

HOT ROLLED CARBON STEEL STRUCTURAL SHAPES



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UNITED STATES STEEL

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HOT ROLLED CARBON STEEL STRUCTURAL SHAPES



Approved By National Bureau
of Standards R216-46,
February 15, 1946

SUPPLEMENTARY INFORMATION

- Structural Tees Cut from Beams
- Plate Size Limitation Tables
- Floor Plates
- Steel Sheet Piling
- Bearing Piles
- Crane Rails
- Corrugated Sheeting
- Standard Mill Practices

COLUMBIA STEEL COMPANY San Francisco

TENNESSEE COAL, IRON & RAILROAD COMPANY . . Birmingham

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Foreword

IN COMPLIANCE with the recommendation of the U. S. Department of Commerce, National Bureau of Standards, this publication provides data pertaining to Simplified Practice Recommendation R216-46 for Hot Rolled Carbon Steel Structural Shapes and includes nominal dimensions, weights, properties and dimensions for detailing.

Data pertaining to other rolled products in common use by designers and fabricators are included as a matter of ready reference.

This publication supersedes earlier U.S.S publications Simplified Structural Steel Shapes, Structural Sections and Pocket Companion.

This edition is issued jointly by

COLUMBIA STEEL COMPANY

TENNESSEE COAL, IRON AND RAILROAD COMPANY

UNITED STATES STEEL COMPANY

Each company sells all the products listed, regardless of where produced.

The following symbols used with the sections indicate in which district or districts they are produced.

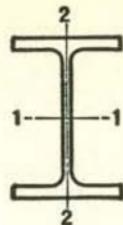
- P. Produced in Pittsburgh district of United States Steel Company.
- C. Produced in Chicago district of United States Steel Company.
- B. Produced in Birmingham district by Tennessee Coal, Iron and Railroad Company.
- S. Produced in Pacific Coast district by Columbia Steel Company.
- G. Produced in Geneva district by Geneva Steel Company.

SECTIONS OBTAINABLE IN USS HIGH-STRENGTH LOW-ALLOY STEELS

All the structural and car building sections shown in this publication except CB-362 and unequal angle A645 (2" x 1 1/4") can be furnished in U.S.S High-Strength, Low-Alloy Steels. Sections in U.S.S High-Strength, Low-Alloy Steels are not produced in all districts which produce the same sections in carbon steel. Consult the District Sales Office regarding the plant from which specific sections can be furnished.

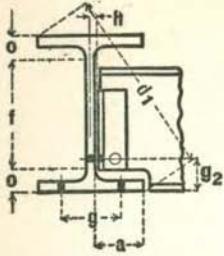


WIDE FLANGE
CB SECTIONS
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange		Web Thick- ness	Axis 1-1			Axis 2-2		
					Lbs.	In. ²	In.	In.	In. ⁴	In. ²	In.	In. ⁴	In. ²
P. C.	36" WF	300	88.17	36.72	16.655	1.680	.945	20290.2	1105.1	15.17	1225.2	147.1	3.73
	CB 362	280	82.32	36.50	16.595	1.570	.885	18819.3	1031.2	15.12	1127.5	135.9	3.70
	36 x 16½	260	76.56	36.24	16.555	1.440	.845	17233.8	951.1	15.00	1020.6	123.3	3.65
	R=1.02	245	72.03	36.06	16.512	1.350	.802	16092.2	892.5	14.95	944.7	114.4	3.62
		230	67.73	35.88	16.475	1.260	.765	14988.4	835.5	14.88	870.9	105.7	3.59
P. C.	36" WF	194	57.11	36.48	12.117	1.260	.770	12103.4	663.6	14.56	355.4	58.7	2.49
	CB 361	182	53.54	36.32	12.072	1.180	.725	11281.5	621.2	14.52	327.7	54.3	2.47
	36 x 12	170	49.98	36.16	12.027	1.100	.680	10470.0	579.1	14.47	300.6	50.0	2.45
	R=.80	160	47.09	36.00	12.000	1.020	.653	9738.8	541.0	14.38	275.4	45.9	2.42
		150	44.16	35.84	11.972	.940	.625	9012.1	502.9	14.29	250.4	41.8	2.38
P. C.	33" WF	240	70.52	33.50	15.865	1.400	.830	13585.1	811.1	13.88	874.3	110.2	3.52
	CB 332	220	64.73	33.25	15.810	1.275	.775	12312.1	740.6	13.79	782.4	99.0	3.48
	33 x 15¾	200	58.79	33.00	15.750	1.150	.715	11048.2	669.6	13.71	691.7	87.8	3.43
	R=.96												
P. C.	33" WF	152	44.71	33.50	11.565	1.055	.635	8147.6	486.4	13.50	256.1	44.3	2.39
	CB 331	141	41.51	33.31	11.535	.960	.605	7442.2	446.8	13.39	229.7	39.8	2.35
	33 x 11½	130	38.26	33.10	11.510	.855	.580	6699.0	404.8	13.23	201.4	35.0	2.29
	R=.75												
P. C.	30" WF	210	61.78	30.38	15.105	1.315	.775	9872.4	649.9	12.64	707.9	93.7	3.38
	CB 302	190	55.90	30.12	15.040	1.185	.710	8825.9	586.1	12.57	624.6	83.1	3.34
	30 x 15	172	50.65	29.88	14.985	1.065	.655	7891.5	528.2	12.48	550.1	73.4	3.30
	R=.91												
P. C.	30" WF	132	38.83	30.30	10.551	1.000	.615	5753.1	379.7	12.17	185.0	35.1	2.18
	CB 301	124	36.45	30.16	10.521	.930	.585	5347.1	354.6	12.11	169.7	32.3	2.16
	30 x 10½	116	34.13	30.00	10.500	.850	.564	4919.1	327.9	12.00	153.2	29.2	2.12
	R=.70	108	31.77	29.82	10.484	.760	.548	4461.0	299.2	11.85	135.1	25.8	2.06
P. C.	27" WF	177	52.10	27.31	14.090	1.190	.725	6728.6	492.8	11.36	518.9	73.7	3.16
	CB 272	160	47.04	27.08	14.023	1.075	.658	6018.6	444.5	11.31	458.0	65.3	3.12
	27 x 14	145	42.68	26.88	13.965	.975	.600	5414.3	402.9	11.26	406.9	58.3	3.09
	R=.86												
P. C.	27" WF	114	33.53	27.28	10.070	.932	.570	4080.5	299.2	11.03	149.6	29.7	2.11
	CB 271	102	30.01	27.07	10.018	.827	.518	3604.1	266.3	10.96	129.5	25.9	2.08
	27 x 10	94	27.65	26.91	9.990	.747	.490	3266.7	242.8	10.87	115.1	23.0	2.04

For key to symbols in first column, refer to page 3.



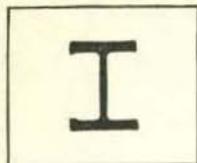
WIDE FLANGE CB SECTIONS

DIMENSIONS OF SECTIONS



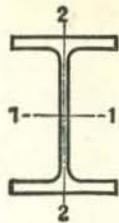
Section Index and Nominal Depth	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g
			Width	Thickness	Thickness	Half Thickness	a	f	o	d_1	Min. g_2	Clear. h	
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
36" WF	300	36 $\frac{3}{4}$	16 $\frac{5}{8}$	11 $\frac{1}{16}$	1 $\frac{5}{16}$	$\frac{1}{2}$	7 $\frac{7}{8}$	31 $\frac{1}{8}$	21 $\frac{1}{16}$	40 $\frac{3}{8}$	4	$\frac{3}{16}$	5 $\frac{1}{2}$
CB 362	280	36 $\frac{1}{2}$	16 $\frac{5}{8}$	1 $\frac{9}{16}$	$\frac{7}{8}$	$\frac{7}{16}$	7 $\frac{7}{8}$	31 $\frac{1}{8}$	21 $\frac{1}{16}$	40 $\frac{3}{8}$	4	$\frac{1}{2}$	5 $\frac{1}{2}$
36 x 16 $\frac{1}{2}$	260	36 $\frac{1}{4}$	16 $\frac{1}{2}$	1 $\frac{7}{16}$	$\frac{7}{8}$	$\frac{7}{16}$	7 $\frac{7}{8}$	31 $\frac{1}{8}$	2 $\frac{9}{16}$	39 $\frac{7}{8}$	3 $\frac{3}{4}$	$\frac{1}{2}$	5 $\frac{1}{2}$
R = 1.02	245	36	16 $\frac{1}{2}$	1 $\frac{3}{8}$	1 $\frac{13}{16}$	$\frac{3}{8}$	7 $\frac{7}{8}$	31 $\frac{1}{8}$	2 $\frac{7}{16}$	39 $\frac{3}{4}$	3 $\frac{3}{4}$	$\frac{7}{16}$	5 $\frac{1}{2}$
	230	35 $\frac{7}{8}$	16 $\frac{1}{2}$	1 $\frac{1}{4}$	$\frac{3}{4}$	$\frac{3}{8}$	7 $\frac{7}{8}$	31 $\frac{1}{8}$	2 $\frac{3}{8}$	39 $\frac{1}{2}$	3 $\frac{1}{2}$	$\frac{7}{16}$	5 $\frac{1}{2}$
36" WF	194	36 $\frac{1}{2}$	12 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{3}{16}$	$\frac{3}{8}$	5 $\frac{5}{8}$	32 $\frac{1}{4}$	2 $\frac{1}{8}$	38 $\frac{1}{2}$	3 $\frac{1}{4}$	$\frac{7}{16}$	5 $\frac{1}{2}$
CB 361	182	36 $\frac{3}{8}$	12 $\frac{1}{8}$	1 $\frac{3}{16}$	$\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{5}{8}$	32 $\frac{1}{4}$	2 $\frac{1}{16}$	38 $\frac{3}{8}$	3 $\frac{1}{4}$	$\frac{7}{16}$	5 $\frac{1}{2}$
36 x 12	170	36 $\frac{1}{8}$	12	1 $\frac{1}{8}$	1 $\frac{11}{16}$	$\frac{3}{8}$	5 $\frac{5}{8}$	32 $\frac{1}{4}$	1 $\frac{15}{16}$	38 $\frac{3}{8}$	3 $\frac{1}{4}$	$\frac{7}{16}$	5 $\frac{1}{2}$
R = .80	160	36	12	1	1 $\frac{11}{16}$	$\frac{5}{16}$	5 $\frac{5}{8}$	32 $\frac{1}{4}$	1 $\frac{7}{8}$	38	3	$\frac{3}{8}$	5 $\frac{1}{2}$
	150	35 $\frac{7}{8}$	12	1 $\frac{5}{16}$	$\frac{5}{8}$	$\frac{5}{16}$	5 $\frac{5}{8}$	32 $\frac{1}{4}$	1 $\frac{13}{16}$	37 $\frac{7}{8}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
33" WF	240	33 $\frac{1}{2}$	15 $\frac{7}{8}$	1 $\frac{3}{8}$	$\frac{7}{8}$	$\frac{7}{16}$	7 $\frac{1}{2}$	28 $\frac{5}{8}$	2 $\frac{7}{16}$	37 $\frac{1}{8}$	3 $\frac{3}{4}$	$\frac{1}{2}$	5 $\frac{1}{2}$
CB 332	220	33 $\frac{3}{4}$	15 $\frac{3}{4}$	1 $\frac{1}{4}$	1 $\frac{3}{16}$	$\frac{3}{8}$	7 $\frac{1}{2}$	28 $\frac{5}{8}$	2 $\frac{5}{16}$	36 $\frac{1}{8}$	3 $\frac{1}{2}$	$\frac{7}{16}$	5 $\frac{1}{2}$
33 x 15 $\frac{3}{4}$	200	33	15 $\frac{3}{4}$	1 $\frac{1}{8}$	$\frac{3}{4}$	$\frac{3}{8}$	7 $\frac{1}{2}$	28 $\frac{5}{8}$	2 $\frac{3}{16}$	36 $\frac{5}{8}$	3 $\frac{1}{2}$	$\frac{7}{16}$	5 $\frac{1}{2}$
R = .96													
33" WF	152	33 $\frac{1}{2}$	11 $\frac{5}{8}$	1 $\frac{1}{16}$	$\frac{5}{8}$	$\frac{5}{16}$	5 $\frac{1}{2}$	29 $\frac{3}{4}$	1 $\frac{7}{8}$	35 $\frac{1}{2}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 331	141	33 $\frac{1}{4}$	11 $\frac{1}{2}$	1 $\frac{15}{16}$	$\frac{5}{8}$	$\frac{5}{16}$	5 $\frac{1}{2}$	29 $\frac{3}{4}$	1 $\frac{3}{4}$	35 $\frac{1}{4}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
33 x 11 $\frac{1}{2}$	130	33 $\frac{3}{8}$	11 $\frac{1}{2}$	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{5}{16}$	5 $\frac{1}{2}$	29 $\frac{3}{4}$	1 $\frac{11}{16}$	35 $\frac{3}{8}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
R = .75													
30" WF	210	30 $\frac{3}{8}$	15 $\frac{1}{8}$	1 $\frac{5}{16}$	1 $\frac{3}{16}$	$\frac{3}{8}$	7 $\frac{1}{8}$	25 $\frac{3}{4}$	2 $\frac{5}{16}$	34	3 $\frac{1}{2}$	$\frac{7}{16}$	5 $\frac{1}{2}$
CB 302	190	30 $\frac{1}{8}$	15	1 $\frac{3}{16}$	$\frac{3}{4}$	$\frac{3}{8}$	7 $\frac{1}{8}$	25 $\frac{3}{4}$	2 $\frac{3}{16}$	33 $\frac{3}{4}$	3 $\frac{1}{2}$	$\frac{7}{16}$	5 $\frac{1}{2}$
30 x 15	172	29 $\frac{7}{8}$	15	1 $\frac{11}{16}$	1 $\frac{11}{16}$	$\frac{5}{16}$	7 $\frac{1}{8}$	25 $\frac{3}{4}$	2 $\frac{1}{16}$	33 $\frac{1}{2}$	3 $\frac{1}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
R = .91													
30" WF	132	30 $\frac{1}{4}$	10 $\frac{1}{2}$	1	$\frac{5}{8}$	$\frac{5}{16}$	5	26 $\frac{7}{8}$	1 $\frac{11}{16}$	32 $\frac{1}{8}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 301	124	30 $\frac{3}{8}$	10 $\frac{1}{2}$	1 $\frac{15}{16}$	$\frac{5}{8}$	$\frac{5}{16}$	5	26 $\frac{7}{8}$	1 $\frac{5}{8}$	31 $\frac{7}{8}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
30 x 10 $\frac{1}{2}$	116	30	10 $\frac{1}{2}$	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{5}{16}$	5	26 $\frac{7}{8}$	1 $\frac{9}{16}$	31 $\frac{3}{4}$	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
R = .70	108	29 $\frac{7}{8}$	10 $\frac{1}{2}$	$\frac{3}{4}$	$\frac{9}{16}$	$\frac{5}{16}$	5	26 $\frac{7}{8}$	1 $\frac{1}{2}$	31 $\frac{3}{8}$	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
27" WF	177	27 $\frac{3}{4}$	14 $\frac{1}{8}$	1 $\frac{3}{16}$	$\frac{3}{4}$	$\frac{3}{8}$	6 $\frac{3}{4}$	23	2 $\frac{1}{8}$	30 $\frac{3}{4}$	3 $\frac{1}{4}$	$\frac{7}{16}$	5 $\frac{1}{2}$
CB 272	160	27 $\frac{7}{8}$	14	1 $\frac{11}{16}$	1 $\frac{11}{16}$	$\frac{5}{16}$	6 $\frac{3}{4}$	23	2 $\frac{1}{16}$	30 $\frac{1}{2}$	3 $\frac{1}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
27 x 14	145	26 $\frac{7}{8}$	14	1	$\frac{5}{8}$	$\frac{5}{16}$	6 $\frac{3}{4}$	23	1 $\frac{15}{16}$	30 $\frac{3}{8}$	3 $\frac{1}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
R = .86													
27" WF	114	27 $\frac{1}{4}$	10 $\frac{1}{8}$	1 $\frac{5}{16}$	$\frac{9}{16}$	$\frac{5}{16}$	4 $\frac{3}{4}$	24	1 $\frac{5}{8}$	29 $\frac{1}{8}$	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 271	102	27 $\frac{3}{8}$	10	1 $\frac{3}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	4 $\frac{3}{4}$	24	1 $\frac{9}{16}$	28 $\frac{7}{8}$	2 $\frac{3}{4}$	$\frac{3}{16}$	5 $\frac{1}{2}$
27 x 10	94	26 $\frac{7}{8}$	10	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{4}$	4 $\frac{3}{4}$	24	1 $\frac{7}{16}$	28 $\frac{3}{4}$	2 $\frac{3}{4}$	$\frac{3}{16}$	5 $\frac{1}{2}$
R = .64													

Gages g_2 are based on 1 $\frac{1}{4}$ " edge distance (7/8" maximum rivet).



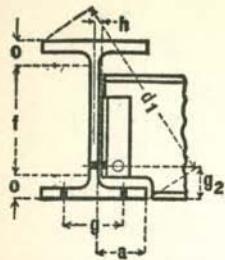
WIDE FLANGE
CB SECTIONS

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange			Web Thick- ness	Axis 1-1			Axis 2-2		
					Width	Thickness	In.		I	S	r	I	S	r
					Lbs.	In. ²	In.		In.	In. ³	In.	In. ⁴	In. ³	In.
P. C.	24" WF	160	47.04	24.72	14.091	.135	.656	5110.3	413.5	10.42	492.6	69.9	3.23	
	CB 243	145	42.62	24.49	14.043	1.020	.608	4561.0	372.5	10.34	434.3	61.8	3.19	
	24 x 14 R=.70	130	38.21	24.25	14.000	.900	.565	4009.5	330.7	10.24	375.2	53.6	3.13	
	24" WF	120	35.29	24.31	12.088	.930	.556	3635.3	299.1	10.15	254.0	42.0	2.68	
P. C.	CB 242	110	32.36	24.16	12.042	.855	.510	3315.0	274.4	10.12	229.1	38.0	2.66	
	24 x 12 R=.70	100	29.43	24.00	12.000	.775	.468	2987.3	248.9	10.08	203.5	33.9	2.63	
	24" WF	94	27.63	24.29	9.061	.872	.516	2683.0	220.9	9.85	102.2	22.6	1.92	
	CB 241	84	24.71	24.09	9.015	.772	.470	2364.3	196.3	9.78	88.3	19.6	1.89	
P. C.	24 x 9 R=.54	76	22.37	23.91	8.985	.682	.440	2096.4	175.4	9.68	76.5	17.0	1.85	
	21" WF	142	41.76	21.46	13.132	1.095	.659	3403.1	317.2	9.03	385.9	58.8	3.04	
	CB 213	127	37.34	21.24	13.061	.985	.588	3017.2	284.1	8.99	338.6	51.8	3.01	
	21 x 13 R=.65	112	32.93	21.00	13.000	.865	.527	2620.6	249.6	8.92	289.7	44.6	2.96	
P. C.	21" WF	96	28.21	21.14	9.038	.935	.575	2088.9	197.6	8.60	109.3	24.2	1.97	
	CB 212	82	24.10	20.86	8.962	.795	.499	1752.4	168.0	8.53	89.6	20.0	1.93	
	21 x 9 R=.65	73	21.46	21.24	8.295	.740	.455	1600.3	150.7	8.64	66.2	16.0	1.76	
	21" WF	68	20.02	21.13	8.270	.685	.430	1478.3	139.9	8.59	60.4	14.6	1.74	
P. C.	CB 211	62	18.23	20.99	8.240	.615	.400	1326.8	126.4	8.53	53.1	12.9	1.71	
	21 x 8 1/4 R=.54	114	33.51	18.48	11.833	.991	.595	2033.8	220.1	7.79	255.6	43.2	2.76	
	CB 183	105	30.86	18.32	11.792	.911	.554	1852.5	202.2	7.75	231.0	39.2	2.73	
	18 x 11 3/4 R=.60	96	28.22	18.16	11.750	.831	.512	1674.7	184.4	7.70	206.8	35.2	2.71	
P. C.	18" WF	85	24.97	18.32	8.838	.911	.526	1429.9	156.1	7.57	99.4	22.5	2.00	
	CB 182	77	22.63	18.16	8.787	.831	.475	1286.8	141.7	7.54	88.6	20.2	1.98	
	18 x 8 3/4 R=.60	70	20.56	18.00	8.750	.751	.438	1153.9	128.2	7.49	78.5	17.9	1.95	
	18" WF	64	18.80	17.87	8.715	.686	.403	1045.8	117.0	7.46	70.3	16.1	1.93	
P. C.	CB 181	60	17.64	18.25	7.558	.695	.416	984.0	107.8	7.47	47.1	12.5	1.63	
	18 x 7 1/2 R=.43	55	16.19	18.12	7.532	.630	.390	889.9	98.2	7.41	42.0	11.1	1.61	
	18" WF	50	14.71	18.00	7.500	.570	.358	800.6	89.0	7.38	37.2	9.9	1.59	

For key to symbols in first column, refer to page 3.



WIDE FLANGE
CB SECTIONS

DIMENSIONS OF SECTIONS



Section Index and Nominal Depth	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g
			Width	Thickness	Thickness	Half Thickness	a	f	o	d ₁	Min. g ₂	Clear. h	
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
24" WF	160	24 $\frac{3}{4}$	14 $\frac{1}{8}$	1 $\frac{1}{8}$	1 $\frac{1}{16}$	$\frac{5}{16}$	6 $\frac{3}{4}$	20 $\frac{3}{4}$	2	28 $\frac{1}{2}$	3 $\frac{1}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 243	145	24 $\frac{1}{2}$	14	1	$\frac{5}{8}$	$\frac{5}{16}$	6 $\frac{3}{4}$	20 $\frac{3}{4}$	1 $\frac{7}{8}$	28 $\frac{1}{4}$	3 $\frac{1}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
24 x 14 R=.70	130	24 $\frac{1}{4}$	14	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{5}{16}$	6 $\frac{3}{4}$	20 $\frac{3}{4}$	1 $\frac{3}{4}$	28	3	$\frac{3}{8}$	5 $\frac{1}{2}$
24" WF	120	24 $\frac{1}{4}$	12 $\frac{1}{8}$	1 $\frac{5}{16}$	$\frac{9}{16}$	$\frac{5}{16}$	5 $\frac{3}{4}$	20 $\frac{7}{8}$	1 $\frac{11}{16}$	27 $\frac{1}{8}$	3	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 242	110	24 $\frac{1}{8}$	12	$\frac{7}{8}$	$\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{3}{4}$	20 $\frac{7}{8}$	1 $\frac{5}{8}$	27	$2\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
24 x 12 R=.70	100	24	12	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{3}{4}$	20 $\frac{7}{8}$	1 $\frac{9}{16}$	26 $\frac{7}{8}$	$2\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
24" WF	94	24 $\frac{1}{4}$	9	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{1}{4}$	4 $\frac{1}{4}$	21 $\frac{3}{8}$	1 $\frac{7}{16}$	25 $\frac{7}{8}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
CB 241	84	24 $\frac{1}{8}$	9	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{4}$	4 $\frac{1}{4}$	21 $\frac{3}{8}$	1 $\frac{8}{16}$	25 $\frac{3}{4}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
24 x 9 R=.54	76	23 $\frac{7}{8}$	9	1 $\frac{11}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	4 $\frac{1}{4}$	21 $\frac{3}{8}$	1 $\frac{1}{4}$	25 $\frac{5}{8}$	2 $\frac{1}{2}$	$\frac{5}{16}$	5 $\frac{1}{2}$
21" WF	142	21 $\frac{1}{2}$	13 $\frac{1}{8}$	1 $\frac{1}{8}$	1 $\frac{11}{16}$	$\frac{3}{8}$	6 $\frac{1}{4}$	17 $\frac{3}{4}$	1 $\frac{7}{8}$	25 $\frac{1}{4}$	3	$\frac{7}{16}$	5 $\frac{1}{2}$
CB 213	127	21 $\frac{1}{4}$	13	1	$\frac{5}{16}$	$\frac{5}{16}$	6 $\frac{1}{4}$	17 $\frac{3}{4}$	1 $\frac{3}{4}$	25	3	$\frac{3}{8}$	5 $\frac{1}{2}$
21 x 13 R=.65	112	21	13	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{1}{4}$	6 $\frac{1}{4}$	17 $\frac{3}{4}$	1 $\frac{5}{8}$	24 $\frac{3}{4}$	3	$\frac{5}{16}$	5 $\frac{1}{2}$
21" WF	96	21 $\frac{1}{8}$	9	1 $\frac{5}{16}$	$\frac{9}{16}$	$\frac{5}{16}$	4 $\frac{1}{4}$	18	1 $\frac{9}{16}$	23	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 212	82	20 $\frac{7}{8}$	9	1 $\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	4 $\frac{1}{4}$	18	1 $\frac{15}{16}$	22 $\frac{3}{4}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
21 x 9 R=.65													
21" WF	73	21 $\frac{1}{4}$	8 $\frac{1}{4}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{4}$	4	18 $\frac{5}{8}$	1 $\frac{5}{16}$	22 $\frac{7}{8}$	2 $\frac{1}{2}$	$\frac{5}{16}$	5 $\frac{1}{2}$
CB 211	68	21 $\frac{1}{8}$	8 $\frac{1}{4}$	1 $\frac{11}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	4	18 $\frac{5}{8}$	1 $\frac{1}{4}$	22 $\frac{3}{4}$	2 $\frac{1}{2}$	$\frac{5}{16}$	5 $\frac{1}{2}$
21 x 8 $\frac{3}{4}$ R=.54	62	21	8 $\frac{1}{4}$	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	4	18 $\frac{5}{8}$	1 $\frac{13}{16}$	22 $\frac{5}{8}$	2 $\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{1}{2}$
18" WF	114	18 $\frac{1}{2}$	11 $\frac{7}{8}$	1	$\frac{5}{8}$	$\frac{5}{16}$	5 $\frac{5}{8}$	15 $\frac{1}{8}$	1 $\frac{11}{16}$	22	3	$\frac{3}{8}$	5 $\frac{1}{2}$
CB 183	105	18 $\frac{3}{8}$	11 $\frac{3}{4}$	1 $\frac{15}{16}$	$\frac{9}{16}$	$\frac{5}{16}$	5 $\frac{5}{8}$	15 $\frac{1}{8}$	1 $\frac{5}{8}$	21 $\frac{7}{8}$	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$
18 x 11 $\frac{3}{4}$ R=.60	96	18 $\frac{1}{8}$	11 $\frac{3}{4}$	1 $\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{5}{8}$	15 $\frac{1}{8}$	1 $\frac{1}{2}$	21 $\frac{3}{4}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
18" WF	85	18 $\frac{3}{8}$	8 $\frac{7}{8}$	1 $\frac{15}{16}$	$\frac{9}{16}$	$\frac{1}{4}$	4 $\frac{1}{8}$	15 $\frac{3}{8}$	1 $\frac{1}{2}$	20 $\frac{3}{8}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
CB 182	77	18 $\frac{1}{8}$	8 $\frac{3}{4}$	1 $\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	4 $\frac{1}{8}$	15 $\frac{3}{8}$	1 $\frac{3}{8}$	20 $\frac{3}{8}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
18 x 8 $\frac{3}{4}$ R=.60	70	18	8 $\frac{3}{4}$	$\frac{3}{4}$	$\frac{7}{16}$	$\frac{1}{4}$	4 $\frac{1}{8}$	15 $\frac{3}{8}$	1 $\frac{5}{16}$	20	$2\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$
	64	17 $\frac{7}{8}$	8 $\frac{3}{4}$	1 $\frac{11}{16}$	$\frac{7}{16}$	$\frac{3}{16}$	4 $\frac{1}{8}$	15 $\frac{3}{8}$	1 $\frac{1}{4}$	20	$2\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{1}{2}$
18" WF	60	18 $\frac{1}{4}$	7 $\frac{1}{2}$	1 $\frac{11}{16}$	$\frac{7}{16}$	$\frac{3}{16}$	3 $\frac{5}{8}$	15 $\frac{7}{8}$	1 $\frac{3}{16}$	19 $\frac{7}{8}$	2 $\frac{1}{2}$	$\frac{1}{4}$	3 $\frac{1}{2}$
CB 181	55	18 $\frac{1}{8}$	7 $\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	3 $\frac{5}{8}$	15 $\frac{7}{8}$	1 $\frac{1}{8}$	19 $\frac{7}{8}$	2 $\frac{1}{2}$	$\frac{1}{4}$	3 $\frac{1}{2}$
18 x 7 $\frac{1}{2}$ R=.43	50	18	7 $\frac{1}{2}$	$\frac{9}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	3 $\frac{5}{8}$	15 $\frac{7}{8}$	1 $\frac{15}{16}$	19 $\frac{1}{2}$	2 $\frac{1}{4}$	$\frac{1}{4}$	3 $\frac{1}{2}$

Gages g₂ are based on 1 $\frac{1}{4}$ " edge distance (7/8" maximum rivet).

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PLATES

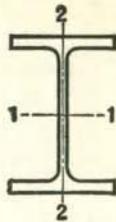
PLATES

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WIDE FLANGE CB SECTIONS

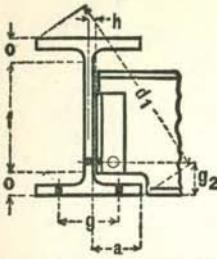
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange		Web Thick- ness	Axis 1-1			Axis 2-2		
					Lbs.	In. ²	In.	In.	In.	In. ⁴	In. ³	In.	
P. C.	16" WF CB 163	96	28.22	16.32	11.533	.875	.535	1355.1	166.1	6.93	207.2	35.9	2.71
	16 x 11½ R=.60	88	25.87	16.16	11.502	.795	.504	1222.6	151.3	6.87	185.2	32.2	2.67
P. C.	16" WF CB 162	78	22.92	16.32	8.586	.875	.529	1042.6	127.8	6.74	87.5	20.4	1.95
	16 x 8½ R=.60	71	20.86	16.16	8.543	.795	.486	936.9	115.9	6.70	77.9	18.2	1.93
P. C.	16" WF CB 161	64	18.80	16.00	8.500	.715	.443	833.8	104.2	6.66	68.4	16.1	1.91
	16 x 7 R=.43	58	17.04	15.86	8.464	.645	.407	746.4	94.1	6.62	60.5	14.3	1.88
P. C.	16" WF CB 161	50	14.70	16.25	7.073	.628	.380	655.4	80.7	6.68	34.8	9.8	1.54
	16 x 7 R=.43	45	13.24	16.12	7.039	.563	.346	583.3	72.4	6.64	30.5	8.7	1.52
P. C.	16" WF CB 161	40	11.77	16.00	7.000	.503	.307	515.5	64.4	6.62	26.5	7.6	1.50
	16 x 7 R=.43	36	10.59	15.85	6.992	.428	.299	446.3	56.3	6.49	22.1	6.3	1.45
P. C.	14" WF CB 146	426	125.25	18.69	16.695	3.033	1.875	6610.3	707.4	7.26	2359.5	282.7	4.34
	14 x 16 R=.60	398	116.98	18.31	16.590	2.843	1.770	6013.7	656.9	7.17	2169.7	261.6	4.31
P. C.	14" WF CB 146	370	108.78	17.94	16.475	2.658	1.655	5454.2	608.1	7.08	1986.0	241.1	4.27
	14 x 16 R=.60	342	100.59	17.56	16.365	2.468	1.545	4911.5	559.4	6.99	1806.9	220.8	4.24
P. C.	14" WF CB 146	314	92.30	17.19	16.235	2.283	1.415	4399.4	511.9	6.90	1631.4	201.0	4.20
	14 x 16 R=.60	287	84.37	16.81	16.130	2.093	1.310	3912.1	465.5	6.81	1466.5	181.8	4.17
P. C.	14" WF CB 146	264	77.63	16.50	16.025	1.938	1.205	3526.0	427.4	6.74	1331.2	166.1	4.14
	14 x 16 R=.60	246	72.33	16.25	15.945	1.813	1.125	3228.9	397.4	6.68	1226.6	153.9	4.12
P. C.	14" WF CB 146	237	69.69	16.12	15.910	1.748	1.090	3080.9	382.2	6.65	1174.8	147.7	4.11
	14 x 16 R=.60	228	67.06	16.00	15.865	1.688	1.045	2942.4	367.8	6.62	1124.8	141.8	4.10
P. C.	14" WF CB 146	219	64.36	15.87	15.825	1.623	1.005	2798.2	352.6	6.59	1073.2	135.6	4.08
	14 x 16 R=.60	211	62.07	15.75	15.800	1.563	.990	2671.4	339.2	6.56	1028.6	130.2	4.07
P. C.	14" WF CB 146	202	59.39	15.63	15.750	1.503	.930	2538.8	324.9	6.54	979.7	124.4	4.06
	14 x 16 R=.60	193	56.73	15.50	15.710	1.438	.890	2402.4	310.0	6.51	930.1	118.4	4.05
P. C.	14" WF CB 146	184	54.07	15.38	15.660	1.378	.840	2274.8	295.8	6.49	882.7	112.7	4.04
	14 x 16 R=.60	176	51.73	15.25	15.640	1.313	.820	2149.6	281.9	6.45	837.9	107.1	4.02
P. C.	14" WF CB 146	167	49.09	15.12	15.600	1.248	.780	2020.8	267.3	6.42	790.2	101.3	4.01
	14 x 16 R=.60	158	46.47	15.00	15.550	1.188	.730	1900.6	253.4	6.40	745.0	95.8	4.00
P. C.	14" WF CB 146	150	44.08	14.88	15.515	1.128	.695	1786.9	240.2	6.37	702.5	90.6	3.99
	14 x 16 R=.60	142	41.85	14.75	15.500	1.063	.680	1672.2	226.7	6.32	660.1	85.2	3.97
P. C.	14" WF CB 146	320	94.12	16.81	16.710	2.093	1.890	4141.7	492.8	6.63	1635.1	195.7	4.17
	14 x 16 R=.60	136	39.98	14.75	14.740	1.063	.660	1593.0	216.0	6.31	567.7	77.0	3.77
P. C.	14" WF CB 145	127	37.33	14.62	14.690	.998	.610	1476.7	202.0	6.29	527.6	71.8	3.76
	14 x 16 R=.60	119	34.99	14.50	14.650	.938	.570	1373.1	189.4	6.26	491.8	67.1	3.75
P. C.	14" WF CB 145	111	32.65	14.37	14.620	.873	.540	1266.5	176.3	6.23	454.9	62.2	3.73
	14 x 16 R=.60	103	30.26	14.25	14.575	.813	.495	1165.8	163.6	6.21	419.7	57.6	3.72
P. C.	14" WF CB 145	95	27.94	14.12	14.545	.748	.465	1063.5	150.6	6.17	383.7	52.8	3.71
	14 x 16 R=.60	87	25.56	14.00	14.500	.688	.420	966.9	138.1	6.15	349.7	48.2	3.70

*Column Core Section.

For key to symbols in first column, refer to page 3.



WIDE FLANGE CB SECTIONS

DIMENSIONS OF SECTIONS



Section Index and Nominal Depth	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g	
			Width	Thickness	Thickness	Half Thickness	a	f	o	d ₁	Min. g ₂	Clear. h		
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	
16" WF														
CB 163	96	16 $\frac{3}{8}$	11 $\frac{1}{2}$	$\frac{7}{8}$	$\frac{3}{16}$	$\frac{5}{16}$	5 $\frac{1}{2}$	13 $\frac{1}{8}$	1 $\frac{5}{8}$	20	2 $\frac{3}{4}$	$\frac{3}{8}$	5 $\frac{1}{2}$	
16 x 11 $\frac{1}{2}$	88	16 $\frac{1}{8}$	11 $\frac{1}{2}$	$\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	5 $\frac{1}{2}$	13 $\frac{1}{8}$	1 $\frac{1}{2}$	19 $\frac{7}{8}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$	
R=.60														
16" WF	78	16 $\frac{3}{8}$	8 $\frac{5}{8}$	$\frac{7}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	4	13 $\frac{3}{8}$	1 $\frac{1}{2}$	18 $\frac{1}{2}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$	
CB 162	71	16 $\frac{1}{8}$	8 $\frac{1}{2}$	$\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	4	13 $\frac{3}{8}$	1 $\frac{3}{8}$	18 $\frac{1}{4}$	2 $\frac{3}{4}$	$\frac{5}{16}$	5 $\frac{1}{2}$	
16 x 8 $\frac{1}{2}$	64	16	8 $\frac{1}{2}$	$\frac{11}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	4	13 $\frac{3}{8}$	1 $\frac{5}{16}$	18 $\frac{1}{8}$	2 $\frac{1}{2}$	$\frac{5}{16}$	5 $\frac{1}{2}$	
R=.60	58	15 $\frac{7}{8}$	8 $\frac{1}{2}$	$\frac{5}{8}$	$\frac{7}{16}$	$\frac{1}{4}$	4	13 $\frac{3}{8}$	1 $\frac{1}{4}$	18	2 $\frac{1}{2}$	$\frac{5}{16}$	5 $\frac{1}{2}$	
16" WF	50	16 $\frac{1}{4}$	7 $\frac{1}{8}$	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	3 $\frac{3}{8}$	14	1 $\frac{1}{8}$	17 $\frac{3}{4}$	2 $\frac{1}{2}$	$\frac{1}{4}$	3 $\frac{1}{2}$	
CB 161	45	16 $\frac{1}{8}$	7	$\frac{9}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	3 $\frac{3}{8}$	14	1 $\frac{1}{16}$	17 $\frac{5}{8}$	2 $\frac{1}{4}$	$\frac{1}{4}$	3 $\frac{1}{2}$	
16 x 7	40	16	7	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	3 $\frac{3}{8}$	14	1	17 $\frac{1}{2}$	2 $\frac{1}{4}$	$\frac{1}{4}$	3 $\frac{1}{2}$	
R=.43	36	15 $\frac{7}{8}$	7	$\frac{7}{16}$	$\frac{5}{16}$	$\frac{3}{16}$	3 $\frac{3}{8}$	14	1 $\frac{5}{16}$	17 $\frac{3}{8}$	2 $\frac{1}{4}$	$\frac{1}{4}$	3 $\frac{1}{2}$	
	426	18 $\frac{3}{4}$	16 $\frac{3}{4}$	3 $\frac{1}{16}$	1 $\frac{7}{8}$	1 $\frac{5}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	3 $\frac{5}{8}$	25 $\frac{1}{8}$	5	1		
	398	18 $\frac{1}{4}$	16 $\frac{5}{8}$	2 $\frac{13}{16}$	1 $\frac{13}{16}$	1 $\frac{7}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	3 $\frac{7}{16}$	24 $\frac{3}{4}$	4 $\frac{3}{4}$	$\frac{15}{16}$		
	370	18	16 $\frac{1}{2}$	2 $\frac{11}{16}$	1 $\frac{11}{16}$	1 $\frac{13}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	3 $\frac{1}{4}$	24 $\frac{3}{8}$	4 $\frac{1}{2}$	$\frac{7}{8}$		
	342	17 $\frac{1}{2}$	16 $\frac{3}{8}$	2 $\frac{7}{16}$	1 $\frac{9}{16}$	1 $\frac{13}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	3 $\frac{1}{16}$	24	4 $\frac{1}{4}$	$\frac{7}{8}$		
	314	17 $\frac{1}{4}$	16 $\frac{1}{4}$	2 $\frac{5}{16}$	1 $\frac{11}{16}$	3 $\frac{1}{4}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{7}{8}$	23 $\frac{3}{4}$	4 $\frac{1}{4}$	$\frac{13}{16}$		
	287	16 $\frac{3}{4}$	16 $\frac{1}{8}$	2 $\frac{3}{16}$	1 $\frac{5}{16}$	1 $\frac{11}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{11}{16}$	23 $\frac{3}{8}$	4	$\frac{3}{4}$		
	264	16 $\frac{1}{2}$	16	$\frac{11}{16}$	1 $\frac{1}{4}$	$\frac{5}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{9}{16}$	23	3 $\frac{3}{4}$	$\frac{11}{16}$		
	246	16 $\frac{1}{4}$	16	1 $\frac{13}{16}$	1 $\frac{1}{8}$	$\frac{3}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{7}{16}$	22 $\frac{7}{8}$	3 $\frac{3}{4}$	$\frac{5}{8}$		
	237	16 $\frac{1}{8}$	15 $\frac{7}{8}$	1 $\frac{3}{4}$	1 $\frac{1}{8}$	$\frac{9}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{5}{8}$	22 $\frac{3}{4}$	3 $\frac{3}{4}$	$\frac{5}{8}$		
	228	16	15 $\frac{5}{8}$	1 $\frac{11}{16}$	1 $\frac{1}{16}$	$\frac{9}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{1}{4}$	22 $\frac{1}{2}$	3 $\frac{1}{2}$	$\frac{9}{16}$		
	219	15 $\frac{7}{8}$	15 $\frac{7}{8}$	1 $\frac{5}{8}$	1	$\frac{1}{2}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{1}{4}$	22 $\frac{3}{8}$	3 $\frac{1}{2}$	$\frac{9}{16}$		
	211	15 $\frac{3}{4}$	15 $\frac{3}{4}$	1 $\frac{9}{16}$	1	$\frac{1}{2}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{9}{16}$	22 $\frac{3}{8}$	3 $\frac{1}{2}$	$\frac{9}{16}$		
	202	15 $\frac{5}{8}$	15 $\frac{3}{4}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{1}{8}$	22 $\frac{1}{4}$	3 $\frac{1}{2}$	$\frac{9}{16}$		
	193	15 $\frac{1}{2}$	15 $\frac{3}{4}$	1 $\frac{7}{16}$	1 $\frac{7}{8}$	1 $\frac{16}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{1}{16}$	22 $\frac{1}{8}$	3 $\frac{1}{4}$	$\frac{7}{2}$		
	184	15 $\frac{3}{8}$	15 $\frac{5}{8}$	1 $\frac{3}{8}$	1 $\frac{7}{8}$	1 $\frac{16}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2	22	3 $\frac{1}{4}$	$\frac{1}{2}$		
	176	15 $\frac{1}{4}$	15 $\frac{5}{8}$	1 $\frac{15}{16}$	1 $\frac{13}{16}$	1 $\frac{16}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	1 $\frac{15}{16}$	21 $\frac{7}{8}$	3 $\frac{1}{4}$	$\frac{1}{2}$		
	167	15 $\frac{1}{8}$	15 $\frac{5}{8}$	1 $\frac{1}{4}$	1 $\frac{13}{16}$	3 $\frac{8}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	1 $\frac{7}{8}$	21 $\frac{1}{4}$	3 $\frac{1}{4}$	$\frac{11}{16}$		
	158	15	15 $\frac{1}{2}$	1 $\frac{13}{16}$	3 $\frac{4}{8}$	3 $\frac{8}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	1 $\frac{13}{16}$	21 $\frac{5}{8}$	3	$\frac{7}{16}$		
	150	14 $\frac{7}{8}$	15 $\frac{1}{2}$	1 $\frac{1}{8}$	1 $\frac{11}{16}$	3 $\frac{8}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	1 $\frac{3}{4}$	21 $\frac{1}{2}$	3	$\frac{7}{16}$		
	142	14 $\frac{3}{4}$	15 $\frac{1}{2}$	1 $\frac{11}{16}$	1 $\frac{1}{16}$	3 $\frac{8}{8}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	1 $\frac{11}{16}$	21 $\frac{1}{2}$	3	$\frac{7}{16}$		
*320	16 $\frac{3}{4}$	16 $\frac{3}{4}$	2 $\frac{1}{16}$	1 $\frac{7}{8}$	1 $\frac{15}{16}$	7 $\frac{3}{8}$	11 $\frac{3}{8}$	2 $\frac{11}{16}$	23 $\frac{3}{4}$	4	1			
	136	14 $\frac{3}{4}$	14 $\frac{3}{4}$	1 $\frac{1}{16}$	1 $\frac{15}{16}$	3 $\frac{8}{8}$	7	11 $\frac{3}{8}$	1 $\frac{11}{16}$	20 $\frac{7}{8}$	3	$\frac{7}{16}$		
	127	14 $\frac{5}{8}$	14 $\frac{3}{4}$	1	$\frac{5}{8}$	1 $\frac{16}{16}$	7	11 $\frac{3}{8}$	1 $\frac{5}{8}$	20 $\frac{3}{4}$	3	$\frac{5}{8}$		
	119	14 $\frac{1}{2}$	14 $\frac{5}{8}$	1 $\frac{15}{16}$	1 $\frac{9}{16}$	1 $\frac{16}{16}$	7	11 $\frac{3}{8}$	1 $\frac{15}{16}$	20 $\frac{6}{8}$	2 $\frac{3}{4}$	$\frac{5}{8}$		
	CB 145	111	14 $\frac{3}{8}$	14 $\frac{5}{8}$	1 $\frac{7}{8}$	1 $\frac{16}{16}$	5 $\frac{16}{16}$	7	11 $\frac{3}{8}$	1 $\frac{1}{2}$	20 $\frac{1}{2}$	2 $\frac{3}{4}$	$\frac{5}{8}$	
	14 x 14 $\frac{1}{2}$	103	14 $\frac{1}{4}$	14 $\frac{5}{8}$	1 $\frac{13}{16}$	1 $\frac{1}{2}$	1 $\frac{1}{4}$	7	11 $\frac{3}{8}$	1 $\frac{17}{16}$	20 $\frac{1}{2}$	2 $\frac{3}{4}$	$\frac{5}{16}$	
R=.60	95	14 $\frac{1}{8}$	14 $\frac{1}{2}$	1 $\frac{3}{4}$	1 $\frac{1}{2}$	1 $\frac{1}{4}$	7	11 $\frac{3}{8}$	1 $\frac{13}{8}$	20 $\frac{1}{4}$	20 $\frac{1}{4}$	2 $\frac{3}{4}$	$\frac{5}{16}$	
	87	14	14 $\frac{1}{2}$	1 $\frac{11}{16}$	1 $\frac{7}{16}$	1 $\frac{4}{4}$	7	11 $\frac{3}{8}$	1 $\frac{15}{16}$	20 $\frac{1}{4}$	21 $\frac{1}{2}$	2 $\frac{3}{4}$	$\frac{5}{16}$	

*Column Core Section.
Gages g₂ are based on 1 $\frac{1}{4}$ " edge distance (7/8" maximum rivet).

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SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

PILING

FLOOR
PLATES

PLATES

MILL
PRACTICES

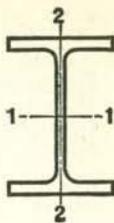
INDEX



WIDE FLANGE

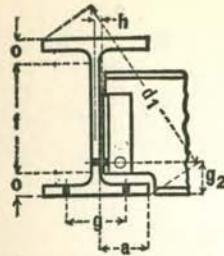
CB SECTIONS

PROPERTIES OF SECTIONS



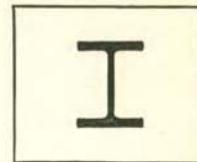
District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange		Web Thick- ness	Axis 1-1			Axis 2-2		
					Width	Thick- ness		In.	In.	In.	In.	In.	
P. C.	14" WF	84	24.71	14.18	12.023	.778	.451	928.4	130.9	6.13	225.5	37.5	3.02
	CB 144	78	22.94	14.06	12.000	.718	.428	851.2	121.1	6.09	206.9	34.5	3.00
	14 x 12												
	R = .60												
P. C.	14" WF	74	21.76	14.19	10.072	.783	.450	796.8	112.3	6.05	133.5	26.5	2.48
	CB 143	68	20.00	14.06	10.040	.718	.418	724.1	103.0	6.02	121.2	24.1	2.46
	14 x 10	61	17.94	13.91	10.000	.643	.378	641.5	92.2	5.98	107.3	21.5	2.45
	R = .60												
P. C.	14" WF	53	15.59	13.94	8.062	.658	.370	542.1	77.8	5.90	57.5	14.3	1.92
	CB 142	48	14.11	13.81	8.031	.593	.339	484.9	70.2	5.86	51.3	12.8	1.91
	14 x 8	43	12.65	13.68	8.000	.528	.308	429.0	62.7	5.82	45.1	11.3	1.89
	R = .60												
P. C.	14" WF	38	11.17	14.12	6.776	.513	.313	385.3	54.6	5.87	24.6	7.3	1.49
	CB 141	34	10.00	14.00	6.750	.453	.287	339.2	48.5	5.83	21.3	6.3	1.46
	14 x 6 3/4	30	8.81	13.86	6.733	.383	.270	289.6	41.8	5.73	17.5	5.2	1.41
	R = .43												
P. C.		190	55.86	14.38	12.670	1.736	1.060	1892.5	263.2	5.82	589.7	93.1	3.25
		161	47.38	13.88	12.515	1.486	.905	1541.8	222.2	5.70	486.2	77.7	3.20
		133	39.11	13.38	12.365	1.236	.755	1221.2	182.5	5.59	389.9	63.1	3.16
		120	35.31	13.12	12.320	1.106	.710	1071.7	163.4	5.51	345.1	56.0	3.13
	12" WF	106	31.19	12.88	12.230	.986	.620	930.7	144.5	5.46	300.9	49.2	3.11
	CB 124	99	29.09	12.75	12.190	.921	.580	858.5	134.7	5.43	278.2	45.7	3.09
	12 x 12	92	27.06	12.62	12.155	.856	.545	788.9	125.0	5.40	256.4	42.2	3.08
	R = .60	85	24.98	12.50	12.105	.796	.495	723.3	115.7	5.38	235.5	38.9	3.07
		79	23.22	12.38	12.080	.736	.470	663.0	107.1	5.34	216.4	35.8	3.05
		72	21.16	12.25	12.040	.671	.430	597.4	97.5	5.31	195.3	32.4	3.04
		65	19.11	12.12	12.000	.606	.390	533.4	88.0	5.28	174.6	29.1	3.02
P. C.	12" WF	58	17.06	12.19	10.014	.641	.359	476.1	78.1	5.28	107.4	21.4	2.51
	CB 123	53	15.59	12.06	10.000	.576	.345	426.2	70.7	5.23	96.1	19.2	2.48
	12 x 10												
	R = .60												
P. C.	12" WF	50	14.71	12.19	8.077	.641	.371	394.5	64.7	5.18	56.4	14.0	1.96
	CB 122	45	13.24	12.06	8.042	.576	.336	350.8	58.2	5.15	50.0	12.4	1.94
	12 x 8	40	11.77	11.94	8.000	.516	.294	310.1	51.9	5.13	44.1	11.0	1.94
	R = .60												
P. C.	12" WF	36	10.59	12.24	6.565	.540	.305	280.8	45.9	5.15	23.7	7.2	1.50
	CB 121	31	9.12	12.09	6.525	.465	.265	238.4	39.4	5.11	19.8	6.1	1.47
	12 x 6 1/2	27	7.97	11.96	6.500	.400	.240	204.1	34.1	5.06	16.6	5.1	1.44
	R = .37												

For key to symbols in first column, refer to page 3.



WIDE FLANGE CB SECTIONS

DIMENSIONS OF SECTIONS



Section Index and Nominal Depth	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g
			Width	Thickness	Thickness	Half Thickness	a	f	o	d ₁	Min. g ₂	Clear. h	
	Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
14" WF													
CB 144	84	14 $\frac{1}{8}$	12	$\frac{3}{4}$	$\frac{7}{16}$	$\frac{1}{4}$	$5\frac{3}{4}$	$11\frac{3}{8}$	$1\frac{3}{8}$	$18\frac{5}{8}$	$2\frac{3}{4}$	$\frac{5}{16}$	$5\frac{1}{2}$
14 x 12 R = .60	78	14	12	$\frac{11}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	$5\frac{3}{4}$	$11\frac{3}{8}$	$1\frac{5}{16}$	$18\frac{1}{2}$	$2\frac{1}{2}$	$\frac{5}{16}$	$5\frac{1}{2}$
14" WF													
CB 143	74	14 $\frac{1}{4}$	$10\frac{1}{8}$	$13\frac{5}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	$4\frac{3}{4}$	$11\frac{3}{8}$	$1\frac{3}{8}$	$17\frac{1}{2}$	$2\frac{3}{4}$	$\frac{5}{16}$	$5\frac{1}{2}$
14 x 10 R = .60	68	14	10	$11\frac{1}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	$4\frac{3}{4}$	$11\frac{3}{8}$	$1\frac{5}{16}$	$17\frac{1}{4}$	$2\frac{1}{2}$	$\frac{5}{16}$	$5\frac{1}{2}$
14 x 8 R = .60	61	$13\frac{7}{8}$	10	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	$4\frac{3}{4}$	$11\frac{3}{8}$	$1\frac{1}{4}$	$17\frac{1}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
14" WF													
CB 142	53	14	8	$11\frac{1}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	$3\frac{7}{8}$	$11\frac{3}{8}$	$1\frac{1}{4}$	$16\frac{1}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
14 x 8 R = .60	48	$13\frac{3}{4}$	8	$9\frac{1}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	$3\frac{7}{8}$	$11\frac{3}{8}$	$1\frac{3}{16}$	16	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
14 x 8 R = .43	43	$13\frac{7}{8}$	8	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	$3\frac{7}{8}$	$11\frac{3}{8}$	$1\frac{1}{8}$	$15\frac{7}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
14" WF													
CB 141	38	14 $\frac{1}{8}$	$6\frac{3}{4}$	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	$3\frac{1}{4}$	$12\frac{1}{8}$	1	$15\frac{3}{4}$	$2\frac{1}{4}$	$\frac{1}{4}$	$3\frac{1}{2}$
14 x 6 $\frac{3}{4}$ R = .43	34	14	$6\frac{3}{4}$	$\frac{7}{16}$	$\frac{5}{16}$	$\frac{3}{16}$	$3\frac{1}{4}$	$12\frac{1}{8}$	$1\frac{5}{16}$	$15\frac{3}{8}$	$2\frac{1}{4}$	$\frac{1}{4}$	$3\frac{1}{2}$
14 x 6 $\frac{3}{4}$ R = .43	30	$13\frac{7}{8}$	$6\frac{3}{4}$	$\frac{3}{8}$	$\frac{5}{16}$	$\frac{1}{8}$	$3\frac{1}{4}$	$12\frac{1}{8}$	$\frac{7}{8}$	$15\frac{1}{2}$	$2\frac{1}{4}$	$\frac{3}{16}$	$3\frac{1}{2}$
12" WF													
CB 140	190	$14\frac{3}{8}$	$12\frac{5}{8}$	$1\frac{3}{4}$	$11\frac{1}{16}$	$\frac{9}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$25\frac{1}{16}$	$19\frac{1}{4}$	$3\frac{3}{4}$	$\frac{5}{8}$	$5\frac{1}{2}$
12 x 10 R = .60	161	$13\frac{3}{8}$	$12\frac{1}{2}$	$1\frac{1}{2}$	$15\frac{1}{16}$	$\frac{7}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$21\frac{1}{16}$	$18\frac{3}{4}$	$3\frac{1}{2}$	$\frac{5}{8}$	$5\frac{1}{2}$
12 x 8 R = .60	133	$13\frac{3}{8}$	$12\frac{3}{8}$	$1\frac{1}{4}$	$\frac{3}{4}$	$\frac{3}{8}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$11\frac{1}{16}$	$18\frac{1}{4}$	$3\frac{3}{4}$	$\frac{7}{16}$	$5\frac{1}{2}$
12" WF													
CB 124	120	$13\frac{1}{8}$	$12\frac{3}{8}$	$1\frac{1}{8}$	$\frac{3}{4}$	$\frac{3}{8}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$11\frac{1}{16}$	18	$\frac{3}{8}$	$\frac{7}{16}$	$5\frac{1}{2}$
12 x 8 R = .60	106	$12\frac{7}{8}$	$12\frac{1}{4}$	1	$\frac{5}{8}$	$\frac{5}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$19\frac{1}{16}$	$17\frac{7}{8}$	3	$\frac{3}{8}$	$5\frac{1}{2}$
12 x 8 R = .60	99	$12\frac{3}{4}$	$12\frac{1}{4}$	$1\frac{5}{16}$	$\frac{5}{8}$	$\frac{5}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$11\frac{1}{2}$	$17\frac{3}{4}$	$2\frac{3}{4}$	$\frac{3}{8}$	$5\frac{1}{2}$
12 x 8 R = .60	92	$12\frac{5}{8}$	$12\frac{1}{8}$	$\frac{7}{8}$	$\frac{9}{16}$	$\frac{5}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$1\frac{1}{16}$	$17\frac{1}{2}$	$2\frac{3}{4}$	$\frac{3}{8}$	$5\frac{1}{2}$
12" WF													
CB 123	85	$12\frac{1}{2}$	$12\frac{1}{8}$	$1\frac{13}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$13\frac{1}{8}$	$17\frac{1}{2}$	$2\frac{3}{4}$	$\frac{5}{16}$	$5\frac{1}{2}$
12 x 8 R = .60	79	$12\frac{3}{8}$	$12\frac{1}{8}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{4}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$15\frac{1}{16}$	$17\frac{3}{8}$	$2\frac{3}{4}$	$\frac{5}{16}$	$5\frac{1}{2}$
12 x 8 R = .60	72	$12\frac{1}{4}$	12	$1\frac{1}{16}$	$\frac{7}{16}$	$\frac{1}{4}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$1\frac{1}{4}$	$17\frac{1}{4}$	$2\frac{1}{2}$	$\frac{5}{16}$	$5\frac{1}{2}$
12" WF													
CB 122	65	$12\frac{1}{8}$	12	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	$5\frac{3}{4}$	$9\frac{3}{4}$	$13\frac{1}{16}$	$17\frac{1}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12 x 8 R = .60	58	$12\frac{1}{4}$	10	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	$4\frac{7}{8}$	$9\frac{3}{4}$	$1\frac{1}{4}$	$15\frac{7}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12 x 8 R = .60	53	12	10	$\frac{9}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	$4\frac{7}{8}$	$9\frac{3}{4}$	$13\frac{1}{16}$	$15\frac{5}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12" WF													
CB 121	50	$12\frac{1}{4}$	$8\frac{1}{8}$	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{3}{16}$	$3\frac{7}{8}$	$9\frac{3}{4}$	$1\frac{1}{4}$	$14\frac{5}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12 x 8 R = .60	45	12	8	$\frac{9}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	$3\frac{7}{8}$	$9\frac{3}{4}$	$1\frac{3}{16}$	$14\frac{1}{2}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12 x 8 R = .60	40	12	8	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	$3\frac{7}{8}$	$9\frac{3}{4}$	$1\frac{7}{8}$	$14\frac{3}{8}$	$2\frac{1}{2}$	$\frac{1}{4}$	$5\frac{1}{2}$
12" WF													
CB 121	36	$12\frac{1}{4}$	$6\frac{5}{8}$	$\frac{9}{16}$	$\frac{5}{16}$	$\frac{3}{16}$	$3\frac{1}{8}$	$10\frac{5}{8}$	$1\frac{5}{16}$	14	$2\frac{1}{4}$	$\frac{1}{4}$	$3\frac{1}{2}$
12 x 6 $\frac{1}{2}$ R = .37	31	$12\frac{1}{8}$	$6\frac{1}{2}$	$\frac{7}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	$3\frac{1}{8}$	$10\frac{5}{8}$	$1\frac{3}{16}$	$13\frac{5}{8}$	$2\frac{1}{4}$	$\frac{3}{16}$	$3\frac{1}{2}$
12 x 6 $\frac{1}{2}$ R = .37	27	12	$6\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	$3\frac{1}{8}$	$10\frac{5}{8}$	$1\frac{3}{16}$	$13\frac{5}{8}$	$2\frac{1}{4}$	$\frac{3}{16}$	$3\frac{1}{2}$

Gages g₂ are based on 1 $\frac{1}{4}$ " edge distance (1 $\frac{1}{8}$ " maximum rivet).

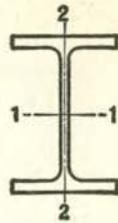
- I CBL-SJ
- I STD.&H.
- C CAR & SHIP
- L EQUAL
- L UNEQUAL
- L BULB
- T SPLIT
- CAR SECTIONS
- CRANE RAILS
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WIDE FLANGE

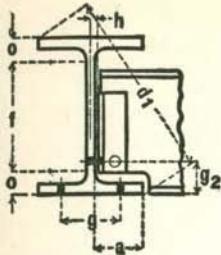
CB SECTIONS

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange		Web Thick- ness	Axis 1-1			Axis 2-2		
					Width	Thickness		I	S	r	I	S	r
					Lbs.	In. ²	In.	In.	In.	In.	In. ⁴	In. ²	In.
P.C.	10" WF CB 103 10 x 10 R = .50	112	32.92	11.38	10.415	1.248	.755	718.7	126.3	4.67	235.4	45.2	2.67
		100	29.43	11.12	10.345	1.118	.685	625.0	112.4	4.61	206.6	39.9	2.65
		89	26.19	10.88	10.275	.998	.615	542.4	99.7	4.55	180.6	35.2	2.63
		77	22.67	10.62	10.195	.868	.535	457.2	86.1	4.49	153.4	30.1	2.60
		72	21.18	10.50	10.170	.808	.510	420.7	80.1	4.46	141.8	27.9	2.59
		66	19.41	10.38	10.117	.748	.457	382.5	73.7	4.44	129.2	25.5	2.58
		60	17.66	10.25	10.075	.683	.415	343.7	67.1	4.41	116.5	23.1	2.57
		54	15.88	10.12	10.028	.618	.368	305.7	60.4	4.39	103.9	20.7	2.56
		49	14.40	10.00	10.000	.558	.340	272.9	54.6	4.35	93.0	18.6	2.54
P.C.	10" WF CB 102 10 x 8 R = .50	45	13.24	10.12	8.022	.618	.350	248.6	49.1	4.33	53.2	13.3	2.00
		39	11.48	9.94	7.990	.528	.318	209.7	42.2	4.27	44.9	11.2	1.98
		33	9.71	9.75	7.964	.433	.292	170.9	35.0	4.20	36.5	9.2	1.94
		29	8.53	10.22	5.799	.500	.289	157.3	30.8	4.29	15.2	5.2	1.34
P.C.	CB 101 10 x 5 3/4 R = .32	25	7.35	10.08	5.762	.430	.252	133.2	26.4	4.26	12.7	4.4	1.31
		21	6.19	9.90	5.750	.340	.240	106.3	21.5	4.14	9.7	3.4	1.25
		67	19.70	9.00	8.287	.933	.575	271.8	60.4	3.71	88.6	21.4	2.12
		58	17.06	8.75	8.222	.808	.510	227.3	52.0	3.65	74.9	18.2	2.10
P.C.	CB 83 8 x 8 R = .40	48	14.11	8.50	8.117	.683	.405	183.7	43.2	3.61	60.9	15.0	2.08
		40	11.76	8.25	8.077	.558	.365	146.3	35.5	3.53	49.0	12.1	2.04
		35	10.30	8.12	8.027	.493	.315	126.5	31.1	3.50	42.5	10.6	2.03
		31	9.12	8.00	8.000	.433	.288	109.7	27.4	3.47	37.0	9.2	2.01
P.C.	8" WF CB 82 8 x 6 1/2 R = .40	28	8.23	8.06	6.540	.463	.285	97.8	24.3	3.45	21.6	6.6	1.62
		24	7.06	7.93	6.500	.398	.245	82.5	20.8	3.42	18.2	5.6	1.61
		20	5.88	8.14	5.268	.378	.248	69.2	17.0	3.43	8.50	3.2	1.20
		17	5.00	8.00	5.250	.308	.230	56.4	14.1	3.36	6.72	2.6	1.16

For key to symbols in first column, refer to page 3.



WIDE FLANGE

CB SECTIONS

DIMENSIONS OF SECTIONS



Section Index and Nominal Depth	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g
			Lbs.	In.	In.	In.	Thickness	Half Thickness	a	f	o	d ₁	Min. g ₂
10" WF CB 103 10 x 10 R = .50	112	11 3/8	10 3/8	1 1/4	3/4	3/8	4 7/8	7 7/8	1 3/4	15 1/2	3	7/16	5 1/2
	100	11 1/8	10 3/8	1 1/8	11 1/16	3/8	4 7/8	7 7/8	1 5/8	15 1/4	3	7/16	5 1/2
	89	10 7/8	10 1/4	1	5/8	5/16	4 7/8	7 7/8	1 1/2	15	2 3/4	3/8	5 1/2
	77	10 5/8	10 1/4	7/8	9/16	5/16	4 7/8	7 7/8	1 3/8	14 3/4	2 3/4	3/8	5 1/2
	72	10 1/2	10 1/8	13 1/16	1/2	1/4	4 7/8	7 7/8	1 5/16	14 5/8	2 3/4	5/16	5 1/2
	66	10 3/8	10 1/8	3/4	1/16	1/4	4 7/8	7 7/8	1 3/4	14 1/2	2 1/2	5/16	5 1/2
	60	10 1/4	10 1/8	11 1/16	7/16	1/4	4 7/8	7 7/8	1 3/16	14 3/8	2 1/2	5/16	5 1/2
	54	10 1/8	10	5/8	3/8	3/16	4 7/8	7 7/8	1 1/8	14 1/4	2 1/2	1/4	5 1/2
	49	10	10	9/16	3/8	3/16	4 7/8	7 7/8	1 1/16	14 1/8	2 1/2	1/4	5 1/2
10" WF CB 102 10 x 8 R = .50	45	10 1/8	8	5/8	3/8	3/16	3 7/8	7 7/8	1 1/8	13	2 1/2	1/4	5 1/2
CB 102	39	10	8	1/2	5/16	3/16	3 7/8	7 7/8	1 1/16	12 7/8	2 1/2	1/4	5 1/2
10 x 8	33	9 3/4	8	7/16	5/16	3/16	3 7/8	7 7/8	15 1/16	12 5/8	2 1/4	1/4	5 1/2
10" WF CB 101 10 x 5 3/4 R = .32	29	10 1/4	5 3/4	1/2	5/16	3/16	2 3/4	8 1/2	7/8	11 3/4	2 1/4	1/4	2 3/4
CB 101	25	10 1/8	5 3/4	7/16	1/4	1/8	2 3/4	8 1/2	13 1/16	11 5/8	2 1/4	3/16	2 3/4
10 x 5 3/4 R = .32	21	9 7/8	5 3/4	5/16	1/4	1/8	2 3/4	8 1/2	11 1/16	11 1/2	2	3/16	2 3/4
8" WF CB 83 8 x 8 R = .40	67	9	8 1/4	15 1/16	9/16	5/16	3 7/8	6 3/8	1 5/16	12 1/4	2 3/4	3/8	5 1/2
	58	8 3/4	8 1/4	13 1/16	1/2	1/4	3 7/8	6 3/8	13 1/16	12	2 1/2	5/16	5 1/2
	48	8 1/2	8 1/8	11 1/16	7/16	3/16	3 7/8	6 3/8	11 1/16	11 7/8	2 1/2	1/4	5 1/2
	40	8 1/4	8 1/8	9/16	3/8	3/16	3 7/8	6 3/8	15 1/16	11 5/8	2 1/4	1/4	5 1/2
	35	8 1/8	8	1/2	5/16	3/16	3 7/8	6 3/8	7/8	11 1/2	2 1/4	1/4	5 1/2
	31	8	8	7/16	5/16	3/16	3 7/8	6 3/8	13 1/16	11 3/8	2 1/4	1/4	5 1/2
8" WF CB 82 8 x 6 1/2 R = .40	28	8	6 1/2	7/16	5/16	1/8	3 1/8	6 3/8	13 1/16	10 1/2	2 1/4	3/16	3 1/2
CB 82	24	7 7/8	6 1/2	3/8	1/4	1/8	3 1/8	6 3/8	13 1/16	10 1/4	2 1/4	3/16	3 1/2
8 x 5 3/4 R = .32	17	8	5 3/4	5/16	1/4	1/8	2 1/2	6 3/4	11 1/16	9 3/4	2 1/4	3/16	2 3/4
8" WF CB 81	20	8 1/8	5 1/4	3/8	1/4	1/8	2 1/2	6 3/4	5/8	9 5/8	2 1/4	3/16	2 3/4
8 x 5 3/4 R = .32	17	8	5 1/4	5/16	1/4	1/8	2 1/2	6 3/4	11 1/16	9 3/4	2 1/4	3/16	2 3/4

Gages g₂ are based on 1 1/4" edge distance (7/8" maximum rivet).

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RAILS

CORRUG.
SHEETS

PILING
FLOOR
PLATES

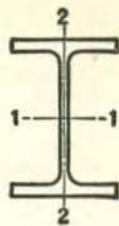
PLATES
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PRACTICES

INDEX

WIDE FLANGE

LIGHT BEAMS, STANCHIONS
AND JOISTS

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	Flange		Web Thick- ness	Axis 1-1			Axis 2-2		
					Width	Thickness		I	S	r	I	S	r
					Lbs.	In. ³	In.	In.	In.	In.	In. ⁴	In. ³	In.

LIGHT BEAMS

P.C.	{	CBL 12	22.0	6.47	12.31	4.030	.424	.260	155.7	25.3	4.91	4.55	2.26	0.84
		12 x 4	19.0	5.62	12.16	4.010	.349	.240	130.1	21.4	4.81	3.67	1.83	0.81
		R = .30	16.5	4.86	12.00	4.000	.269	.230	105.3	17.5	4.65	2.79	1.39	0.76
P.C.	{	CBL 10	19.0	5.61	10.25	4.020	.394	.250	96.2	18.8	4.14	4.19	2.08	0.86
		10 x 4	17.0	4.98	10.12	4.010	.329	.240	81.8	16.2	4.05	3.45	1.72	0.83
		R = .30	15.0	4.40	10.00	4.000	.269	.230	68.8	13.8	3.95	2.79	1.39	0.80
P.C.	{	CBL 8	15.0	4.43	8.12	4.015	.314	.245	48.0	11.8	3.29	3.30	1.65	0.86
		8 x 4	13.0	3.83	8.00	4.000	.254	.230	39.5	9.88	3.21	2.62	1.31	0.83
P.C.	{	CBL 6	16.0	4.72	6.25	4.030	.404	.260	31.7	10.1	2.59	4.32	2.14	0.96
		6 x 4	12.0	3.53	6.00	4.000	.279	.230	21.7	7.24	2.48	2.89	1.44	0.90
		R = .25												

STANCHIONS

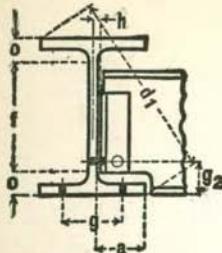
P.C.	{	CBS 6	25.0	7.35	6.37	6.080	.456	.320	53.5	16.8	2.69	17.1	5.6	1.52
		6 x 6	20.0	5.88	6.20	6.018	.367	.258	41.7	13.4	2.66	13.3	4.4	1.50
		R = .25	15.5	4.59	6.00	6.000	.269	.240	30.3	10.1	2.56	9.69	3.2	1.45
P.	{	CB 51	18.5	5.45	5.12	5.025	.420	.265	25.4	9.94	2.16	8.89	3.54	1.28
		5 x 5	16.0	4.70	5.00	5.000	.360	.240	21.3	8.53	2.13	7.51	3.00	1.26
		R = .3												

JOISTS

P.C.	{	CBJ 12	14.0	4.14	11.91	3.970	.224	.200	88.2	14.8	4.61	2.25	1.13	0.74
		12 x 4												
		R = .30												
P.C.	{	CBJ 10	11.5	3.39	9.87	3.950	.204	.180	51.9	10.5	3.92	2.01	1.02	0.77
		10 x 4												
		R = .30												
P.C.	{	CBJ 8	10.0	2.95	7.90	3.940	.204	.170	30.8	7.79	3.23	1.99	1.01	0.82
		8 x 4												
		R = .30												
P.C.	{	CBJ 6	8.5	2.50	5.83	3.940	.194	.170	14.8	5.07	2.43	1.89	0.96	0.87
		6 x 4												
		R = .25												

For key to symbols in first column, refer to page 3.

WIDE FLANGE

LIGHT BEAMS, STANCHIONS
AND JOISTS

DIMENSIONS OF SECTIONS



Section Index and Nominal Size	Weight per Foot	Depth of Section	Flange		Web		Distance						Usual Gage g
			Width	Thickness	Thickness	Half Thickness	a	f	o	d ₁	Min. g ₂	Clear. h	
			Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	

LIGHT BEAMS

CBL 12	22.0	12 $\frac{1}{4}$	4	$\frac{7}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$10\frac{3}{4}$	$\frac{3}{4}$	13	2	$\frac{3}{16}$	$2\frac{1}{4}$
12 x 4	19.0	12 $\frac{1}{8}$	4	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$10\frac{3}{4}$	$1\frac{1}{16}$	12 $\frac{3}{4}$	2	$\frac{3}{16}$	$2\frac{1}{4}$
R = .30	16.5	12	4	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$10\frac{3}{4}$	$\frac{5}{8}$	12 $\frac{5}{8}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$
CBL 10	19.0	10 $\frac{1}{4}$	4	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$8\frac{7}{8}$	$1\frac{1}{16}$	11	2	$\frac{3}{16}$	$2\frac{1}{4}$
10 x 4	17.0	10 $\frac{1}{8}$	4	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$8\frac{7}{8}$	$\frac{5}{8}$	10 $\frac{7}{8}$	2	$\frac{3}{16}$	$2\frac{1}{4}$
R = .30	15.0	10	4	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$8\frac{7}{8}$	$\frac{9}{16}$	10 $\frac{3}{4}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$
*CBL 8	15.0	8 $\frac{1}{8}$	4	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$6\frac{7}{8}$	$\frac{5}{8}$	9	2	$\frac{3}{16}$	$2\frac{1}{4}$
8 x 4	13.0	8	4	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$6\frac{7}{8}$	$\frac{9}{16}$	9	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$
R = .30													
*CBL 6	16.0	6 $\frac{1}{4}$	4	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$4\frac{7}{8}$	$1\frac{1}{16}$	7 $\frac{3}{8}$	2	$\frac{3}{16}$	$2\frac{1}{4}$
6 x 4	12.0	6	4	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$	$4\frac{7}{8}$	$\frac{9}{16}$	7 $\frac{1}{4}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$
R = .25													

*These sections as produced in the Pittsburgh District have a flange slope of 3° and the flange thickness shown is the average thickness.

STANCHIONS

CBS 6	25.0	6 $\frac{3}{8}$	6	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	$2\frac{1}{8}$	$4\frac{7}{8}$	$\frac{3}{4}$	$8\frac{7}{8}$	$2\frac{1}{4}$	$\frac{1}{4}$	$3\frac{1}{2}$
6 x 6	20.0	6 $\frac{1}{4}$	6	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{16}$	$2\frac{1}{8}$	$4\frac{7}{8}$	$1\frac{1}{16}$	$8\frac{5}{8}$	2	$\frac{3}{16}$	$3\frac{1}{2}$
R = .25	15.5	6	6	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{8}$	$2\frac{1}{8}$	$4\frac{7}{8}$	$\frac{9}{16}$	$8\frac{1}{2}$	2	$\frac{3}{16}$	$3\frac{1}{2}$
*CB 51	18.5	5 $\frac{1}{8}$	5	$\frac{7}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	$2\frac{3}{8}$	$3\frac{11}{16}$	$1\frac{1}{16}$	$7\frac{1}{8}$	$2\frac{3}{4}$	$\frac{3}{16}$	3
5 x 5	16.0	5	5	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	$2\frac{3}{8}$	$3\frac{11}{16}$	$\frac{5}{8}$	7	$2\frac{3}{4}$	$\frac{3}{16}$	3
R = .3													

*This section has a flange slope of 3° and the flange thickness shown is the average thickness.

JOISTS

CBJ 12														
12 x 4	14.0	11 $\frac{7}{8}$	4	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{8}$	$1\frac{1}{8}$	$10\frac{3}{4}$	$\frac{9}{16}$	12 $\frac{1}{2}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$	
R = .30														
CBJ 10	11.5	9 $\frac{7}{8}$	4	$\frac{3}{16}$	$\frac{3}{16}$	$\frac{1}{8}$	$1\frac{1}{8}$	$8\frac{7}{8}$	$\frac{1}{2}$	$10\frac{5}{8}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$	
10 x 4														
R = .30														
CBJ 8	10.0	7 $\frac{7}{8}$	4	$\frac{3}{16}$	$\frac{3}{16}$	$\frac{1}{8}$	$1\frac{1}{8}$	$6\frac{7}{8}$	$\frac{1}{2}$	$8\frac{7}{8}$	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$	
8 x 4														
R = .30														
CBJ 6	8.5	5 $\frac{7}{8}$	4	$\frac{3}{16}$	$\frac{3}{16}$	$\frac{1}{8}$	$1\frac{1}{8}$	5	$\frac{7}{16}$	7	$1\frac{3}{4}$	$\frac{3}{16}$	$2\frac{1}{4}$	
6 x 4														
R = .25														

Gages g₂ are based on 1 $\frac{1}{4}$ " edge distance (1 $\frac{1}{2}$ " maximum rivet).

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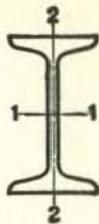
PLATES

MILL
PRACTICES

INDEX

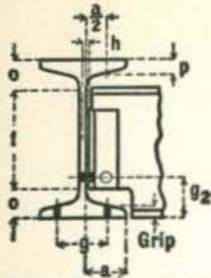
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BEAMS
AMERICAN STANDARD
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Beam	Width of Flange	Aver. Flange Thick- ness	Web Thickness	Axis 1-1			Axis 2-2		
								In.	In.	In.	In.	In.	
P. C.	24" 1							I	S	x	I	S	x
	B 18	120.0	35.13		8.048	1.102	.798	3010.8	250.9	9.26	84.9	21.1	1.56
	24 x 7 $\frac{3}{8}$ R=.60	105.9	30.98	24	7.875	1.102	.625	2811.5	234.3	9.53	78.9	20.0	1.60
P. C.	24" 1	100.0	29.25		7.247	.871	.747	2371.8	197.6	9.05	58.4	13.4	1.29
	B 1	90.0	26.30	24	7.124	.871	.624	2230.1	185.8	9.21	45.5	12.8	1.32
	24 x 7 R=.60	79.9	23.33		7.000	.871	.500	2087.2	173.9	9.46	42.9	12.2	1.36
P. C.	20" 1												
	B 2	95.0	27.74	20	7.200	.916	.800	1599.7	160.0	7.59	50.5	14.0	1.35
	20 x 7 R=.70	85.0	24.80		7.053	.916	.653	1501.7	150.2	7.78	47.0	13.3	1.38
P. C.	20" 1												
	B 3	75.0	21.90	20	6.391	.789	.641	1263.5	126.3	7.60	30.1	9.4	1.17
	20 x 6 $\frac{1}{4}$ R=.60	65.4	19.08		6.250	.789	.500	1169.5	116.9	7.83	27.9	8.9	1.21
P.C.B.	18" 1												
	B 4	70.0	20.46	18	6.251	.691	.711	917.5	101.9	6.70	24.5	7.8	1.09
	18 x 6 R=.56	54.7	15.94		6.000	.691	.460	795.5	88.4	7.07	21.2	7.1	1.15
P.C.B.G.	15" 1												
	B 7	50.0	14.59	15	5.640	.622	.550	481.1	64.2	5.74	16.0	5.7	1.05
	15 x 5 $\frac{1}{2}$ R=.51	42.9	12.49		5.500	.622	.410	441.8	58.9	5.95	14.6	5.3	1.08
P. C.	12" 1												
	B 8	50.0	14.57	12	5.477	.659	.687	301.6	50.3	4.55	16.0	5.8	1.05
	12 x 5 $\frac{1}{4}$ R=.56	40.8	11.84		5.250	.659	.460	268.9	44.8	4.77	13.8	5.3	1.08
P.C.B.G.	12" 1												
	B 9	35.0	10.20	12	5.078	.544	.428	227.0	37.8	4.72	10.0	3.9	0.99
	12 x 5 R=.45	31.8	9.26		5.000	.544	.350	215.8	36.0	4.83	9.5	3.8	1.01
P.C.B.G.	10" 1												
	B 10	35.0	10.22	10	4.944	.491	.594	145.8	29.2	3.78	8.5	3.4	0.91
	10 x 4 $\frac{5}{8}$ R=.41	25.4	7.38		4.660	.491	.310	122.1	24.4	4.07	6.9	3.0	0.97
P.C.B.G.	8" 1												
	B 12	23.0	6.71	8	4.171	.425	.441	64.2	16.0	3.09	4.4	2.1	0.81
	8 x 4 R=.37	18.4	5.34		4.000	.425	.270	56.9	14.2	3.26	3.8	1.9	0.84
P.C.B.S.	7" 1												
	B 13	20.0	5.83	7	3.860	.392	.450	41.9	12.0	2.68	3.1	1.6	0.74
	7 x 3 $\frac{5}{8}$ R=.35	15.3	4.43		3.660	.392	.250	36.2	10.4	2.86	2.7	1.5	0.78

For key to symbols in first column, refer to page 3.



BEAMS
AMERICAN STANDARD
DIMENSIONS OF SECTIONS



Section Index and Depth	Weight per Foot	Flange		Web		Distance								Max. Flange Rivet
		Lbs.	in.	Width	Thickness, p	Thickness	Half Thickness	a	f	o	Min. g _z	Clear. h	Gage g	Grip
						in.	in.	in.	in.	in.	in.	in.	in.	in.
24" I B 18 R=.60	120.0 105.9	8 7 $\frac{3}{8}$	11 $\frac{1}{8}$ 11 $\frac{1}{8}$	13 $\frac{1}{16}$ 5 $\frac{5}{8}$	7 $\frac{1}{16}$ 5 $\frac{5}{16}$	3 $\frac{5}{8}$ 3 $\frac{5}{8}$	20 $\frac{1}{8}$ 20 $\frac{1}{8}$	11 $\frac{15}{16}$ 11 $\frac{15}{16}$	3 $\frac{1}{4}$ 3 $\frac{1}{4}$	1 $\frac{1}{2}$ $\frac{3}{8}$	4 4	11 $\frac{1}{8}$ 11 $\frac{1}{8}$	1 1	
24" I B 1 R=.60	100.0 90.0 79.9	7 $\frac{1}{4}$ 7 $\frac{1}{8}$ 7	7 $\frac{1}{8}$ 5 $\frac{5}{8}$ 5 $\frac{5}{8}$	3 $\frac{1}{4}$ 3 $\frac{1}{4}$ 3 $\frac{1}{4}$	3 $\frac{1}{8}$ 3 $\frac{1}{8}$ 3 $\frac{1}{4}$	20 $\frac{3}{4}$ 20 $\frac{3}{4}$ 20 $\frac{3}{4}$	1 $\frac{5}{8}$ 1 $\frac{5}{8}$ 1 $\frac{5}{8}$	3 3 3	7 $\frac{1}{16}$ 3 $\frac{3}{8}$ 5 $\frac{5}{16}$	4 4 4	7 $\frac{1}{8}$ 7 $\frac{1}{8}$ 7 $\frac{1}{8}$	1 1 1		
20" I B 2 R=.70	95.0 85.0	7 $\frac{1}{4}$ 7	15 $\frac{1}{16}$ 15 $\frac{1}{16}$	13 $\frac{1}{16}$ 11 $\frac{1}{16}$	7 $\frac{1}{16}$ 5 $\frac{5}{16}$	3 $\frac{1}{4}$ 3 $\frac{1}{4}$	16 $\frac{1}{2}$ 16 $\frac{1}{2}$	1 $\frac{3}{4}$ 1 $\frac{3}{4}$	3 $\frac{1}{4}$ 3 $\frac{1}{4}$	1 $\frac{1}{2}$ 3 $\frac{3}{8}$	4 4	15 $\frac{1}{16}$ 7 $\frac{7}{8}$	1 1	
20" I B 3 R=.60	75.0 65.4	6 $\frac{3}{8}$ 6 $\frac{1}{4}$	13 $\frac{1}{16}$ 13 $\frac{1}{16}$	5 $\frac{5}{8}$ 3 $\frac{1}{2}$	5 $\frac{1}{16}$ 3 $\frac{1}{4}$	2 $\frac{7}{8}$ 2 $\frac{7}{8}$	16 $\frac{7}{8}$ 16 $\frac{7}{8}$	1 $\frac{9}{16}$ 1 $\frac{9}{16}$	3 3	3 $\frac{1}{8}$ 5 $\frac{5}{16}$	3 $\frac{1}{2}$ 3 $\frac{1}{2}$	15 $\frac{1}{16}$ 3 $\frac{3}{4}$	7 $\frac{1}{8}$ 7 $\frac{1}{8}$	
18" I B 4 R=.56	70.0 54.7	6 $\frac{1}{4}$ 6	11 $\frac{1}{16}$ 11 $\frac{1}{16}$	3 $\frac{1}{4}$ 3 $\frac{1}{2}$	3 $\frac{1}{8}$ 1 $\frac{1}{4}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	15 $\frac{1}{4}$ 15 $\frac{1}{4}$	1 $\frac{3}{8}$ 1 $\frac{3}{8}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	7 $\frac{1}{16}$ 5 $\frac{5}{16}$	3 $\frac{1}{2}$ 3 $\frac{1}{2}$	11 $\frac{1}{16}$ 11 $\frac{1}{16}$	7 $\frac{1}{8}$ 7 $\frac{1}{8}$	
15" I B 7 R=.51	50.0 42.9	5 $\frac{5}{8}$ 5 $\frac{1}{2}$	5 $\frac{5}{8}$ 5 $\frac{5}{8}$	3 $\frac{1}{16}$ 3 $\frac{1}{16}$	5 $\frac{1}{16}$ 3 $\frac{1}{4}$	2 $\frac{3}{2}$ 2 $\frac{3}{2}$	12 $\frac{3}{2}$ 12 $\frac{3}{2}$	1 $\frac{1}{4}$ 1 $\frac{1}{4}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	3 $\frac{1}{8}$ 5 $\frac{5}{16}$	3 $\frac{1}{2}$ 3 $\frac{1}{2}$	% $\frac{1}{16}$ % $\frac{1}{16}$	% $\frac{1}{4}$ % $\frac{1}{4}$	
12" I B 8 R=.56	50.0 40.8	5 $\frac{1}{2}$ 5 $\frac{1}{4}$	11 $\frac{1}{16}$ 11 $\frac{1}{16}$	11 $\frac{1}{16}$ 3 $\frac{1}{2}$	3 $\frac{1}{8}$ 3 $\frac{1}{4}$	2 $\frac{3}{8}$ 2 $\frac{3}{8}$	9 $\frac{3}{8}$ 9 $\frac{3}{8}$	1 $\frac{5}{16}$ 1 $\frac{5}{16}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	7 $\frac{1}{16}$ 5 $\frac{5}{16}$	3 3	% $\frac{1}{8}$ % $\frac{1}{8}$	% $\frac{1}{4}$ % $\frac{1}{4}$	
12" I B 9 R=.45	35.0 31.8	5 $\frac{3}{8}$ 5	9 $\frac{1}{16}$ 9 $\frac{1}{16}$	7 $\frac{1}{16}$ 3 $\frac{1}{8}$	3 $\frac{1}{4}$ 3 $\frac{1}{16}$	2 $\frac{3}{8}$ 2 $\frac{3}{8}$	9 $\frac{3}{4}$ 9 $\frac{3}{4}$	1 $\frac{1}{8}$ 1 $\frac{1}{8}$	2 $\frac{1}{2}$ 2 $\frac{1}{2}$	5 $\frac{1}{16}$ 3 $\frac{1}{4}$	3 3	1 $\frac{1}{2}$ 1 $\frac{1}{2}$	1 $\frac{1}{4}$ 1 $\frac{1}{4}$	
10" I B 10 R=.41	35.0 25.4	5 4 $\frac{5}{8}$	1 $\frac{1}{2}$ 1 $\frac{1}{2}$	5 $\frac{5}{8}$ 5 $\frac{5}{16}$	5 $\frac{1}{16}$ 3 $\frac{1}{8}$	2 $\frac{1}{8}$ 2 $\frac{1}{8}$	8 8	1 1	2 $\frac{1}{2}$ 2 $\frac{1}{2}$	3 $\frac{1}{8}$ 1 $\frac{1}{4}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	1 $\frac{1}{2}$ 1 $\frac{1}{2}$	1 $\frac{1}{4}$ 1 $\frac{1}{4}$	
8" I B 12 R=.37	23.0 18.4	4 $\frac{1}{8}$ 4	7 $\frac{1}{16}$ 7 $\frac{1}{16}$	7 $\frac{1}{16}$ 5 $\frac{5}{16}$	1 $\frac{1}{4}$ 1 $\frac{1}{8}$	1 $\frac{7}{8}$ 1 $\frac{7}{8}$	6 $\frac{1}{4}$ 6 $\frac{1}{4}$	7 $\frac{1}{8}$ 7 $\frac{1}{8}$	2 $\frac{3}{4}$ 2 $\frac{3}{4}$	5 $\frac{1}{16}$ 3 $\frac{1}{16}$	2 $\frac{1}{4}$ 2 $\frac{1}{4}$	7 $\frac{1}{16}$ 7 $\frac{1}{16}$	1 $\frac{1}{4}$ 1 $\frac{1}{4}$	
7" I B 13 R=.35	20.0 15.3	3 $\frac{7}{8}$ 3 $\frac{5}{8}$	3 $\frac{1}{8}$ 3 $\frac{1}{8}$	7 $\frac{1}{16}$ 1 $\frac{1}{8}$	1 $\frac{1}{4}$ 1 $\frac{1}{8}$	1 $\frac{3}{4}$ 1 $\frac{3}{4}$	5 $\frac{3}{8}$ 5 $\frac{3}{8}$	1 $\frac{15}{16}$ 1 $\frac{15}{16}$	2 2 $\frac{1}{4}$	5 $\frac{1}{16}$ 3 $\frac{1}{16}$	2 $\frac{1}{4}$ 2 $\frac{1}{4}$	3 $\frac{1}{8}$ 3 $\frac{1}{8}$	5 $\frac{1}{8}$ 5 $\frac{1}{8}$	

Gages g_z are based on 1 $\frac{1}{4}$ " edge distance (1 $\frac{1}{8}$ " maximum rivet).

I
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C
STD.

EQUAL
UNEQUAL

BULD
T
SPLIT
CAR SECTION

CRANE RAILS
CORRUG. SHEETS

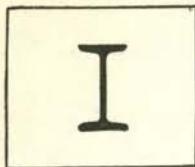
PILING

FLOOR PLATES

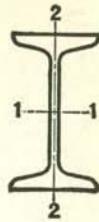
PLATES

MILL PRACTICES

INDEX



BEAMS
AMERICAN STANDARD
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Beam	Width of Flange	Aver. Flange Thick- ness	Web Thickness	Axis 1-1			Axis 2-2		
								Lbs.	In. ²	In.	In.	In.	In.
P.C.B.G.	6" 1												
	B 14	17.25	5.02										
	6 x 3 $\frac{3}{8}$ R=.33	12.5	3.61	6	3.565	.359	.465	26.0	8.7	2.28	2.3	1.3	0.68
P.C. P.C.S.	5" 1												
	B 15	14.75	4.29										
	5 x 3 R=.31	10.0	2.87	5	3.284	.326	.494	15.0	6.0	1.87	1.7	1.0	0.63
P.C.B.G. P.C.B.S.G.	4" 1												
	B 16	9.5	2.76										
	4 x 2 $\frac{5}{8}$ R=.29	7.7	2.21	4	2.796	.293	.326	6.7	3.3	1.56	0.91	0.65	0.58
P.C.B. P.C.B.S.	3" 1												
	B 17	7.5	2.17										
	3 x 2 $\frac{3}{8}$ R=.27	5.7	1.64	3	2.509	.260	.349	2.9	1.9	1.15	0.59	0.47	0.52

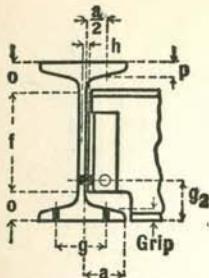
H-BEAMS

District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Beam	Width of Flange	Aver. Flange Thick- ness	Web Thickness	Axis 1-1			Axis 2-2		
								Lbs.	In. ²	In.	In.	In.	In.
P.C.	H 4												
	8 x 8 R=.313	34.3	10.07	8	8.000	.459	.375	115.5	28.9	3.40	35.1	8.8	1.87
	H 3a												
P.C.	6 x 6 R=.313	25.0	7.35	6	5.938	.481	.313	47.0	15.7	2.53	14.9	5.0	1.43
	H 3												
	6 x 6 R=.313	20.0	5.88	6	5.938	.380	.250	38.8	12.9	2.57	11.4	3.8	1.39
P.C.B.	H 2												
	5 x 5 R=.313	18.9	5.54	5	5.000	.417	.313	23.8	9.5	2.08	7.8	3.1	1.20
	H 1												
P.C.B.S.G.	4 x 4 R=.313	13.0	3.82	4	3.937	.372	.250	10.4	5.2	1.65	3.4	1.7	.94

For key to symbols in first column, refer to page 3.

BEAMS

AMERICAN STANDARD DIMENSIONS OF SECTIONS



Section Index and Depth	Weight per Foot	Flange		Web		Distance								Max. Flange Rivet
		Width Lbs.	Thickness, p In.	Thickness, p In.	Half Thickness, p In.	a In.	f In.	o In.	Min. g2 In.	Clear h In.	Gage g In.	Grip In.	In.	
6" I B 14 R=.33	17.25	3 $\frac{5}{8}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{1}{4}$	1 $\frac{1}{2}$	4 $\frac{1}{2}$	$\frac{3}{4}$	2	$\frac{5}{16}$	2	$\frac{3}{8}$	$\frac{5}{8}$	
	12.5	3 $\frac{3}{8}$	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	1 $\frac{1}{2}$	4 $\frac{1}{2}$	$\frac{3}{4}$	2	$\frac{3}{16}$	2	$\frac{5}{16}$	$\frac{5}{8}$	
5" I B 15 R=.31	14.75	3 $\frac{1}{4}$	$\frac{5}{16}$	$\frac{1}{2}$	$\frac{1}{4}$	1 $\frac{3}{8}$	3 $\frac{5}{8}$	$\frac{11}{16}$	2	$\frac{5}{16}$	1 $\frac{3}{4}$	$\frac{5}{16}$	$\frac{1}{2}$	
	10.0	3	$\frac{5}{16}$	$\frac{1}{4}$	$\frac{1}{8}$	1 $\frac{3}{8}$	3 $\frac{5}{8}$	$\frac{11}{16}$	2	$\frac{3}{16}$	1 $\frac{3}{4}$	$\frac{5}{16}$	$\frac{1}{2}$	
4" I B 16 R=.29	9.5	2 $\frac{3}{4}$	$\frac{5}{16}$	$\frac{5}{16}$	$\frac{3}{16}$	1 $\frac{1}{4}$	2 $\frac{3}{4}$	$\frac{5}{8}$	2	$\frac{1}{4}$	1 $\frac{1}{2}$	$\frac{5}{16}$	$\frac{1}{2}$	
	7.7	2 $\frac{5}{8}$	$\frac{5}{16}$	$\frac{3}{16}$	$\frac{1}{8}$	1 $\frac{1}{4}$	2 $\frac{3}{4}$	$\frac{5}{8}$	2	$\frac{3}{16}$	1 $\frac{1}{2}$	$\frac{5}{16}$	$\frac{1}{2}$	
3" I B 17 R=.27	7.5	2 $\frac{1}{2}$	$\frac{1}{4}$	$\frac{3}{8}$	$\frac{3}{16}$	1 $\frac{1}{8}$	1 $\frac{7}{8}$	$\frac{9}{16}$	$\frac{1}{4}$	1 $\frac{1}{2}$	$\frac{1}{4}$	$\frac{3}{8}$	
	5.7	2 $\frac{3}{8}$	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{8}$	1 $\frac{1}{8}$	1 $\frac{7}{8}$	$\frac{9}{16}$	$\frac{3}{16}$	1 $\frac{1}{2}$	$\frac{1}{4}$	$\frac{3}{8}$	

H-BEAMS

Section Index and Depth	Weight per Foot	Flange		Web		Distance								Max. Flange Rivet
		Width Lbs.	Thickness, p In.	Thickness, p In.	Half Thickness, p In.	a In.	f In.	o In.	Min. g2 In.	Clear h In.	Gage g In.	Grip In.	In.	
H 4 R=.313	34.3	8	$\frac{7}{16}$	$\frac{3}{8}$	$\frac{3}{16}$	3 $\frac{13}{16}$	6 $\frac{1}{4}$	$\frac{7}{8}$	2 $\frac{1}{4}$	5	$\frac{7}{16}$	$\frac{7}{8}$	
H 3a R=.313	25.0	6	$\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{16}$	2 $\frac{13}{16}$	4 $\frac{1}{4}$	$\frac{7}{8}$	2 $\frac{1}{4}$	3 $\frac{1}{2}$	$\frac{1}{2}$	$\frac{7}{8}$	
H 3 R=.313	20.0	6	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	2 $\frac{7}{8}$	4 $\frac{7}{16}$	$\frac{3}{4}$	2	3 $\frac{1}{2}$	$\frac{3}{8}$	$\frac{7}{8}$	
H 2 R=.313	18.9	5	$\frac{7}{16}$	$\frac{5}{16}$	$\frac{3}{16}$	2 $\frac{3}{8}$	3 $\frac{3}{8}$	$\frac{13}{16}$	2	2 $\frac{3}{4}$	$\frac{7}{16}$	$\frac{3}{4}$	
H 1 R=.313	13.0	4	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$	1 $\frac{7}{8}$	2 $\frac{1}{2}$	$\frac{3}{4}$	2	2 $\frac{1}{4}$	$\frac{3}{8}$	$\frac{5}{8}$	

Gages g are based on 1 $\frac{1}{4}$ " edge distance ($\frac{7}{8}$ " maximum rivet).

L STD.
C CAR & SHIP

EQUAL

UNEQUAL

BULB

SPLIT

CAR SECTIONS

CRANE RAILS

CORRUG. SHEETS

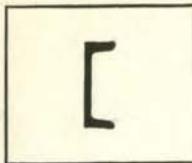
PILING

FLOOR PLATES

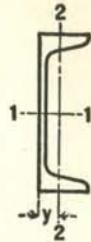
PLATES

MILL PRACTICES

INDEX



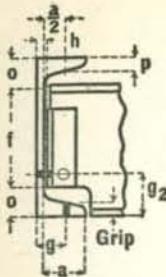
CHANNELS
AMERICAN STANDARD
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Channel	Width of Flange	Aver. Flange Thickness	Web Thickness	Axis 1-1				Axis 2-2			
								I	S	x	In.	I	S	x	y
		Lbs.	In. ²	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
P.C.	†C 60	58.0	16.98	18	4.200	.625	.700	670.7	74.5	6.29	18.5	5.6	1.04	0.88	
	18 x 4	51.9	15.18		4.100	.625	.600	622.1	69.1	6.40	17.1	5.3	1.06	0.87	
	R=.625	45.8	13.38		4.000	.625	.500	573.5	63.7	6.55	15.8	5.1	1.09	0.89	
P.C.B.G.	42.7	12.48			3.950	.625	.450	549.2	61.0	6.64	15.0	4.9	1.10	0.90	
	C 1	50.0	14.64	15	3.716	.650	.716	401.4	53.6	5.24	11.2	3.8	0.87	0.80	
	15 x 3 $\frac{3}{8}$	40.0	11.70		3.520	.650	.520	346.3	46.2	5.44	9.3	3.4	0.89	0.78	
P.C.B.	R=.50	33.9	9.90		3.400	.650	.400	312.6	41.7	5.62	8.2	3.2	0.91	0.79	
P.C.	C 20	50.0	14.66	13	4.412	.610	.787	312.9	48.1	4.62	16.7	4.9	1.07	0.98	
P.C.B.	13 x 4	40.0	11.71		4.185	.610	.560	271.4	41.7	4.82	13.9	4.3	1.09	0.97	
P.C.B.	R=.48	35.0	10.24		4.072	.610	.447	250.7	38.6	4.95	12.5	4.0	1.10	0.99	
P.C.B.	31.8	9.30			4.000	.610	.375	237.5	36.5	5.05	11.6	3.9	1.11	1.01	
P.C.B.G.	C 2	30.0	8.79	12	3.170	.501	.510	161.2	26.9	4.28	5.2	2.1	0.77	0.68	
	12 x 3	25.0	7.32		3.047	.501	.387	143.5	23.9	4.43	4.5	1.9	0.79	0.68	
	R=.38	20.7	6.03		2.940	.501	.280	128.1	21.4	4.61	3.9	1.7	0.81	0.70	
P.C.B.G.	C 3	30.0	8.80	10	3.033	.436	.673	103.0	20.6	3.42	4.0	1.7	0.67	0.65	
	10 x 2 $\frac{5}{8}$	25.0	7.33		2.886	.436	.526	90.7	18.1	3.52	3.4	1.5	0.68	0.62	
	R=.34	20.0	5.86		2.739	.436	.379	78.5	15.7	3.66	2.8	1.3	0.70	0.61	
P.C.B.	15.3	4.47			2.600	.436	.240	66.9	13.4	3.87	2.3	1.2	0.72	0.64	
	C 4	20.0	5.86	9	2.648	.413	.448	60.6	13.5	3.22	2.4	1.2	0.65	0.59	
	9 x 2 $\frac{1}{2}$	15.0	4.39		2.485	.413	.285	50.7	11.3	3.40	1.9	1.0	0.67	0.59	
P.C.B.G.	R=.33	13.4	3.89		2.430	.413	.230	47.3	10.5	3.49	1.8	0.97	0.67	0.61	
	C 5	18.75	5.49	8	2.527	.390	.487	43.7	10.9	2.82	2.00	1.00	0.60	0.57	
	8 x 2 $\frac{1}{4}$	13.75	4.02		2.343	.390	.303	35.8	9.0	2.99	1.50	0.86	0.62	0.56	
P.C.B.S.G.	R=.32	11.50	3.36		2.260	.390	.220	32.3	8.1	3.10	1.30	0.79	0.63	0.58	
	C 6	14.75	4.32	7	2.299	.366	.419	27.1	7.7	2.51	1.40	0.79	0.57	0.53	
	7 x 2 $\frac{3}{8}$	12.25	3.58		2.194	.366	.314	24.1	6.9	2.59	1.20	0.71	0.58	0.53	
P.C.B.S.G.	R=.31	9.80	2.85		2.090	.366	.210	21.1	6.0	2.72	0.98	0.63	0.59	0.55	
	C 7	13.00	3.81	6	2.157	.343	.437	17.3	5.8	2.13	1.10	0.65	0.53	0.52	
	6 x 2	10.50	3.07		2.034	.343	.314	15.1	5.0	2.22	0.87	0.57	0.53	0.50	
P.C.B.S.G.	R=.30	8.20	2.39		1.920	.343	.200	13.0	4.3	2.34	0.70	0.50	0.54	0.52	
	C 8	9.00	2.63	5	1.885	.320	.325	8.8	3.5	1.83	0.64	0.45	0.49	0.48	
	5 x 1 $\frac{3}{4}$	6.70	1.95		1.750	.320	.190	7.4	3.0	1.95	0.48	0.38	0.50	0.49	
P.C.B.S.G.	R=.29														
	C 9	7.25	2.12	4	1.720	.296	.320	4.5	2.3	1.47	0.44	0.35	0.46	0.46	
	4 x 1 $\frac{1}{8}$	5.40	1.56		1.580	.296	.180	3.8	1.9	1.56	0.32	0.29	0.45	0.46	
P.C.B.	R=.28														
P.C.B.	C 10	6.00	1.75	3	1.596	.273	.356	2.1	1.4	1.08	0.31	0.27	0.42	0.46	
P.C.B.S.	3 x 1 $\frac{1}{2}$	5.00	1.46		1.498	.273	.258	1.8	1.2	1.12	0.25	0.24	0.41	0.44	
P.C.B.S.	R=.27	4.10	1.19		1.410	.273	.170	1.6	1.1	1.17	0.20	0.21	0.41	0.44	

†C 60 is not an American standard channel.

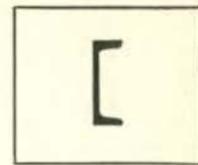
For key to symbols in first column, refer to page 3.



CHANNELS

AMERICAN STANDARD

DIMENSIONS OF SECTIONS



Section Index and Depth	Weight per Foot	Flange		Web		Distance								Max. Flange Rivet	
		Width	Thickness, p	Thickness	Half Thickness	a	f	o	Min. g ₂	Clear. h	Gage g	Grip			
†C 60	58.0	41 $\frac{1}{4}$	5 $\frac{1}{8}$	11 $\frac{1}{16}$	3 $\frac{1}{8}$	31 $\frac{1}{2}$	15 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	$\frac{3}{4}$	21 $\frac{1}{2}$	5 $\frac{1}{8}$	1		
18	51.9	41 $\frac{1}{8}$	5 $\frac{1}{8}$	5 $\frac{1}{16}$	5 $\frac{1}{16}$	31 $\frac{1}{2}$	15 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	11 $\frac{1}{16}$	21 $\frac{1}{2}$	5 $\frac{1}{8}$	1		
R=.625	45.8	4	5 $\frac{1}{8}$	3 $\frac{1}{2}$	1 $\frac{1}{4}$	31 $\frac{1}{2}$	15 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	9 $\frac{1}{16}$	21 $\frac{1}{2}$	5 $\frac{1}{8}$	1		
R=.50	42.7	4	5 $\frac{1}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	31 $\frac{1}{2}$	15 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	1 $\frac{1}{2}$	21 $\frac{1}{2}$	5 $\frac{1}{8}$	1		
C 1	50.0	33 $\frac{3}{4}$	5 $\frac{1}{8}$	3 $\frac{1}{4}$	3 $\frac{1}{8}$	3	12 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	19 $\frac{1}{16}$	21 $\frac{1}{4}$	5 $\frac{1}{8}$	1		
15	40.0	31 $\frac{1}{2}$	5 $\frac{1}{8}$	9 $\frac{1}{16}$	1 $\frac{1}{4}$	3	12 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	5 $\frac{1}{8}$	2	5 $\frac{1}{8}$	1		
R=.50	33.9	3 $\frac{3}{8}$	5 $\frac{1}{8}$	7 $\frac{1}{16}$	3 $\frac{1}{16}$	3	12 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	1 $\frac{1}{2}$	2	5 $\frac{1}{8}$	1		
C 20	50.0	4 $\frac{3}{8}$	5 $\frac{1}{8}$	13 $\frac{1}{16}$	7 $\frac{1}{16}$	3 $\frac{5}{8}$	10 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	7 $\frac{1}{8}$	21 $\frac{1}{2}$	5 $\frac{1}{8}$	1		
13	40.0	4 $\frac{1}{8}$	5 $\frac{1}{8}$	9 $\frac{1}{16}$	5 $\frac{1}{16}$	3 $\frac{5}{8}$	10 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	5 $\frac{1}{8}$	21 $\frac{1}{2}$	9 $\frac{1}{16}$	1		
R=.48	35.0	4 $\frac{1}{8}$	5 $\frac{1}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	3 $\frac{5}{8}$	10 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	2 $\frac{3}{8}$	21 $\frac{1}{2}$	9 $\frac{1}{16}$	1		
R=.48	31.8	4	5 $\frac{1}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{16}$	3 $\frac{5}{8}$	10 $\frac{3}{8}$	15 $\frac{1}{16}$	2 $\frac{3}{4}$	7 $\frac{1}{16}$	21 $\frac{1}{2}$	9 $\frac{1}{16}$	1		
C 2	30.0	3 $\frac{1}{8}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{4}$	2 $\frac{5}{8}$	9 $\frac{7}{8}$	11 $\frac{1}{16}$	2 $\frac{1}{2}$	9 $\frac{1}{16}$	1 $\frac{3}{4}$	1 $\frac{1}{2}$	7 $\frac{1}{8}$		
12	25.0	3	1 $\frac{1}{2}$	3 $\frac{1}{8}$	3 $\frac{1}{16}$	2 $\frac{5}{8}$	9 $\frac{7}{8}$	13 $\frac{1}{16}$	2 $\frac{1}{2}$	7 $\frac{1}{16}$	1 $\frac{3}{4}$	1 $\frac{1}{2}$	7 $\frac{1}{8}$		
R=.38	20.7	3	1 $\frac{1}{2}$	5 $\frac{1}{16}$	1 $\frac{1}{8}$	2 $\frac{5}{8}$	9 $\frac{7}{8}$	14 $\frac{1}{16}$	2 $\frac{1}{2}$	3 $\frac{1}{8}$	1 $\frac{3}{4}$	1 $\frac{1}{2}$	7 $\frac{1}{8}$		
C 3	30.0	3	7 $\frac{1}{16}$	11 $\frac{1}{16}$	3 $\frac{1}{8}$	2 $\frac{3}{8}$	8 $\frac{1}{8}$	15 $\frac{1}{16}$	2 $\frac{1}{2}$	3 $\frac{1}{4}$	13 $\frac{1}{4}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
10	25.0	2 $\frac{7}{8}$	7 $\frac{1}{16}$	9 $\frac{1}{16}$	1 $\frac{1}{4}$	2 $\frac{3}{8}$	8 $\frac{1}{8}$	15 $\frac{1}{16}$	2 $\frac{1}{2}$	5 $\frac{1}{8}$	13 $\frac{1}{4}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
R=.34	20.0	2 $\frac{3}{4}$	7 $\frac{1}{16}$	3 $\frac{1}{8}$	3 $\frac{1}{16}$	2 $\frac{3}{8}$	8 $\frac{1}{8}$	15 $\frac{1}{16}$	2 $\frac{1}{2}$	7 $\frac{1}{16}$	11 $\frac{1}{2}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
R=.34	15.3	2 $\frac{3}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	1 $\frac{1}{8}$	2 $\frac{3}{8}$	8 $\frac{1}{8}$	15 $\frac{1}{16}$	2 $\frac{1}{2}$	5 $\frac{1}{16}$	11 $\frac{1}{2}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
C 4	20.0	2 $\frac{5}{8}$	7 $\frac{1}{16}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	2 $\frac{1}{4}$	7 $\frac{1}{4}$	7 $\frac{1}{8}$	2 $\frac{1}{2}$	1 $\frac{1}{2}$	11 $\frac{1}{2}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
9	15.0	2 $\frac{1}{2}$	7 $\frac{1}{16}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	2 $\frac{1}{4}$	7 $\frac{1}{4}$	7 $\frac{1}{8}$	2 $\frac{1}{2}$	3 $\frac{1}{8}$	13 $\frac{1}{8}$	7 $\frac{1}{16}$	3 $\frac{1}{4}$		
R=.33	13.4	2 $\frac{9}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	1 $\frac{1}{8}$	2 $\frac{1}{4}$	7 $\frac{1}{4}$	7 $\frac{1}{8}$	2 $\frac{1}{2}$	7 $\frac{1}{16}$	13 $\frac{1}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{4}$		
C 5	18.75	2 $\frac{1}{2}$	3 $\frac{1}{8}$	1 $\frac{1}{2}$	1 $\frac{1}{4}$	2	6 $\frac{3}{8}$	13 $\frac{1}{16}$	2 $\frac{1}{4}$	9 $\frac{1}{16}$	11 $\frac{1}{2}$	3 $\frac{1}{8}$	3 $\frac{1}{4}$		
8	13.75	2 $\frac{9}{8}$	3 $\frac{1}{8}$	9 $\frac{1}{16}$	3 $\frac{1}{16}$	2	6 $\frac{3}{8}$	13 $\frac{1}{16}$	2 $\frac{1}{4}$	3 $\frac{1}{8}$	13 $\frac{1}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{4}$		
R=.32	11.5	2 $\frac{3}{4}$	3 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{1}{8}$	2	6 $\frac{3}{8}$	13 $\frac{1}{16}$	2 $\frac{1}{4}$	5 $\frac{1}{16}$	13 $\frac{1}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{4}$		
C 6	14.75	2 $\frac{1}{4}$	3 $\frac{1}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	1 $\frac{7}{8}$	5 $\frac{3}{8}$	13 $\frac{1}{16}$	2	1 $\frac{1}{2}$	11 $\frac{1}{4}$	3 $\frac{1}{8}$	5 $\frac{1}{8}$		
7	12.25	2 $\frac{1}{4}$	3 $\frac{1}{8}$	9 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{7}{8}$	5 $\frac{3}{8}$	13 $\frac{1}{16}$	2	3 $\frac{1}{8}$	11 $\frac{1}{4}$	3 $\frac{1}{8}$	5 $\frac{1}{8}$		
R=.31	9.8	2 $\frac{7}{8}$	3 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{1}{8}$	1 $\frac{7}{8}$	5 $\frac{3}{8}$	13 $\frac{1}{16}$	2	5 $\frac{1}{16}$	11 $\frac{1}{4}$	3 $\frac{1}{8}$	5 $\frac{1}{8}$		
C 7	13.0	2 $\frac{1}{8}$	3 $\frac{1}{8}$	7 $\frac{1}{16}$	1 $\frac{1}{4}$	1 $\frac{3}{4}$	4 $\frac{1}{2}$	$\frac{3}{4}$	2	1 $\frac{1}{2}$	13 $\frac{1}{8}$	5 $\frac{1}{8}$	5 $\frac{1}{8}$		
6	10.5	2	3 $\frac{1}{8}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{3}{4}$	4 $\frac{1}{2}$	$\frac{3}{4}$	2	3 $\frac{1}{8}$	11 $\frac{1}{8}$	3 $\frac{1}{8}$	5 $\frac{1}{8}$		
R=.30	8.2	1 $\frac{7}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{16}$	1 $\frac{1}{8}$	1 $\frac{3}{4}$	4 $\frac{1}{2}$	$\frac{3}{4}$	2	1 $\frac{1}{4}$	11 $\frac{1}{8}$	5 $\frac{1}{16}$	5 $\frac{1}{8}$		
C 8	9.0	1 $\frac{7}{8}$	5 $\frac{1}{16}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{1}{2}$	3 $\frac{5}{8}$	11 $\frac{1}{16}$	2	3 $\frac{1}{8}$	11 $\frac{1}{8}$	5 $\frac{1}{16}$	1 $\frac{1}{2}$		
5	6.7	1 $\frac{3}{4}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{1}{8}$	1 $\frac{1}{2}$	3 $\frac{5}{8}$	11 $\frac{1}{16}$	2	1 $\frac{1}{4}$	11 $\frac{1}{8}$	5 $\frac{1}{16}$	1 $\frac{1}{2}$		
R=.29	C 9	7.25	1 $\frac{3}{4}$	5 $\frac{1}{16}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{3}{8}$	2 $\frac{3}{4}$	5 $\frac{1}{8}$	2	3 $\frac{1}{8}$	1	5 $\frac{1}{16}$	1 $\frac{1}{2}$	
4	R=.28	5.4	1 $\frac{1}{8}$	5 $\frac{1}{16}$	3 $\frac{1}{16}$	1 $\frac{1}{8}$	1 $\frac{3}{8}$	2 $\frac{3}{4}$	5 $\frac{1}{8}$	2	1 $\frac{1}{4}$	1	5 $\frac{1}{16}$	1 $\frac{1}{2}$	
C 10	6.0	1 $\frac{5}{8}$	1 $\frac{1}{4}$	3 $\frac{1}{8}$	3 $\frac{1}{16}$	1 $\frac{1}{4}$	1 $\frac{3}{4}$	5 $\frac{1}{8}$	1 $\frac{1}{16}$	7 $\frac{1}{8}$	5 $\frac{1}{16}$	1 $\frac{1}{2}$		
3	R=.27	5.0	1 $\frac{1}{2}$	1 $\frac{1}{4}$	1 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{1}{4}$	1 $\frac{3}{4}$	5 $\frac{1}{8}$	1 $\frac{1}{16}$	7 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{1}{2}$	
R=.27	4.1	1 $\frac{3}{8}$	1 $\frac{1}{4}$	3 $\frac{1}{16}$	1 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{3}{4}$	5 $\frac{1}{8}$	1 $\frac{1}{16}$	7 $\frac{1}{8}$	1 $\frac{1}{4}$	1 $\frac{1}{2}$		

Gages g₂ are based on 1 $\frac{1}{4}$ " edge distance (7 $\frac{1}{8}$ " maximum rivet).
†C 60 is not an American standard channel.

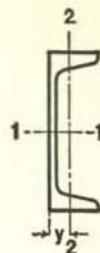
- [STD.]
- [CAR & SHIP]
- EQUAL
- UNEQUAL
- BULB
- SPLIT
- CAR SECTIONS
- CRANE RAILS
- CORRUG. SHEETS
- PILING
- FLOOR PLATES
- PLATES
- MILL PRACTICES
- INDEX



CHANNELS

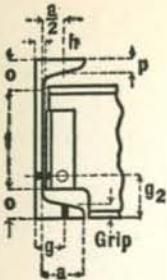
CAR BUILDING AND SHIPBUILDING

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Channel	Width of Flange	Aver. Flange Thick-ness	Web Thick-ness	Axis 1-1			Axis 2-2			
								In. ²	In.	In.	In. ⁴	In. ²	In.	
P.C.	C 60	58.0	16.98	18	4.200	.625	.700	670.7	74.5	6.29	18.5	5.6	1.04	0.88
	18 x 4	51.9	15.18		4.100	.625	.600	622.1	69.1	6.40	17.1	5.3	1.06	0.87
	R=.625	45.8	13.38		4.000	.625	.500	573.5	63.7	6.55	15.8	5.1	1.09	0.89
		42.7	12.48		3.950	.625	.450	549.2	61.0	6.64	15.0	4.9	1.10	0.90
P.C.G.	C 20	50.0	14.66	13	4.412	.610	.787	312.9	48.1	4.62	16.7	4.9	1.07	0.98
P.C.B.G.	13 x 4	40.0	11.71		4.185	.610	.560	271.4	41.7	4.82	13.9	4.3	1.09	0.97
P.C.B.G.	R=.48	35.0	10.24		4.072	.610	.447	250.7	38.6	4.95	12.5	4.0	1.10	0.99
P.C.B.G.		31.8	9.30		4.000	.610	.375	237.5	36.5	5.05	11.6	3.9	1.11	1.01
P.C.B.G.	C 170	50.0	14.64	12	4.135	.700	.835	268.1	44.7	4.28	17.8	5.8	1.10	1.06
	12 x 4	45.0	13.16		4.012	.700	.712	250.4	41.7	4.36	16.1	5.4	1.11	1.05
	R=.50	40.0	11.70		3.890	.700	.590	232.8	38.8	4.46	14.5	5.1	1.12	1.05
		35.0	10.23		3.767	.700	.467	215.1	35.8	4.59	12.9	4.8	1.12	1.07
P.G.	C 171	37.0	10.80	12	3.600	.600	.600	203.4	33.9	4.34	10.3	3.8	0.98	0.89
	12 x 3½	32.9	9.60		3.500	.600	.500	189.0	31.5	4.44	9.4	3.6	0.99	0.89
	R=.60	30.9	9.00		3.450	.600	.450	181.8	30.3	4.50	8.9	3.5	0.99	0.90
P.G.	C 26	41.1	12.06	10	4.319	.575	.794	156.3	31.3	3.61	16.4	5.1	1.17	1.11
	10 x 4	33.6	9.81		4.100	.575	.575	138.0	27.6	3.75	13.7	4.6	1.18	1.11
	R=.575	28.5	8.31		3.950	.575	.425	125.5	25.1	3.89	11.8	4.2	1.19	1.15
P.G.	C 27	28.3	8.23	10	3.500	.575	.475	116.9	23.4	3.77	8.6	3.4	1.02	0.96
	10 x 3½	24.9	7.23		3.400	.575	.375	108.6	21.7	3.88	7.6	3.2	1.03	0.98
	R=.575													
P.C.	C 28	25.3	7.38	10	3.550	.500	.425	106.0	21.2	3.79	7.9	3.0	1.04	0.94
	10 x 3½	21.9	6.38		3.450	.500	.325	97.6	19.5	3.91	7.0	2.8	1.05	0.98
	R=.50													
P.C.G.	C 32	25.4	7.41	9	3.500	.550	.450	87.3	19.4	3.43	8.0	3.2	1.04	1.00
	9 x 3½	23.9	6.96		3.450	.550	.400	84.3	18.7	3.48	7.5	3.1	1.04	1.01

For key to symbols in first column, refer to page 3.



CHANNELS

CAR BUILDING AND SHIP BUILDING

DIMENSIONS OF SECTIONS

Section Index and Depth	Weight per Foot	Flange		Web		Distance							Max. Flange Rivet				
		Width Lbs.	Thickness, p In.	Thickness, in.	Half Thickness, in.	a			f		o		Min. g ₂ , in.	Clear. h, in.	Gage g, in.	Grip, in.	
						a, in.	f, in.	o, in.	a, in.	f, in.	o, in.	in.					
C 60 18 R=.625	58.0	41/4	5/8	11/16	3/8	31/2	153/8	15/16	23/4	3/4	21/2	5/8	1				
	51.9	41/8	5/8	5/8	5/16	31/2	153/8	15/16	23/4	11/16	21/2	5/8	1				
	45.8	4	5/8	1/2	1/4	31/2	153/8	15/16	23/4	9/16	21/2	5/8	1				
	42.7	4	5/8	7/16	1/4	31/2	153/8	15/16	23/4	3/2	21/2	5/8	1				
C 20 13 R=.48	50.0	43/8	5/8	13/16	7/16	35/8	103/8	15/16	23/4	7/8	21/2	5/8	1				
	40.0	41/8	5/8	9/16	5/16	35/8	103/8	15/16	23/4	5/8	21/2	9/16	1				
	35.0	41/8	5/8	7/16	3/4	35/8	103/8	15/16	23/4	3/2	21/2	9/16	1				
	31.8	4	5/8	3/8	3/16	35/8	103/8	15/16	23/4	7/16	21/2	9/16	1				
C 170 12 R=.50	50.0	41/8	11/16	7/8	7/16	33/8	91/2	11/4	21/2	15/16	21/2	11/16	1				
	45.0	4	11/16	11/16	3/8	33/8	91/2	11/4	21/2	3/4	21/2	11/16	1				
	40.0	37/8	11/16	5/8	5/16	33/8	91/2	11/4	21/2	11/16	21/2	11/16	1				
	35.0	33/8	11/16	1/2	1/4	33/8	91/2	11/4	21/2	9/16	21/2	11/16	1				
C 171 12 R=.60	37.0	35/8	5/8	5/8	5/16	3	91/2	11/4	21/2	11/16	21/4	5/8	7/8				
	32.9	31/2	5/8	1/2	1/4	3	91/2	11/4	21/2	9/16	21/4	9/16	7/8				
	30.9	31/2	5/8	7/16	1/4	3	91/2	11/4	21/2	1/2	21/4	9/16	7/8				
C 26 10 R=.575	41.1	45/16	9/16	13/16	7/16	31/2	71/2	11/4	21/2	7/8	21/2	9/16	7/8				
	33.6	41/8	9/16	9/16	5/16	31/2	71/2	11/4	21/2	5/8	21/2	9/16	7/8				
	28.5	4	9/16	7/16	1/4	31/2	71/2	11/4	21/2	3/2	21/2	9/16	7/8				
C 27 10 R=.575	28.3	31/2	9/16	1/2	1/4	3	75/8	13/16	21/2	9/16	2	9/16	7/8				
	24.9	33/8	9/16	3/8	3/16	3	75/8	13/16	21/2	7/16	2	9/16	7/8				
C 28 10 R=.50	25.3	31/2	1/2	7/16	1/4	31/8	77/8	11/16	21/2	1/2	2	1/2	7/8				
	21.9	31/2	1/2	5/16	3/16	31/8	77/8	11/16	21/2	3/8	2	1/2	7/8				
C 32 9 R=.55	25.4	31/2	9/16	7/16	1/4	3	63/4	11/8	21/2	1/2	2	9/16	7/8				
	23.9	31/2	9/16	7/16	3/16	3	63/4	11/8	21/2	1/2	2	9/16	7/8				

Gages g are usual standard gages, but may be varied if conditions require.

Gages g₂ are based on 1 1/4" edge distance (7/8" maximum rivet).

CAR &
SHIP

EQUAL
UNEQUAL

SPLIT
CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

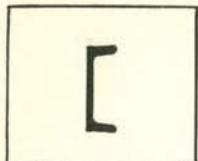
PILING

FLOOR
PLATES

PLATES

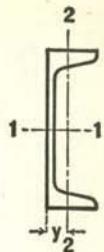
MILL
PRACTICES

INDEX



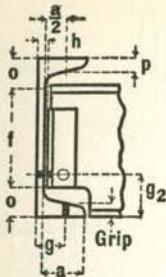
CHANNELS
CAR BUILDING AND
SHIP BUILDING

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Channel	Width of Flange	Aver. Flange Thickness	Web Thick- ness	Axis 1-1			Axis 2-2			y
								I	S	r	I	S	r	
								In. ⁴	In. ³	In.	In. ⁴	In. ³	In.	
P.C.G.	C 36	22.8	6.63	8	3.500	.525	.425	63.3	15.8	3.09	7.4	3.0	1.05	1.04
	8 x 3½	21.4	6.23		3.450	.525	.375	61.2	15.3	3.13	6.9	2.9	1.05	1.05
	R=.525													
P.B.G.	C 37	20.0	5.83	8	3.025	.500	.400	54.0	13.5	3.05	4.7	2.2	0.90	0.86
	8 x 3	18.7	5.43		2.975	.500	.350	51.9	13.0	3.09	4.4	2.1	0.90	0.88
	R=.50													
P.C.	C 41	22.7	6.60	7	3.600	.500	.500	47.1	13.5	2.67	7.5	3.0	1.07	1.07
	7 x 3½	19.1	5.55		3.450	.500	.350	42.8	12.2	2.78	6.3	2.7	1.07	1.11
	R=.50													
P.	C 42	17.6	5.12	7	3.000	.475	.375	37.3	10.7	2.70	4.2	2.0	0.90	0.90
	7 x 3													
	R=.475													
P.G.	C 46	18.0	5.22	6	3.500	.475	.375	29.4	9.8	2.38	6.1	2.6	1.08	1.15
	6 x 3½													
	R=.475													
P.C.	C 56	15.3	4.48	6	3.500	.385	.340	25.3	8.4	2.38	5.1	2.1	1.08	1.08
	6 x 3½													
	R=.385													
P.	C 47	16.3	4.75	6	3.000	.475	.375	25.8	8.6	2.33	4.0	1.9	0.91	0.95
	6 x 3	15.1	4.37		2.938	.475	.313	24.7	8.2	2.38	3.6	1.8	0.91	0.97
	R=.475													
P.	C 48	12.0	3.52	6	2.500	.375	.313	18.6	6.2	2.30	2.0	1.1	0.75	0.72
	6 x 2½													
	R=.375													
P.	C 200	13.8	4.00	4	2.500	.500	.500	8.8	4.4	1.49	2.2	1.4	0.74	0.86
	4 x 2½													
	R=.28													
P. P.C.	*C 192	9.0	2.64	3	2.125	.351	.500	3.1	2.1	1.09	0.97	0.68	0.61	0.71
	*C 193	7.1	2.08		1.938	.351	.313	2.7	1.8	1.14	0.71	0.56	0.58	0.68
	3 x 1½													
	R=.19													

*C 193 and C 192 are identical except that C 193 flanges are flared out to 3½" at toe of flanges.
For key to symbols in first column refer to page 3.



CHANNELS

CAR BUILDING AND SHIP BUILDING

DIMENSIONS OF SECTIONS

Section Index and Depth	Weight per Foot	Flange		Web		Distance								Max. Flange Rivet		
		Width	Thickness, p	Thickness	Half Thickness	a	f	o	Min. g _z	Clear. h	Gage g	Grip	In.	In.	In.	
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
C 36 8 R=.525	22.8 21.4	3½	½	⅜	¼	3½	5¾	11½	2½	½	2	½	½	½	⅞	L EQUAL
C 37 8 R=.50	20.0 18.7	3	½	⅜	⅜	25/8	5¾	11½	2½	½	1¾	½	½	½	⅞	L UNEQUAL
C 41 7 R=.50	22.7 19.1	35/8	½	½	¼	3½	47/8	11½	2½	½	2	½	½	½	⅞	BULB
C 42 7 R=.475	17.6	3	½	⅜	⅜	25/8	5	1	2½	½	1¾	½	½	½	⅞	T SPLIT
C 46 6 R=.475	18.0	3½	½	⅔	⅓	3½	4	1	2½	½	2	½	½	½	⅞	CAR SECTIONS
C 56 6 R=.385	15.3	3½	⅔	⅔	⅓	3½	43/8	13½	2	½	2	¾	¾	¾	⅞	CRANE RAILS
C 47 6 R=.475	16.3 15.1	3	½	⅔	⅓	25/8	4	1	2½	½	1¾	½	½	½	¾	CORRUG. SHEETS
C 48 6 R=.375	12.0	2½	⅔	⅕	⅓	2½	41/2	¾	2	¾	1½	¾	¾	¾	⅞	PILING
C 200 4 R=.28	13.8	2½	½	½	¼	2	23/8	13½	2	½	1½	½	½	½	⅞	FLOOR PLATES
*C 192 *C 193 3 R=.19	9.0 7.1	2½	⅔	½	¼	15/8	17/8	¾	...	¾	PLATES

Gages g are usual standard gages, but may be varied if conditions require.

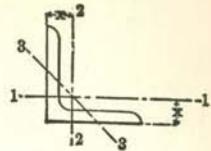
Gages g_z are based on 1½" edge distance (⅞" maximum rivet).

*C 193 and C 192 are identical except that C 193 flanges are flared out to 3½" at toe of flanges.



EQUAL ANGLES

PROPERTIES OF SECTIONS

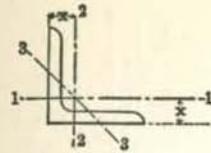


District Rolled	Section Index	Size	Thickness	Weight per Foot	Area of Section	Axis 1-1 and Axis 2-2				Axis 3-3
						In.	In.	Lbs.	In. ²	
P.C.B.	A 1 R = 5/8	8 x 8	1 1/8	56.9	16.73	98.0	17.5	2.42	2.41	1.55
			1	51.0	15.00	89.0	15.8	2.44	2.37	1.56
			5/8	45.0	13.23	79.6	14.0	2.45	2.32	1.56
			3/4	38.9	11.44	69.7	12.2	2.47	2.28	1.57
			5/8	32.7	9.61	59.4	10.3	2.49	2.23	1.58
			11/16	29.6	8.68	54.1	9.3	2.50	2.21	1.58
			1/2	26.4	7.75	48.6	8.4	2.51	2.19	1.58
P.C.B.G.	A 2 R = 1/2	6 x 6	o1	37.4	11.00	35.5	8.6	1.80	1.86	1.16
P.C.B.G.			5/8	33.1	9.73	31.9	7.6	1.81	1.82	1.17
P.C.B.G.			3/4	28.7	8.44	28.2	6.7	1.83	1.78	1.17
P.C.B.G.			5/8	24.2	7.11	24.2	5.7	1.84	1.73	1.17
P.C.B.G.			11/16	21.9	6.43	22.1	5.1	1.85	1.71	1.18
P.C.B.G.			1/2	19.6	5.75	19.9	4.6	1.86	1.68	1.18
P.C.B.G.			11/16	17.2	5.06	17.7	4.1	1.87	1.66	1.19
P.C.B.G.	P.G.		3/8	14.9	4.36	15.4	3.5	1.88	1.64	1.19
P.C.			5/16	12.6	3.66	13.0	3.0	1.89	1.61	1.19
P.C.B.S.	A 3 R = 1/2	5 x 5	5/8	27.2	7.98	17.8	5.2	1.49	1.57	0.96
P.C.B.S.			3/4	23.6	6.94	15.7	4.5	1.50	1.52	0.97
P.C.B.S.			5/8	20.0	5.86	13.6	3.9	1.52	1.48	0.97
P.C.B.S.			1/2	16.2	4.75	11.3	3.2	1.54	1.43	0.98
P.C.B.S.			7/16	14.3	4.18	10.0	2.8	1.55	1.41	0.98
P.C.B.S.			3/8	12.3	3.61	8.7	2.4	1.56	1.39	0.99
P.C.B.S.			5/16	10.3	3.03	7.4	2.0	1.56	1.36	0.99
P.C.B.G.	A 4 R = 3/8	4 x 4	3/4	18.5	5.44	7.7	2.8	1.19	1.27	0.77
			5/8	15.7	4.61	6.7	2.4	1.20	1.23	0.77
			1/2	12.8	3.75	5.6	2.0	1.22	1.18	0.78
			7/16	11.3	3.31	5.0	1.8	1.23	1.16	0.78
			3/8	9.8	2.86	4.4	1.5	1.23	1.14	0.79
			5/16	8.2	2.40	3.7	1.3	1.24	1.12	0.79
			*1/4	6.6	1.94	3.0	1.0	1.25	1.09	0.79
P.C.B.G.	A 5 R = 3/8	3 1/2 x 3 1/2	1/2	11.1	3.25	3.6	1.5	1.06	1.06	0.68
			5/16	9.8	2.87	3.3	1.3	1.07	1.04	0.68
			3/8	8.5	2.48	2.9	1.2	1.07	1.01	0.69
			5/16	7.2	2.09	2.5	0.98	1.08	0.99	0.69
			1/4	5.8	1.69	2.0	0.79	1.09	0.97	0.69

*Special gage.

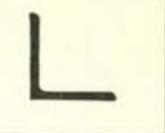
oWhen produced in Birmingham District, leg length will exceed standard tolerance.

For key to symbols in first column, refer to page 3.



EQUAL ANGLES

PROPERTIES OF SECTIONS



District Rolled	Section Index	Size	Thickness	Weight per Foot	Area of Section	Axis 1-1 and Axis 2-2				Axis 3-3
						I	S	r	x	
		In.	In.	Lbs.	In. ²	In. ⁴	In. ³	In.	In.	In.
P.C.B.S.	A 7 R=5/16	3 x 3	1/2	9.4	2.75	2.2	1.1	0.90	0.93	0.58
			7/16	8.3	2.43	2.0	0.95	0.91	0.91	0.58
			5/8	7.2	2.11	1.8	0.83	0.91	0.89	0.58
			13/16	6.1	1.78	1.5	0.71	0.92	0.87	0.59
			3/4	4.9	1.44	1.2	0.58	0.93	0.84	0.59
			11/16	3.71	1.09	0.96	0.44	0.94	0.82	0.59
P.C.B.			11/16	7.7	2.25	1.2	0.73	0.74	0.81	0.47
P.C.B.S.			5/8	5.9	1.73	0.98	0.57	0.75	0.76	0.48
P.C.B.S.			13/16	5.0	1.47	0.85	0.48	0.76	0.74	0.49
P.C.B.S.			3/4	4.1	1.19	0.70	0.39	0.77	0.72	0.49
P.C.B.S.			11/16	3.07	0.90	0.55	0.30	0.78	0.69	0.49
P.C.B.S.	†A 11 R=3/4	2 1/2 x 2 1/2	5/8	4.7	1.36	0.48	0.35	0.59	0.64	0.39
			13/16	3.92	1.15	0.42	0.30	0.60	0.61	0.39
			1/2	3.19	0.94	0.35	0.25	0.61	0.59	0.39
			11/16	2.44	0.71	0.28	0.19	0.62	0.57	0.40
			1/2	1.65	0.48	0.19	0.13	0.63	0.55	0.40
			1/2							
P.C.B.S.			11/16	2.34	0.69	0.14	0.13	0.45	0.47	0.29
P.C.B.S.			13/16	1.80	0.53	0.11	0.10	0.46	0.44	0.29
P.C.B.S.			1/2	1.23	0.36	0.08	0.07	0.46	0.42	0.30
P.C.B.S.	†A 15 R=3/16	1 1/4 x 1 1/4	1/2	1.92	0.56	0.08	0.09	0.37	0.40	0.24
			13/16	1.48	0.43	0.06	0.07	0.38	0.38	0.24
			1/2	1.01	0.30	0.04	0.05	0.38	0.35	0.25
			1/2							
			1/2							
			1/2							
P.C.B.S.	†A 16 R=1/8	1 x 1	1/2	1.49	0.44	0.04	0.06	0.29	0.34	0.19
			13/16	1.16	0.34	0.03	0.04	0.30	0.32	0.19
			1/2	0.80	0.23	0.02	0.03	0.31	0.30	0.19
			1/2							
			1/2							
			1/2							

*Special gage.

†Bar size.

When produced in Birmingham District, leg length will exceed standard tolerance.

For key to symbols in first column, refer to page 3.

EQUAL
UNEQUAL
BULB

T
T
SPLIT

CAR
SECTIONS

CRANE
RAILS

CORRUG.
Sheets

PILING

FLOOR
PLATES

PLATES

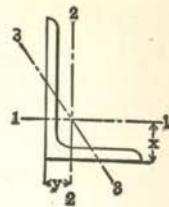
MILL
PRACTICES

INDEX



UNEQUAL ANGLES

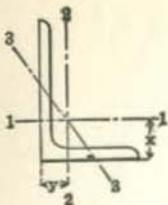
PROPERTIES OF SECTIONS



District Rolled	Section Index	Size	Thickness	Weight per Foot	Area of Section	Axis 1-1				Axis 2-2				Axis 3-3 $\frac{x}{r}$ min.
						In.	In.	Lbs.	In. ²	In. ⁴	In. ³	In.	In.	
C.G.	A 94 $R=\frac{1}{2}$	9 x 4	1	40.8	12.00	97.0	17.6	2.84	3.50	12.0	4.0	1.00	1.00	0.83
			$\frac{7}{8}$	36.1	10.61	86.8	15.7	2.86	3.45	10.8	3.6	1.01	0.95	0.84
			$\frac{3}{4}$	31.3	9.19	76.1	13.6	2.88	3.41	9.6	3.1	1.02	0.91	0.84
			$\frac{5}{8}$	26.3	7.73	64.9	11.5	2.90	3.36	8.3	2.6	1.04	0.86	0.85
			$\frac{1}{16}$	23.8	7.00	59.1	10.4	2.91	3.33	7.6	2.4	1.04	0.83	0.85
			$\frac{1}{2}$	21.3	6.25	53.2	9.3	2.92	3.31	6.9	2.2	1.05	0.81	0.85
P.C.B.	A 18 $R=\frac{1}{2}$	8 x 6	o1	44.2	13.00	80.8	15.1	2.49	2.65	38.8	8.9	1.73	1.65	1.28
			$\frac{7}{8}$	39.1	11.48	72.3	13.4	2.51	2.61	34.9	7.9	1.74	1.61	1.28
			$\frac{3}{4}$	33.8	9.94	63.4	11.7	2.53	2.56	30.7	6.9	1.76	1.56	1.29
			$\frac{5}{8}$	28.5	8.36	54.1	9.9	2.54	2.52	26.3	5.9	1.77	1.52	1.29
			$\frac{1}{16}$	25.7	7.56	49.3	9.0	2.55	2.50	24.0	5.3	1.78	1.50	1.30
			$\frac{1}{2}$	23.0	6.75	44.3	8.0	2.56	2.47	21.7	4.8	1.79	1.47	1.30
			$\frac{1}{16}$	20.2	5.93	39.2	7.1	2.57	2.45	19.3	4.2	1.80	1.45	1.31
P.C.G.	A 50 $R=\frac{1}{2}$	8 x 4	1	37.4	11.00	69.6	14.1	2.52	3.05	11.6	3.9	1.03	1.05	0.85
			$\frac{7}{8}$	33.1	9.73	62.5	12.5	2.53	3.00	10.5	3.5	1.04	1.00	0.85
			$\frac{3}{4}$	28.7	8.44	54.9	10.9	2.55	2.95	9.4	3.1	1.05	0.95	0.85
			$\frac{5}{8}$	24.2	7.11	46.9	9.2	2.57	2.91	8.1	2.6	1.07	0.91	0.86
			$\frac{1}{16}$	21.9	6.43	42.8	8.4	2.58	2.88	7.4	2.4	1.07	0.88	0.86
			$\frac{1}{2}$	19.6	5.75	38.5	7.5	2.59	2.86	6.7	2.2	1.08	0.86	0.86
			$\frac{1}{16}$	17.2	5.06	34.1	6.6	2.60	2.83	6.0	1.9	1.09	0.83	0.87
P.C.G.	A 60 $R=\frac{1}{2}$	7 x 4	$\frac{7}{8}$	30.2	8.86	42.9	9.7	2.20	2.55	10.2	3.5	1.07	1.05	0.86
			$\frac{3}{4}$	26.2	7.69	37.8	8.4	2.22	2.51	9.1	3.0	1.09	1.01	0.86
			$\frac{5}{8}$	22.1	6.48	32.4	7.1	2.24	2.46	7.8	2.6	1.10	0.96	0.86
			$\frac{1}{16}$	20.0	5.87	29.6	6.5	2.24	2.44	7.2	2.4	1.11	0.94	0.87
			$\frac{1}{2}$	17.9	5.25	26.7	5.8	2.25	2.42	6.5	2.1	1.11	0.92	0.87
			$\frac{1}{16}$	15.8	4.62	23.7	5.1	2.26	2.39	5.8	1.9	1.12	0.89	0.88
			$\frac{3}{8}$	13.6	3.98	20.6	4.4	2.27	2.37	5.1	1.6	1.13	0.87	0.88

oWhen produced in Birmingham District, leg length will exceed standard tolerance.

For key to symbols in first column, refer to page 3.



UNEQUAL ANGLES

PROPERTIES OF SECTIONS



District Rolled	Section Index	Size	Thickness	Weight per Foot	Area of Section	Axis 1-1				Axis 2-2				Axis 3-3
						I	S	r	x	I	S	r	y	
		In.	In.	Lbs.	In. ²	In. ⁴	In. ³	In.	In.	In. ⁴	In. ³	In.	In.	r min.
P.C.B.G.	A 20 R=1/2	6 x 4	7/8	27.2	7.98	27.7	7.2	1.86	2.12	9.8	3.4	1.11	1.12	0.86
P.C.B.G.			3/4	23.6	6.94	24.5	6.2	1.88	2.08	8.7	3.0	1.12	1.08	0.86
P.C.B.G.			5/8	20.0	5.86	21.1	5.3	1.90	2.03	7.5	2.5	1.13	1.03	0.86
P.C.B.G.			7/16	18.1	5.31	19.3	4.8	1.90	2.01	6.9	2.3	1.14	1.01	0.87
P.C.B.G.			1/2	16.2	4.75	17.4	4.3	1.91	1.99	6.3	2.1	1.15	0.99	0.87
P.C.B.G.			9/16	14.3	4.18	15.5	3.8	1.92	1.96	5.6	1.9	1.16	0.96	0.87
P.C.B.G.			5/8	12.3	3.61	13.5	3.3	1.93	1.94	4.9	1.6	1.17	0.94	0.88
P.C.G.			7/16	10.3	3.03	11.4	2.8	1.94	1.92	4.2	1.4	1.17	0.92	0.88
P.C.†B.	A 21 R=1/2	6 x 3 1/2	1/2	15.3	4.50	16.6	4.2	1.92	2.08	4.3	1.6	0.97	0.83	0.76
P.C.B.			5/8	11.7	3.42	12.9	3.2	1.94	2.04	3.3	1.2	0.99	0.79	0.77
P.C.B.			7/16	9.8	2.87	10.9	2.7	1.95	2.01	2.9	1.0	1.00	0.76	0.77
P.C.			1/4	7.9	2.31	8.9	2.2	1.96	1.99	2.3	0.85	1.01	0.74	0.78
P.C.B.G.	A 23 R=3/16	5 x 3 1/2	9/16	19.8	5.81	13.9	4.3	1.55	1.75	5.6	2.2	0.98	1.00	0.75
P.C.B.G.			5/8	16.8	4.92	12.0	3.7	1.56	1.70	4.8	1.9	0.99	0.95	0.75
P.C.B.G.			7/16	13.6	4.00	10.0	3.0	1.58	1.66	4.1	1.6	1.01	0.91	0.75
P.C.B.G.			1/2	12.0	3.53	8.9	2.6	1.59	1.63	3.6	1.4	1.01	0.88	0.76
P.C.B.G.			5/8	10.4	3.05	7.8	2.3	1.60	1.61	3.2	1.2	1.02	0.86	0.76
P.C.B.G.			7/16	8.7	2.56	6.6	1.9	1.61	1.59	2.7	1.0	1.03	0.84	0.76
P.C.G.			1/4	7.0	2.06	5.4	1.6	1.61	1.56	2.2	0.83	1.04	0.81	0.76
P.C.B.S.			1/2	12.8	3.75	9.5	2.9	1.59	1.75	2.6	1.1	0.83	0.75	0.65
P.C.B.S.	A 24 R=3/8	5 x 3	7/16	11.3	3.31	8.4	2.6	1.60	1.73	2.3	1.0	0.84	0.73	0.65
P.C.B.S.			5/8	9.8	2.86	7.4	2.2	1.61	1.70	2.0	0.89	0.84	0.70	0.65
P.C.B.S.			7/16	8.2	2.40	6.3	1.9	1.61	1.68	1.8	0.75	0.85	0.68	0.66
C.S.			1/4	6.6	1.94	5.1	1.5	1.62	1.66	1.4	0.61	0.86	0.66	0.66

*Special gage.

†In Chicago District, length of either or both legs may be exceeded by at least $\frac{1}{16}$ " over permissible over-tolerance.

*When produced in Birmingham District, leg length will exceed standard tolerance.

For key to symbols in first column, refer to page 3.

L
UNEQUAL

L
BULB

T
T
SPLIT

CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

PILING

FLOOR
PLATES

PLATES

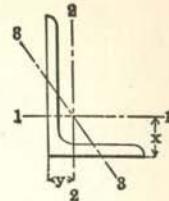
MILL
PRACTICES

INDEX



UNEQUAL ANGLES

PROPERTIES OF SECTIONS

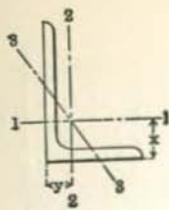


District Rolled	Section Index	Size	Thick- ness	Weight per Foot	Area of Section	Axis 1-1				Axis 2-2				Axis 3-3	
						In.	In.	In.	In. ²	In.	In. ⁴	In.	In. ³	In.	In.
P.C.			$\frac{5}{8}$	14.7	4.30	6.4	2.4	1.22	1.29	4.5	1.8	1.03	1.04	0.72	
P.C.B.			$\frac{1}{2}$	11.9	3.50	5.3	1.9	1.23	1.25	3.8	1.5	1.04	1.00	0.72	
P.C.B.	A 26	$4 \times 3\frac{1}{2}$ $R = \frac{3}{8}$	$\frac{7}{16}$	10.6	3.09	4.8	1.7	1.24	1.23	3.4	1.4	1.05	0.98	0.72	
P.C.B.			$\frac{3}{8}$	9.1	2.67	4.2	1.5	1.25	1.21	3.0	1.2	1.06	0.96	0.73	
P.C.B.			$\frac{5}{16}$	7.7	2.25	3.6	1.3	1.26	1.18	2.6	1.0	1.07	0.93	0.73	
P.C.B.			$\frac{1}{4}$	6.2	1.81	2.9	1.0	1.27	1.16	2.1	0.81	1.07	0.91	0.73	
P.C.B.G.	A 27 $R = \frac{3}{8}$		$\frac{5}{8}$	13.6	3.98	6.0	2.3	1.23	1.37	2.9	1.4	0.85	0.87	0.64	
			$\frac{1}{2}$	11.1	3.25	5.1	1.9	1.25	1.33	2.4	1.1	0.86	0.83	0.64	
			$\frac{7}{16}$	9.8	2.87	4.5	1.7	1.25	1.30	2.2	1.0	0.87	0.80	0.64	
			$\frac{3}{8}$	8.5	2.48	4.0	1.5	1.26	1.28	1.9	0.87	0.88	0.78	0.64	
			$\frac{5}{16}$	7.2	2.09	3.4	1.2	1.27	1.26	1.7	0.73	0.89	0.76	0.65	
			$\frac{1}{4}$	5.8	1.69	2.8	1.0	1.28	1.24	1.4	0.60	0.90	0.74	0.65	
P.C.B.S.G.	A 28 $R = \frac{3}{8}$	$3\frac{1}{2} \times 3$	$\frac{1}{2}$	10.2	3.00	3.5	1.5	1.07	1.13	2.3	1.1	0.88	0.88	0.62	
			$\frac{7}{16}$	9.1	2.65	3.1	1.3	1.08	1.10	2.1	0.98	0.89	0.85	0.62	
			$\frac{3}{8}$	7.9	2.30	2.7	1.1	1.09	1.08	1.9	0.85	0.90	0.83	0.62	
			$\frac{5}{16}$	6.6	1.93	2.3	0.95	1.10	1.06	1.6	0.72	0.90	0.81	0.63	
			$\frac{1}{4}$	5.4	1.56	1.9	0.78	1.11	1.04	1.3	0.59	0.91	0.79	0.63	
			$\frac{1}{2}$	9.4	2.75	3.2	1.4	1.09	1.20	1.4	0.76	0.70	0.70	0.53	
P.C.B.			$\frac{7}{16}$	8.3	2.43	2.9	1.3	1.09	1.18	1.2	0.68	0.71	0.68	0.54	
P.C.B.S.	A 29	$3\frac{1}{2} \times 2\frac{1}{2}$ $R = \frac{5}{16}$	$\frac{3}{8}$	7.2	2.11	2.6	1.1	1.10	1.16	1.1	0.59	0.72	0.66	0.54	
P.C.B.S.			$\frac{5}{16}$	6.1	1.78	2.2	0.93	1.11	1.14	0.94	0.50	0.73	0.64	0.54	
P.C.B.S.			$\frac{1}{4}$	4.9	1.44	1.8	0.75	1.12	1.11	0.78	0.41	0.74	0.61	0.54	
P.C.B.			$\frac{1}{2}$	8.5	2.50	2.1	1.0	0.91	1.00	1.3	0.74	0.72	0.75	0.52	
P.C.B.			$\frac{7}{16}$	7.6	2.21	1.9	0.93	0.92	0.98	1.2	0.66	0.73	0.73	0.52	
P.C.B.S.	A 32	$3 \times 2\frac{1}{2}$ $R = \frac{5}{16}$	$\frac{3}{8}$	6.6	1.92	1.7	0.81	0.93	0.96	1.0	0.58	0.74	0.71	0.52	
P.C.B.S.			$\frac{5}{16}$	5.6	1.62	1.4	0.69	0.94	0.93	0.90	0.49	0.74	0.68	0.53	
P.C.B.S.			$\frac{1}{4}$	4.5	1.31	1.2	0.56	0.95	0.91	0.74	0.40	0.75	0.66	0.53	

*Special gage.

oWhen produced in Birmingham District, leg length will exceed standard tolerance.

For key to symbols in first column, refer to page 3.



UNEQUAL ANGLES

PROPERTIES OF SECTIONS



District Rolled	Section Index	Size	Thickness	Weight per Foot	Area of Section	Axis 1-1				Axis 2-2				Axis 3-3
						I	S	r	x	I	S	r	y	r min.
In.	In.	In.	In. ²	In. ⁴	In. ³	In.	In.	In.	In.	In. ⁴	In. ³	In.	In.	In.
P.C.B.	A 33 R = $\frac{5}{16}$	3 x 2	$\frac{1}{2}$	7.7	2.25	1.9	1.0	0.92	1.08	0.67	0.47	0.55	0.58	0.43
P.C.B.			$\frac{3}{16}$	6.8	2.00	1.7	0.89	0.93	1.06	0.61	0.42	0.55	0.56	0.43
P.C.B.S.			$\frac{5}{16}$	5.9	1.73	1.5	0.78	0.94	1.04	0.54	0.37	0.56	0.54	0.43
P.C.B.S.			$\frac{5}{16}$	5.0	1.47	1.3	0.66	0.95	1.02	0.47	0.32	0.57	0.52	0.43
P.C.B.S.			$\frac{1}{4}$	4.1	1.19	1.1	0.54	0.95	0.99	0.39	0.26	0.57	0.49	0.43
P.C.B.S.			$\frac{5}{16}$	3.07	0.90	0.84	0.41	0.97	0.97	0.31	0.20	0.58	0.47	0.44
P.C.B.S.	$\dagger A 35$ $R = \frac{1}{4}$	$2\frac{1}{2} \times 2$	$\frac{5}{16}$	5.3	1.55	0.91	0.55	0.77	0.83	0.51	0.36	0.58	0.58	0.42
			$\frac{3}{16}$	4.5	1.31	0.79	0.47	0.78	0.81	0.45	0.31	0.58	0.56	0.42
			$\frac{1}{4}$	3.62	1.06	0.65	0.38	0.78	0.79	0.37	0.25	0.59	0.54	0.42
			$\frac{5}{16}$	2.75	0.81	0.51	0.29	0.79	0.76	0.29	0.20	0.60	0.51	0.43
P.C.S.	$\dagger A 48$ $R = \frac{1}{4}$	$2\frac{1}{2} \times 1\frac{1}{2}$	$\frac{5}{16}$	3.92	1.15	0.71	0.44	0.79	0.90	0.19	0.17	0.41	0.40	0.32
			$\frac{3}{16}$	3.19	0.94	0.59	0.36	0.79	0.88	0.16	0.14	0.41	0.38	0.32
			$\frac{5}{16}$	2.44	0.72	0.46	0.28	0.80	0.85	0.13	0.11	0.42	0.35	0.33
P.C.B.S.	$\dagger A 37$ $R = \frac{1}{4}$	$2 \times 1\frac{1}{2}$	$\frac{1}{4}$	2.77	0.81	0.32	0.24	0.62	0.66	0.15	0.14	0.43	0.41	0.32
			$\frac{3}{16}$	2.12	0.62	0.25	0.18	0.63	0.64	0.12	0.11	0.44	0.39	0.32
			$\frac{5}{16}$	1.44	0.42	0.17	0.13	0.64	0.62	0.09	0.08	0.45	0.37	0.33
P.	$\dagger A 645$ $R = \frac{1}{4}$	$2 \times 1\frac{1}{4}$	$\frac{1}{4}$	2.55	0.75	0.30	0.23	0.63	0.71	0.09	0.10	0.34	0.33	0.27
			$\frac{3}{16}$	1.96	0.57	0.23	0.18	0.64	0.69	0.07	0.08	0.35	0.31	0.27
			$\frac{5}{16}$	1.36	0.40	0.17	0.13	0.65	0.65	0.05	0.05	0.36	0.28	0.27
P.C.	$\dagger A 39$ $R = \frac{1}{4}$	$1\frac{3}{4} \times 1\frac{1}{4}$	$\frac{1}{4}$	2.34	0.69	0.20	0.18	0.54	0.60	0.09	0.10	0.35	0.35	0.27
			$\frac{3}{16}$	1.80	0.53	0.16	0.14	0.55	0.58	0.07	0.08	0.36	0.33	0.27
			$\frac{5}{16}$	1.23	0.36	0.11	0.09	0.56	0.56	0.05	0.05	0.37	0.31	0.27

*Special gage.

†Bar size.

For key to symbols in first column, refer to page 3.



CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

FLOOR
PLATES

PLATES

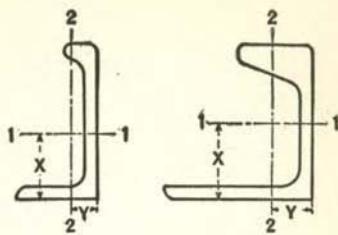
MILL
PRACTICES

INDEX



BULB ANGLES

PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot Lbs.	Area of Section In. ²	Width of Flange In.	Thickness		Axis 1-1				Axis 2-2			
					Web	Flange	I	S	r	x	I	S	r	y
					In.	In.	In. ⁴	In. ³	In.	In.	In. ⁴	In. ³	In.	In.

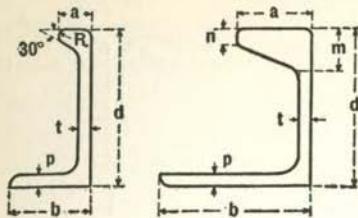
SHIP BUILDING

P.G.	{ BA 313 10 x 3½	32.3 29.9 27.2 24.8 22.4	9.49 8.78 7.98 7.28 6.57	3.69 3.63 3.57 3.51 3.45	.64 .58 .52 .46 .40	.61 .58 .485 .455 .425	118.1 110.7 102.9 95.4 88.0	22.1 20.9 19.6 18.4 17.2	3.53 3.55 3.59 3.62 3.66	4.69 4.70 4.80 4.82 4.85	6.2 5.6 5.1 4.6 4.1	2.2 2.0 1.8 1.6 1.5	0.81 0.80 0.80 0.80 0.79	0.75 0.75 0.72 0.70 0.68
P.	{ BA 312 9 x 3½	23.8 21.6 19.4	7.00 6.35 5.70	3.57 3.51 3.45	.50 .44 .38	.465 .435 .405	73.3 67.7 62.2	15.1 14.1 13.1	3.24 3.27 3.30	4.19 4.21 4.22	4.7 4.2 3.7	1.7 1.5 1.4	0.82 0.82 0.81	0.72 0.70 0.68
P.G.	{ BA 311 8 x 3½	24.3 20.0 16.0	7.14 5.87 4.70	3.68 3.56 3.44	.58 .46 .34	.55 .43 .37	57.0 48.9 40.9	12.7 11.1 9.4	2.83 2.89 2.95	3.53 3.61 3.62	5.2 4.2 3.3	1.9 1.5 1.2	0.85 0.85 0.84	0.78 0.72 0.69
P.	{ BA 309 7 x 3½	21.1 17.1 13.6	6.19 5.03 3.98	3.68 3.56 3.44	.56 .44 .32	.54 .41 .35	37.5 32.0 26.4	9.2 8.0 6.7	2.46 2.52 2.58	2.95 3.03 3.01	4.8 3.9 3.0	1.8 1.4 1.1	0.88 0.88 0.87	0.80 0.74 0.71
P.C.G.	{ BA 307 6 x 3½	17.4 13.9 10.7	5.12 4.06 3.13	3.69 3.57 3.45	.52 .40 .28	.49 .365 .305	22.7 19.0 15.3	6.3 5.3 4.4	2.10 2.16 2.21	2.42 2.47 2.45	4.3 3.4 2.6	1.6 1.2 0.94	0.92 0.91 0.91	0.82 0.76 0.73
P.	{ BA 303 5 x 2½	9.8 7.3	2.88 2.13	2.56 2.44	.36 .24	.33 .27	9.1 7.1	3.1 2.4	1.78 1.83	2.06 2.01	1.1 0.81	0.56 0.42	0.63 0.62	0.55 0.51
P.	BA 145 3 x 2	3.8	1.12	2.00	.19	.19	1.3	0.74	1.09	1.24	0.31	0.20	0.54	0.45

CAR BUILDING

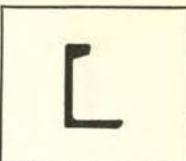
P.C.	BA 125 5 x 4½	19.1	5.64	4.50	.438	.438	20.8	7.9	1.91	2.39	7.9	2.4	1.18	1.23
P.C.	BA 124 5 x 3½	13.0	3.82	3.50	.375	.375	13.5	4.9	1.88	2.22	3.3	1.2	0.92	0.86
P.	BA 122 4 x 3½	14.3	4.21	3.50	.500	.500	8.7	3.7	1.44	1.65	3.9	1.5	0.96	0.99
P.C.B.	BA 123 4 x 3½	11.9	3.48	3.50	.375	.375	7.9	3.5	1.50	1.77	3.1	1.2	0.94	0.94

For key to symbols in first column, refer to page 3.



BULB ANGLES

DIMENSIONS OF SECTIONS



Section Index and Nominal Size	Weight per Foot Lbs.	Flange		Web		Bulb			
		Width b In.	Thickness p In.	Depth d In.	Thickness t In.	Width a In.	Radius R In.	Thickness m In.	Thickness n In.

SHIP BUILDING

BA 313 10 x 3½	32.3	3¾	5/8	10	5/8	11½/16	.40	—	—
	29.9	35/8	9/16	10	9/16	17/8	.40	—	—
	27.2	35/8	1/2	10	1/2	11¾/16	.40	—	—
	24.8	31/2	7/16	10	7/16	13/4	.40	—	—
	22.4	31/2	7/16	10	3/8	11½/16	.40	—	—
BA 312 9 x 3½	23.8	35/8	7/16	9	1/2	111/16	.36	—	—
	21.6	31/2	7/16	9	7/16	15/8	.36	—	—
	19.4	31/2	3/8	9	3/8	1½/16	.36	—	—
BA 311 8 x 3½	24.3	35/8	9/16	8	9/16	15/8	.32	—	—
	20.0	31/2	7/16	8	7/16	11½	.32	—	—
	16.0	31/2	3/8	8	5/16	13/8	.32	—	—
BA 309 7 x 3½	21.1	35/8	9/16	7	9/16	1½	.28	—	—
	17.1	31/2	7/16	7	7/16	13/8	.28	—	—
	13.6	31/2	3/8	7	5/16	1½/4	.28	—	—
BA 307 6 x 3½	17.4	3¾	1/2	6	1/2	15/16	.24	—	—
	13.9	35/8	3/8	6	3/8	13/16	.24	—	—
	10.7	31/2	5/16	6	1/4	1½/16	.24	—	—
BA 303 5 x 2½	9.8	2½	5/16	5	3/8	1	.20	—	—
	7.3	2½	1/4	5	1/4	7/8	.20	—	—
BA 145 3 x 2	3.8	2	3/16	3	3/16	5/16	.25	—	—

CAR BUILDING

BA 125 5 x 4½	19.1	4½	7/16	5	7/16	2½	—	1½/32	5/16
								29/32	5/16
BA 124 5 x 3½	13.0	3½	3/8	5	3/8	1½	—	29/32	5/16
BA 122 4 x 3½	14.3	3½	1/2	4	1/2	1½	—	15/16	1/2
								29/32	1/2
BA 123 4 x 3½	11.9	3½	3/8	4	3/8	1½	—	29/32	1/2



SPLIT

CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

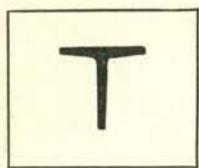
PILING

FLOOR
PLATES

PLATES

MILL
PRACTICES

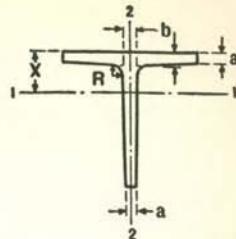
INDEX



TEES

EQUAL AND UNEQUAL

PROPERTIES AND DIMENSIONS OF SECTIONS



District Rolled	Section Index	Weight per Foot	Area of Section	Size					Axis 1-1				Axis 2-2		
				Flange	Stem	Thickness		Radius of Fillet R	I	S	x	x	I	S	x
						Toe a	Root b								
Lbs.	In. ²	In.	In.	In.	In.	In.	In.	In.	In. ⁴	In. ³	In.	In.	In. ⁴	In. ³	In.

EQUAL TEES

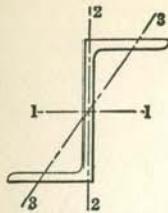
P.C.	T1	13.5	3.97	4	4	$\frac{1}{2}$	$\frac{3}{16}$	$\frac{1}{2}$	5.7	2.0	1.20	1.18	2.8	1.4	0.84
P.C.	T8	7.8	2.27	3	3	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{5}{16}$	1.8	0.86	0.90	0.88	0.90	0.60	0.63
P.C.	T9	6.7	1.95	3	3	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	1.6	0.74	0.90	0.86	0.75	0.50	0.62
P.C.	†T 10	6.4	1.87	$2\frac{1}{2}$	$2\frac{1}{2}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{4}$	1.0	0.59	0.74	0.76	0.52	0.42	0.53
P.C.	†T 11	5.5	1.60	$2\frac{1}{2}$	$2\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{1}{4}$	0.88	0.50	0.74	0.74	0.44	0.35	0.52
P.C.	†T 13	4.1	1.19	$2\frac{1}{4}$	$2\frac{1}{4}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{1}{4}$	0.52	0.32	0.66	0.65	0.25	0.22	0.46
P.C.	†T 14	4.3	1.26	2	2	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{1}{4}$	0.44	0.31	0.59	0.61	0.23	0.23	0.43
P.C.	†T 15	3.62	1.05	2	2	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{1}{4}$	0.37	0.26	0.59	0.59	0.18	0.18	0.42

UNEQUAL TEES

P. {	T 50	13.6	4.00	5	$3\frac{1}{8}$	* $\frac{1}{2}, \frac{13}{32}$	* $\frac{9}{16}, \frac{5}{8}$	$\frac{3}{8}$	2.7	1.1	0.82	0.76	5.2	2.1	1.14
		11.5	3.37	5	3	$\frac{3}{8}, \frac{13}{32}$	$\frac{7}{16}, \frac{5}{8}$	$\frac{3}{8}$	2.4	1.1	0.84	0.76	3.9	1.6	1.10
P.	T 60	11.2	3.29	4	$4\frac{1}{2}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	6.3	2.0	1.39	1.31	2.1	1.1	0.80
P.C.	T 61	9.2	2.68	4	3	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{3}{8}$	2.0	0.90	0.86	0.78	2.1	1.1	0.89
P.	T 62	8.5	2.48	4	$2\frac{1}{2}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{3}{8}$	1.2	0.62	0.69	0.62	2.1	1.0	0.92
P.C.	T 79	6.1	1.77	3	$2\frac{1}{2}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{5}{16}$	0.94	0.52	0.73	0.68	0.75	0.50	0.65

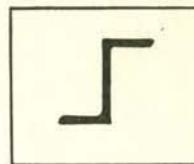
†Bar Size.

*Where two dimensions are shown, the first is for the flange, the second for the stem.
For key to symbols in first column, refer to page 3.



ZEES

PROPERTIES AND DIMENSIONS OF SECTIONS



District Rolled	Section Index	Weight per Foot	Area of Section	Size			Axis 1-1			Axis 2-2			Axis 3-3
				Lbs.	In. ²	In.	In.	In.	In. ⁴	In. ³	In.	In. ⁴	In. ³
P.C. {	Z 1 $R = \frac{5}{16}$	21.1 15.7	6.19 4.59	6 $\frac{1}{8}$ 6	3 $\frac{5}{8}$ 3 $\frac{1}{2}$	$\frac{1}{2}$ $\frac{3}{8}$	34.4 25.3	11.2 8.4	2.36 2.35	12.9 9.1	3.8 2.8	1.44 1.41	0.84 0.83
	Z 5 $R = \frac{5}{16}$	17.9	5.25	5	3 $\frac{1}{4}$	$\frac{1}{2}$	19.2	7.7	1.91	9.1	3.0	1.31	0.74
P.C. {	Z 4 $R = \frac{5}{16}$	16.4 14.0 11.6	4.81 4.10 3.40	5 $\frac{1}{8}$ 5 $\frac{5}{16}$ 5	3 $\frac{3}{8}$ 3 $\frac{5}{16}$ 3 $\frac{1}{4}$	$\frac{7}{16}$ $\frac{3}{8}$ $\frac{5}{16}$	19.1 16.2 13.4	7.4 6.4 5.3	1.99 1.99 1.98	9.2 7.7 6.2	2.9 2.5 2.0	1.38 1.37 1.35	0.77 0.76 0.75
P.C.	Z 8 $R = \frac{5}{16}$	15.9	4.66	4 $\frac{1}{16}$	3 $\frac{1}{8}$	$\frac{1}{2}$	11.2	5.5	1.55	8.0	2.8	1.31	0.67
P.C.B. {	Z 7 $R = \frac{5}{16}$	12.5 10.3 8.2	3.66 3.03 2.41	4 $\frac{1}{8}$ 4 $\frac{1}{16}$ 4	3 $\frac{3}{16}$ 3 $\frac{1}{8}$ 3 $\frac{1}{16}$	$\frac{3}{8}$ $\frac{5}{16}$ $\frac{1}{4}$	9.6 7.9 6.3	4.7 3.9 3.1	1.62 1.62 1.62	6.8 5.5 4.2	2.3 1.8 1.4	1.36 1.34 1.33	0.69 0.68 0.67
P.C.	Z 12 $R = \frac{5}{16}$	12.6	3.69	3	2 $\frac{11}{16}$	$\frac{1}{2}$	4.6	3.1	1.12	4.9	2.0	1.15	0.53
P.C.B.	Z 11 $R = \frac{5}{16}$	9.8	2.86	3	2 $\frac{11}{16}$	$\frac{3}{8}$	3.9	2.6	1.16	3.9	1.6	1.17	0.54
P.C.B.	Z 10 $R = \frac{5}{16}$	6.7	1.97	3	2 $\frac{11}{16}$	$\frac{1}{4}$	2.9	1.9	1.21	2.8	1.1	1.19	0.55

For key to symbols in first column, refer to page 3.



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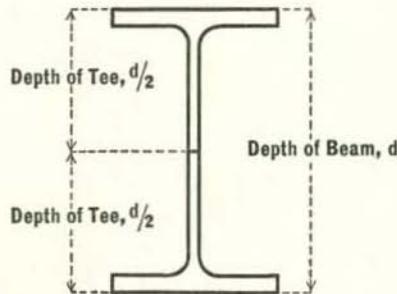
STRUCTURAL TEES

CUT FROM

CB SECTIONS AND STANDARD BEAMS

In addition to sections of rolled tees the following series include sections produced by shearing or gas cutting either standard beams or CB sections.

Generally, any beam or channel section from 3" to 36" in depth can be split to form tees or angles.



The following tolerances, over or under, apply to the depth $d/2$ of the tee or angle which is one-half of the beam or channel depth:

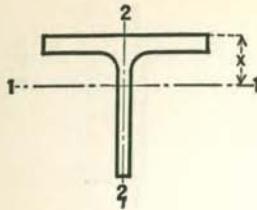
Beams or Channels under 6"	1/8"
Beams or Channels 6" to 15" incl.	3/16"
Beams or Channels over 15" to 20"	1/4"
Beams over 20" to 24"	5/16"
Beams over 24"	3/8"

The above tolerances for depth of tees or angles include the allowable tolerances in depth for the beams or channels before splitting. Tolerances both for dimensions and straightness, as set up for the beams or channels from which these tees or angles are cut, will apply.

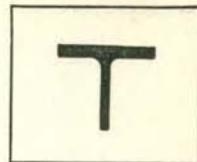
These sections should be ordered either in pairs or so as to utilize all of the beam or channel from which they are produced.

All structural tees or angles are produced in Pittsburgh District only.

STRUCTURAL TEES



CUT FROM
CB SECTIONS



PROPERTIES OF SECTIONS

District Produced	Section Index	Weight per Foot	Area of Section	Depth of Tee	Flange		Stem Thick-ness	Axis 1-1				Axis 2-2		
					Width	Thickness		I	S	r	x	I	S	r
		Lbs.	In. ²	In.	In.	In.	In.	In. ⁴	In. ³	In.	In.	In. ⁴	In. ³	In.
P.	T18 WF	150	44.09	18.36	16.655	1.680	.945	1222.7	85.9	5.27	4.13	612.6	73.6	3.73
	140	41.16	18.25	16.595	1.570	.885	1133.3	79.9	5.25	4.07	563.7	67.9	3.70	
	TCB 18	130	38.28	18.12	16.555	1.440	.845	1059.2	75.4	5.26	4.07	510.3	61.6	3.65
	(CB 362)	122.5	36.01	18.03	16.512	1.350	.802	994.3	71.1	5.25	4.04	472.3	57.2	3.62
		115	33.86	17.94	16.475	1.260	.765	935.8	67.2	5.26	4.02	435.5	52.9	3.59
P.	T18 WF	97	28.56	18.24	12.117	1.260	.770	904.0	67.3	5.63	4.81	177.7	29.3	2.49
	91	26.77	18.16	12.072	1.180	.725	844.0	63.0	5.61	4.77	163.9	27.1	2.47	
	TCB 18	85	24.99	18.08	12.027	1.100	.680	784.7	58.8	5.60	4.74	150.3	25.0	2.45
	(CB 361)	80	23.54	18.00	12.000	1.020	.653	741.0	56.0	5.61	4.76	137.7	22.9	2.42
		75	22.08	17.92	11.972	.940	.625	696.7	53.0	5.62	4.79	125.2	20.9	2.38
P.	T16 WF	120	35.26	16.75	15.865	1.400	.830	822.5	63.2	4.83	3.73	437.2	55.1	3.52
	TCB16.5	110	32.36	16.63	15.810	1.275	.775	754.1	58.4	4.83	3.71	391.2	49.5	3.48
	(CB 332)	100	29.40	16.50	15.750	1.150	.715	683.6	53.3	4.82	3.67	345.8	43.9	3.43
P.	T16 WF	76	22.35	16.75	11.565	1.055	.635	591.9	47.4	5.15	4.26	128.1	22.1	2.39
	TCB16.5	70.5	20.76	16.66	11.535	.960	.605	551.8	44.7	5.16	4.30	114.9	19.9	2.35
	(CB 331)	65	19.13	16.55	11.510	.855	.580	513.0	42.1	5.18	4.37	100.7	17.5	2.29
P.	T15 WF	105	30.89	15.19	15.105	1.315	.775	578.0	48.7	4.33	3.31	354.0	46.9	3.38
	TCB 15	95	27.95	15.06	15.040	1.185	.710	520.4	44.1	4.31	3.26	312.3	41.5	3.34
	(CB 302)	86	25.32	14.94	14.985	1.065	.655	471.0	40.2	4.31	3.23	275.1	36.7	3.30
P.	T15 WF	66	19.41	15.15	10.551	1.000	.615	420.7	37.4	4.66	3.90	92.5	17.5	2.18
	62	18.22	15.08	10.521	.930	.585	394.8	35.3	4.65	3.90	84.8	16.1	2.16	
	TCB 15	58	17.07	15.00	10.500	.850	.564	371.8	33.6	4.67	3.94	76.6	14.6	2.12
	(CB 301)	54	15.88	14.91	10.484	.760	.548	349.5	32.1	4.69	4.03	67.6	12.9	2.06
P.	T13 WF	88.5	26.05	13.655	14.090	1.190	.725	391.8	36.7	3.88	2.97	259.4	36.8	3.16
	TCB13.5	80	23.52	13.54	14.023	1.075	.658	351.4	33.1	3.87	2.91	229.0	32.7	3.12
	(CB 272)	72.5	21.34	13.44	13.965	.975	.600	316.3	29.9	3.85	2.85	203.5	29.1	3.09
P.	T13 WF	57	16.77	13.64	10.070	.932	.570	288.9	28.3	4.15	3.42	74.8	14.9	2.11
	TCB13.5	51	15.01	13.535	10.018	.827	.518	257.7	25.4	4.14	3.39	64.8	12.9	2.08
	(CB 271)	47	13.83	13.455	9.990	.747	.490	238.5	23.7	4.15	3.41	57.5	11.2	2.04
P.	T12 WF	80	23.54	12.36	14.091	1.135	.656	271.6	27.6	3.40	2.51	246.3	35.0	3.23
	TCB 12	72.5	21.31	12.245	14.043	1.020	.608	246.2	25.2	3.40	2.48	217.1	30.9	3.19
	(CB 243)	65	19.13	12.13	14.000	.900	.565	222.6	23.1	3.41	2.47	187.6	26.8	3.13

Section Index in parentheses refers to beam from which tee is cut.
For key to symbols in first column, refer to page 3.

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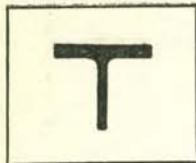
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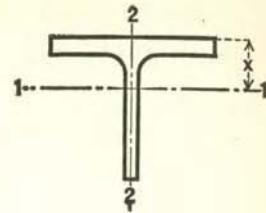
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STRUCTURAL TEES



CUT FROM
CB SECTIONS

PROPERTIES OF SECTIONS

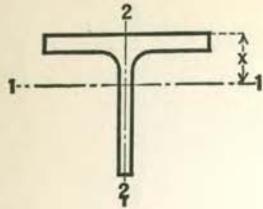


District Produced	Section Index	Weight per Foot	Area of Section	Depth of Tee	Flange		Stem Thickness	Axis 1-1				Axis 2-2		
					Width	Thickness		I	S	r	x	I	S	r
					In.	In.		In.	In.	In.	In.	In.	In.	In.
P. {	T12 WF	60	17.64	12.155	12.088	.930	.556	213.6	22.4	3.48	2.62	127.0	21.0	2.68
	TCB 12	55	16.18	12.08	12.042	.855	.510	195.2	20.5	3.47	2.57	114.5	19.0	2.66
	(CB 242)	50	14.71	12.00	12.000	.775	.468	176.7	18.7	3.46	2.54	101.8	17.0	2.63
P. {	T12 WF	47	13.81	12.145	9.061	.872	.516	185.9	20.3	3.67	2.99	51.1	11.3	1.92
	TCB 12	42	12.35	12.045	9.015	.772	.470	165.9	18.3	3.66	2.97	44.2	9.80	1.89
	(CB 241)	38	11.18	11.955	8.985	.682	.440	151.1	16.9	3.68	3.00	38.3	8.51	1.85
P. {	T10 WF	71	20.89	10.73	13.132	1.095	.659	177.3	20.8	2.91	2.18	193.0	29.4	3.04
	TCB10.5	63.5	18.67	10.62	13.061	.985	.588	155.8	18.3	2.89	2.11	169.3	25.9	3.01
	(CB 213)	56	16.48	10.50	13.000	.865	.527	136.4	16.2	2.88	2.06	144.8	22.3	2.96
P. {	T10 WF	48	14.11	10.57	9.038	.935	.575	137.1	17.1	3.11	2.55	54.7	12.1	1.97
	TCB10.5	41	12.05	10.43	8.962	.795	.499	115.4	14.5	3.09	2.48	44.8	10.0	1.93
	(CB 212)													
P. {	T10 WF	36.5	10.73	10.62	8.295	.740	.455	110.2	13.7	3.21	2.60	33.1	7.98	1.76
	TCB10.5	34	10.01	10.57	8.270	.685	.430	102.8	12.9	3.20	2.59	30.2	7.30	1.74
	(CB 211)	31	9.12	10.495	8.240	.615	.400	93.7	11.9	3.21	2.59	26.6	6.45	1.71
P. {	T9 WF	57	16.77	9.24	11.833	.991	.595	102.6	13.9	2.47	1.85	127.8	21.6	2.76
	TCB 9	52.5	15.45	9.16	11.792	.911	.554	93.9	12.8	2.47	1.82	115.5	19.6	2.73
	(CB 183)	48	14.13	9.08	11.750	.831	.512	85.3	11.7	2.46	1.78	103.4	17.6	2.71
P. {	T9 WF	42.5	12.49	9.16	8.838	.911	.526	84.4	11.9	2.60	2.05	49.7	11.3	2.00
	TCB 9	38.5	11.32	9.08	8.787	.831	.475	75.3	10.6	2.58	1.99	44.3	10.1	1.98
	(CB 182)	35	10.28	9.00	8.750	.751	.438	68.1	9.67	2.57	1.96	39.2	8.97	1.95
P. {	T9 WF	32	9.40	8.935	8.715	.686	.403	61.8	8.82	2.56	1.93	35.2	8.07	1.93
	TCB 9	27.5	8.09	9.06	7.532	.630	.390	59.6	8.63	2.71	2.16	21.0	5.57	1.61
	(CB 181)	25	7.35	9.00	7.500	.570	.358	53.9	7.85	2.71	2.14	18.6	4.96	1.59
P. {	T8 WF	48	14.13	8.16	11.533	.875	.535	64.7	9.82	2.14	1.57	103.6	18.0	2.71
	TCB 8	44	12.95	8.08	11.502	.795	.504	59.5	9.11	2.14	1.55	92.6	16.1	2.67
	(CB 163)													
P. {	T8 WF	39	11.46	8.16	8.586	.875	.529	60.0	9.45	2.28	1.81	43.8	10.2	1.95
	TCB 8	35.5	10.43	8.08	8.543	.795	.486	54.0	8.57	2.28	1.77	38.9	9.11	1.93
	(CB 162)	32	9.40	8.00	8.500	.715	.443	48.3	7.71	2.27	1.73	34.2	8.05	1.91
P. {	T8 WF	29	8.52	7.93	8.464	.645	.407	43.6	7.00	2.26	1.70	30.2	7.14	1.88
	TCB 8	25	7.35	8.125	7.073	.628	.380	42.2	6.77	2.40	1.89	17.4	4.92	1.54
	(CB 161)	22.5	6.62	8.06	7.039	.563	.346	37.8	6.10	2.39	1.87	15.2	4.33	1.52
P. {	T8 WF	20	5.88	8.00	7.000	.503	.307	33.2	5.37	2.37	1.82	13.3	3.79	1.50
	TCB 8	18	5.30	7.93	6.992	.428	.299	30.7	5.10	2.41	1.90	11.1	3.17	1.45

Section index in parentheses refers to beam from which tee is cut.

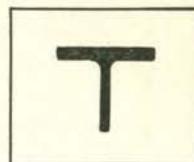
For key to symbols in first column, refer to page 3.

STRUCTURAL TEES



CUT FROM
CB SECTIONS

PROPERTIES OF SECTIONS



District Produced	Section Index	Weight per Foot	Area of Section	Depth of Tee	Flange		Stem Thickness	Axis 1-1				Axis 2-2		
					Width	Thickness		In.	In.	In.	In.	In.	In.	
P.	T 7 WF TCB 7 (CB 146)	105.5	31.04	7.875	15.800	1.563	.980	102.2	16.2	1.81	1.57	514.3	65.1	4.07
		101	29.70	7.815	15.750	1.503	.930	95.7	15.2	1.80	1.53	489.8	62.2	4.06
		96.5	28.36	7.75	15.710	1.438	.890	90.1	14.4	1.78	1.49	465.1	59.2	4.05
		92	27.04	7.69	15.660	1.378	.840	83.9	13.4	1.76	1.45	441.4	56.4	4.04
		88	25.87	7.625	15.640	1.313	.820	80.2	12.9	1.76	1.42	418.9	53.6	4.02
		83.5	24.55	7.56	15.600	1.248	.780	75.0	12.1	1.75	1.39	395.1	50.7	4.01
		79	23.24	7.50	15.550	1.188	.730	69.3	11.3	1.73	1.34	372.5	47.9	4.00
		75	22.04	7.44	15.515	1.128	.695	64.9	10.6	1.72	1.31	351.3	45.3	3.99
		71	20.92	7.375	15.500	1.063	.680	62.1	10.2	1.72	1.29	330.1	42.6	3.97
P.	T 7 WF TCB 7 (CB 145)	68	19.99	7.375	14.740	1.063	.660	60.0	9.89	1.73	1.31	283.9	38.5	3.77
		63.5	18.67	7.31	14.690	.998	.610	54.7	9.04	1.71	1.26	263.8	35.9	3.76
		59.5	17.49	7.25	14.650	.938	.570	50.4	8.36	1.70	1.22	245.9	33.6	3.75
		55.5	16.33	7.185	14.620	.873	.540	46.7	7.80	1.69	1.19	227.4	31.1	3.73
		51.5	15.13	7.125	14.575	.813	.495	42.4	7.10	1.67	1.15	209.9	28.8	3.72
		47.5	13.97	7.06	14.545	.748	.465	39.1	6.58	1.67	1.12	191.9	26.4	3.71
P.	T 7 WF TCB 7 (CB 144)	43.5	12.78	7.00	14.500	.688	.420	34.9	5.88	1.65	1.08	174.8	24.1	3.70
		42	12.36	7.09	12.023	.778	.451	37.4	6.36	1.74	1.21	112.7	18.8	3.02
		39	11.47	7.03	12.000	.718	.428	34.8	5.96	1.74	1.19	103.5	17.2	3.00
		37	10.88	7.095	10.072	.783	.450	36.1	6.26	1.82	1.32	66.7	13.3	2.48
P.	T 7 WF TCB 7 (CB 143)	34	10.00	7.03	10.040	.718	.418	33.0	5.74	1.81	1.29	60.6	12.1	2.46
		30.5	8.97	6.955	10.000	.643	.378	29.2	5.13	1.80	1.25	53.6	10.7	2.45
		26.5	7.79	6.97	8.062	.658	.370	27.7	4.95	1.88	1.38	28.8	7.14	1.92
P.	T 7 WF TCB 7 (CB 142)	24	7.06	6.905	8.031	.593	.339	24.9	4.49	1.88	1.35	25.6	6.38	1.91
		21.5	6.32	6.84	8.000	.528	.308	22.2	4.02	1.87	1.33	22.6	5.64	1.89
		19	5.59	7.06	6.776	.513	.313	23.5	4.27	2.05	1.56	12.3	3.64	1.49
P.	T 7 WF TCB 7 (CB 141)	17	5.00	7.00	6.750	.453	.287	21.1	3.86	2.05	1.55	10.6	3.15	1.46
		15	4.41	6.93	6.733	.383	.270	19.0	3.55	2.08	1.59	8.77	2.61	1.41
		80.5	23.69	6.94	12.515	1.486	.905	62.6	11.5	1.63	1.47	243.1	38.9	3.20
P.	T 6 WF TCB 6 (CB 124)	66.5	19.56	6.69	12.365	1.236	.755	48.4	9.03	1.57	1.33	195.0	31.5	3.16
		60	17.65	6.56	12.320	1.106	.710	43.4	8.22	1.57	1.28	172.5	28.0	3.13
		53	15.59	6.44	12.230	.986	.620	36.7	7.01	1.53	1.20	150.4	24.6	3.11
		49.5	14.54	6.375	12.190	.921	.580	33.7	6.46	1.52	1.16	139.1	22.8	3.09
		46	13.53	6.31	12.155	.856	.545	31.0	5.98	1.51	1.13	128.2	21.1	3.08
		42.5	12.49	6.25	12.105	.796	.495	27.8	5.38	1.49	1.08	117.7	19.5	3.07
		39.5	11.61	6.19	12.080	.736	.470	25.8	5.02	1.48	1.06	108.2	17.9	3.05
		36	10.58	6.125	12.040	.671	.430	23.1	4.53	1.48	1.02	97.6	16.2	3.04
		32.5	9.55	6.06	12.000	.606	.390	20.6	4.06	1.47	.98	87.3	14.6	3.02

Section Index in parentheses refers to beam from which tee is cut.

For key to symbols in first column, refer to page 3.

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PLATES

PLATES

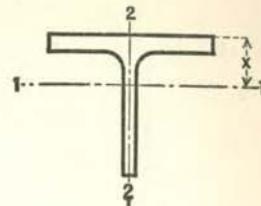
MILL
PRACTICES

STRUCTURAL TEES



CUT FROM CB SECTIONS

PROPERTIES OF SECTIONS



District Produced	Section Index	Weight per Foot	Area of Section	Depth of Tee	Flange		Stem Thickness	Axis 1-1				Axis 2-2		
					Width	Thickness		In.	In.	In.	In.	In.	In.	
P.	T 6 WF	29	8.53	6.095	10.014	.641	.359	19.0	3.75	1.49	1.03	53.7	10.7	2.51
	TCB 6 (CB 123)	26.5	7.80	6.03	10.000	.576	.345	17.7	3.54	1.51	1.02	48.0	9.60	2.48
P.	T 6 WF	25	7.36	6.095	8.077	.641	.371	18.7	3.80	1.60	1.17	28.2	6.98	1.96
	TCB 6 (CB 122)	22.5	6.62	6.03	8.042	.576	.336	16.6	3.40	1.59	1.13	25.0	6.20	1.94
P.	T 6 WF	18	5.29	6.12	6.565	.540	.305	15.3	3.14	1.70	1.26	11.9	3.62	1.50
	TCB 6 (CB 121)	15.5	4.56	6.045	6.525	.465	.265	13.0	2.69	1.69	1.22	9.91	3.04	1.47
	TCBL 6 (CBL 12)	13.5	3.99	5.980	6.500	.400	.240	11.4	2.39	1.69	1.21	8.30	2.55	1.44
P.	T 6 WF	11	3.24	6.16	4.030	.424	.260	11.7	2.58	1.90	1.63	2.27	1.13	.84
	TCBL 6 (CBL 12)	9.5	2.81	6.08	4.010	.349	.240	10.2	2.32	1.91	1.67	1.84	.92	.81
	TCBJ 6 (CBJ 12)	8.25	2.43	6.00	4.000	.269	.230	9.02	2.13	1.93	1.76	1.39	.70	.76
P.	T 6 WF	56	16.46	5.69	10.415	1.248	.755	28.8	6.42	1.32	1.21	117.7	22.6	2.67
	TCB 5 (CB 103)	50	14.72	5.56	10.345	1.118	.685	24.8	5.62	1.30	1.14	103.3	20.0	2.65
	T 5 WF	44.5	13.09	5.44	10.275	.998	.615	21.3	4.88	1.28	1.07	90.3	17.6	2.63
	TCB 5 (CB 103)	38.5	11.33	5.31	10.195	.868	.535	17.7	4.10	1.25	1.00	76.7	15.1	2.60
	T 5 WF	36	10.59	5.25	10.170	.808	.510	16.4	3.83	1.24	.97	70.9	13.9	2.59
	TCB 5 (CB 103)	33	9.70	5.19	10.117	.748	.457	14.5	3.39	1.22	.92	64.6	12.8	2.58
	T 5 WF	30	8.83	5.125	10.075	.683	.415	12.8	3.02	1.21	.88	58.2	11.6	2.57
	TCB 5 (CB 103)	27	7.94	5.06	10.028	.618	.368	11.2	2.64	1.18	.84	51.95	10.4	2.56
	T 5 WF	24.5	7.20	5.00	10.000	.558	.340	10.1	2.40	1.18	.81	46.5	9.30	2.54
	TCB 5 (CB 103)	22.5	6.62	5.06	8.022	.618	.350	10.3	2.48	1.25	.91	26.6	6.63	2.00
P.	T 5 WF	19.5	5.74	4.97	7.990	.528	.318	8.96	2.19	1.25	.88	22.5	5.62	1.98
	TCB 5 (CB 102)	16.5	4.85	4.875	7.964	.433	.292	7.80	1.95	1.27	.88	18.2	4.58	1.94
	T 5 WF	14.5	4.27	5.11	5.799	.500	.289	8.38	2.07	1.40	1.05	7.61	2.62	1.34
P.	TCB 5 (CB 101)	12.5	3.67	5.04	5.762	.430	.252	7.12	1.77	1.39	1.02	6.34	2.20	1.31
	T 5 WF	10.5	3.10	4.95	5.750	.340	.240	6.31	1.62	1.43	1.06	4.87	1.69	1.25
	TCB 5 (CB 101)	9.50	2.80	5.13	4.020	.394	.250	6.70	1.74	1.55	1.28	2.09	1.04	.86
P.	TCBL 5 (CBL 10)	8.50	2.49	5.06	4.010	.329	.240	6.07	1.62	1.56	1.32	1.73	.86	.83
	TCBL 5 (CBL 10)	7.50	2.20	5.00	4.000	.269	.230	5.46	1.50	1.57	1.37	1.39	.70	.80
P.	TCBJ 5 (CBJ 10)	5.75	1.69	4.94	3.950	.204	.180	4.15	1.16	1.57	1.35	1.00	.51	.77

Section Index in parentheses refers to beam from which tee is cut.

For key to symbols in first column, refer to page 3.

STRUCTURAL TEES

CUT FROM

**CB SECTIONS AND
STANDARD BEAMS**



PROPERTIES OF SECTIONS

District Produced	Section Index	Weight per Foot	Area of Section	Depth of Tee	Flange		Stem Thickness	Axis 1-1				Axis 2-2			
					Width	Thickness		In.	In.	In.	In.	In.	In.	In.	
P.	T 4 WF TCB 4 (CB 83)	33.5	9.85	4.50	8.287	.933	.575	10.94	3.07	1.05	.94	44.3	10.7	2.12	
		29	8.53	4.375	8.222	.808	.510	9.11	2.60	1.03	.87	37.50	9.10	2.10	
		24	7.06	4.25	8.117	.683	.405	6.92	2.00	.99	.78	30.45	7.50	2.08	
		20	5.88	4.125	8.077	.558	.365	5.80	1.71	.99	.74	24.50	6.05	2.04	
		17.5	5.15	4.06	8.027	.493	.315	4.88	1.45	.97	.69	21.25	5.30	2.03	
P.	T 4 WF TCB 4 (CB 82)	15.5	4.56	4.00	8.000	.433	.288	4.31	1.30	.97	.67	18.50	4.60	2.01	
		14	4.11	4.03	6.540	.463	.285	4.22	1.28	1.01	.73	10.8	3.30	1.62	
		12	3.53	3.965	6.500	.398	.245	3.53	1.08	1.00	.70	9.10	2.80	1.61	
P.	T 4 WF TCB 4 (CB 81)	10	2.94	4.07	5.268	.378	.248	3.66	1.13	1.12	.83	4.25	1.61	1.20	
		8.5	2.50	4.00	5.250	.308	.230	3.21	1.01	1.13	.84	3.36	1.28	1.16	
P.	TCBL 4 (CBL 8)	7.50	2.22	4.06	4.015	.314	.245	3.29	1.07	1.22	1.00	1.65	.82	.86	
		6.50	1.91	4.00	4.000	.254	.230	2.90	.98	1.23	1.03	1.31	.66	.83	
P.	TCBJ 4 (CBJ 8)	5.00	1.48	3.95	3.940	.204	.170	2.15	.72	1.21	.96	1.00	.51	.82	
		8.00	2.36	3.13	4.030	.404	.260	1.66	.68	.84	.67	2.16	1.07	.96	
P.	TCBL 3 (CBL 6)	6.00	1.77	3.00	4.000	.279	.230	1.30	.56	.86	.67	1.44	.72	.90	
		4.25	1.25	2.92	3.940	.194	.170	.90	.40	.85	.64	.94	.48	.87	
P.	TB 6 (B 8)	25	7.35	6.00	5.477	.660	.687	25.2	6.05	1.85	1.84	7.85	2.87	1.03	
		20.4	5.99	6.00	5.250	.660	.460	18.8	4.26	1.77	1.57	6.77	2.58	1.06	
P.	TB 6 (B 9)	17.5	5.14	6.00	5.078	.544	.428	17.2	3.95	1.83	1.65	4.93	1.94	.98	
		15.9	4.67	6.00	5.000	.544	.350	14.9	3.31	1.78	1.51	4.68	1.87	1.00	
P.	TB 5 (B 10)	17.5	5.15	5.00	4.944	.491	.594	12.5	3.63	1.56	1.56	4.18	1.69	.90	
		12.7	3.73	5.00	4.660	.491	.310	7.81	2.05	1.45	1.20	3.39	1.46	.95	
P.	TB 4 (B 12)	11.5	3.38	4.00	4.171	.425	.441	3.50	1.77	1.22	1.15	2.15	1.03	.80	
		9.2	2.70	4.00	4.000	.425	.270	3.50	1.14	1.14	.94	1.86	.93	.83	
P.	TB 3.5 (B 13)	10	2.94	3.50	3.860	.392	.450	3.36	1.36	1.07	1.04	1.58	.82	.73	
		7.65	2.24	3.50	3.660	.392	.250	2.18	.81	.99	.81	1.32	.72	.77	
P.	TB 3 (B 14)	8.625	2.53	3.00	3.565	.359	.465	2.13	1.02	.92	.91	1.15	.65	.67	
		6.25	1.83	3.00	3.330	.359	.230	1.27	.55	.83	.69	.93	.56	.71	

Section Index in parentheses refers to beam from which tee is cut.

For key to symbols in first column, refer to page 3.

CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

PILING

FLOOR
PLATES

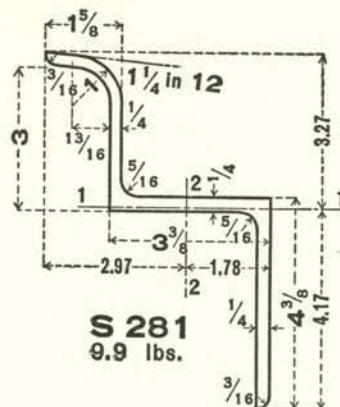
PLATES

MILL
PRACTICES

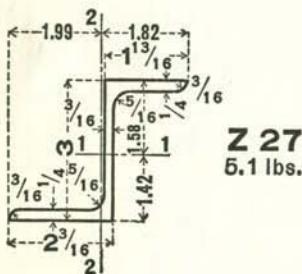
INDEX

MISCELLANEOUS CAR BUILDING SECTIONS

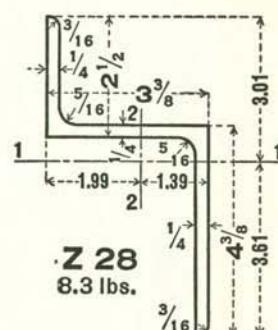
W SIDE PLATE SECTION



SIDE POST SECTION



SIDE PLATE SECTION

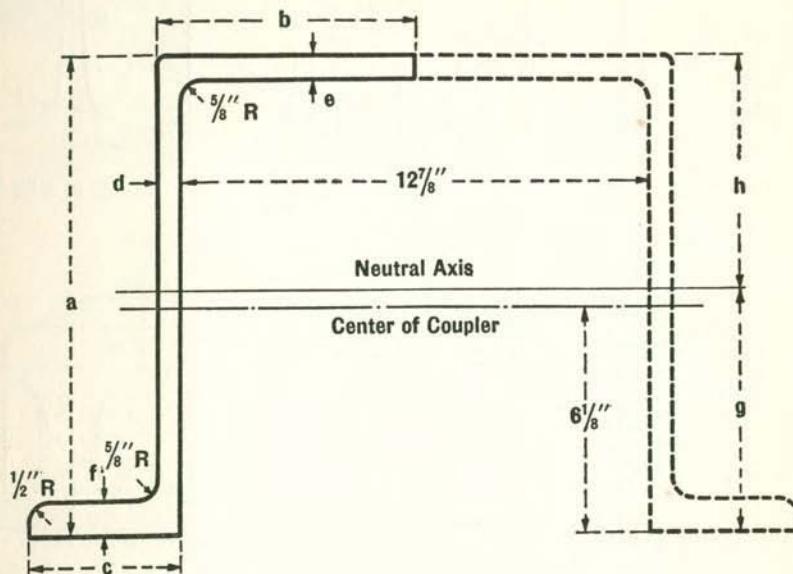


District Rolled	Section Index	Depth	Weight per Foot	Area	Axis 1-1		Axis 2-2	
					In.	In. ²	In.	In. ²
		In.	Lbs.	In. ²	In. ⁴	In. ²	In. ⁴	In. ²
P.C.	S 281	7 7/16	9.9	2.89	11.26	2.70	6.94	2.34
P.C.B.	Z 27	3	5.10	1.50	2.13	1.34	1.16	0.58
P.C.	Z 28	3 3/8	8.30	2.44	6.53	1.81	4.48	2.25

For key to symbols in first column, refer to page 3.

MISCELLANEOUS CAR BUILDING SECTIONS

CENTER SILL SECTION Z26



SECTION AS ROLLED

District Rolled	Section Index	Weight	Area	a	b	c	d	e	f
		per Foot	of Section						
P.C.G.	Z-26	51.2	15.06	13 1/16	7 1/32	4 3/16	19/32	19/32	15/16
		41.2	12.12	12 15/16	6 29/32	4 1/16	15/32	15/32	13/16
		36.2	10.65	12 7/8	6 27/32	4	13/32	13/32	3/4
		31.3	9.20	12 13/16	6 25/32	3 15/16	11/32	11/32	1 1/16

For Key to symbols in first column, refer to page 3.

DATA FOR COMPLETE SILL (TWO Z-26 SECTIONS)

Weight per Foot	Area	Moment of Inertia	Section Modulus		End Ratio		g	h
			Top	Bottom	Top	Bottom		
			In. ³	In. ³	In.	In.		
102.4	30.12	771.4	122.8	113.8	.0279	.0390	6.780	6.283
82.4	24.24	626.0	98.6	95.0	.0366	.0461	6.588	6.349
72.4	21.30	552.2	86.1	85.5	.0431	.0509	6.458	6.417
62.6	18.40	481.7	74.1	76.3	.0517	.0568	6.315	6.498

CAR
SECTIONS

CRANE
RAILS

CORRUG.
SHEETS

PILING

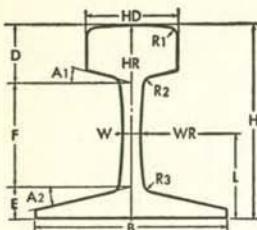
FLOOR
PLATES

PLATES

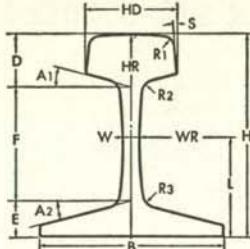
MILL
PRACTICES

INDEX

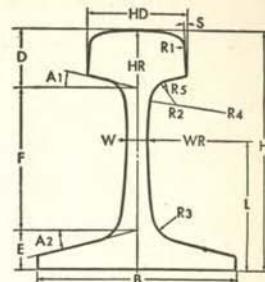
CRANE RAILS



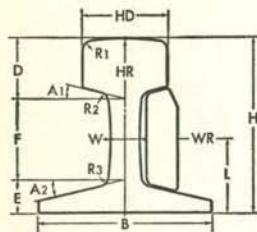
A.S.C.E.-A.R.E.A. 100 LB.



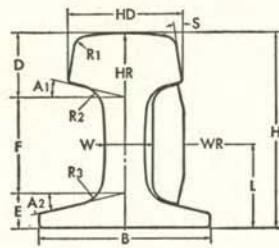
A.R.A. SERIES A & B 100 LB.



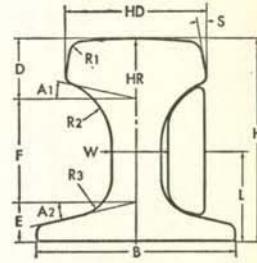
A.R.E.A. 115 & 132 LB.



C.I.S.-105 LB. with Splice Bar



C.I.S.-135 LB. with Splice Bar

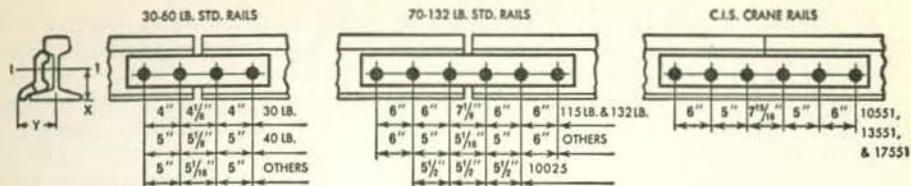


C.I.S.-175 LB. with Splice Bar

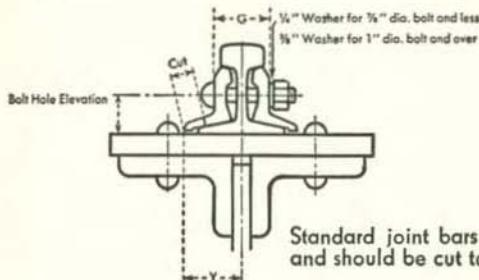
District Rolled	Weight per Yd. and Type	Section Index	Dimensions, Inches														
			H	Depth	Base Width	Head Width	Web (min.)	Head Depth	Fishing (Web Depth)	Base Thickness	Head Angle Base Angle	Slope of Head	¶ of Web Radius	Head Radius	Web Radius	Head Fillet Radius	Web Fillet Rad. Top
PCB	30 lb. A.S.C.E.	3040	3 1/8	3 1/8	11 1/16	21 1/64	7/8	12 3/8	17 1/8	13°	str.	125/64	12	12	5 1/16	1 1/4	1 1/4
B	40 lb. A.R.A.-B	4030	3 3/8	6 1/2	13 1/16	15 1/64	3/8	11 1/64	15 5/64	13°	4°	17 1/128	12	12	5 1/16	1 1/4	1 1/4
PC	40 lb. A.S.C.E.	4040	3 1/2	3 1/2	17 1/8	25 1/64	11 1/64	15 5/64	5 5/8	13°	str.	17 1/128	12	12	5 1/16	1 1/4	1 1/4
PCB	60 lb. A.S.C.E.	6040	4 1/4	4 1/4	23 1/8	31 1/64	17 1/32	21 7/64	49/64	13°	str.	11 1/128	12	12	5 1/16	1 1/4	1 1/4
PC	70 lb. A.S.C.E.	7040	4 5/8	4 5/8	27 1/16	33 1/64	11 1/32	21 5/64	19 1/16	13°	str.	23 1/64	12	12	5 1/16	1 1/4	1 1/4
PCB	80 lb. A.S.C.E.	8040	5	5	21 1/2	35 1/64	1 1/2	25 1/8	7 1/8	13°	str.	23 1/16	12	12	5 1/16	1 1/4	1 1/4
PCB	85 lb. A.S.C.E.	8540	5 1/16	5 1/16	29 1/16	9 1/16	15 1/64	23 1/8	57/64	13°	str.	21 1/64	12	12	5 1/16	1 1/4	1 1/4
PCB	90 lb. A.R.A.-A	9020	5 5/8	5 1/8	29 1/16	9 1/16	1 1/16	33 1/32	1	1:4	1:16	29 1/32	14	14	3 9/16	3 3/8	3 3/8
PC	90 lb. A.S.C.E.	9040	5 3/8	5 3/8	25 1/8	9 1/16	1 19/32	25 5/64	59/64	13°	str.	24 1/128	12	12	5 1/16	1 1/4	1 1/4
PC	100 lb. A.R.A.-A	10020	6	5 1/2	23 3/4	9 1/16	19 1/16	33 8/32	11 1/16	1:4	1:16	21 5/16	14	14	3 9/16	3 3/8	3 3/8
CB	100 lb. A.R.E.A.	10025	6	5 3/8	21 1/16	9 1/16	21 1/32	39 1/32	1 1/16	1:4	1:16	23 1/32	14	14	3 9/16	3 3/8	5 1/8
PCB	100 lb. A.R.A.-B	10030	5 41/64	59/64	22 1/32	9 1/16	1 45/64	25 5/64	15 64/64	13°	3°	20 5/128	12	12	3 9/16	5 1/16	5 1/16
PC	100 lb. A.S.C.E.	10040	5 3/4	5 3/4	23 1/4	9 1/16	1 45/64	35 5/64	31 1/32	13°	str.	26 5/128	12	12	5 1/16	1 1/4	1 1/4
PC	105 lb. C.I.S.	10551	5 3/16	5 5/16	29 1/16	15 1/16	1 25/32	21 13/32	1	13°	str.	21 3/64	12	12	5 1/16	1 1/4	1 1/4
PCB	115 lb. A.R.E.A.	11525	6 5/8	5 1/2	22 3/32	5 5/8	11 1/16	31 3/16	11 1/8	1:4	1:40	31 1/4	10 & 1	14	3 9/16	3 3/4	3 3/4
PCB	132 lb. A.R.E.A.	13225	7 1/8	6	3	21 1/32	13 1/4	43 1/16	13 1/16	1:4	1:40	3 7/8	10 & 1	16	3 9/16	7/8	5 1/16
C	135 lb. C.I.S.	13551	5 3/4	5 5/16	37 1/16	11 1/4	17 1/8	21 3/16	11 1/16	13°	10°	21 5/32	14	12	7 1/16	3 3/4	3 3/4
C	175 lb. C.I.S.	17551	6	4 1/4	11 1/2	13 1/4	3 7/64	1 1/64	12°	10°	...	18	cc	7 1/16	2	11 1/8	5 1/16

For key to symbols in first column refer to page 3.

CRANE RAIL SPLICES



Detailed drawings covering punching and drilling will be furnished on request.



Standard joint bars are used for crane rails
and should be cut to clear rivets, if necessary.

For New Work and Major Repairs the following Rail Sections are recommended—

Pittsburgh District—4040, 6040, 8540, 10551, 13551 and 17551.

Chicago District—4040, 6040, 8540, 10551, 13551 and 17551.

Birmingham District—3040, 4030, 6040, 8540, 9020, 10025, 10551, 13551 and 17551.

Section Index	Bolt Hole Elevation	RAIL			JOINT BAR					BOLTS			
		Properties			Dimensions, Inches					Dimensions, In.			
		Gross Area	Axis I-I Parallel to Base		Section Index	Length	Size of Hole	To Toe of Joint Bar	Cut From Joint Bar	Diameter	G	Bolt Grip	Length
I	In. ²	In. ⁴	S	In. ²	N.A. from base x	In.	Y						
3040	1 $\frac{25}{64}$	3.00	4.1	2.5	1.52	S 3040	16 $\frac{1}{8}$	1 $\frac{15}{16}$ x 3 $\frac{1}{16}$	2	9 $\frac{1}{16}$	5/8	11 $\frac{1}{16}$	2 $\frac{3}{4}$
4030	1 $\frac{7}{12}$	3.92	7.1	3.4	1.67	S 4040	20	1 $\frac{15}{16}$ x 1 $\frac{1}{8}$	2 $\frac{3}{16}$	3/4	3/4	1 $\frac{15}{16}$	3 $\frac{3}{4}$
4040	1 $\frac{7}{12}$	3.94	6.6	3.6	1.68	S 4040	20	1 $\frac{15}{16}$ x 1 $\frac{1}{8}$	2 $\frac{3}{16}$	9 $\frac{1}{16}$	3/4	1 $\frac{15}{16}$	3 $\frac{3}{4}$
6040	1 $\frac{11}{16}$	5.93	14.6	6.6	2.05	S 6040	24	1 $\frac{15}{16}$ x 1 $\frac{1}{8}$	2 $\frac{11}{16}$	11 $\frac{1}{16}$	3/4	2 $\frac{1}{16}$	37 $\frac{3}{8}$
7040	2 $\frac{9}{64}$	6.81	19.7	8.2	2.22	S 7040	34	3/8 x 1 $\frac{1}{8}$	2 $\frac{15}{16}$	3/4	3/4	2 $\frac{7}{16}$	4 $\frac{1}{8}$
8040	2 $\frac{9}{16}$	7.86	26.4	10.1	2.38	Confer
8540	2 $\frac{17}{64}$	8.33	30.1	11.1	2.47	*S 8540	34	1 x 1 $\frac{1}{4}$	3 $\frac{11}{32}$	7/8	7/8	3 $\frac{5}{32}$	4 $\frac{1}{2}$
9020	2 $\frac{97}{64}$	8.82	38.7	12.6	2.54	*S 9020	34	1 $\frac{1}{8}$ x 1 $\frac{1}{8}$	3 $\frac{13}{16}$	1 $\frac{1}{8}$	3 $\frac{9}{16}$	4 $\frac{1}{8}$	
9040	2 $\frac{45}{128}$	8.83	34.4	12.2	2.55	S 9040	34	1 $\frac{1}{8}$ x 1 $\frac{1}{8}$	3 $\frac{7}{16}$	7/8	1	3 $\frac{1}{4}$	4 $\frac{3}{4}$
10020	2 $\frac{9}{4}$	9.84	48.9	15.0	2.75	S 10020	34	1 $\frac{1}{8}$ x 1 $\frac{1}{8}$	4 $\frac{1}{16}$	1 $\frac{1}{16}$	1	3 $\frac{7}{16}$	4 $\frac{7}{8}$
10025	2 $\frac{45}{64}$	9.95	49.0	15.1	2.75	Confer
10030	2 $\frac{65}{128}$	9.85	41.3	13.7	2.63	Confer
10040	2 $\frac{65}{128}$	9.84	44.0	14.6	2.73	S 10040	34	1 $\frac{1}{8}$ x 1 $\frac{1}{8}$	3 $\frac{5}{8}$	7/8	1	3 $\frac{7}{16}$	4 $\frac{7}{8}$
10551	2 $\frac{13}{64}$	10.30	34.4	12.4	2.41	S 10551	34	1 $\frac{15}{16}$ Round	7/8	3 $\frac{9}{8}$	4 $\frac{3}{4}$
11525	2 $\frac{7}{8}$	11.25	65.6	18.0	2.98	Confer
13225	3 $\frac{3}{8}$	12.95	88.2	22.5	3.20	Confer
13551	2 $\frac{15}{64}$	13.32	50.6	17.2	2.81	S 13551	34	1 $\frac{15}{16}$ Round	1 $\frac{1}{8}$	3 $\frac{3}{8}$	5 $\frac{1}{2}$
17551	2 $\frac{21}{64}$	17.12	70.2	23.3	3.02	S 17551	34	1 $\frac{15}{16}$ Round	1 $\frac{1}{8}$	4 $\frac{1}{8}$	6

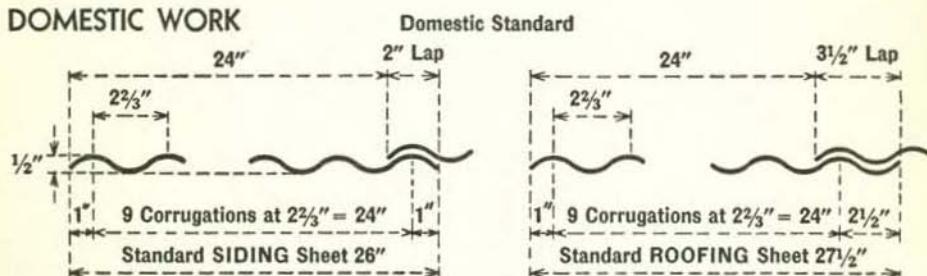
*Not produced in Birmingham District.

CORRUGATED SHEET CONSTRUCTION

Corrugated sheets, in addition to their extensive application as roofing and siding for buildings, are adaptable to other uses such as lining of shafts, supports and forms for floor arches, partitions, enclosures and culverts.

Corrugated sheets are available in steel of regular analysis or in rust-resisting alloys, usually copper bearing steel, either black (unpainted mill finish), painted or galvanized. Although the mills offer a wide choice in types and widths of corrugations, the curved type is generally used. General practice is to furnish in even foot lengths ranging from 60" to 144".

DOMESTIC WORK



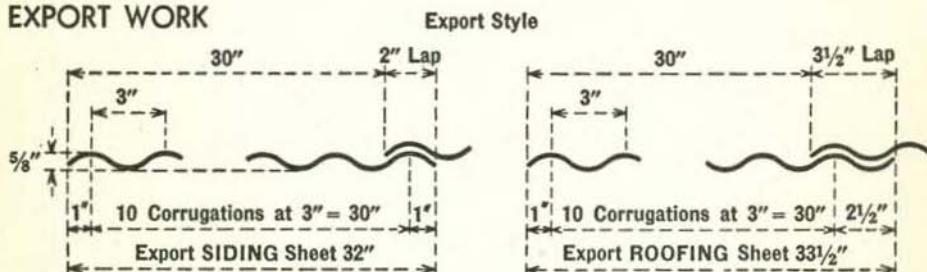
Nominal 2 1/2" widths of corrugation (actual 2 2/3") are preferred for domestic work.

Siding sheets are 26" wide after corrugating, with both edges turned the same way. They are laid with one corrugation side lap as shown in sketch and minimum end lap of 4".

Roofing sheets are 27 1/2" wide after corrugating with one edge turned up and the other down. They are laid with 1 1/2 corrugations side lap as shown in sketch. A minimum end lap of 6" should be used for roof pitch of 4 in 12 or over and 8" for roof of less pitch. Corrugated steel roofing is seldom used for roof pitch under 3 in 12.

Both siding and roofing sheets cover approximately 24" net width.

EXPORT WORK



Nominal 3" widths of corrugation are generally used for export work.

Siding sheets are 32" wide after corrugating, with both edges turned the same way.

Roofing sheets are 33 1/2" wide after corrugating, with 1 edge turned up and the other turned down.

Both siding and roofing cover approximately 30" net width.

Sheet steel flashing must be provided at roof ridge, eaves, windows and wherever necessary to insure watertight results.

CORRUGATED SHEET CONSTRUCTION

STANDARD 2½" CORRUGATED

Black			Galvanized					Maximum Span Between Supports		
Manufacturers Standard Gage		Corrugated Pounds per Sq. Ft.	Galvanized Sheet Gage			Corrugated Pounds per Sq. Ft.				
Gage No.	Pounds per Sq. Ft.	Approx. Thick. Inches	26"	27½"	Sheet Gage	26"	27½"	Roofing	Siding	
12	4.38	.105	4.71	4.77	12	4.53	.109	4.88	4.94	
14	3.13	.075	3.37	3.41	14	3.28	.079	3.53	3.58	
16	2.50	.060	2.69	2.73	16	2.66	.064	2.86	2.90	
18	2.00	.048	2.15	2.18	18	2.16	.052	2.32	2.35	
20	1.50	.036	1.62	1.64	20	1.66	.040	1.78	1.81	
22	1.25	.030	1.35	1.36	22	1.41	.034	1.51	1.53	
24	1.00	.024	1.08	1.09	24	1.16	.028	1.25	1.26	
26	.75	.018	.81	.82	26	.91	.022	.98	.99	
28	.63	.015	.67	.68	28	.78	.019	.84	.85	

To obtain weights of Painted Sheets add 0.010 pounds per square foot to weights of Black Sheets.

EXPORT 3" CORRUGATED

Black			Galvanized					Maximum Span Between Supports		
Manufacturers Standard Gage		Corrugated Pounds per Sq. Ft.	Galvanized Sheet Gage			Corrugated Pounds per Sq. Ft.				
Gage No.	Pounds per Sq. Ft.	Approx. Thick. Inches	32" & 33½" Wide	Gage No.	Pounds per Sq. Ft.	Approx. Thick. Inches	32" & 33½" Wide	Roofing	Siding	
12	4.38	.105	4.86	12	4.53	.109	5.03	5' 9"	5' 10"	
14	3.13	.075	3.47	14	3.28	.079	3.64	5' 9"	5' 10"	
16	2.50	.060	2.78	16	2.66	.064	2.95	5' 9"	5' 10"	
18	2.00	.048	2.22	18	2.16	.052	2.40	5' 9"	5' 10"	
20	1.50	.036	1.67	20	1.66	.040	1.84	5' 9"	5' 10"	
22	1.25	.030	1.39	22	1.41	.034	1.57	4' 9"	5' 10"	
24	1.00	.024	1.11	24	1.16	.028	1.29	3' 9"	4' 10"	

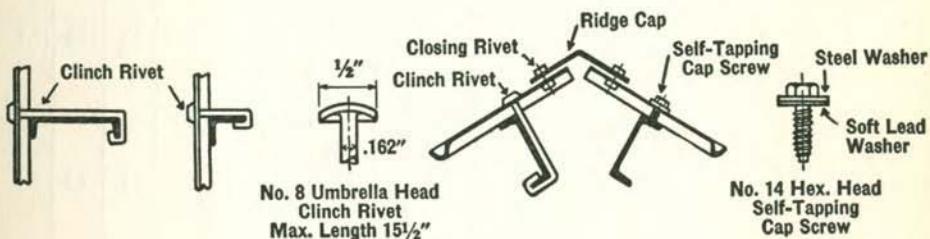
To obtain weights of Painted Sheets add 0.010 pounds per square foot to weights of Black Sheets.

Method of obtaining approximate gross area required:

Roofing = net area + end laps + 15% for side laps of 1½ corrugations.

Siding = net area + end laps + 10% for side laps of 1 corrugation.

CORRUG.
SHEETS



PILING

FLOOR PLATES

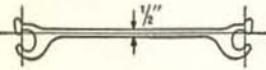
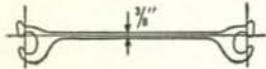
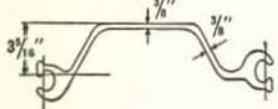
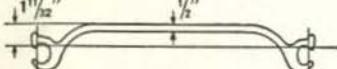
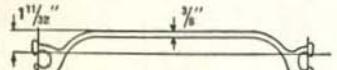
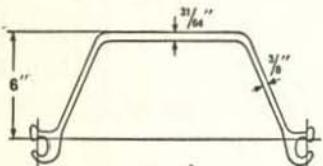
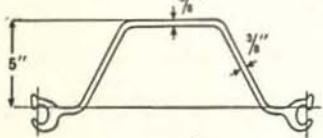
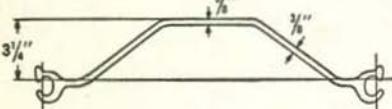
PLATES

MILL
PRACTICES

INDEX

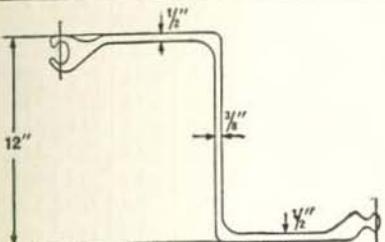
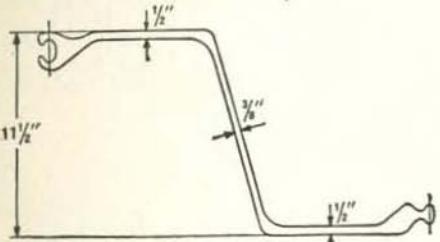
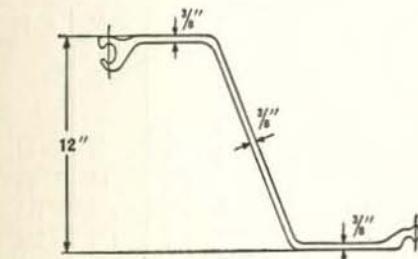
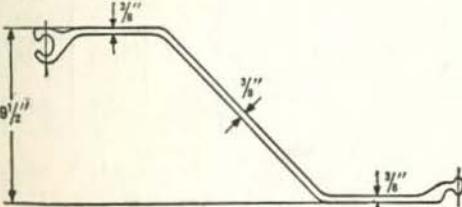
Fastenings for Corrugated Steel

STEEL SHEET PILING SECTIONS

Profile	District Rolled	Section Index	Driving Dis- tance per Pile	Weight		Web Thickness	Section Modulus	
				Per Foot	Per Square Foot of Wall		Per Pile	Per Foot of Wall
				In.	Lbs.		In.	In. ²
  	C.	INTERLOCK WITH EACH OTHER	MP 102	15	40.0	32.0	1/2	
			MP 101	15	35.0	28.0	3/8	
			MP 117	15	38.8	31.0	3/8	8.9 7.1
    	P.	MP 113	16	37.3	28.0	1/2	3.3 2.5	
		MP 112	16	30.7	23.0	3/8	3.2 2.4	
	P.C.	INTERLOCK WITH EACH OTHER	MP 110	16	42.7	32.0	31/64	20.4 15.3
	P.C.		MP 116	16	36.0	27.0	3/8	14.3 10.7
	P.C.		MP 115	19 5/8	36.0	22.0	3/8	8.8 5.4

For key to symbols in first column, refer to page 3.

STEEL SHEET PILING SECTIONS-Z PILES

Profile	District Rolled	Section Index	Driving Dis- tance per Pile	Weight		Web Thick- ness	Section Modulus	
				Per Foot	Per Square Foot of Wall		Per Pile	Per Foot of Wall
				In.	Lbs.		In. ²	In. ³
	P.	INTERLOCK WITH EACH OTHER	MZ 38	18	57.0	38.0	5/8	70.2 46.8
	P.	INTERLOCK WITH EACH OTHER	MZ 32	21	56.0	32.0	5/8	67.0 38.3
	P.	INTERLOCK WITH EACH OTHER	MZ 27	18	40.5	27.0	5/8	45.3 30.2
	P.	INTERLOCK WITH EACH OTHER	MZ 22	22	40.3	22.0	5/8	34.8 19.0

Complete data regarding these sections will be found in a separate publication entitled "Steel Sheet Piling." For key to symbols in first column, refer to page 3.

PILING

FLOOR
PLATES

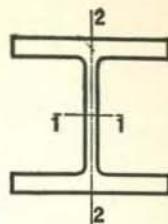
PLATES

MILL
PRACTICES

INDEX



BEARING PILES
WIDE FLANGE CBP SECTIONS
PROPERTIES OF SECTIONS



District Rolled	Section Index and Nominal Size	Weight per Foot	Area of Section	Depth of Section	FLANGE		Web Thick- ness	Axis 1-1			Axis 2-2			
					Width	Thick- ness		In.	In.	In.	In. ⁴	In. ³	In.	
P.C.	CBP 145 14 x 14½	117	34.44	14.234	14.885	.805	.805	1228.5	172.6	5.97	443.1	59.5	3.59	
		102	30.01	14.032	14.784	.704	.704	1055.1	150.4	5.93	379.6	51.3	3.56	
	CBP 124 12 x 12	89	26.19	13.856	14.696	.616	.616	909.1	131.2	5.89	326.2	44.4	3.53	
		73	21.46	13.636	14.586	.506	.506	733.1	107.5	5.85	261.9	35.9	3.49	
P.C.	CBP 124	74	21.76	12.122	12.217	.607	.607	566.5	93.5	5.10	184.7	30.2	2.91	
P.C.	12 x 12	53	15.58	11.780	12.046	.436	.436	394.8	67.0	5.03	127.3	21.2	2.86	
P.C.	CBP 103	57	16.76	10.012	10.224	.564	.564	294.7	58.9	4.19	100.6	19.7	2.45	
P.C.	10 x 10	42	12.35	9.720	10.078	.418	.418	210.8	43.4	4.13	71.4	14.2	2.40	
P.C.	CBP 83 8 x 8	36	10.60	8.026	8.158	.446	.446	119.8	29.9	3.36	40.4	9.9	1.95	

Complete data regarding these sections will be found in a separate publication entitled "Steel Bearing Piles."
 For key to symbols in first column, refer to page 3.

FLOOR PLATES
ALLOWABLE UNIFORM LOAD IN LB. PER SQ. FT.

Weight of Plate Included - Simply Supported Along Two Opposite Edges - Bending Stress, 16,000 psi

Plate Thickness Inches	SPAN—Feet and Inches										
	1'-0"	1'-6"	2'-0"	2'-6"	3'-0"	3'-6"	4'-0"	4'-6"	5'-0"	5'-6"	6'-0"
1/8	333	148	83	53	37						
3/16	750	333	188	120	83	61	47				
1/4	1333	593	333	213	148	109	83	65	53		
5/16	2083	926	521	333	231	170	130	103	83	69	58
3/8	3000	1333	750	480	333	245	188	148	120	99	83
7/16	4083	1815	1021	653	454	333	255	202	163	135	113
1/2	5333	2370	1333	853	593	435	333	263	213	176	148
5/8	8333	3704	2083	1333	926	680	521	412	333	275	231
3/4	12000	5333	3000	1920	1333	980	750	593	480	397	333
1	21333	9481	5333	3413	2370	1741	1333	1053	853	705	5958
Deflection Coefficient	.0166	.0372	.0662	.1034	.1490	.2027	.2648	.3351	.4138	.5006	.5958

Deflections for loadings above stepped line will exceed 1/100th of the span.

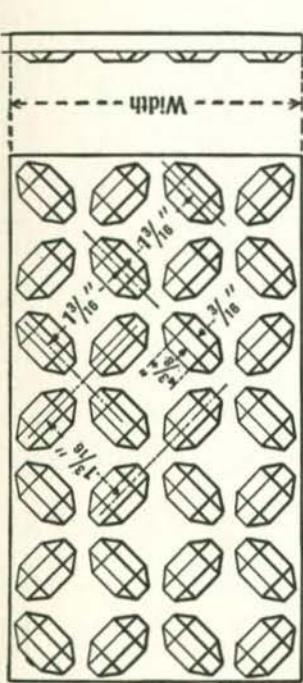
The deflection coefficient at the bottom of each span column is a constant, which, when divided by the plate thickness under consideration, in inches, gives the deflection in inches at the center of the span for the tabular loading shown.

To find the deflection in inches for any uniform load less than tabulated above, find the deflection for the tabular load for a given span and plate thickness; multiply this deflection by the load per sq. ft. desired; and divide by the tabular allowable safe load above.

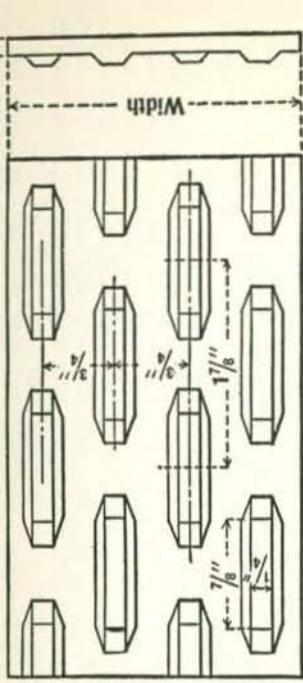
Plate Thickness in inches is the body or base thickness, and does not include the depth of the projections.

EXTREME SIZES OF RECTANGULAR AND CIRCULAR FLOOR PLATES

CARBON STEEL—SECTION S-300



CARBON STEEL—SECTION M-41 Thickness



Chicago and Pittsburgh Districts.
Weights are approximate and may vary.
***Not rolled in Chicago District.**

• Weights are approximate and may vary.
• Not rolled in Chicago District.

Thicknesses inches		Widths in inches		Lengths in inches		Thicknesses inches	
		Over 6 to 12 12 Incl. Incl.	Over 12 to 18 18 Incl. Incl.	Over 18 to 24 24 Incl. Incl.	Over 24 to 30 30 Incl. Incl.	Over 30 to 60 60 Incl. Incl.	Over 60 to 72 72 Incl. Incl.
per Sq.-Ft., Weight-lbs.		6.50	144	180	240	360	480
		8.70	144	180	300	600	600
		11.25	144	180	300	600	600
		13.80	144	180	300	600	600
		16.35	120	180	300	600	600
		18.90	120	180	300	600	600
		21.45	120	180	300	600	600
		26.55	120	180	300	600	600
		31.65	120	180	300	480	480
		41.85	...	300	360	480	360
		1	1	1	1	1	1

PLATES
Pittsburgh
District

PLATES ROLLED IN PITTSBURGH DISTRICT
EXTREME SIZES OF RECTANGULAR UNIVERSAL MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.
2 INCHES THICK AND UNDER

EXTREME SIZES OF RECTANGULAR UNIVERSAL MILL PLATES

CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T.S.

OVER 2 INCHES THICK

Thickness inches	Over 6 to 7 Incl.	Over 7 to 8 Incl.	Over 8 to 9 Incl.	Over 9 to 9½ Incl.	Width in inches										Length in inches										Thickness inches		
					Over 11 to 11 Incl.	Over 10 to 13 Incl.	Over 11 to 13 Incl.	Over 13 to 15 Incl.	Over 15 to 17 Incl.	Over 17 to 19 Incl.	Over 19 to 21 Incl.	Over 21 to 23 Incl.	Over 23 to 25 Incl.	Over 25 to 27 Incl.	Over 27 to 29 Incl.	Over 29 to 31 Incl.	Over 31 to 33 Incl.	Over 33 to 35 Incl.	Over 35 to 37 Incl.	Over 37 to 39 Incl.	Over 39 to 41 Incl.	Over 41 to 43 Incl.	Over 43 to 45 Incl.	Over 45 to 46 Incl.			
2½	276	252	232	216	764	646	561	536	505	662	649	644	640	637	722	716	711	708	704	675	632	596	535	485	444		
2½	252	216	204	192	688	582	505	485	457	531	523	521	517	510	506	644	630	627	620	597	556	536	481	458	417		
3½	204	180	573	491	415	360	473	546	537	531	523	517	497	455	460	457	455	406	474	447	423	401	381		
3½	491	415	360	473	546	464	464	460	457	455	453	433	406	405	406	398	383	383	344	327	312		
4½	430	363	315	414	406	403	400	398	394	396	396	355	379	377	379	377	300	286	273	243	231	212	
4½	382	323	363	410	414	361	358	355	354	352	337	316	322	317	303	284	268	254	240	229	218	208	
5½	345	291	252	325	325	322	320	318	318	317	317	303	293	291	289	283	260	232	220	209	200	190	
5½	264	229	301	291	295	295	295	295	295	295	276	266	264	253	237	223	211	200	190	182	183	
6½	210	276	273	273	273	273	273	273	273	273	250	248	246	244	234	226	207	196	186	176	169	
6½	194	254	254	254	254	254	254	254	254	254	232	232	232	232	226	216	203	191	181	172	163	
7½	236	234	234	234	234	234	234	234	234	234	226	226	226	226	216	216	203	191	181	172	163	
7½	226	220	220	220	220	220	220	220	220	220	218	216	216	216	212	212	202	188	178	168	152	
8½	205	205	203	201	200	199	198	198	198	198	189	187	187	187	187	186	177	167	157	147	136	
9½	192	191	191	189	189	188	188	188	188	188	178	178	178	178	178	178	168	158	149	141	134	
9½	180	180	180	179	179	178	178	178	178	178	177	177	177	177	177	177	168	158	149	141	133	
10	161	160	160	160	160	160	160	160	160	160	167	167	167	167	167	159	149	141	133	126	115	
10½	153	152	152	152	152	152	152	152	152	152	158	158	158	158	158	142	134	127	120	114	109	
11	145	145	145	145	145	145	145	145	145	145	151	151	151	151	151	144	135	127	120	114	109	
11½	139	139	139	139	139	139	139	139	139	139	144	144	144	144	144	138	137	132	123	116	110	
12	132	132	132	132	132	132	132	132	132	132	126	126	126	126	126	121	114	114	113	105	101	95
12½	127	127	127	127	127	127	127	127	127	127	122	122	122	122	122	117	114	114	113	107	101	95
13	121	121	121	121	121	121	121	121	121	121	117	117	117	117	117	110	103	98	93	88	84	80
13½	117	117	117	117	117	117	117	117	117	117	112	112	112	112	112	105	99	94	89	84	81	78
14	110	108	108	108	108	108	108	108	108	108	101	98	98	98	98	95	90	86	81	78	74	71
14½	94	94	94	94	94	94	94	94	94	94	84	84	84	84	84	80	76	72	69	66	63	60

PLATES
Pittsburgh
District

All Sizes must be gas cut to width and length. Plate requirements in excess of dimensions shown may be submitted for special consideration.

In general circles can be furnished in diameters equal to widths of plates shown.

PLATES ROLLED IN PITTSBURGH DISTRICT

EXTREME SIZES OF RECTANGULAR AND CIRCULAR SHEARED MILL PLATES

CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

2 INCHES THICK AND UNDER

Thickness inches	Widths in inches	Lengths in inches												Circles Maximum Diameter, inches	Thickness inches									
		24	30	36	42	48	48½	54	60	66	72	78	84	90	90½	96	102	108	114	120	126	132	138	144
7/16	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65	7.65
1/4	10.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20	7.20
5/16	12.75	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
3/8	15.30	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
7/16	17.85	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
1/2	20.40	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
9/16	22.95	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
5/8	25.50	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
11/16	28.05	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
3/4	30.60	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00	9.00
13/16	33.15	4.95	5.15	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20
7/8	35.70	4.95	4.95	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20
1	40.80	4.50	4.65	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20
1 1/8	45.90	4.50	4.65	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20
1 1/4	51.00	4.00	4.50	5.00	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20
1 1/2	61.20	4.00	4.20	5.00	5.20	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00
1 1/4	71.40	4.00	4.20	5.00	5.20	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00
2	81.60	4.00	4.20	5.00	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20	5.20

EXTREME SIZES OF RECTANGULAR SHEARED MILL PLATES

OVER 2 INCHES THICK

Thicknesses Inches	Widths in Inches												Lengths in Inches											
	Over 46 to 47 Incl.	Over 47 to 48 Incl.	Over 48 to 54 Incl.	Over 54 to 60 Incl.	Over 60 to 66 Incl.	Over 66 to 72 Incl.	Over 72 to 78 Incl.	Over 78 to 84 Incl.	Over 84 to 90 Incl.	Over 90 to 96 Incl.	Over 96 to 102 Incl.	Over 102 to 108 Incl.	Over 108 to 114 Incl.	Over 114 to 120 Incl.	Over 120 to 126 Incl.	Over 126 to 132 Incl.	Over 132 to 138 Incl.	Over 138 to 144 Incl.	Over 144 to 150 Incl.	Over 150 to 156 Incl.	Over 156 to 162 Incl.	Over 162 to 168 Incl.	Over 168 to 174 Incl.	Over 174 to 180 Incl.
2 1/4	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600
2 1/2	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650	650
3 1/4	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600
4	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659	659
4 1/2	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494
5 1/2	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440	440
6	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584	584
6 1/2	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337	337
7	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311	311
7 1/2	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292	292
8	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279	279
8 1/2	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257	257
9	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244	244
9 1/2	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229	229
10	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218	218
10 1/2	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205	205
11	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188	188
11 1/2	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180	180
12	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181	181
12 1/2	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177	177
13	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168	168
13 1/2	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161	161
14	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156	156
14 1/2	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150
15	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145

All Sizes must be gas cut to width and length. Plate requirements in excess of dimensions shown may be submitted for special consideration.
 In general circles can be furnished in diameters equal to widths of plates shown.

PLATES
Pittsburgh District

PLATES
Chicago
District

PLATES ROLLED IN CHICAGO DISTRICT

EXTREME SIZES OF RECTANGULAR UNIVERSAL MILL PLATES

CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

2 INCHES THICK AND UNDER

Thickness inches	Widths in inches											Lengths in inches	Thickness inches
	6 $\frac{1}{4}$	6 $\frac{1}{2}$	7	7 $\frac{1}{2}$	8	8 $\frac{1}{2}$	9	9 $\frac{1}{2}$	10	12	14		
1 $\frac{1}{4}$	10.20	1080	1080	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	12.75	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{3}{8}$	15.30	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	17.85	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	20.40	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	22.95	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	25.50	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	30.60	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	35.70	1200	1320	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1	40.80	1200	1272	1320	1320	1320	1320	1320	1320	1320	1320	1320	14
1 $\frac{1}{2}$	45.90	1080	1128	1164	1212	1200	1200	1188	1188	1164	1152	1140	14
1 $\frac{1}{2}$	51.00	972	1002	1044	1092	1080	1080	1068	1068	1044	1032	1020	14
1 $\frac{1}{2}$	56.10	888	924	948	984	972	972	960	948	936	924	924	14
1 $\frac{1}{2}$	61.20	804	840	864	900	900	900	888	888	864	852	840	14
1 $\frac{1}{2}$	66.30	744	756	792	828	828	816	816	804	792	780	768	14
1 $\frac{1}{2}$	71.40	684	708	732	768	768	756	756	744	732	726	720	14
1 $\frac{1}{2}$	76.50	636	660	684	714	714	708	708	702	696	684	678	14
2	81.60	600	612	636	672	666	660	660	648	648	636	630	14

Plate requirements in excess of dimensions shown may be submitted for special consideration.

EXTREME SIZES OF RECTANGULAR UNIVERSAL MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.
OVER 2 INCHES THICK

		WIDTHS IN INCHES										LENGTHS IN INCHES										Thickness inches		
		6 1/4	6 1/2	7	7 1/2	8	8 1/2	9	9 1/2	10	12	14	16	18	20	22	24	26	28	30	Thickness inches			
2 1/4	528	552	570	594	588	588	582	576	570	564	558	558	552	552	546	546	510	510	2 1/4					
2 1/2	468	486	510	528	528	528	522	522	516	510	504	504	498	498	492	492	492	492	456	456	2 1/2			
2 3/4	420	444	462	480	474	474	474	474	468	462	456	456	450	450	450	450	444	444	414	414	2 3/4			
3	438	438	432	432	432	426	420	414	414	408	408	408	408	408	408	378	378	3			
3 1/2	372	372	366	366	366	360	354	354	348	348	348	348	348	348	348	348	324	324	3 1/2		
4	324	324	324	318	318	318	312	312	306	306	306	306	306	306	306	306	300	300	4		
4 1/2	282	282	282	282	282	276	276	270	270	270	270	270	270	270	270	270	264	264	4 1/2		
5	252	252	252	252	252	246	246	240	240	240	240	240	240	240	240	234	234	5		
5 1/2	228	228	228	228	228	222	222	216	216	216	216	216	216	216	216	216	198	198	5 1/2	
6	210	204	204	204	204	198	198	198	198	198	198	198	198	198	198	192	192	6		

All sizes must be gas cut to length. Plate requirements in excess of dimensions shown may be submitted for special consideration.

PLATES
Chicago District

PLATES ROLLED IN CHICAGO DISTRICT

EXTREME SIZES OF RECTANGULAR AND CIRCULAR SHEARED MILL PLATES CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

2 INCHES THICK AND UNDER

Thickness inches	Width, per Sq. Ft. lbs.	Widths in inches												Lengths in inches						Circles Maximum Diameter, inches	Thickness inches	
		24	30	48	54	Over 54 to 88½	84	90	96	102	108	114	120	126	132	138	144	146	148			
3/16	7.65	... 720	... 720	720	720	720	500	480	450	420	400	360	320	300	320	300	300	300	300	84	3/16	
1/4	10.20	... 720	720	720	720	720	520	500	480	470	440	400	390	350	320	320	300	300	300	134	1/4	
5/16	12.75	720	720	720	720	720	720	720	720	720	660	600	520	480	400	330	300	300	300	300	140	5/16
3/8	15.30	720	720	720	720	720	720	720	720	720	660	600	520	480	400	330	300	300	300	300	146	3/8
7/16	17.85	720	720	720	720	720	720	720	720	720	660	600	520	480	440	400	360	360	360	360	146	7/16
1/2	20.40	720	720	720	720	720	720	720	720	720	720	720	660	580	520	480	440	400	360	360	148	1/2
9/16	22.95	720	720	720	720	720	720	720	720	720	720	720	660	580	520	480	440	420	360	360	148	9/16
5/8	25.50	720	720	720	720	720	720	720	720	720	720	720	660	600	540	500	480	420	360	360	150	5/8
11/16	28.05	720	720	720	720	720	720	720	720	720	720	720	660	600	540	500	480	420	360	360	150	11/16
3/4	30.60	720	720	720	720	720	720	720	720	720	720	720	660	600	540	500	480	420	400	360	150	3/4
13/16	33.15	... 720	720	720	720	720	720	720	720	720	720	720	660	600	540	520	480	420	400	360	150	13/16
7/8	35.70	... 720	720	720	720	720	720	720	720	720	720	720	660	600	540	520	480	420	400	360	150	7/8
1	40.80	... 720	720	720	720	720	720	720	720	720	720	720	660	600	540	520	480	420	400	360	150	1
13/8	45.90	... 720	720	720	720	720	720	720	720	720	720	720	660	600	540	520	480	420	400	360	150	13/8
1 1/4	51.00	... 720	720	720	720	720	720	720	720	720	720	720	660	600	540	520	480	420	400	360	150	1 1/4
1 1/2	61.20	... 720	720	720	720	720	720	720	720	720	660	630	500	460	420	400	360	320	320	150	1 1/2	
1 3/4	71.40	... 720	720	720	720	720	720	720	720	720	680	640	600	575	520	480	440	420	400	360	150	1 3/4
2	81.60	... 720	720	720	720	720	720	720	720	720	640	600	560	530	500	480	420	400	360	360	150	2

Plate requirements in excess of dimensions shown may be submitted for special consideration.

EXTREME SIZES OF RECTANGULAR SHEARED MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.
OVER 2 INCHES THICK

Thickness Inches	Widths in Inches												Lengths in Inches						
	48	54	60	66	72	78	84	90	96	102	108	114		120	126	132	138	144	146
2½	720	720	680	680	600	560	520	490	465	435	410	395	380	360	335	300	280	260	240
3	680	630	580	530	460	430	400	430	405	385	360	340	310	290	260	235	200	220	200
3½	635	590	540	500	460	435	395	365	325	300	285	265	245	225	205	185	160	180	160
4	650	605	465	430	380	350	300	275	245	225	205	195	175	155	145	145	145	145	145
4½	490	450	415	405	370	345	320	270	245	225	210	200	185	170	165	155	140	135	135
5	445	405	365	335	305	280	255	240	225	205	190	180	170	155	145	135	130	130	130
5½	400	365	335	310	280	255	235	220	195	175	165	155	145	135	130	125	125	125	125
6	365	340	315	285	260	240	225	205	185	175	165	155	145	135	130	125	125	125	125
6½	310	285	265	245	225	205	190	175	160	150	140	130	125	120	115	110	105	100	100
7	315	295	270	255	235	220	205	190	175	160	150	140	130	125	120	115	110	105	100
7½	275	250	230	215	200	185	170	155	140	130	120	115	110	105	100	95	90	85	80
8	255	235	220	200	185	170	160	145	130	125	120	115	110	105	100	95	90	85	80
8½	245	220	200	185	170	160	155	145	135	130	125	120	115	110	105	100	95	90	85
9	230	210	190	175	160	150	145	135	125	120	115	110	105	100	95	90	85	80	75
9½	215	200	180	170	160	150	145	135	125	120	115	110	105	100	95	90	85	80	75
10	205	185	170	155	140	130	125	120	115	110	105	100	95	90	85	80	75	70	65
10½	195	175	160	145	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55
11	185	165	150	135	125	115	110	105	100	95	90	85	80	75	70	65	60	55	50
11½	175	150	145	130	120	110	105	100	95	90	85	80	75	70	65	60	55	50	45
12	170	155	140	125	120	110	105	100	95	90	85	80	75	70	65	60	55	50	45
12½	160	145	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50	45
13	155	140	130	125	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50
13½	140	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50	45	40
14	140	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50	45	40
14½	140	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50	45	40
15	140	130	120	115	110	105	100	95	90	85	80	75	70	65	60	55	50	45	40

All sizes must be gas cut to width and length. Plate requirements in excess of dimensions shown may be submitted for special consideration.
 In general circles can be furnished in diameters equal to widths of plates shown.

PLATES
 Chicago District

PLATES
Birmingham
District

PLATES ROLLED IN BIRMINGHAM DISTRICT
EXTREME SIZES OF RECTANGULAR UNIVERSAL MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

Thickness inches	Weight lbs., per sq. ft.	Widths in inches						Maximum Lengths in inches						Thickness inches
		10 Thru 12	Over 12 Thru 16	Over 16 Thru 20	Over 20 Thru 24	Over 24 Thru 28	Over 28 Thru 30	Over 30 Thru 32	Over 32 Thru 34	Over 34 Thru 36	Over 36 Thru 38	Over 38 Thru 40	Over 40 Thru 42	
1/4	10.20	865	865	865	865	865	865	865	865	865	865	865	865	1/4
5/16	12.75	865	865	865	865	865	865	865	865	865	865	865	865	5/16
3/8	15.30	865	865	865	865	865	865	865	865	865	865	865	865	3/8
7/16	17.85	865	865	865	865	865	865	865	865	865	865	865	865	7/16
1/2	20.40	865	865	865	865	865	865	865	865	865	865	865	865	1/2
9/16	22.95	865	865	865	865	865	865	865	865	865	865	865	865	9/16
5/8	25.50	865	865	865	865	865	865	865	865	865	865	865	865	5/8
11/16	28.05	865	865	865	865	865	865	865	865	865	865	865	865	11/16
3/4	30.60	865	865	865	865	865	865	865	865	865	865	865	865	3/4
13/16	33.15	865	865	865	865	865	865	865	865	865	865	865	865	13/16
7/8	35.70	865	865	865	865	865	865	865	865	865	865	865	865	7/8
1	40.80	865	865	865	865	865	865	865	865	865	865	865	865	1
1 1/8	45.90	865	865	865	865	865	865	865	865	865	865	865	865	1 1/8
1 1/4	51.00	865	865	865	865	865	865	865	865	865	865	865	865	1 1/4
1 1/8	56.10	865	865	865	865	865	865	865	865	865	865	865	865	1 1/8
1 1/2	61.20	865	865	865	865	865	865	865	865	865	865	865	865	1 1/2
1 5/8	66.30	865	865	865	865	865	865	865	865	865	865	865	865	1 5/8
1 1/4	71.40	865	865	865	865	865	865	865	865	865	865	865	865	1 1/4
1 1/8	76.50	865	865	865	865	865	865	865	865	865	865	865	865	1 1/8
2	81.60	800	800	800	800	800	800	800	800	800	800	800	800	2

Minimum sheared length—42". Minimum gas cut length—48".
Plates up to 1 1/8" inclusive are sheared to length; over 1 1/8" are gas cut.

EXTREME SIZES OF RECTANGULAR AND CIRCULAR SHEARED MILL PLATES

CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

1½ INCHES THICK AND UNDER

Thicknesses inches	Weight Lbs., per Sq. Ft.	Widths in inches												Maximum Lengths in inches												Thicknesses inches
		Over 36 Thru 66	Over 66 Thru 72	Over 72 Thru 78	Over 78 Thru 84	Over 84 Thru 90	Over 90 Thru 96	Over 96 Thru 98	Over 98 Thru 100	Over 100 Thru 102	Over 102 Thru 104	Over 104 Thru 106	Over 106 Thru 108	Over 108 Thru 110	Over 110 Thru 112	Over 112 Thru 114	Over 114 Thru 116	Over 116 Thru 118	Over 118 Thru 120	Over 120 Thru 122	Over 122 Thru 124	Over 124 Thru 126	Over 126 Thru 128			
¾	7.65	600	540	500	460	430	400	400	400	400	400	400	400	370	370	340	340	340	320	320	320	320	320	320	120	
½	10.20	600	600	560	560	510	510	510	510	510	510	510	510	480	480	440	440	440	400	400	400	400	400	400	124	
5/16	12.75	600	600	600	600	600	600	550	550	550	550	550	550	550	530	530	500	500	500	480	480	480	480	480	480	128
3/8	15.30	720	720	660	660	660	660	660	660	660	660	660	660	600	550	550	550	550	520	520	520	520	520	520	132	
7/16	17.85	720	720	720	720	660	660	660	660	660	660	660	660	550	550	550	550	550	520	520	520	520	520	520	136	
1/2	20.40	720	720	720	720	720	680	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	140	
9/16	22.95	720	720	720	720	720	720	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	144	
5/8	25.50	720	720	720	720	720	720	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	148	
11/16	28.05	720	720	720	720	720	680	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	152	
3/4	30.60	720	720	720	720	680	680	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	156	
13/16	33.15	720	720	720	720	680	680	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	160	
7/8	35.70	720	720	720	720	720	680	680	680	680	680	680	680	640	640	640	640	640	600	600	600	600	600	600	164	
1	40.80	720	720	720	720	670	670	670	670	670	670	670	670	620	620	620	620	620	500	500	500	500	500	500	168	
1 1/8	45.90	720	650	720	650	600	540	540	510	510	510	510	510	480	480	480	480	480	460	460	460	460	460	460	172	

Widths 36" and Under: Sheared within the following size limitations:

Thickness Width
¾" thru 1½" 12" thru 36"
5/16" thru 1 1/8" 24" thru 36"

Minimum sheared length—50"
Widths over 36" to 120" incl.: Rotary side sheared.
Widths over 120": Sides sheared on straight shear.
*Circles 1 1/8" thick are gas cut to size.

PLATES
Birmingham
District

PLATES ROLLED IN BIRMINGHAM DISTRICT
 EXTREME SIZES OF RECTANGULAR SHEARED MILL PLATES
 CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.

OVER 1½ INCHES THICK (Gas Cut)

Thickness inches	WIDTHS IN INCHES												MAXIMUM LENGTHS IN INCHES															
	Over 27 Thru 28	Over 28 Thru 30	Over 30 Thru 32	Over 32 Thru 34	Over 34 Thru 36	Over 36 Thru 38	38	Over 38 Thru 40	Over 40 Thru 42	Over 42 Thru 44	Over 44 Thru 46	Over 46 Thru 48	Over 48 Thru 50	Over 50 Thru 52	Over 52 Thru 54	Over 54 Thru 56	Over 56 Thru 58	Over 58 Thru 60	Over 60 Thru 62	Over 62 Thru 64	Over 64 Thru 66	Thickness inches						
1 1/4	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	694	673	652	633	61/4		
1 3/8	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	648	628	608	589	572		
1 1/2	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	633	612	591	572	521		
1 5/8	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	656	596	529	497	482		
1 3/4	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	582	561	523	489	458		
1 7/8	270	290	310	330	350	380	410	720	720	720	720	720	720	720	720	720	720	720	720	720	720	563	541	503	469	439		
2	270	290	310	295	275	250	653	623	595	570	547	525	505	486	469	453	437	423	409	397	385	2	2	2	2	2		
2 1/4	270	290	240	240	230	220	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
2 1/2	265	240	240	230	220	205	190	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
2 3/4	240	235	220	205	195	185	170	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
3	215	210	195	185	175	165	155	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
3 1/2	185	175	165	155	145	135	130	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
4	156	150	140	130	125	115	110	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
4 1/2	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240	240		
5	240	240	237	227	218	209	201	195	187	182	176	169	164	159	153	150	146	142	138	134	
5 1/2	235	224	215	205	197	189	182	175	169	163	157	152	147	142	138	134	130	126	122	118	114
6	214	204	195	187	179	172	165	159	153	148	143	138	133	129	125	121	117	113	109	105	101
6 1/2	197	188	179	171	164	157	152	146	140	135	131	126	122	118	114	110	106	102	98	94	90
7	182	173	163	158	151	145	140	134	129	124	120	115	111	107	104	100	97	94	90	86	82
7 1/2	169	161	153	147	140	135	129	124	120	115	111	107	103	100	97	94	90	86	82	78	74
8	157	150	143	136	131	125	120	115	111	107	103	100	97	94	90	86	82	78	74	70	66

For maximum circle diameters, see table on page 63.

EXTREME SIZES OF RECTANGULAR AND CIRCULAR SHEARED MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.
OVER 1½ INCHES THICK (Gas Cut)

Thicknesses Inches	Widths in Inches												Maximum Lengths in Inches												Circles Maximum Diameter, Inches	Thicknesses Inches
	Over 68 Thru 70	Over 70 Thru 72	Over 72 Thru 74	Over 74 Thru 76	Over 76 Thru 78	Over 78 Thru 80	Over 80 Thru 82	Over 82 Thru 84	Over 84 Thru 86	Over 86 Thru 88	Over 88 Thru 92	Over 92 Thru 96	Over 96 Thru 100	Over 100 Thru 104	Over 104 Thru 108	Over 108 Thru 112	Over 112 Thru 116	Over 116 Thru 120	Over 120 Thru 124	Over 124 Thru 128	Over 128	1½				
1½	615	598	581	566	551	537	524	511	498	487	476	465	445	426	409	393	378	364	351	339	327	128	1½	1½		
1¾	555	540	525	511	497	484	473	461	450	439	429	419	401	384	368	354	340	327	315	304	294	128	1¾	1¾		
1½	506	492	478	465	453	441	430	419	409	399	390	381	364	348	334	321	308	297	286	276	266	128	1½	1½		
1¾	468	455	442	430	419	408	398	388	378	369	361	353	337	322	309	297	285	275	265	255	247	128	1¾	1¾		
1¾	432	420	408	397	386	376	367	357	349	340	332	325	310	297	285	273	263	253	243	234	226	128	1¾	1¾		
1½	401	389	378	368	358	349	340	331	323	315	308	301	287	275	263	253	243	233	225	217	209	128	1½	1½		
2	373	362	352	343	333	324	316	308	301	293	286	280	267	255	245	235	225	216	208	201	194	128	2	2		
2¼	240	240	240	240	240	240	240	240	240	240	240	240	233	223	213	204	196	188	181	174	168	128	2¼	2¼		
2½	240	240	240	240	240	240	240	240	240	240	240	240	233	222	216	206	197	188	180	173	166	160	153	148	2½	
2¾	240	240	240	240	240	239	233	226	220	214	209	204	198	194	184	176	168	161	154	148	142	136	131	128	2¾	
3	240	236	229	222	216	210	205	199	194	190	185	180	172	164	157	150	144	138	133	128	128	124	3	3		
3½	214	208	202	196	191	186	181	177	172	168	164	160	153	147	140	135	129	124	120	120	120	120	120	120	3½	
4	185	179	174	169	165	160	156	152	148	145	141	138	131	126	120	115	115	105	105	105	105	105	105	105	108	
4½	162	157	153	148	144	140	137	133	130	126	123	120	115	110	105	101	101	101	101	101	101	101	101	101	104	
5	151	146	140	137	133	129	127	124	119	118	115	111	108	105	102	100	100	100	100	100	100	100	100	100	100	
5½	134	130	126	123	119	116	113	110	109	105	102	100	97	95	92	92	92	92	92	92	92	92	92	92	92	
6	121	118	114	111	108	105	102	100	99	96	93	91	89	89	87	85	85	85	85	85	85	85	85	85	85	
6½	111	108	105	102	99	96	93	90	88	85	83	81	81	81	81	81	81	81	81	81	81	81	81	81	81	
7	102	99	96	93	90	88	85	83	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	
7½	94	91	89	86	83	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	81	
8	87	85	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	82	

PLATES
Birmingham
District

PLATES
Geneva
District

EXTREME SIZES OF RECTANGULAR AND CIRCULAR SHEARED MILL PLATES
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T. S.
1½ INCHES THICK AND UNDER

Thickness, inches	Weight, lbs. per sq. ft.	Widths in inches												Lengths in inches					Thickness, inches	Diameter, inches
		36	42	48½	54	60	66	72	78	84	90	96	102	108	114	120	121			
7/16	7.65																	96	96	
1/4	10.20	600	600	480	480	480	480	480	480	480	480	480	480	480	480	480	480	120	14	
5/16	12.75	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	16	
3/8	15.30	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	18	
7/16	17.85	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	16	
1/2	20.40	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	14	
9/16	22.95	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	16	
5/8	25.50	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	18	
11/16	28.05	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	16	
3/4	30.60	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	600	120	14	
13/16	33.15	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	120	16	
7/8	35.70	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	120	18	
1	40.80	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	120	1	
11/8	45.90	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	120	18	
11/4	51.00	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	114	14	
11/2	61.20	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	480	108	14	

For items shown under heavy line, the minimum quantity of one size which the mill can accept is 200^o, either in one length or multiples adding up to a minimum of 200^o.
 For flange, firebox and higher qualities where tests from both ends are required—reduce above maximum lengths by 20 inches.
 Circles—minimum diameter 36 inches. Plate requirements in excess of dimensions shown may be submitted for special consideration.

EXTREME SIZES OF RECTANGULAR SHEARED MILL PLATE
CARBON STEEL—STRUCTURAL GRADE—72,000 PSI MAXIMUM T.S.
OVER 1½ INCHES THICK

Thickness, inches,	Widths in inches									
	49	54	60	66	72	78	84	90	96	
1½	370	445	425	390	360	335	330	240	215	200
1¾	345	410	385	360	335	310	285	220	200	
1⅜	320	380	360	335	310	290	270			
2	300	355	335	315	295	275	255			
2½	285	335	315	300	280	260	240			
2¼	270	315	300	280	265	245	225			
2¾	255	300	285	270	250	230	215			
2½	240	285								
2¾	230	270	255	235	220	205				
2½	220	260	245	225	210					
2¾	210	250	235	215	200					
3	200	240	225	210						

All sizes must be gas cut to width and length.

For all items shown on this page, the minimum quantity for one size which the mill can accept is 200' either in one length or multiples adding up to a minimum of 200'.

For Range, firebox and higher qualities where tests from both ends are required—reduce above maximum lengths by 20 inches.

Plate requirements in excess of dimensions shown may be submitted for special consideration.

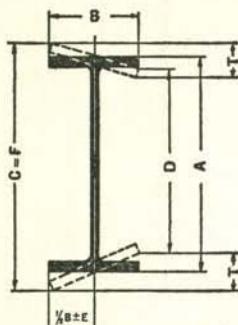
PLATES
**Geneva
District**

STANDARD MILL PRACTICES

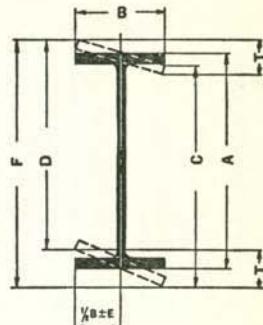
PERMISSIBLE VARIATIONS FOR DIMENSIONS AND WEIGHT

Rolling structural shapes involves factors such as roll wear, subsequent roll dressing, temperature variations, etc., which cause the finished shapes to vary from published profiles. Structural shapes are furnished to standard rolling tolerances published by the American Iron and Steel Institute in "Steel Products Manual: Carbon Steel Structural Sections," August, 1943.

The permissible variation from the theoretical or specified weight is 2.5 per cent.



WIDE
FLANGE BEAMS



SECTION

Nominal Depth, In.	A Depth, In.		B Width of Flange, In.		T or T'	C minus D	E	F Maximum Overall Depth at any Cross-Section, Measured Parallel with Web, In.
	Over	Under	Over	Under	Out of Square, In.	Out of Parallel, In.	Web off Center, In.	Over Nominal
To 12 incl. ^a	1/8	1/8	1/4	3/16	3/16	3/16	3/16	1/4
Over 12	1/8	1/8	1/4	3/16	1/4	1/4	3/16	1/4

^aIncludes all H-Beams rolled on mills having vertical rolls.

LENGTH

Nominal Depth, In.	Variations from Specified Length for Lengths Given, In.			
	To 30 ft., incl.		Over 30 ft.	
	Over	Under	Over	Under
Beams up to 24 incl.	3/8	3/8	3/8 plus 1/16 for each additional 5 ft. or fraction thereof.	3/8
Beams over 24 and all Columns	1/2	1/2	1/2 plus 1/16 for each additional 5 ft. or fraction thereof.	1/2

ENDS OUT-OF-SQUARE

1/64 in. per inch of depth, or of flange width if it is greater than depth.

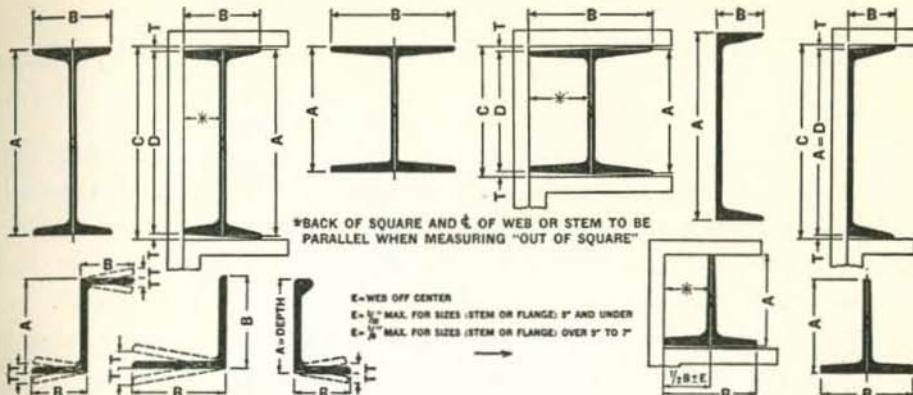
CAMBER OR SWEEP

Beams: 1/8 in. $\times \frac{\text{number of feet of total length}}{10}$

When Ordered As Columns:
$$\left\{ \begin{array}{l} \text{Lengths to 45 ft., inclusive: } 1/8'' \times \frac{\text{number of feet of total length}}{10}, \text{ but not over } 3/8''. \\ \text{Lengths over 45 ft.: } 3/8'' + 1/8'' \times \frac{\text{number of feet of total length, minus 45}}{10} \end{array} \right.$$

STANDARD MILL PRACTICES

PERMISSIBLE VARIATIONS FOR DIMENSIONS



STANDARD BEAMS, H-BEAMS, CHANNELS, ZEES—SECTION

Sections	Specified Size, In.	A Depth, In.		B Flange Width, In.		T or T' Out of Square per Inch of B, In.	Out of Parallel per Inch of B, In. C Minus D
		Over	Under	Over	Under		
Beams	3, 4, 5, 6, 7	3/32	1/16	1/8	1/8	1/32	1/32
	8, 10, 12,	1/8	3/32	5/32	5/32	1/32	1/32
	15, 18, 20, 24	3/16	1/8	3/16	3/16	1/32	1/32
H-Beams*	4	3/32	1/16	1/8	1/8	1/32	1/32
	5	3/32	1/16	5/32	5/32	1/32	1/32
	6 and 8	1/8	3/32	3/16	3/16	1/32	1/32
Channels	3, 4, 5, 6, 7	3/32	1/16	1/8	1/8	1/32	1/32
	8, 9, 10, 12, 13	1/8	3/32	5/32	5/32	1/32	1/32
	15 and 18	3/16	1/8	1/8	3/16	1/32	1/32
Zees	3 and 4	1/8	1/16	1/8	3/32	3/128 ^b
	5 and 8	1/8	1/16	1/8	1/8	3/128 ^b

* These tolerances apply to H-Beams rolled on standard structural mills.

^b 3/128" per inch = 1 1/2".

ANGLES, BULB ANGLES, ROLLED TEES—SECTION

Sections	Specified Size, In.	A Depth, In.		B Flange Width, In. or Length of Leg, In.		T Out of Square per Inch of B, In.
		Over	Under	Over	Under	
Angles*	3, 3 1/2, 4			1/8	3/32	3/128 ^b
	5 and 6			1/8	1/8	3/128 ^b
	7, 8, 9			3/16	1/8	3/128 ^b
Bulb Angles	3 and 4	1/8	1/16	1/8	3/32	3/128 ^b
	5 and 6	1/8	1/16	1/8	1/8	3/128 ^b
	7, 8, 9, 10	1/8	1/16	3/16	1/8	3/128 ^b
Rolled Tees	3, 4, 5	3/32	1/16	1/8	1/8	1/32

* For unequal leg angles, longer leg determines classification.

^b 3/128" per inch = 1 1/2".

ALL STANDARD SECTIONS—LENGTH

Sections	Variations from Specified Length for Lengths Given, In.							
	To 30 ft. incl.		Over 30 ft. to 40 ft. incl.		Over 40 ft. to 50 ft. incl.		Over 50 ft.	
	Over	Under	Over	Under	Over	Under	Over	Under
Beams, Standard Mill								
H-Beams, Channels	3/8	3/8	5/8	3/8	7/8	3/8	1	3/8
Angles, Bulb Angles, Tees, Zees	3/4	0	1	0	1 1/4	0	1 1/4	0

ENDS OUT-OF-SQUARE

Beams, Channels, 1/64 in. per inch of depth.

Standard Mill H-Beams

3/128 in. per inch of leg length or 1 1/2".

Angles*

3/128 in. per inch of depth or 1 1/2".

Bulb Angles

3/128 in. per inch of depth or 1 1/2".

Rolled Tees*

1/64 in. per inch of flange or stem.

Zees

3/128 in. per inch of sum of both flange lengths.

* Tolerances for ends out-of-square are determined on the longer members of the section.

CAMBER

number of feet of total length

5

STANDARD MILL PRACTICES

SURFACE FINISH AND CONDITIONING

Correcting minor imperfections at any location in structural sections by grinding or by chipping to sound metal and depositing weld metal by arc-fusion welding, in accordance with the limitations prescribed below, is regular practice.

Imperfections that do not affect the full utility of the piece shall not be considered as injurious defects. Such pieces may be processed by the following methods in order to give them a workmanlike finish.

- (1) For material less than $3/8$ " in thickness, when the imperfections are not more than $1/32$ " in depth they may be removed by grinding or chipping.
- (2) For material $3/8$ " and over in thickness, when the imperfections are not more than $1/16$ " in depth they may be removed by grinding or chipping.
- (3) For material $3/8$ " and over in thickness, when the imperfections are more than $1/16$ " in depth, the pieces may be chipped and welded under limiting conditions, listed below under "Chipping and Welding."

After the imperfection has been completely removed, the maximum depth of depression shall not exceed the following:

THICKNESS OF MATERIAL INCHES	DEPTH OF DEPRESSION MAXIMUM, INCHES
Grinding or Chipping only	
To $3/8$ " excl.	$1/32$
$3/8$ and over	$1/16$
Chipping and Welding	
$3/8$ to $3/4$ excl.	$3/32$
$3/4$ to $1-1/4$ excl.	$3/16$
$1-1/4$ to $2-1/4$ excl.	$1/4$
$2-1/4$ and over	$3/8$

The cross-sectional area of any piece shall not be reduced by grinding or chipping more than 1.5 per cent at any cross-section, nor shall the total area of the ground or chipped surface of any piece exceed 2 per cent of the total surface area of that piece.

An experienced mill inspector shall inspect the work after the chipping operation to see that the defects have been completely removed and that the limitations specified above have not been exceeded. All welding shall be done by qualified welders using suitable coated welding rods. The welds must be sound; the weld metal being thoroughly fused on all surfaces and edges without under-cutting or overlap. Weld metal shall project at least $1/16$ in. above the rolled surface after welding, and the projecting metal shall be removed by chipping or grinding to make it flush with the rolled surface and produce a workmanlike finish.

STANDARD MILL PRACTICES

CAMBERING OF ROLLED BEAMS

This refers to the cold cambering of large depth beams to produce a predetermined design. The maximum lengths that can be cambered depend on the length that can be rolled of a given section, to a maximum of 100 feet. The maximum cambers that can be furnished and the minimum lengths for given cambers are shown in the following table.

Sections	Maximum Camber, Inches								
	5	4½	4	3½	3	2½	2	1½	1
	Minimum Lengths for Given Camber, Feet								
Wide Flange 24" and over	85	75	65	55	50	45	40	35	30
Wide Flange 21"; Standard 24"	80	70	60	50	45	40	35	30	25

Camber will approximate a simple regular curve nearly the full length of the beam, or between any two points as specified. Reverse or other compound curves can not be undertaken. Camber is to be specified by the ordinate at the mid-length of the portion of the beam to be curved; ordinates at other points are not to be specified. The camber ordinate is subject to a tolerance of nothing under to 1/2 in. over for lengths 50 ft. and less; and for lengths over 50 ft., 1/8 in. is to be added to the over tolerance for each additional 10 ft. or fraction thereof.

MINIMUM CAMBER, IN INCHES, LIKELY TO REMAIN PERMANENT

Wide Flange Sections	Lengths in Feet						
	85	75	65	55	50	45	40
CB 362, 361.....	3½	3	2½	1½	1¼	1	¾
332, 331.....	4	3½	2½	1¾	1½	1¼	1
302, 301.....	4½	3½	2¾	2	1½	1¼	1
272, 271.....	5	4	3	2	1¾	1½	1¼
243, 242, 241.....	5	4½	3¼	2½	2	1½	1¼

Wide Flange Sections and Standard Beams	Lengths in Feet						
	80	70	60	50	45	40	35
CB 213, 212, 211.....	5	4½	3½	2½	1¾	1½	1
24" B18, B1.....	5	3¾	2¾	2	1½	1¼	1

Cambers less than minimum shown above will not be furnished.

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