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Question 1

33/100

-20, 10/30

Solution

a) The fissile Isotope in  $U_3Si_5$  will be U-235 with the enrichment in the natural (enriched) of 0.7%

b) \* Let find the heat flux of  $U_3Si_5$

$M_{U_3Si_5} =$  Necessary equation  $N_{U_{235}} = 9Na \frac{\delta}{M_{U_3Si_5}}$

$$\Rightarrow q = \frac{N_{U_{235}} \times M_{U_3Si_5}}{Na \times \delta} =$$

-14

$M_{U_3Si_5}$

c)  $U_3Si_5$  can not be ~~an~~ potential fuel compare to  $U_3Si_2$  because of its characteristics and its properties that are ~~poor~~ for the making of the fuel.

-6, Which characteristics and properties?

## Question (2)

-12, 23/35

### Solution

$$\delta_{gap} = 80 \mu m \quad R_f = 4.5 mm \quad \delta_c = 0.6 mm \quad LHR = 250 W/cm$$

$$T_{cool} = 580 K \quad h_{cool} = 2.5 W/cm^2 K$$

$$\begin{aligned} * T_{co} &= \frac{LHR}{2\pi R_f h_{cool}} + T_{cool} \\ &= \frac{250 W/cm}{2 \times 3.14159 \times 0.45 cm \times 2.5 W/cm^2 K} + 580 K \\ &= 615 K \end{aligned}$$

$$\begin{aligned} * T_{c1} &= \frac{LHR \delta_c}{2\pi R_f k_c} + T_{co} \\ &= \frac{250 W/cm \times 0.06 cm}{2 \times 3.14159 \times 0.45 cm \times 0.2 W/cm K} + 615 K \\ &\approx 642 K \end{aligned}$$

( $k_c$  for  $U_3Si_2$   
table 8.1  
in HW3)

$$T_s = \frac{LHR}{2\pi R_f h_{gap}} + T_{ci}$$

$$h_{gap} = \frac{k_{He}}{\delta_{gap}} =$$

$$= \frac{0.0026}{0.008} = 0.325 \text{ W/cm}^2\text{K}$$

$$(k_{gas} = A \times 10^{-6} T^{0.79})$$

$$k_{He} = 16 \times 10^{-6} \times (642)^{0.79}$$

$$= 0.0026$$

$$\Rightarrow T_s = \frac{250 \text{ W/cm}}{2 \times 3.14159 \times 0.45 \times 0.325} + 642 \text{ K}$$

$$\Rightarrow T_s = 914 \text{ K}$$

-1, math error.  $T_s = 958.2 \text{ K}$

b) maximum stress

$$E (\epsilon_{rr} - \epsilon_{\theta\theta}) = (1 + \nu) (\sigma_{rr} - \sigma_{\theta\theta})$$

$$\text{or } \sigma_{\theta} = \frac{\alpha_F E_F (LHR)}{16\pi (1 - \nu_F) K_F} \left( 1 - 3 \frac{r^2}{R_F^2} \right)$$

$$r = R_F \text{ (maximum)}$$

$$\begin{aligned}\sigma_{\theta} &= \frac{\alpha_F E_F (\text{LHR})}{16\pi(1-\nu_F)k_F} \times 2 \\ &= \frac{7.5 \times 10^{-6} \text{ K}^{-1} \times 246.7 \times 2}{16 \times 3.14159 \times (1-0.25) \times 0.2} \quad -3, \text{ LHR} = 250\end{aligned}$$

$$\Rightarrow \boxed{\sigma_{\theta} = 493 \times 10^{-6} \text{ GPa}}$$

c.) The stress will be higher in case of  $\text{VO}_2$  because  $\text{VO}_2$  express a  $T_S$  > than the one for VN  
 -3, higher stress because thermal conductivity is much lower.

$$\begin{aligned}\text{d.) } \sigma_{rr}(R_i) &= -P \\ \text{and } \sigma_{rr}(R_o) &= 0\end{aligned}$$

-5, These aren't really assumptions, they are boundary conditions. There are many other actual assumptions

### Question 3

a.) Assumption 0/35

$$\sigma_{rr}(R_i) = -P$$

$$\sigma_{rr}(R_o) = 0$$