text{ cm}^2/\text{s}$$

$$D_3 = 2.0 \times 10^{-30} \dot{F} = 6.785 \times 10^{-19} \text{ cm}^2/\text{s}$$

-1, No fissioning so  $D = D_1$

$$D = 2.2743 \times 10^{-12} \text{ cm}^2/\text{s}$$

-2, In post irradiation annealing, no new gas is produced

$$f = 4 \sqrt{\frac{D t}{\pi a^2}} - \frac{3}{2} \frac{D t}{a^2}$$

$$t = \left( \frac{f}{b} \right)^2 \left( \frac{\pi a^2}{D} \right) = \left( \frac{0.1}{b} \right)^2 \left( \frac{\pi (8 \times 10^{-4})^2}{2.2743 \times 10^{-12}} \right) = 2.46 \times 10^2 \text{ s}$$

$$N_r = y \dot{F} t = 0.3017 (3.3424 \times 10^{-11}) (2.46 \times 10^2) (0.1) = 2.518 \times 10^{-17} \text{ cm}^{-3}$$

### Problem 3 (30 points)

-8, 22/30

A ZIRLO cladding tube is in reactor at 600 K for one year. The initial wall thickness is 0.6 mm.

a) What is the oxide weight gain in mg/dm<sup>2</sup> after this time? (10 pts)

$$\delta = \frac{w}{14.7}$$

$$\delta = \delta^* + k_L (t - t^*)$$

$$\delta^* = S_1 \exp \frac{-550}{T} = S_1 \exp \frac{-550}{600} = 2.039 \mu\text{m}$$

$$t^* = 6.67 \times 10^{-7} \exp \frac{11949}{T} = 6.67 \times 10^{-7} \exp \frac{11949}{600} = 295 \text{ d}$$

$$k_L = 7.48 \times 10^6 \exp \frac{-12500}{T} = 7.48 \times 10^6 \exp \frac{-12500}{600} = 6.7 \times 10^{-3} \frac{\mu\text{m}}{\text{d}}$$

$$\delta = 2.039 \mu\text{m} + 6.7 \times 10^{-3} \frac{\mu\text{m}}{\text{d}} (365 \text{ d} - 295 \text{ d}) = 2.508 \mu\text{m}$$

$$w = \delta (14.7) = 2.508 \mu\text{m} (14.7) = 36.87 \frac{\text{mg}}{\text{dm}^2}$$

b) What is the ZIRLO wall thickness after this time? (5 pts)

$$t_g = t_0 + \delta = 0.6 \text{ mm} + 2.508 \mu\text{m} = 0.60251 \text{ mm}$$

-2, metal lost = oxide thickness/1.56

-2, thickness is lost not gained

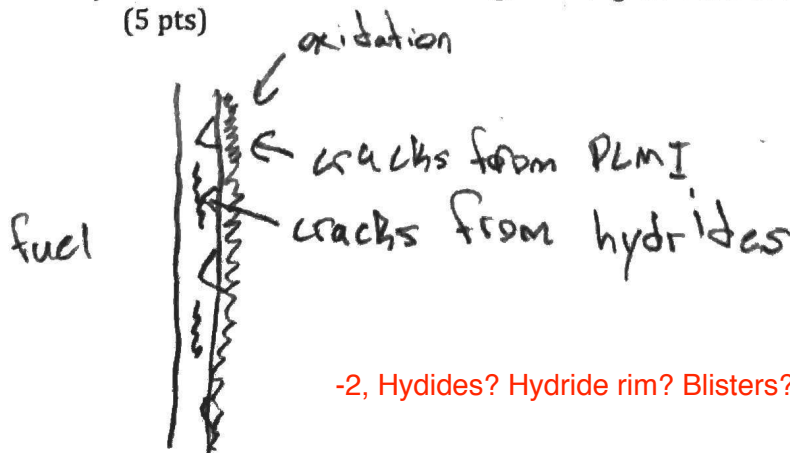
c) Assuming the hydrogen pickup fraction is 15%, what is the weight PPM of hydrogen in the cladding after one year? (10 pts)

$$C_H^{\text{clad}} = \frac{2f \delta_{\text{ox}} f_{\text{H}_2\text{O}} \left( \frac{M_H}{M_O} \right)}{\left[ t - \frac{\delta}{PDR} \right] \rho_{\text{mat}}} \times 10^6 = \frac{2(0.15)(2.508)(5.68)(0.26)(1/16) \times 10^6}{\left[ 365 - \left( \frac{2.508}{1.56} \right) \right] 6.5}$$

$$C_H^{\text{clad}} = 29.4 \text{ wt. ppm}$$

-2, t is thickness not time

d) Draw a section of the cladding, showing the various microstructure changes (5 pts)



-2, Hydrides? Hydride rim? Blisters?



**Problem 4 (15 points)**

- a) What are the primary differences between a loss of coolant accident and a reactivity insertion accident, regarding the fuel and cladding behavior? (5 pts)

LOCA causes the cladding to  $\alpha \rightarrow \beta$  transition, and oxidation breaks away causing rapid hydrogen pick up; while in a RIA the cladding can only balloon or burst. In regards to fuel, RIA can cause fuel melting or crumbling.

-3, RIA is much faster, increases heat generation. LOCA changes surface temperature of the fuel

- b) What are similarities between the fuel and cladding behavior in a RIA and a LOCA? (5 pts)

Both cause significant thermal stresses  
& can result in cladding burst/ballooning

- c) List a potential accident tolerant fuel concept and describe how it could meet the primary goal of the accident tolerant fuel program. (5 pts)

One potential concept is improving fuel properties, this will lower operating temperatures and raise melting temps  $\therefore$  when in a LOCA the change in temp needed for melting is significantly increased.

-2.5, What will you do to the fuel to change its properties