SET-XP® High-Strength Epoxy Adhesive

SIMPSON Strong-Tie

SET-XP Cure Schedule

Base Materia	l Temperature	Gel Time	Cure Time
°F	°C	(minutes)	(hrs.)
50	10	75	72
60	16	60	48
70	21	45	24
90	32	35	24
110	43	20	24

For water-saturated concrete, the cure times must be doubled.

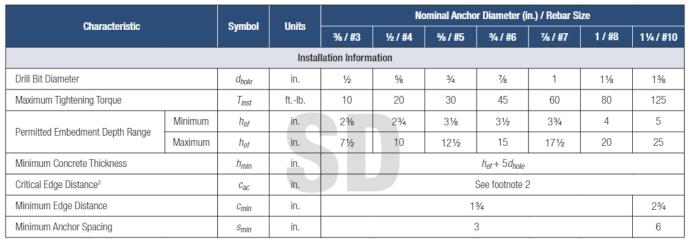
SET-XP Typical Properties

	Dranarhi	Class C	Test
	Property	(>60°F)	Method
Consistency		non-sag	ASTM C881
	Hardened to Hardened Concrete, 2-Day Cure ¹	2,900 psi	
Bond Strength, Slant Shear	Hardened to Hardened Concrete, 14-Day Cure ¹	3,200 psi	ASTM C882
	Fresh to Hardened Concrete, 14-Day Cure ²	2,000 psi	
Compressive Yield Strength, 7-D	lay Cure ²	14,100 psi	ASTM D695
Compressive Modulus, 7-Day Cu	ure ²	612,000 psi	ASTM D695
Heat Deflection Temperature, 7-	Day Cure ²	136°F (58°C)	ASTM D648
Glass Transition Temperature, 7-	Day Cure ²	126°F (52°C)	ASTM E1356
Decomposition Temperature, 24	-Hour Cure ²	500°F (260°C)	ASTM E2550
Water Absorption, 24-Hours, 7-D	Day Cure ²	0.10%	ASTM D570
Shore D Hardness, 24-Hour Cur	e ²	84	ASTM D2240
Linear Coefficient of Shrinkage,	7-Day Cure ²	0.002 in./in.	ASTM D2566
Coefficient of Thermal Expansion	72	2.4 x 10 ⁻⁵ in./in.°F	ASTM C531

- 1. Material and curing conditions: 60° ± 2°F.
- 2. Material and curing conditions: 73° \pm 2°F.

SET-XP Installation Information and Additional Data for Threaded Rod and Rebar¹





- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- 2. $c_{ac} = h_{ef} (\tau_{k,uncr}/1,160)^{0.4} \times [3.1 0.7(h/h_{ef})]$, where:

 $[h/h_{ef}] \leq 2.4$

 $\tau_{k,uncr}$ = the characteristic bond strength in uncracked concrete, given in the tables that follow $\leq k_{uncr} ((h_{ef} \times f_c')^{0.5}/(\pi \times d_{hole}))$

h =the member thickness (inches)

 h_{ef} = the embedment depth (inches)

^{*} See p. 12 for an explanation of the load table icons.

SET-XP® Design Information — Concrete



SET-XP Tension Strength Design Data for Threaded Rod1



Minimum Tensile Stress An Tension Resistance of Stee Tension Resistance of Stee Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 an Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	rea el — ASTM F1554, G el — ASTM A193, Gr el — Type 410 Stainl el — Type 304 and 3 id B8M) — Steel Failure	Grade 36 ade B7	rength in To	ension in ²	0.078 4,525 9,750 8,580	0.142 8,235 17,750	0.226 13,110 28,250	0.334 19,370 41,750	7/8 0.462 26,795 57,750	0.606 35,150 75,750	0.969 56,200 121,125
Tension Resistance of Stee Tension Resistance of Stee Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	el — ASTM F1554, G el — ASTM A193, Gr el — Type 410 Stainl el — Type 304 and 3 d B8M) — Steel Failure	Grade 36 ade B7	A _{se}	in ²	4,525 9,750	8,235	13,110	19,370	26,795	35,150	56,200
Tension Resistance of Stee Tension Resistance of Stee Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	el — ASTM F1554, G el — ASTM A193, Gr el — Type 410 Stainl el — Type 304 and 3 d B8M) — Steel Failure	ade B7			4,525 9,750	8,235	13,110	19,370	26,795	35,150	56,200
Tension Resistance of Stee Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	el — ASTM A193, Gr el — Type 410 Stainl el — Type 304 and 3 d B8M) — Steel Failure	ade B7	N _{sa}	lb.	9,750				-	-	
Threaded Rod Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	el — Type 410 Stainl el — Type 304 and 3 d B8M) — Steel Failure	less	N _{sa}	lb.		17,750	28,250	41,750	57,750	75,750	121 125
(ASTM A193, Grade B6) Tension Resistance of Stee (ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	el — Type 304 and 3 d B8M) — Steel Failure		N _{sa}	lb.	0 500						121,120
(ASTM A193, Grade B8 and Strength Reduction Factor Effectiveness Factor — Uncracked Concrete	d B8M) — Steel Failure	16 Stainless		1	0,500	15,620	24,860	36,740	50,820	66,660	106,590
Effectiveness Factor — Uncracked Concrete					4,445	8,095	12,880	19,040	26,335	34,540	55,235
	Concrete Breal		φ	_				0.757			
		kout Strength i	n Tension (2,500 p	si ≤ f' _C ≤	3,000 psi) ¹	12				
Effectiveness Factor — Cracked Concrete	Effectiveness Factor — Uncracked Concrete			_				24			
Enougeonous Lactor Oracinoa Collorete	Effectiveness Factor — Cracked Concrete			_				17			
Strength Reduction Factor — Breakout Failure			φ	_	0.65 ⁹						
	Bond St	trength in Tensi	on (2,500 p	osi ≤ f'c	≤ 8,000 p	si) ¹²					
Characteristic Bond Streng	yth ^{5,13}		τ _{k,uncr}	psi	770	1,150	1,060	970	885	790	620
Uncracked Concrete 2,3,4 Permitted Embedment Dep	oth Dango	Minimum	h	in.	2%	23/4	31/8	31/2	33/4	4	5
Permitted Embedment Dep	r emilited Embedment Depth hange		h _{ef}	111.	71/2	10	121/2	15	171/2	20	25
Characteristic Bond Streng	yth ^{5,10,11, 13}		τ _{k,cr}	psi	595	510	435	385	355	345	345
Cracked Concrete 2,3,4 Permitted Embedment Den	Permitted Embedment Depth Range		ь	in	3 4	5	6	7	8	10	
Permitted Embedment Dep	our Range	Maximum	h _{ef}	in.	7½ 10	12½	15	171/2	20	25	
Bond Stre	ength in Tension —	Bond Strength	Reduction	Factors	s for Cont	nuous Spe	ecial Inspe	ection			
Strength Reduction Factor — Dry Concrete			фdry, ci	_				0.658			
Strength Reduction Factor — Water-Saturate	ed Concrete — h _{ef} ≤	12d _a	φ _{sat,ci}	_	0.5	55 ⁸			0.458		
Additional Factor for Water-Saturated Concre	ete — h _{ef} ≤ 12d _a		K _{sat,ci} 6	_			1			0.	84
Strength Reduction Factor — Water-Saturate	ed Concrete — h _{ef} >	→ 12d _a	φ _{sat,ci}	_				0.458			
Additional Factor for Water-Saturated Concre	ete — $h_{ef} > 12d_a$		K _{sat,ci} 6	_				0.57			
Bond Str	rength in Tension —	– Bond Strengt	h Reductio	n Facto	rs for Per	iodic Spec	ial Inspec	tion			
Strength Reduction Factor — Dry Concrete			фdry,pi	_				0.558			
Strength Reduction Factor — Water-Saturate	ed Concrete — h _{ef} ≤	12d _a	фsat,pi					0.458			
Additional Factor for Water-Saturated Concre	ete — h _{ef} ≤ 12d _a		K _{sat,pi} 6	_		1		0.93		0.	71
Strength Reduction Factor — Water-Saturate	ed Concrete — h _{ef} >	12d _a	фsat,pi	_				0.458			
Additional Factor for Water-Saturated Concre	ete — h _{ef} > 12d _a		K _{sat,pi} 6	_				0.48			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 or ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature of 150°F. Maximum long-term temperature of 110°F.
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased by 72%.
- 6. In water-saturated concrete, multiply $\tau_{k,uncr}$ and $\tau_{k,cr}$ by K_{sat}
- 7. The value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 8. The value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 9. The value of φ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.4 (c) for Condition B are met. If the load combinations of ACI 318-11 Section 9.2 are used and the requirements of ACI 318-11 D.4.4 (c) for Condition A are met, refer to ACI 318-11 D.4.4 to determine the appropriate value of φ. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.5 to determine the appropriate value of φ.
- 10. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for %" anchors must be multiplied by $\alpha_{N,seis} = 0.80$.
- 11. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 1" anchors must be multiplied by $\alpha_{N,sels} = 0.92$.
- 12. The values of f_c' used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of f_c' used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.

^{*} See p. 12 for an explanation of the load table icons.



SET-XP Tension Strength Design Data for Rebar¹

IBC		IBC	
-----	--	-----	--







	Observatoristic		0					Rebar Siz	e		
	Characteristic		Symbol	Units	#3	#4	#5	#6	#7	#8	#10
		Ste	el Strength in	Tension							
	Minimum Tensile Stress Area		A _{se}	in ²	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Rebar	Tension Resistance of Steel — (ASTM A615 Grade 60)	Rebar	N _{sa}	lb.	9,900	18,000	27,900	39,600	54,000	71,100	110,700
Strength Reduction Factor — Steel Failure			φ	_				0.65 ⁷			
	Concrete Bro	eakout Stren	gth in Tension	(2,500 psi	≤ f' _C ≤ 8,0	000 psi) ¹⁰					
Effectiveness Factor — Unc	racked Concrete		k _{uncr}	_				24			
Effectiveness Factor — Crac	cked Concrete		K _{CT}	_				17			
Strength Reduction Factor —	– Breakout Failure		φ	_				0.65 ⁹			
	Bond	Strength in T	Cension (2,500	psi ≤ f¹ _C ≤	8,000 psi)10					
	Characteristic Bond Strength ^{5,11}		τ _{k,uncr}	psi	895	870	845	820	795	770	720
Uncracked Concrete ^{2,3,4}	Permitted Embedment	Minimum			2%	23/4	31/8	31/2	3¾	4	5
	Depth Range	Maximum	h _{ef}	in.	71/2	10	121/2	15	171/2	20	25
	Characteristic Bond Strength ^{5,11}		$\tau_{\textit{k,cr}}$	psi	365	735	660	590	515	440	275
Cracked Concrete ^{2,3,4}	Permitted Embedment Depth Range	Minimum	h	in	3	4	5	6	7	8	10
		Maximum	- h _{ef}	in.	71/2	10	121/2	15	17½	20	25
	Bond Strength in Tension -	— Bond Strei	ngth Reduction	Factors for	or Continu	ious Spec	ial Inspec	tion			
Strength Reduction Factor —	– Dry Concrete		Φdry,ci	_	0.658						
Strength Reduction Factor —	– Water-Saturated Concrete – h _{ef} :	≤ 12d _a	φsat,ci	_	0.	55 ⁸			0.458		
Additional Factor for Water-S	Saturated Concrete — h _{ef} ≤ 12d _a		K _{sat,ci} 6	_			1			0.	84
Strength Reduction Factor —	– Water-Saturated Concrete – h _{ef} :	> 12d _a	φsat,ci	_				0.458			
Additional Factor for Water-S	Saturated Concrete – h _{ef} > 12d _a		K _{sat,ci} 6	_				0.57			
	Bond Strength in Tension	— Bond Str	ength Reducti	on Factors	for Period	dic Specia	al Inspecti	ion			
Strength Reduction Factor —	– Dry Concrete		Фdry,pi	_				0.558			
Strength Reduction Factor —	– Water-Saturated Concrete – h _{ef} :	≤ 12d _a	Φsat,pi	_				0.458			
Additional Factor for Water-S	Saturated Concrete — h _{ef} ≤ 12d _a		K _{sat,pf} s	_		1		0.93		0.	71
Strength Reduction Factor —	– Water-Saturated Concrete – h _{ef} :	> 12da	Фsat,pi	_				0.458			
Additional Factor for Water-S	Saturated Concrete – h _{ef} > 12d _a		K _{sat,pl} 6	_				0.48			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 or ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature of 150°F. Maximum long-term temperature of 110°F.
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased by 72%.
- 6. In water-saturated concrete, multiply $\tau_{k,uncr}$ and $\tau_{k,cr}$ by K_{sat} .

C-A-2021 @2021 SIMPSON STRONG-TIE COMPANY INC.

- 7. The value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 8. The value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 9. The value of φ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.4 (c) for Condition B are met. If the load combinations of ACI 318-11 Section 9.2 are used and the requirements of ACI 318-11 D.4.4 (c) for Condition A are met, refer to ACI 318-11 D.4.4 to determine the appropriate value of φ. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.5 to determine the appropriate value of φ.
- 10. The values of f'_C used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of f'_C used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.

SET-XP® Design Information — Concrete



SET-XP Shear Strength Design Data for Threaded Rod¹

IBC		LW

Characteristic		Cumbal	ol Units	Nominal Anchor Diameter (in.)							
	onal actoristic		Units	3/8	1/2	%	3/4	7∕8	1	1¼	
	Steel	Strength	in Shea	ır							
	Minimum Shear Stress Area	A _{Se}	in. ²	0.078	0.142	0.226	0.334	0.462	0.606	0.969	
	Shear Resistance of Steel — ASTM F1554, Grade 36			2,260	4,940	7,865	11,625	16,080	21,090	33,720	
	Shear Resistance of Steel — ASTM A193, Grade B7	V _{sa}		4,875	10,650	16,950	25,050	34,650	45,450	72,675	
	Shear Resistance of Steel — Type 410 Stainless (ASTM A193, Grade B6)		lb.	4,290	9,370	14,910	22,040	30,490	40,000	63,955	
Threaded Rod	Shear Resistance of Steel — Type 304 and 316 Stainless (ASTM A193, Grade B8 & B8M)			2,225	4,855	7,730	11,420	15,800	20,725	33,140	
Hou	Reduction for Seismic Shear — ASTM F1554, Grade 36			0.87	0.78		0.	68		0.65	
	Reduction for Seismic Shear — ASTM A193, Grade B7			0.87	0.78		0.	68		0.65	
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B6)	α _{V,seis} 5	_	0.69	0.82		0.75		0.83	0.72	
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B8 & B8M)				0.69	0.82	0.75 0.8			0.83	0.72
	Strength Reduction Factor — Steel Failure	φ	_		0.65 ²						
	Concrete Br	eakout S	trength i	n Shear							
Outside D	iameter of Anchor	d _o	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
Load Bear	ring Length of Anchor in Shear	ℓ _e	in.		Mir	n. of <i>h_{ef}</i> and	d 8 times a	nchor diam	eter		
Strength F	Strength Reduction Factor — Breakout Failure						0.703				
	Concrete F	ryout Str	ength in	Shear							
Coefficien	t for Pryout Strength	K _{CP}	_		1.0) for $h_{ef} < 2$	2.50"; 2.0 1	for $h_{ef} \ge 2.5$	50"		
Strength F	Reduction Factor — Pryout Failure	φ	_				0.704				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- 2. The value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 3. The value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.3 (c) for Condition B are met. If the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.3 (c) for Condition A are met, refer to ACI 318-11 D.4.3 to determine the appropriate value of ϕ . If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 4. The value of φ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 5.3 or ACI 318-11 D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of φ.
- 5. The values of V_{sa} are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, V_{sa} must be multiplied by α_{V,sais} for the corresponding anchor steel type.



SET-XP Shear Strength Design Data for Rebar¹

IBC	
	l B







Characteristic		Symbol	Units	Rebar Size						
		Symbol	Oillo	#3	#4	#5	#6	#7	#8	#10
	Steel Strength in Shear									
	Minimum Shear Stress Area	A _{se}	in ²	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Rebar	Shear Resistance of Steel — Rebar (ASTM A615 Grade 60)	V _{sa}	lb.	4,950	10,800	16,740	23,760	32,400	42,660	66,420
Reduction for Seismic Shear — Rebar (ASTM A615 Grade 60)		α _{V,seis} 5	_	0.85	35 0.88 0.84 0.77		0.59			
	Strength Reduction Factor — Steel Failure	φ	_	0.60²						
Concrete Breakout Strength in Shear										
Outsid	e Diameter of Anchor	d_0	in.	0.375	0.5	0.625	0.75	0.875	1	1.25
Load-E	Bearing Length of Anchor in Shear	ℓ_e	in.		Min	. of <i>h_{ef}</i> and	d 8 times a	nchor diam	eter	
Streng	th Reduction Factor — Breakout Failure	φ	_				0.70 ³			
Concrete Pryout Strength in Shear										
Coeffic	cient for Pryout Strength	K _{CP}	_		1.0) for <i>h_{ef} < 2</i>	2.50"; 2.0	for $h_{ef} \ge 2.5$	50"	
Streng	th Reduction Factor — Pryout Failure	φ	_				0.704			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 or ACI 318-11.
- 2. The value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 3. The value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.3 (c) for Condition B are met. If the load combinations of ACI 318-14 5.3 or ACI 318-15 Section 9.2 are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.3 (c) for Condition A are met, refer to ACI 318-11 D.4.3 to determine the appropriate value of ϕ . If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 4. The value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 5.3 or ACI 318-11 D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- 5. The values of V_{Sa} are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, V_{Sa} must be multiplied by α_{V,Sals}.

For additional load tables, visit **strongtie.com/setxp**.



C-A-2021 @2021 SIMPSON STRONG-TIE COMPANY INC.

Anchor Designer[™] Software for ACI 318, ETAG and CSA

Simpson Strong-Tie® Anchor Designer software accurately analyzes existing design or suggests anchor solutions based on user-defined design elements in cracked and uncracked concrete conditions.

SET-XP® Design Information — Concrete



SET-XP Development Length for Rebar Dowels







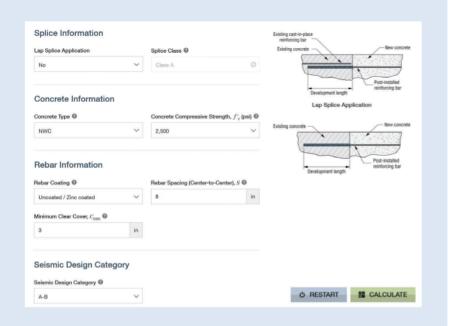


				Dev	elopment Length, in. (mm)	
Rebar Size	Drill Bit Diameter (in.)	Clear Cover in. (mm)	f' _c = 2,500 psi (17.2 MPa) Concrete	f' _c = 3,000 psi (20.7 MPa) Concrete	f' _c = 4,000 psi (27.6 MPa) Concrete	f' _c = 6,000 psi (41.4 MPa) Concrete	f' _c = 8,000 psi (55.2 MPa) Concrete
#3 (9.5)	1/2	1 ½ (38)	12 (305)	12 (305)	12 (305)	12 (305)	12 (305)
#4 (12.7)	5/8	1 ½ (38)	14.4 (366)	14 (356)	12 (305)	12 (305)	12 (305)
#5 (15.9)	3/4	1 ½ (38)	18 (457)	17 (432)	14.2 (361)	12 (305)	12 (305)
#6 (19.1)	7/8	1 ½ (38)	21.6 (549)	20 (508)	17.1 (434)	14 (356)	13 (330)
#7 (22.2)	1	3 (76)	31.5 (800)	29 (737)	25 (635)	21 (533)	18 (457)
#8 (25.4)	11//8	3 (76)	36 (914)	33 (838)	28.5 (724)	24 (610)	21 (533)
#9 (28.7)	1%	3 (76)	40.5 (1,029)	38 (965)	32 (813)	27 (686)	23 (584)
#10 (32.3)	1%	3 (76)	45 (1,143)	42 (1,067)	35.6 (904)	30 (762)	26 (660)
#11 (35.8)	1¾	3 (76)	51 (1,295)	47 (1,194)	41 (1,041)	33 (838)	29 (737)

- 1. Tabulated development lengths are for static, wind and seismic load cases in Seismic Design Category A and B. Development lengths in SDC C through F must comply with ACI 318-14 Chapter 18 or ACI 318-11 Chapter 12, as applicable. The value of f'_C used to calculate development lengths shall not exceed 2,500 psi in SDC C through F.
- 2. Rebar is assumed to be ASTM A615 Grade 60 or A706 (f_y = 60,000 psi). For rebar with a higher yield strength, multiply tabulated values by f_y / 60,000 psi.
- 3. Concrete is assumed to be normal-weight concrete. For lightweight concrete, multiply tabulated values by 1.33.
- 4. Tabulated values assume bottom cover of less than 12" cast below rebars ($\Psi_t = 1.0$).
- 5. Uncoated rebar must be used.
- 6. The value of K_{tr} is assumed to be 0. Refer to ACI 318-14 Section 25.4.2.3 or ACI 318 Section 12.2.3.

Rebar Development Length Calculator

Rebar Development Length Calculator is a web application that supports the design of post-installed rebar in concrete applications by calculating the necessary tension and compression development lengths required in accordance with ACI 318-18 / ACI 318-14.





SET-XP Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction 1, 3, 4, 5, 6, 8, 9, 10, 11

IBC	1	→		*
	2572 6752	337 Est	据3	

Diameter (in.) or	Drill Bit Diameter	Minimum Embedment ²	Allowable Load Based	on Bond Strength ⁷ (lb.)
Rebar Size Ńo.	(in.)	(in.)	Tension Load	Shear Load
	Threade	ed Rod Installed in the Face of C	MU Wall	
3/8	1/2	3%	1,490	1,145
1/2	5/8	4½	1,825	1,350
5/8	3/4	5%	1,895	1,350
3/4	7/8	6½	1,895	1,350
	Reb	ar Installed in the Face of CMU	Wall	
#3	1/2	3%	1,395	1,460
#4	5/8	41/2	1,835	1,505
#5	3/4	5%	2,185	1,505

- 1. Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on p. 43.
- 2. Embedment depth shall be measured from the outside face of masonry wall.
- Critical and minimum edge distance and spacing shall comply with the information on p. 38. Figure 2 on p. 38 illustrates critical and minimum edge and end distances.
- 4. Minimum allowable nominal width of CMU wall shall be 8". No more than one anchor shall be permitted per masonry cell.
- Anchors shall be permitted to be installed at any location in the face of the fully grouted masonry wall construction (cell, web, bed joint), except anchors shall not be installed within 1 ½" of the head joint, as show in Figure 2 on p. 38.
- 6. Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 7. Tabulated allowable loads are based on a safety factor of 5.0.
- 8. Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 below, as applicable.
- 9. Threaded rod and rebar installed in fully grouted masonry walls are permitted to resist dead, live, seismic and wind loads.
- 10. Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 11. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.

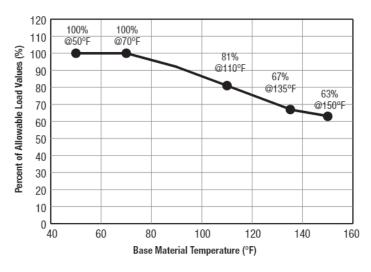


Figure 1. Load Capacity Based on In-Service Temperature for SET-XP® Epoxy Adhesive in the Face of Fully Grouted CMU Wall Construction

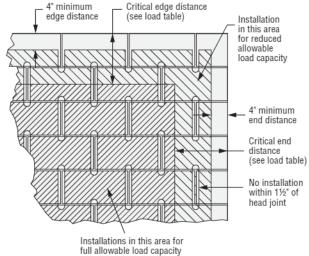
SIMPSON Strong-Tie

SET-XP Edge Distance and Spacing Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction⁷

$\overline{}$			C BEST	CARRY O	+
IBC	₽	0 0			*

		Edge or End Distance ^{1,8}						Spacing ^{2,9}					
		Critical (Full Anchor Capacity) ³ (Redu			Minimum ced Anchor Capacity)⁴			Critical (Full Anchor Capacity)⁵		Minimum (Reduced Anchor Capacity) ⁶			
Rod Dia. (in.) or Rebar Size	Minimum Embed. Depth (in.)	Critical Edge or End Distance, <i>C_{cr}</i> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, <i>C_{min}</i> (in.)	Allowable Load Reduction Factor			Critical Spacing, <i>S_{cr}</i> (in.)	Allowable Load Reduction Factor	Minimum Spacing, S _{min} (in.)		ole Load on Factor	
No.		Load D	irection		Load Direction		Load Direction		Load Direction				
		Tension or	Tension or	Tension or	Tension	Shea	ar ¹⁰	Tension or	Tension or	Tension or	Tension	Shear	
		Shear	Shear	Shear	lension	Perp.	Para.	Shear	Shear	Shear	Tonoidi Circui	Olicai	
3/8	3%	12	1.00	4	0.91	0.72	0.94	8	1.00	4	1.00	1.00	
1/2	41/2	12	1.00	4	1.00	0.58	0.87	8	1.00	4	0.82	1.00	
5/8	5%	12	1.00	4	1.00	0.48	0.87	8	1.00	4	0.82	1.00	
3/4	61/2	12	1.00	4	1.00	0.44	0.85	8	1.00	4	0.82	1.00	
#3	3%	12	1.00	4	0.96	0.62	0.84	8	1.00	4	0.87	0.91	
#4	41/2	12	1.00	4	0.88	0.54	0.82	8	1.00	4	0.87	0.91	
#5	5%	12	1.00	4	0.88	0.43	0.82	8	1.00	4	0.87	1.00	

- Edge distance (C_{Cr} or C_{min}) is the distance measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 2 below for an illustration showing critical and minimum edge and end distances.
- 2. Anchor spacing (S_{cr} or S_{min}) is the distance measured from centerline to centerline of two anchors.
- Critical edge distance, C_{cr}, is the least edge distance at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge distance, C_{min}, is the least edge distance where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance, C_{cr}, by the load reduction factors shown above.
- Critical spacing, S_{cr.} is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adjacent anchors.
- Minimum spacing, S_{min}, is the least spacing where an anchors has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance, S_{cr}, by the load reduction factors shown above.
- 7. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 8. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 9. Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 on p. 40). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.



Shaded area = Placement for full and reduced allowable load capacity in grout-filled CMU

Figure 2. Allowable Anchor Locations for Full and Reduced Load Capacity When Installation Is in the Face of Fully Grouted CMU Masonry Wall Construction



SET-XP Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction 1, 2, 4, 5, 6, 7, 9, 10, 11, 12

IBC +	*
-------	---

Diameter (in.) or	Drill Bit Diameter	Minimum Embedment ³	Allowable Load Based on Bond Strength ^{7,8} (lb.)					
Rebar Size Ńo.	(in.)	(in.)	Tension Load	Shear Perp.	Shear Parallel			
		Threaded Rod In	nstalled in the Top of CMU Wa	all				
1/	5/8	41/2	1,485	590	1,050			
1/2 5/8	78	12	2,440	665	1,625			
5/	3/.	5%	1,700	565	1,435			
5/8 3/4	94	15	2,960	660	1,785			
7/8	1	77/8	1,610	735	1,370			
78		21	4,760 670		1,375			
		Rebar Instal	led in the Top of CMU Wall					
#4	5/8	41/2	1,265	550	865			
#4	9/8	12	2,715	465	1,280			
μг	2/	5%	1,345	590	1,140			
#5	3/4	15	3,090	590	1,285			

- 1. Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on p. 43.
- 2. Allowable loads are for installation in the grouted CMU core opening.
- 3. Embedment depth shall be measured from the horizontal surface of the grouted CMU core opening on top of the masonry wall.
- 4. Critical and minimum edge distance, end distance and spacing shall comply with the information on pp. 38 and 40. Figures 3A and 3B on p. 40 illustrate critical and minimum edge and end distances.
- 5. Minimum allowable nominal width of CMU wall shall be 8" (203 mm).
- 6. Anchors are permitted to be installed in the CMU core opening shown in Figures 3A and 3B on p. 40. Anchors are limited to one installation per CMU core opening.
- 7. Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 8. Tabulated allowable loads are based on a safety factor of 5.0.
- 9. Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 on p. 37, as applicable.
- 10. Threaded rod and rebar installed in fully grouted masonry walls with SET-XP® adhesive are permitted to resist dead, live, seismic and wind loads.
- 11. Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 12. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.



SET-XP Edge and End Distance Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction 1,4,5

IBC 🞵	
-------	--









		Critical (Full Anchor Capacity) ²			Minimum End (Reduced Anchor Capacity) ³				Minimum Edge (Reduced Anchor Capacity) ⁶			
Rod Dia. (in.) or Rebar	Minimum Embed. Depth	Critical Edge, <i>C_{cr}</i> (in.)	Critical End Distance, C _{cr} (in.)	Allowable Load Reduction Factor	Minimum End Distance, <i>C_{min}</i> (in.)		Minimum I Allowable L eduction Fac		Minimum Edge, <i>C_{min}</i> (in.)		lowable Loa duction Fac	
Size No.	(in.)	ı	Load Direction	n		Load D	irection			Load Dir	ection	
		Tension or	Tension or	Tension or	Tension or	Tension	Sh	ear ⁶	Tension or	Tension	Sh	ear ⁶
		Shear	Shear	Shear	Shear	ICHSIOII	Perp.	Parallel	Shear		Perp.	Parallel
1/2	41/2	23/4	20	1.00	313/16	0.88	0.84	0.66	13/4	0.83	0.63	0.77
72	12	23/4	20	1.00	313/16	0.64	0.91	0.34	13/4	0.95	0.55	0.69
5/8	5%	23/4	20	1.00	41/4	0.90	1.00	0.50	13/4	0.82	0.57	0.71
7/8	15	23/4	20	1.00	41/4	0.38	0.85	0.29	13/4	0.91	0.72	0.73
7/8	71/8	23/4	20	1.00	41/4	0.98	0.72	0.57	_	_	_	_
1/8	21	23/4	20	1.00	41/4	0.63	0.96	0.64	_	_	_	_
#4	41/2	23/4	20	1.00	41/4	0.96	0.90	0.76	_	_	_	_
#4	12	23/4	20	1.00	41/4	0.58	1.00	0.46	_	_	_	_
#5	5%	23/4	20	1.00	41/4	1.00	0.86	0.60	_	_	_	_
#3	15	2¾	20	1.00	41/4	0.41	0.76	0.49	_	_	_	

- 1. Edge and end distances (C_{cr} or C_{min}) are the distances measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figures 3A and 3B below for illustrations showing critical and minimum edge and end distances.
- 2. Critical edge and end distances, C_{cr} , are the least edge distances at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 3. Minimum edge and end distances, Cmin, are the least edge distances where an anchor has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance, C_{cr} , by the load reduction factors shown above.
- 4. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 5. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 6. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 below). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.

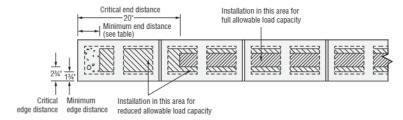


Figure 3A. Allowable Anchor Locations of 1/2" - and 5/4" - Diameter Threaded Rod for Full and Reduced Load Capacity When Installation Is in the Top of Fully Grouted CMU Masonry Wall Construction

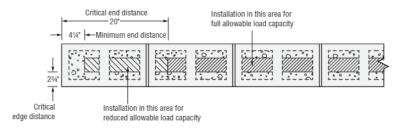
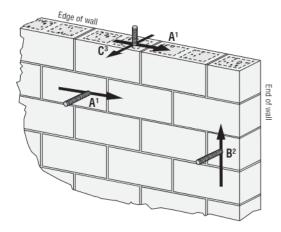


Figure 3B. Allowable Anchor Locations of %"-Diameter Threaded Rod and #4 and #5 Rebar for Full and Reduced Load Capacity When Installation Is in the Top of Fully Grouted CMU Masonry Wall Construction



- 1. Direction of shear load A is parallel to edge of wall and perpendicular to end of wall.
- 2. Direction of shear load B is parallel to end of wall and perpendicular to edge of wall.
- Direction of shear load C is perpendicular to edge of wall.

Figure 5. Direction of Shear Load in Relation to Edge and End of Wall

^{*} See p. 12 for an explanation of the load table icons.



SET-XP Spacing Distance Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction^{1,4,5}



Rod Dia. (in.) or Rebar		Critical (Full Ancho	Spacing or Capacity) ²	Minimum Spacing (Reduced Anchor Capacity) ³			
	Minimum Embed. Depth	Critical Spacing, <i>S_{cr}</i> (in.)	Allowable Load Reduction Factor	Minimum Spacing, <i>S_{cr}</i> (in.)	Allowable Load Reduction Factor		
Size No.	(in.)	Load D	Direction		Load Direction		
		Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear	
1/	41/2	18	1.00	8	0.80	0.92	
1/2	12	48	1.00	8	0.63	0.98	
E/	5%	22.5	1.00	8	0.86	1.00	
5/8	15	60	1.00	8	0.56	1.00	
7/	7%	31.5	1.00	8	0.84	0.82	
7/8	21	84	1.00	8	0.51	0.98	
11.4	41/2	18	1.00	8	0.97	0.93	
#4	12	48	1.00	8	0.75	1.00	
ur.	5%	22.5	1.00	8	1.00	1.00	
#5	15	60	1.00	8	0.82	1.00	

- 1. Anchor spacing (S_{cr} or S_{min}) is the distance measured from centerline to centerline of two anchors.
- Critical spacing, S_{Cr}, is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor perofrmance is not influenced by adjacent anchors.
- 3. Minimum spacing, S_{min} , is the least spacing where an anchor has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance, S_{cr} , by the load reduction factors shown above.
- 4. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 5. Load reduction factor for anchors loaded in tension or shear with spacing critical and minimum shall be obtained by linear interpolation.

SET-XP Allowable Tension and Shear Loads — Threaded Rod in the Face of Hollow CMU Wall Construction^{1,3,4,5,6,8,9,10,11}



Diameter	Drill Bit Diameter	Minimum Embed. ²	Allowable Load Based on Bond Strength ⁷ (lb.)			
(in.)	(in.)	(in.)	Tension	Shear		
3/8	%16	11/4	215	385		
1/2	3/4	11/4	220	410		
5/8	7/8	11/4	225	435		

- 1. Allowable load shall be the lesser of bond values shown in this table and steel values shown on p. 43.
- 2. Embedment depth is considered the minimum wall thickness of 8" x 8" x 16" ASTM C90 concrete masonry blocks, and is measured from the outside to the inside face of the block wall. The minimum length Opti-Mesh plastic screen tube for use in hollow CMU is 3 ½".
- 3. Critical and minimum edge distance and spacing shall comply with the information provided on p. 42. Figure 4 on p. 42 illustrates critical and minimum edge and end distances.
- 4. Anchors are permitted to be installed in the face shell of hollow masonry wall construction as shown in Figure 4.
- 5. Anchors are limited to one or two anchors per masonry cell and must comply with the spacing and edge distance requirements provided.
- 6. Tabulated load values are for anchors installed in hollow masonry walls.
- 7. Tabulated allowable loads are based on a safety factor of 5.0.
- Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 on p. 37, as applicable.
- 9. Threaded rods installed in hollow masonry walls with SET-XP® adhesive are permitted to resist dead, live load and wind load applications.
- 10. Threaded rods must meet or exceed the tensile strength of ASTM F1554, Grade 36, which is 58,000 psi.
- 11. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads must be multiplied by 0.80.
- 12. Screen tubes are required and available on p. 71.

C-A-2021 @2021 SIMPSON STRONG-TIE COMPANY INC.



SET-XP Edge, End and Spacing Distance Requirements and Allowable Load Reduction Factors — Threaded Rod in the Face of Hollow CMU Wall Construction⁷

CONTROL TOPOPHIC MES	IBC			Almann.	Ē
----------------------	-----	--	--	---------	---

		Edge or End Distance ^{1,8}					Spacing ^{2,9}					
	Crit (Full Ancho		Minimum (Reduced Anchor Capacity) ⁴				ical r Capacity) ⁵	Minimum (Reduced Anchor Capacity) ⁶				
Rod Diameter (in.)	Critical Edge or End Distance, <i>C_{cr}</i> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, <i>C_{min}</i> (in.)	Allowab Reductio	ole Load on Factor	Critical Spacing, <i>S_{cr}</i> (in.)	Allowable Load Reduction Factor	Minimum Spacing, <i>S_{min}</i> (in.)	Allowat Reductio	ole Load on Factor		
	Load Di	irection		Load Direction		Load Direction		Load Direction				
	Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear ¹⁰	Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear		
3/8	12	1.00	4	1.00	0.74	8	1.00	4	0.82	0.73		
1/2	12	1.00	4	0.96	0.69	8	1.00	4	0.79	0.73		
5/8	12	1.00	4	0.96	0.55	8	1.00	4	0.75	0.73		

- Edge and end distances (C_{cr} or C_{min}) are the distances measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 4 below for an illustration showing critical and minimum edge and end distances.
- Anchor spacing (S_{cr} or S_{min}) is the distance measured from centerline to centerline of two anchors.
- Critical edge and end distances, C_{Cr}, are the least edge distances at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge and end distances, C_{min}, are the least edge distances where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance, C_{Cr}, by the load reduction factors shown above.
- Critical spacing, S_{cn} is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adjacent anchors.
- Minimum spacing, S_{min}, is the least spacing where an anchors has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance, S_{cr}, by the load reduction factors shown above.
- 7. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 8. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 9. Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act toward the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 on p. 40). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.
- 11. Screen tubes are required and available on p. 71.

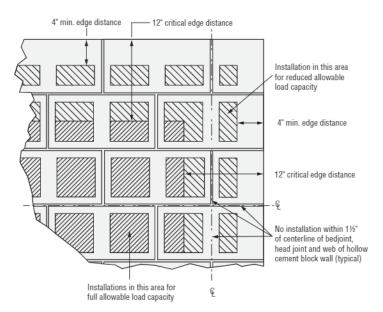


Figure 4. Allowable Anchor Locations for Full and Reduced Load Capacity When Installation Is in the Face of Hollow CMU Masonry Wall Construction

SET-XP® Design Information — Steel

SIMPSON
Strong-Tie

SET-XP Allowable Tension and Shear Loads — Threaded Rod Based on Steel Strength¹

IBC	1	→	*
$\overline{}$	G2.0 B.02	Co. 6 12 12 12 12 12 12 12 12 12 12 12 12 12	_ B:3

		Tension	Load Based o	on Steel Streng	jth² (lb.)	Shear Load Based on Steel Strength ³ (lb.)				
Threaded Tensile Rod Stress			Stainle	ss Steel			Stainless Steel			
Diameter (in.)	Diameter Area	ASTM F1554 Grade 364	ASTM A193 Grade B7 ⁶	ASTM A193 Grade B6 ⁵	ASTM A193 Grades B8 and B8M ⁷	ASTM F1554 Grade 36 ⁴	ASTM A193 Grade B7 ⁶	ASTM A193 Grade B6 ⁵	ASTM A193 Grades B8 and B8M ⁷	
3/8	0.078	1,495	3,220	2,830	1,930	770	1,660	1,460	995	
1/2	0.142	2,720	5,860	5,155	3,515	1,400	3,020	2,655	1,810	
5/8	0.226	4,325	9,325	8,205	5,595	2,230	4,805	4,225	2,880	
3/4	0.334	6,395	13,780	12,125	8,265	3,295	7,100	6,245	4,260	
7/8	0.462	8,845	19,055	16,770	11,435	4,555	9,815	8,640	5,890	

- 1. Allowable load shall be the lesser of bond values given on pp. 43, 43 or 43 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on the following equation: $F_t = 0.33 \times F_u \times Tensile Stress Area$.
- 3. Allowable Shear Steel Strength is based on the following equation: $F_v = 0.17 \text{ x } F_u \text{ x Tensile Stress Area.}$
- 4. Minimum specified tensile strength (Fu = 58,000 psi) of ASTM F1554, Grade 36 used to calculate allowable steel strength.
- 5. Minimum specified tensile strength (F_u = 110,000 psi) of ASTM A193, Grade B6 used to calculate allowable steel strength.
- 6. Minimum specified tensile strength (F_u = 125,000 psi) of ASTM A193, Grade B7 used to calculate allowable steel strength.
- 7. Minimum specified tensile strength (F_U = 75,000 psi) of ASTM A193, Grades B8 and B8M used to calculate allowable steel strength.

SET-XP® Allowable Tension and Shear Loads — Deformed Reinforcing Bar Based on Steel Strength¹



Rebar Size	Tensile Stress Area (in.²)	Tension Load (lb.) Based on Steel Strength		Shear Load (lb.) Based on Steel Strength	
		#3	0.11	2,200	2,640
#4	0.20	4,000	4,800	2,380	3,060
#5	0.31	6,200	7,440	3,690	4,745

- 1. Allowable load shall be the lesser of bond values given on pp. 43, 43 or 43 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (20,000 psi x tensile stress area) for Grade 40 rebar.
- 3. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (24,000 psi x tensile stress area) for Grade 60 rebar.
- 4. Allowable Shear Steel Strength is based on AC58 Section 3.3.3 ($F_v = 0.17 \times F_u \times Tensile Stress Area.$)
- 5. $F_u = 70,000$ psi for Grade 40 rebar.
- 6. $F_U = 90,000$ psi for Grade 60 rebar.

C-A-2021 @2021 SIMPSON STRONG-TIE COMPANY INC.