

1. (a) $T = 625 \text{ K}$, time 400 days, initial wall thickness = 500 μm

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check if it is gone through transition

$$\text{critical time} = t^*(d) = 6.62 \times 10^{-7} \exp\left(\frac{11949}{625}\right) \approx 133 \text{ days} < 400 \text{ days}$$

\Rightarrow past transition time

\Rightarrow we linear fit

$$\delta^* (\mu\text{m}) = 5.1 \times \exp\left(\frac{-550}{625}\right) \approx 2.115393$$

$$K_L \left(\frac{\mu\text{m}}{\text{d}}\right) = 7.48 \times 10^6 \times \exp\left(\frac{-12500}{625}\right) \approx 0.015417$$

$$\Rightarrow \boxed{\delta(\mu\text{m}) = \delta^* + K_L \times (400 - 133) \approx 6.232 \mu\text{m}} \rightarrow \text{oxide thickness}$$

(b)

$$C_H^{\text{clad}} [\text{wt. ppm}] = \frac{2fM_o}{m_{\text{Zr}}} = \frac{2f \times \delta \times \rho_{\text{oxide}} \times f_{\text{ZrO}_2}^o \times \frac{M_H}{M_o}}{\left(t - \frac{\delta}{\text{PBR}}\right) \times \rho_{\text{Zr}}} \times 10^6$$

As given, $\text{PBR} = 1.56$, $\rho_{\text{Zr}} = 6.5 \text{ g/cm}^3$, $\rho_{\text{ZrO}_2} = 5.68 \text{ g/cm}^3$, $f = 18\%$

$$\Rightarrow f_{\text{ZrO}_2}^o = \frac{2 \times 16}{2 \times 16 + 91} = 0.26$$

$$C_H^{\text{clad}} [\text{wt. ppm}] = \frac{2 \times 18\% \times 6.232 [\mu\text{m}] \times 5.68 \text{ g/cm}^3 \times 0.26 \times \frac{1}{16}}{\left(500 - \frac{6.232 [\mu\text{m}]}{1.56}\right) \times 6.5 \text{ g/cm}^3} \times 10^6$$

$$\approx 63.721 [\text{wt. ppm}]$$

looking for $t = 305 \text{ dy}$ in part b

2. Diffusion of the O and e^- is the rate-limiting step in the aqueous corrosion of Zr cladding.

e^- diffusion is "fast"

3. Pilling - Bedworth ratio (PBR) is the ratio of volume of the oxide and volume of the oxidized metal.

$$PBR = \frac{V_{\text{oxide}}}{V_{\text{metal}}} = \frac{\frac{M_{\text{oxide}}}{\rho_{\text{oxide}}}}{\frac{M_{\text{metal}}}{\rho_{\text{metal}}}} = \frac{M_{\text{oxide}} \rho_{\text{metal}}}{M_{\text{metal}} \rho_{\text{oxide}}}$$

when

- $PBR < 1 \Rightarrow$ the oxide layer is too thin to have protective effect eg. Mg
- $PBR > 2 \Rightarrow$ the oxide layer is so thick that it starts to chip off \Rightarrow No protective effect eg. Iron
- $1 < PBR < 2 \Rightarrow$ oxide coating has the passivating effect on the surface of the metal.

4. ① The hydrogen mostly form during the oxidation reaction between the water coolant and cladding surface. And, hydride usually easily to form at the place with lower temperature (\therefore Soret effect) ③

② The Soret effect says hydrogen prefer to move toward lower temperature place, - T solubility, stresses in cladding

③ If the metal pickup the hydride,

\Rightarrow ① Hydride embrittlement ✓

② loss of fracture toughness ✓

③ delay Hydride cracking ✓

④ accelerated corrosion eg. IGSCC ✓

⑤ accelerated irradiation growth. ✓

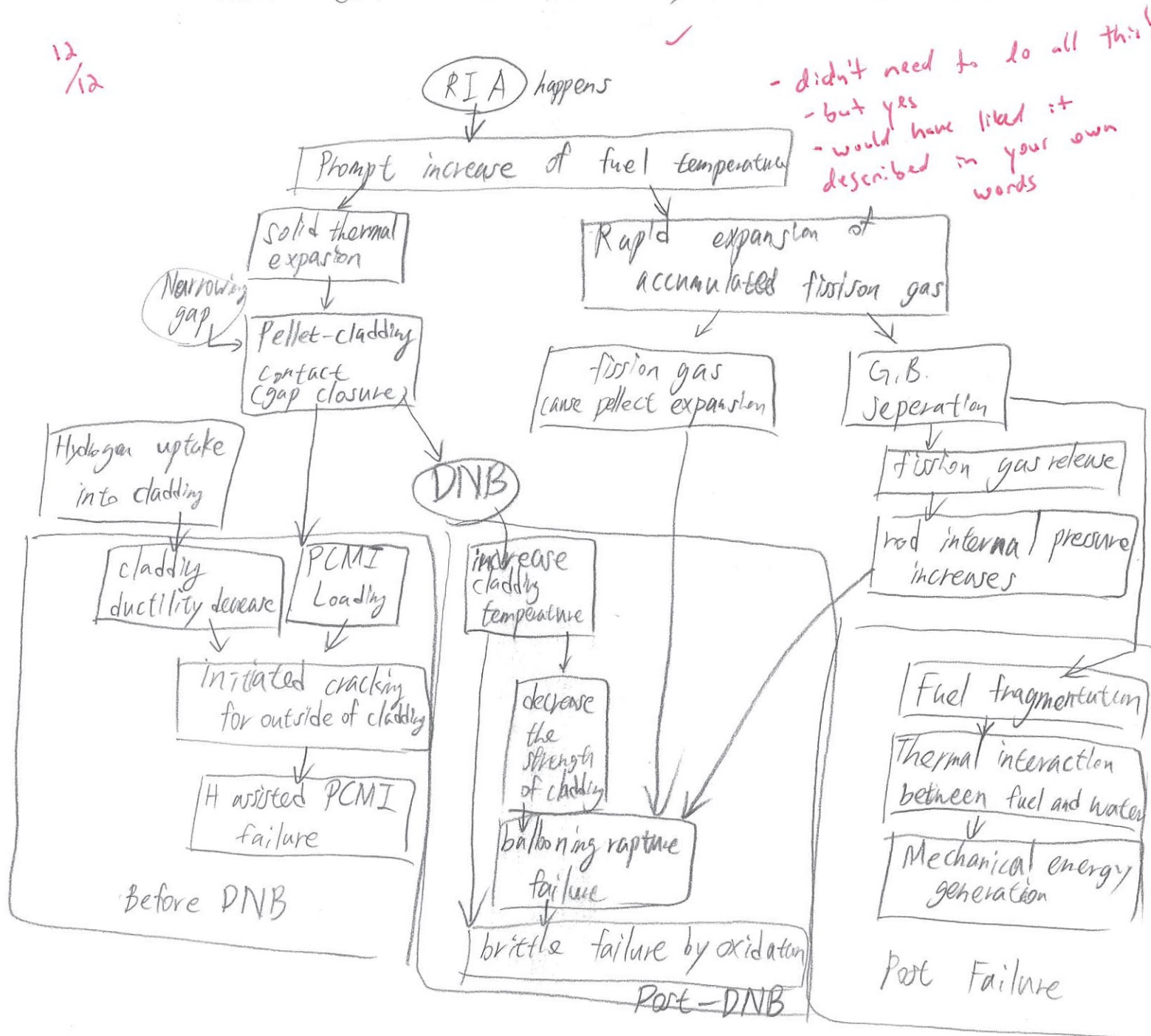
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5. RIA is reactivity insertion accident, which means the rapidly changed ^(initiated) ④

reactivity can cause fuel power \uparrow , temperature $\uparrow \Rightarrow$ generate a lot steam
pressure pulse

② The typical RIA in PWR: Control Rod ejection accident (CREA)
BWR: Control Rod drop accident (CRDA)

③ RIA can be described easily with a flow chart



6. LOCA is the loss of coolant Accident.

⇒ Temp ↑ ∴ radioactive decay increase but cooling decrease ✓

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The main difference between RIA and LOCA is LOCA can evolve to RIA, but RIA does not lose coolant ⇒ not Zr + Steam reaction

- different effects in LOCA.

- slower, more oxidation, plasticity, etc.

7. (eg) ① Improve the reaction kinetics with steam ✓
 ② fission product retention ✓

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ATF option = Ti_3SiC_2 , C_1 for cladding coating ✓

SiC, FeCrAl for Alternative cladding
 dope Cr, SiC, BeO in UO_2 ✓

8. When Zr is exposed to high temperature steam, it will have steam oxidation effect and also interact directly with steam $Zr_{(s)} + 2H_2O_{(g)} \rightarrow ZrO_{2(s)} + 2H_2 + 516 \text{ kJ/mol}$
 \Rightarrow release more heat and could have high risk of hydrogen exploration and hydrogen embrittlement.
- phase changes, breakaway oxidation

9. (eg) change the cladding material to Fe-Cr, Fe-Cr-Al or SiC

10. Limit (eg) 1. Cladding oxidation and hydrogen pickup
Phenomenon - wanted a small description also

4/6 2. Power to melt

11. CRUD is Chalk River Unidentified Deposite, which is an accumulation of the corrosion products, ions, and oxides.

4/6 The impact is mainly at the water chemistry and making higher chance for corrosion of cladding.
- low Km, increases fuel/cladding temp
- radiation source by activating corrosion species

Water chemistry controls : eg ① pH value ✓

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② Impurities (eg. Cl, F) ✓

For ①, we need to maintain the environment to be slightly alkaline by adding (eg) LiOH , H_3BO_3 to make it less corrosive.

②, we need to purify the water frequently to make sure the environment does not contain too much Cl and F \Rightarrow less corrosive.

13. MOX fuel has { shorter fuel rod ✓
smaller fuel diameter ✓
stainless steel cladding ✓
higher heating rate ✓
larger gas plenum ✓
Sodium coolant ✓

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- what are physical phenomena that occur?

- restructuring, high FP inventory, TOG, etc.

