

The following excerpt are pages from the North American Product Technical Guide, Volume 2: Anchor Fastening, Edition 22.

Please refer to the publication in its entirety for complete details on this product including data development, product specifications, general suitability, installation, corrosion and spacing and edge distance guidelines.

US&CA: https://submittals.us.hilti.com/PTGVol2/

To consult directly with a team member regarding our anchor fastening products, contact Hilti's team of technical support specialists between the hours of 7:00am – 6:00pm CST.

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3.3.10 KWIK HUS CARBON STEEL SCREW ANCHOR

PRODUCT DESCRIPTION

KWIK HUS (KH) Carbon Steel Screw Anchor

Anchor System Features and Benefits Quick and easy to install. Carbon Steel KH Length and diameter identification clearly stamped on head facilitates quality control and inspection after installation. • Through fixture installation improves productivity and accurate installation. · Thread design enables quality setting and exceptional load values in wide variety of base material strengths. Anchor is fully removable Anchor size is same as drill bit size and uses standard diameter drill bits. Suitable for reduced edge distances and spacing. Suitable for uncracked normal-weight concrete, lightweight concrete







Grout-filled concrete masonry

MATERIAL SPECIFICATIONS

Hilti KWIK HUS anchors are manufactured from carbon steel. The anchors are dull zinc plated to a minimum thickness of 8 µm.

INSTALLATION PARAMETERS

Figure 1 — Hilti KWIK HUS anchor installation details

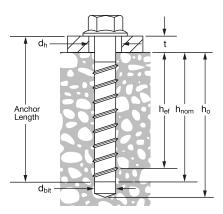


Table 1 — Hilti KWIK HUS specifications

						Nor	ninal and	hor diam	eter			
Setting information	Symbol	Units		3/8			1/2		5,	/8	3,	/4
Nominal bit diameter	d _{bit}	in.		3/8			1/2		5,	/8	3,	/4
Fixture hole diameter	d _h	in.		1/2			5/8		3,	/4	7,	/8
Installation torque ¹	T _{inst}	ft-lb	40 45 85					35	9	5		
Maximum impact wrench torque rating ²	T _{impact,max}	ft-lb	114	4	50	137	4	50	4	50	4	50
Nominal embedment	h _{nom}	in.	1-5/8	2-1/2	3-1/4	<u> </u>			3-1/4	5	4	6-1/4
Effective embedment	h _{ef}	in.	1.11	1.86	2.20	1.52	2.16	3.22	2.39	3.88	2.92	4.84
Minimum hole depth	h _o	in.	1-7/8 2-3/4 3-1/2 2		2-5/8	3-3/8	4-5/8	3-5/8	5-3/8	4-3/8	6-5/8	
Critical edge distance	C _{ac}	in.	2.50	3.12	3.74	2.75	3.70	5.25	3.63	5.81	4.41	7.28
Minimum spacing at critical edge distance	S _{min,cac}	in.		2.25				3			4	4
Minimum edge distance	C _{min}	in.		1.50					1.75			
Minimum spacing at minimum edge distance	S _{min}	in.					3				4	4
Minimum concrete thickness	h _{min}	in.	3-1/4 4 4-7/8			3-3/4	4-3/4	6-3/4	5	7	6	8-1/8
Wrench size	-	in.	n. 9/16 3/4 15/16					1-	1/8			
Effective tensile stress area	A _{se}	in ²	in ² 0.086 0.161 0.268				0.3	392				
Minimum specified ultimate strength	f _{uta}	psi	si 107,120 97,140 90,180 81,600					600				

¹ T_{inst} applies to installations using a calibrated torque wrench.

² Because of variability in measurement procedures, the published torque of an impact tool may not correlate properly with the above setting torques. Over-torquing can damage the anchor and/or reduce its holding capacity.



DESIGN INFORMATION IN CONCRETE PER ACI 318

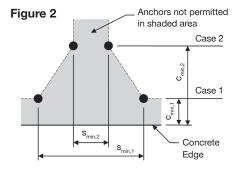
ACI 318 Chapter 17 design

The technical data contained in this section are Hilti Simplified Design Tables. The load values were developed using the Strength Design equations of ACI 318 Chapter 17. KWIK HUS anchor were tested and the test results were evaluated in accordance with ACI 355.2 and AC193. An ICC-ES evaluation report was not published with this information. For a detailed explanation of the Hilti Simplified Design Tables, refer to section 3.1.8.

Table 2 — Hilti KWIK HUS design strength with concrete / pullout failure in uncracked concrete 1,2,3,4,5

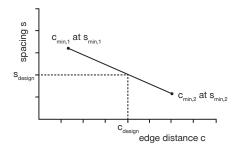
Nominal	Nominal		Tensio	n - φN _n			Shear	· - фV _п	
anchor diameter	embed. in. (mm)	f' _c = 2,500 psi lb (kN)	f' _c = 3,000 psi lb (kN)	f' _c = 4,000 psi lb (kN)	f' _c = 6,000 psi lb (kN)	f' _c = 2,500 psi lb (kN)	f' _c = 3,000 psi lb (kN)	f' _c = 4,000 psi lb (kN)	f'c = 6,000 psi lb (kN)
	1-5/8	910	1,000	1,155	1,415	980	1,075	1,245	1,520
	(41)	(4.0)	(4.4)	(5.1)	(6.3)	(4.4)	(4.8)	(5.5)	(6.8)
3/8	2-1/2	1,980	2,165	2,505	3,065	2,130	2,335	2,695	3,300
3/0	(64)	(8.8)	(9.6)	(11.1)	(13.6)	(9.5)	(10.4)	(12.0)	(14.7)
	3-1/4	2,545	2,790	3,220	3,945	2,740	3,005	3,465	4,245
	(83)	(11.3)	(12.4)	(14.3)	(17.5)	(12.2)	(13.4)	(15.4)	(18.9)
	2-1/4	1,460	1,600	1,850	2,265	1,575	1,725	1,990	2,440
	(57)	(6.5)	(7.1)	(8.2)	(10.1)	(7.0)	(7.7)	(8.9)	(10.9)
1 /0	3	2,475	2,710	3,130	3,835	2,665	2,920	3,375	4,130
1/2	(76)	(11.0)	(12.1)	(13.9)	(17.1)	(11.9)	(13.0)	(15.0)	(18.4)
	4-1/4	4,505	4,935	5,700	6,980	9,705	10,635	12,280	15,040
	(108)	(20.0)	(22.0)	(25.4)	(31.0)	(43.2)	(47.3)	(54.6)	(66.9)
	3-1/4	3,240	3,550	4,100	5,025	3,490	3,825	4,415	5,410
F /O	(83)	(14.4)	(15.8)	(18.2)	(22.4)	(15.5)	(17.0)	(19.6)	(24.1)
5/8	5	6,705	7,345	8,485	10,390	14,445	15,825	18,270	22,380
	(127)	(29.8)	(32.7)	(37.7)	(46.2)	(64.3)	(70.4)	(81.3)	(99.6)
	4	4,380	4,795	5,540	6,785	9,430	10,330	11,930	14,610
0 /4	(102)	(19.5)	(21.3)	(24.6)	(30.2)	(41.9)	(45.9)	(53.1)	(65.0)
3/4	6-1/4	9,345	10,235	11,820	14,475	20,125	22,045	25,455	31,175
	(159)	(41.6)	(45.5)	(52.6)	(64.4)	(89.5)	(98.1)	(113.2)	(138.7)

¹ See section 3.1.8 to convert design strength value to ASD value.



For a specific edge distance, the permitted spacing is calculated as follows:

$$s \geq s_{min,2}^{} + \frac{(s_{min,1}^{} - s_{min,2}^{})}{(c_{min,1}^{} - c_{min,2}^{})} \ (c - c_{min,2}^{})$$



² Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³ Apply spacing, edge distance, and concrete thickness factors in tables 4 to 7 as necessary. Compare to steel values in table 3. The lesser of the values is to be used for the design.

⁴ Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: for sand-lightweight, λ_a = 0.68; for all-lightweight, λ_a = 0.60

⁵ Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Table 3 — Steel design strength for Hilti KWIK HUS anchors^{1,2}

	Hilti KWIK H	IUS anchors
Nominal anchor diameter	Tensile ^{1,3} φN _{sa} lb (kN)	Shear ^{2,4} ϕV_{sa} Ib (kN)
2 /0	5,990	3,095
3/8	(26.6)	(13.8)
1/2	10,165	4,910
1/2	(45.2)	(21.8)
5/8	15,735	6,735
5/6	(70.0)	(30.0)
3/4	20,810	9,995
3/4	(92.6)	(44.5)

¹ See section 3.1.8 to convert design strength value to ASD value.

Table 4 — Load adjustment factors for 3/8-in. diameter Hilti KWIK HUS in uncracked concrete^{1,2}

												Edg	e distar	nce in s	hear					
	/8-in. KI			cing fa		_ ~	je dista			icing fa					II to	and av	way	Conc.	thickne	ss fac-
u	ncracke	d	ir	tensio	n	facto	or in ter	nsion	i	n shear	3	⊥ to	ward e	edge	fr	om edg	je	tor	r in she	ar ⁴
C	concrete)		f_{\scriptscriptstyleAN}			f_{\scriptscriptstyleRN}			f_{AV}			$f_{_{RV}}$			f_{\scriptscriptstyleRV}			f_{\scriptscriptstyleHV}	
Embe	dment	in.	1-5/8	2-1/2	3-1/4	1-5/8	2-1/2	3-1/4	1-5/8	2-1/2	3-1/4	1-5/8	2-1/2	3-1/4	1-5/8	2-1/2	3-1/4	1-5/8	2-1/2	3-1/4
h,	nom	(mm)	(41)	(64)	(83)	(41)	(64)	(83)	(41)	(64)	(83)	(41)	(64)	(83)		(64)	(83)	(41)	(64)	(83)
	1-1/2	(38)	n/a	n/a	n/a	0.61	0.59	0.54	n/a	n/a	n/a	0.49	0.25	0.20	0.61	0.50	0.40	n/a	n/a	n/a
	2	(51)	n/a	n/a	n/a	0.80	0.70	0.62	n/a	n/a	n/a	0.75	0.38	0.31	0.80	0.70	0.62	n/a	n/a	n/a
	2-1/4	(57)	0.84	0.70	0.67	0.90	0.76	0.67	0.65	0.60	0.59	0.90	0.46	0.37	0.90	0.76	0.67	n/a	n/a	n/a
	2-1/2	(64)	0.88	0.72	0.69	1.00	0.82	0.72	0.67	0.61	0.60	1.00	0.54	0.43	1.00	0.82	0.72	n/a	n/a	n/a
e	3	(76)	0.95	0.77	0.73		0.96	0.82	0.71	0.63	0.61		0.71	0.57		0.96	0.82	n/a	n/a	n/a
concrete	3-1/4	(83)	0.99	0.79	0.75		1.00	0.87	0.72	0.64	0.62		0.80	0.64		1.00	0.87	0.95	n/a	n/a
Ö	3-1/2	(89)	1.00	0.81	0.77			0.94	0.74	0.65	0.63		0.89	0.71			0.94	0.98	n/a	n/a
\ <u> </u>	4	(102)		0.86	0.80			1.00	0.78	0.68	0.65		1.00	0.87			1.00	1.00	0.84	n/a
distance (c_a) / $(h) - in$. (mm)	4-1/2	(114)		0.90	0.84				0.81	0.70	0.67			1.00					0.89	n/a
in. (4-7/8	(124)		0.94	0.87				0.84	0.71	0.69								0.93	0.86
- i	5	(127)		0.95	0.88				0.84	0.72	0.69								0.94	0.87
disi (T)	6	(152)		1.00	0.95				0.91	0.76	0.73								1.00	0.96
ge o	7	(178)			1.00				0.98	0.81	0.77									1.00
edge . kness	8	(203)							1.00	0.85	0.80									
< .∪	9	(229)								0.90	0.84									
g (s	10	(254)								0.94	0.88									
-Gi	11	(279)								0.98	0.92									
Spacing (s) thi	12	(305)								1.00	0.96									
(I)	14	(356)									1.00									
	16	(406)																		
	18	(457)																		
	20	(508)																		
	24	(610)																		

¹ Linear interpolation not permitted.

If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 1 and figure 2 of this section to calculate permissable edge distance, spacing and concrete thickness combinations.

² Hilti KWIK HUS anchors are to be considered brittle steel elements.

³ Tensile = $\phi N_{sa} = \phi_s A_{se,N} f_{uta}$ as noted in ACI 318 Chapter 17

⁴ Shear values determined by static shear tests with $φV_{sa}$ ≤ φ 0.60 $A_{sa,V}f_{uta}$ as noted in ACI 318 Chapter 17.

When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

³ Spacing factor reduction in shear, f_{AV} assumes an influence of a nearby edge. If no edge exists, then $f_{AV} = f_{AN}$.

⁴ Concrete thickness reduction factor in shear, f_{HV} assumes an influence of a nearby edge. If no edge exists, then f_{HV} = 1.0.



Table 5 — Load adjustment factors for 1/2-in. diameter Hilti KWIK HUS in uncracked concrete^{1,2}

													Edg	e distar	nce in sh	near				
u	/2-in. Kł ncracke concrete	d		cing factors f_{AN}			ge distator in ten $f_{\scriptscriptstyle{RN}}$			cing factors f_{AV}		⊥ to	oward e $f_{\scriptscriptstyle{RV}}$	dge		and avoing and $f_{\rm RV}$,	Conc. tor	thicknet in shear $f_{\scriptscriptstyle \mathrm{HV}}$	
	dment	in.	2-1/4	3	4-1/4	2-1/4	3	4-1/4	2-1/4	3	4-1/4	2-1/4	3	4-1/4	2-1/4	3	4-1/4	2-1/4	3	4-1/4
h,	nom	(mm)	(57)	(76)	(108)	(57)	(76)	(108)	(57)	(76)	(108)	(57)	(76)	(108)	(57)	(76)	(108)	(57)	(76)	(108)
	1-3/4	(44)	n/a	n/a	n/a	0.68	0.58	0.51	n/a	n/a	n/a	0.45	0.28	0.08	0.68	0.56	0.17	n/a	n/a	n/a
	2	(51)	n/a	n/a	n/a	0.75	0.63	0.54	n/a	n/a	n/a	0.54	0.34	0.10	0.75	0.63	0.21	n/a	n/a	n/a
	2-1/2	(64)	n/a	n/a	n/a	0.91	0.72	0.60	n/a	n/a	n/a	0.76	0.48	0.14	0.91	0.72	0.29	n/a	n/a	n/a
	3	(76)	0.83	0.73	0.66	1.00	0.82	0.66	0.67	0.62	0.55	1.00	0.63	0.19	1.00	0.82	0.38	n/a	n/a	n/a
ē	3-1/2	(89)	0.88	0.77	0.68		0.95	0.73	0.69	0.64	0.56		0.80	0.24		0.95	0.47	n/a	n/a	n/a
concrete	3-3/4	(95)	0.91	0.79	0.69		1.00	0.76	0.71	0.65	0.57		0.89	0.26		1.00	0.53	0.91	n/a	n/a
Ö	4	(102)	0.94	0.81	0.71			0.80	0.72	0.66	0.57		0.98	0.29			0.58	0.94	n/a	n/a
~	4-1/2	(114)	0.99	0.85	0.73			0.87	0.75	0.68	0.58		1.00	0.35			0.69	1.00	n/a	n/a
ance (c _a) / - in. (mm)	4-3/4	(121)	1.00	0.87	0.75			0.91	0.76	0.69	0.59			0.38			0.75		0.88	n/a
distance s (h) - in. (5	(127)		0.89	0.76			0.95	0.78	0.70	0.59			0.41			0.81		0.91	n/a
	6	(152)		0.96	0.81			1.00	0.83	0.75	0.61			0.53			1.00		0.99	n/a
dis	6-3/4	(171)		1.00	0.85				0.87	0.78	0.62			0.64					1.00	0.70
edge	7	(178)			0.86				0.89	0.79	0.63			0.67						0.72
s) / edge dist: thickness (h)	8	(203)			0.91				0.94	0.83	0.65			0.82						0.76
(s) thi	10	(229)			0.97 1.00				1.00	0.87	0.66			0.98						0.81
Da	11	(279)			1.00					0.91	0.00			1.00						0.83
Spacing (s)	12	(305)								0.93	0.70									0.94
Sp	14	(356)								1.00	0.72									1.00
	16	(406)								1.00	0.79									1.00
	18	(457)									0.73									
	20	(508)									0.87									_
	> 24	(610)									0.94									

Table 6 — Load Adjustment Factors for 5/8-in. Diameter Hilti KWIK HUS in uncracked concrete^{1,2}

	_ Loau										nce in shea	r		
	5/8-in. KH uncracked concrete			g factor nsion	factor in	istance tension	in sh	g factor near ³		rd edge	II to and from f_1	d away edge	factor in	nickness n shear ⁴
Embed	ment h _{nom}	in.	3-1/4	5	3-1/4	5	3-1/4	5	3-1/4	5	3-1/4	5	3-1/4	5
LITIDOG	nom	(mm)	(83)	(127)	(83)	(127)	(83)	(127)	(83)	(127)	(83)	(127)	(83)	(127)
	1-3/4	(44)	n/a	n/a	0.62	0.51	n/a	n/a	0.24	0.06	0.47	0.13	n/a	n/a
	2	(51)	n/a	n/a	0.67	0.54	n/a	n/a	0.29	0.08	0.57	0.15	n/a	n/a
	2-1/2	(64)	n/a	n/a	0.76	0.59	n/a	n/a	0.40	0.11	0.76	0.21	n/a	n/a
	3	(76)	0.71	0.63	0.86	0.65	0.61	0.55	0.53	0.14	0.86	0.28	n/a	n/a
distance (c _a) / concrete s (h) - in. (mm)	3-1/2	(89)	0.74	0.65	0.97	0.70	0.63	0.55	0.66	0.18	0.97	0.35	n/a	n/a
JC L	4	(102)	0.78	0.67	1.00	0.76	0.65	0.56	0.81	0.22	1.00	0.43	n/a	n/a
000	4-1/2	(114)	0.81	0.69		0.83	0.66	0.57	0.97	0.26		0.52	n/a	n/a
E E	5	(127)	0.85	0.71		0.89	0.68	0.58	1.00	0.30		0.60	0.85	n/a
S E	5-1/2	(140)	0.88	0.74		0.96	0.70	0.58		0.35		0.70	0.89	n/a
ä ii	6	(152)	0.92	0.76		1.00	0.72	0.59		0.40		0.80	0.93	n/a
sta h) -	7	(178)	0.99	0.80			0.75	0.61		0.50		1.00	1.00	0.65
ı (s) / edge dista thickness (h) ·	8	(203)	1.00	0.84			0.79	0.62		0.61				0.69
dge	9	(229)		0.89			0.83	0.64		0.73				0.74
<u>Ş</u>	10	(254)		0.93			0.86	0.65		0.86				0.78
(S) H	11	(279)		0.97			0.90	0.67		0.99				0.81
ng	12	(305)		1.00			0.94	0.68		1.00				0.85
Spacing (14	(356)					1.00	0.71						0.92
S	16	(406)						0.74						0.98
	18	(457)						0.77						1.00
	20	(508)						0.80						
	24	(610)						0.86						
	> 30	(762)						0.95						

¹ Linear interpolation not permitted.

When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

³ Spacing factor reduction in shear, f_{AV} assumes an influence of a nearby edge. If no edge exists, then $f_{AV} = f_{AN}$.

⁴ Concrete thickness reduction factor in shear, f_{HV} assumes an influence of a nearby edge. If no edge exists, then f_{HV} = 1.0.

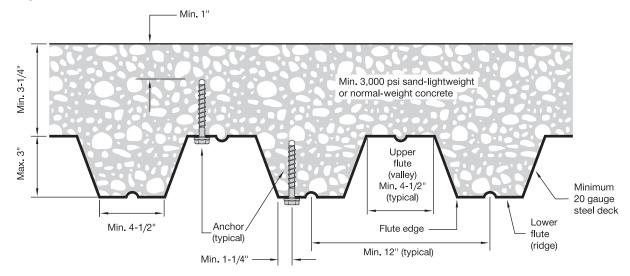
If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 1 and figure 2 of this section to calculate permissable edge distance, spacing and concrete thickness combinations.

Table 7 — Load adjustment factors for 3/4-in. diameter Hilti KWIK HUS in uncracked concrete^{1,2}

									E	Edge distar	nce in shea	r		
unc	3/4-in. KH		Spacing in ter	nsion	Edge d factor in		in sh	g factor near ³		rd edge	from	d away edge	factor in	nickness n shear ⁴
		in.	4	6-1/4	4	6-1/4	4	6-1/4	4	6-1/4	4	6-1/4	4	6-1/4
Embed	ment h _{nom}	(mm)		(159)	·	· ·		,		1		· ·		,
	1.0/4	, ,	(102)	,	(102)	(159)	(102)	(159)	(102)	(159)	(102)	(159)	(102)	(159)
	1-3/4	(44) (51)	n/a	n/a	0.57 0.61	0.48	n/a n/a	n/a	0.10	0.05	0.19	0.10	n/a	n/a
	2-1/2	(64)	n/a n/a	n/a	0.61	0.54	n/a	n/a n/a	0.12	0.08	0.23	0.12	n/a n/a	n/a n/a
	3	(76)	n/a	n/a n/a	0.76	0.54	n/a	n/a	0.16	0.08	0.33	0.17	n/a	n/a
	3-1/2	(89)	n/a	n/a	0.76	0.62	n/a	n/a	0.27	0.11	0.43	0.28	n/a	n/a
ē	4	(102)	0.73	0.64	0.93	0.67	0.58	0.55	0.33	0.14	0.66	0.20	n/a	n/a
edge distance ($c_{\rm a}$) / concrete kness (h) - in. (mm)	4-1/2	(114)	0.76	0.65	1.00	0.72	0.59	0.56	0.39	0.20	0.79	0.41	n/a	n/a
Ö	5	(127)	0.79	0.67	1.00	0.76	0.60	0.56	0.46	0.24	0.92	0.48	n/a	n/a
٥ / و	5-1/2	(140)	0.81	0.69		0.81	0.61	0.57	0.53	0.28	1.00	0.55	n/a	n/a
(°2)	6	(152)	0.84	0.71		0.86	0.62	0.58	0.61	0.31		0.63	0.69	n/a
ance (c _a) / - in. (mm)	7	(178)	0.90	0.74		0.97	0.64	0.59	0.77	0.40		0.79	0.75	n/a
itan) - i	8	(203)	0.96	0.78		1.00	0.66	0.60	0.94	0.48		0.97	0.80	n/a
s) / edge dist thickness (h)	8-1/8	(206)	0.96	0.78			0.66	0.60	0.96	0.50		0.99	0.80	0.65
lge	9	(229)	1.00	0.81			0.68	0.62	1.00	0.58		1.00	0.85	0.68
9 X	10	(254)		0.84			0.70	0.63		0.68			0.89	0.72
(S) Thi	11	(279)		0.88			0.72	0.64		0.78			0.94	0.75
Spacing (s) thi	12	(305)		0.91			0.74	0.65		0.89			0.98	0.79
acii	14	(356)		0.98			0.78	0.68		1.00			1.00	0.85
Sp	16	(406)		1.00			0.82	0.71						0.91
	18	(457)					0.86	0.73						0.96
	20	(508)					0.90	0.76						1.00
	24	(610)					0.98	0.81						
	30	(762)					1.00	0.89						
	> 36	(914)						0.96						

¹ Linear interpolation not permitted.

Figure 3 — Installation of Hilti KWIK HUS in soffit of concrete over steel deck floor and roof assemblies1



¹ Anchors may be placed in the upper or lower flute of the steel deck profile provided the minimum concrete cover above the drilled hole is satisfied. Anchors in the lower flute may be installed with a maximum 1-inch offset in either direction from the center of the flute. The offset distance may be increased proportionally for profiles with lower flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied.

When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

³ Spacing factor reduction in shear, f_{AV} assumes an influence of a nearby edge. If no edge exists, then $f_{AV} = f_{AN}$.

⁴ Concrete thickness reduction factor in shear, $f_{\rm HV}$ assumes an influence of a nearby edge. If no edge exists, then $f_{\rm HV}$ = 1.0.

If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa). Check with table 1 and figure 2 of this section to calculate permissable edge distance, spacing and concrete thickness combinations.



Table 8 — Hilti KWIK HUS in the soffit of uncracked lightweight concrete over metal deck^{1,2,3,4,5,6,7}

100100			oonine or arre	naonoa ngini	roigint contoi		a. acon		
			Installation i	n lower flute			Installation i	n upper flute	
Nominal	Nominal	Tensio	n - φN _n	Shear	· - φV _n	Tensio	n - φN _n	Shear	· - фV _n
anchor diameter	embed. in. (mm)	f' _c = 3,000 psi lb (kN)	f' _c = 4,000 psi lb (kN)	f' _c = 3,000 psi lb (kN)	f' _c = 4,000 psi lb (kN)	f'c = 3,000 psi lb (kN)	f' _c = 4,000 psi lb (kN)	f'c = 3,000 psi lb (kN)	f' c = 4,000 psi lb (kN)
	1-5/8	835	965	1,000	1,000	660	760	2,360	2,360
	(41)	(3.7)	(4.3)	(4.4)	(4.4)	(2.9)	(3.4)	(10.5)	(10.5)
3/8	2-1/2	1,455	1,680	905	905	1,900	2,195	3,655	3,655
3/0	(64)	(6.5)	(7.5)	(4.0)	(4.0)	(8.5)	(9.8)	(16.3)	(16.3)
	3-1/4	2,550	2,945	2,165	2,165	2/2	2/0	2/2	2/2
	(83)	(11.3)	(13.1)	(9.6)	(9.6)	n/a	n/a	n/a	n/a
	2-1/4	850	980	965	965	905	1,045	4,710	4,710
	(57)	(3.8)	(4.4)	(4.3)	(4.3)	(4.0)	(4.6)	(21.0)	(21.0)
1 /0	3	1,990	2,300	1,750	1,750	2/0	2/0	n/o	2/0
1/2	(76)	(8.9)	(10.2)	(7.8)	(7.8)	n/a	n/a	n/a	n/a
	4-1/4	3,485	4,025	2,155	2,155	n/a	n/a	n/a	n/a
	(108)	(15.5)	(17.9)	(9.6)	(9.6)	II/a	II/a	II/a	i iya
	3-1/4	2,715	3,135	2,080	2,080	n/o	n/a	n/a	n/a
5/8	(83)	(12.1)	(13.9)	(9.3)	(9.3)	n/a	n/a	II/a	i iya
3/6	5	6,170	7,125	2,515	2,515	n/o	n/a	n/a	n/a
	(127)	(27.4)	(31.7)	(11.2)	(11.2)	n/a	n/a	n/a	i iya
2//	4	2,715	3,135	2,255	2,255	n/o	n/a	n/a	n/a
3/4	(102)	(12.1)	(13.9)	(10.0)	(10.0)	n/a	n/a	n/a	n/a

¹ See section 3.1.8 to convert design strength value to ASD value.

² Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³ Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is $3 \times h_{nom}$ (nominal embedment).

Tabular values are lightweight concrete and no additional reduction factor is needed.

⁵ No additional reduction factors for spacing or edge distance need to be applied.

⁶ Comparison to steel values in table 3 is not required. Values in tables 8 control.

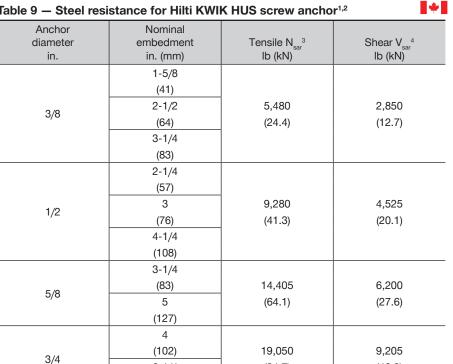
⁷ Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

DESIGN INFORMATION IN CONCRETE PER CSA A23.3

Limit State Design of anchors is described in the provisions of CSA A23.3 Annex D for post-installed anchors tested and assessed in accordance with ACI 355.2 for mechanical anchors and ACI 355.4 for adhesive anchors. This section contains the Limit State Design tables with unfactored characteristic loads that are based on the published loads in table 2 of this section. These tables are followed by factored resistance tables. The factored resistance tables have characteristic design loads that are prefactored by the applicable reduction factors for a single anchor with no anchor-to-anchor spacing or edge distance adjustments for the convenience of the user of this document. All the figures in the previous ACI 318 Chapter 17 design section are applicable to Limit State Design and the tables will reference these figures.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to Section 3.1.8. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at www.hilti.com.

Table 9 - Steel resistance for Hilti KWIK HUS screw anchor^{1,2}



See Section 3.1.8 to convert factored resistance value to ASD value

6-1/4

(159)

(84.7)

(40.9)

² Hilti KWIK HUS screw anchors are to be considered brittle steel elements.

Tensile N_{sar} = $A_{\text{se,N}}$ φ_{s} f_{uta} R as noted in CSA A23.3 Annex D.

Shear determined by static shear tests with $V_{sar} < A_{sa,V} \phi_s$ 0.6 f_{tota} R as noted in CSA A23.3 Annex D.



Table 10 — Hilti KWIK HUS screw anchor design information in accordance with CSA A23.3 Annex D1



Design parameter Symbol Units Nominal anchor diameter								Ref					
Design parameter	Symbol	Units		3/8			1/2		5,	/8	3,	/4	A23.3
Anchor O.D.	da	in.		0.375			0.5		0.6	325	0.	75	
Alleliol C.D.	u _a	(mm)		(9.5)			(12.7)		,	5.9)	<u> </u>).1)	
Effective minimum embedment ²	h _{ef}	in.	1.11	1.86	2.20	1.52	2.16	3.22	2.39	3.88	2.92	4.84	
	· ef	(mm)	(28)	(47)	(56)	(39)	(55)	(82)	(61)	(99)	(74)	(123)	
Minimum concrete thickness	h _{min}	in.	3-1/4	4	4-7/8	3-3/4	4-3/4	6-3/4	5	7	6	8-1/8	
		(mm) in.	(83)	(102)	3.30	(95) 2.75	(121)	(171) 5.25	(127)	(178) 5.82	(152) 4.41	(206) 7.28	
Critical edge distance	Cac	(mm)	(53)	2.92 (74)	(84)	(70)	(99)	(133)	(92)	(148)	(112)	(185)	
Minimum anchor spacing at critical		in.	(00)	2.25	(04)	(10)	(00)	3	(02)	(140)	(112)	, ,	
edge distance	S _{min,cac}	(mm)		(57)				(76)			(10	-	
	in 150 175												
Minimum edge distance	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
Anchor spacing at minimum edge dis-	nimum edge dis- in. 3												
tance	S _{min}	(mm)				(76) (102)				02)			
Minimum hole depth in concrete	h	in.	1-7/8	2-3/4	3 1/2	2-5/8	3-3/8	4-5/8	3-5/8	5-3/8	4-3/8	6-5/8	
Millimum noie deput in concrete	h _o	(mm)	(48)	(70)	(86)	(67)	(86)	(117)	(92)	(137)	(111)	(168)	
Minimum specified ultimate strength	ength f in. 107,120 97,140 90,180 81,600 ength f tata (mm) (739) (670) (623) (563)												
	uta	(mm)		(739)			(670)			22)	(56		
Effective tensile stress area	$A_{se,N}$	in.											
	se,N	(mm)		(55.5)			(103.9)		(17	2.9)	(25)	2.9)	
Steel embedment material resistance factor	_						0	85					8.4.3
for reinforcement	Фѕ	_					0.	03					0.4.5
Resistance modification factor for													
tension,	R	-					0.	70					D.5.3
steel failure modes ⁴													
Resistance modification factor for shear,	R	_					0.	65					D.5.3
steel failure modes ⁴		II-		10			200		1.1	405	10	050	
Factored steel resistance in tension	N _{sar}	lb (kN)	5,8 (26			,	200).9)		· '	405 I.1)	· '	050 I.7)	D.6.1.2
		lb	2,8				525		6,2		· ,	205	
Factored steel resistance in shear	V _{sar}	(kN)	(12).1)		(27		1).9)	D.7.1.2
Coefficient for factored concrete		(,	(,		`	,		(=:		` `	,	
breakout resistance, uncracked concrete	k _{c,uncr}	-			1	0				11	1.2		D.6.2.2
Modification factor for anchor		_					1	0					D.6.2.6
resistance, tension, uncracked concrete	d concrete ⁵ 1 c.N												
Anchor category	-	-	'						D.5.3 (c)				
Concrete material resistance factor	Фс	-	- 0.65						8.4.2				
Resistance modification factor for tension and shear, concrete failure	R	_					1	00					D.5.3 (c)
modes, Condition B ⁶	''	_					1.	00					D.3.3 (C)
Factored pullout resistance in 20 MPa	L.	lb											Door
uncracked concrete ⁷	N _{pr,uncr}	(kN)					N	IA					D.6.3.2

Design information in this table is taken from tables 2 of this section and converted with use of CSA A23.3 Annex D.

See figure 1 of this section.

For concrete over metal deck applications where the concrete thickness over the top flute is less than h_{min} in this table, see figure 3 and table 3 of this section.

The KWIK HUS is considered a brittle steel element as defined by CSA A23.3 Annex D section D.2.

For all design cases, $\psi_{e,N} = 1.0$.

For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A

For all design cases, ψ_{cP} = 1.0. NA (not applicable) denotes that this value does not control for design.

Table 11 — Hilti KWIK HUS screw anchor factored resistance with concrete / pullout failure in uncracked concrete^{1,2,3,4,5}

Nominal				Tensio	on - N _r			Shea	ır - V _r	
anchor diameter in.	Effective embed. in. (mm)	Nominal embed. in. (mm)	f' c = 20 MPa (2,900psi) Ib (kN)	f' c = 25 MPa (3,625 psi) lb (kN)	f' c = 30 MPa (4,350 psi) Ib (kN)	f' c = 40 MPa (5,800 psi) lb (kN)	f' c = 20 MPa (2,900 psi) lb (kN)	f' c = 25 MPa (3,625 psi) lb (kN)	f' c = 30 MPa (4,350 psi) lb (kN)	f' _c = 40 MPa (5,800 psi) lb (kN)
	1-1/8	1-5/8	970	1,085	1,185	1,370	970	1,085	1,185	1,370
	(28)	(41)	(4.3)	(4.8)	(5.3)	(6.1)	(4.3)	(4.8)	(5.3)	(6.1)
3/8	1-7/8	2-1/2	2,105	2,355	2,580	2,980	2,105	2,355	2,580	2,980
3/0	(47)	(64)	(9.4)	(10.5)	(11.5)	(13.2)	(9.4)	(10.5)	(11.5)	(13.2)
	2-3/16	3-1/4	2,740	3,060	3,355	3,875	2,740	3,060	3,355	3,875
	(56)	(83)	(12.2)	(13.6)	(14.9)	(17.2)	(12.2)	(13.6)	(14.9)	(17.2)
	1-1/2	2-1/4	1,590	1,780	1,950	2,250	1,590	1,780	1,950	2,250
	(39)	(57)	(7.1)	(7.9)	(8.7)	(10.0)	(7.1)	(7.9)	(8.7)	(10.0)
1/2	2	3	2,665	2,980	3,265	3,770	2,665	2,980	3,265	3,770
1/2	(55)	(76)	(11.9)	(13.3)	(14.5)	(16.8)	(11.9)	(13.3)	(14.5)	(16.8)
	3-1/4	4-1/4	4,850	5,425	5,945	6,860	9,705	10,850	11,885	13,725
	(82)	(108)	(21.6)	(24.1)	(26.4)	(30.5)	(43.2)	(48.3)	(52.9)	(61.1)
	2-3/8	3-1/4	3,485	3,900	4,270	4,930	3,485	3,900	4,270	4,930
5/8	(61)	(83)	(15.5)	(17.3)	(19.0)	(21.9)	(15.5)	(17.3)	(19.0)	(21.9)
3/0	4	5	7,210	8,060	8,830	10,195	14,420	16,120	17,660	20,390
	(99)	(127)	(32.1)	(35.9)	(39.3)	(45.4)	(64.1)	(71.7)	(78.6)	(90.7)
	2-15/16	4	4,660	5,210	5,705	6,590	9,320	10,420	11,415	13,180
3/4	(74)	(102)	(20.7)	(23.2)	(25.4)	(29.3)	(41.4)	(46.3)	(50.8)	(58.6)
3/4	4-13/16	6-1/4	9,985	11,165	12,230	14,120	19,970	22,325	24,455	28,240
	(123)	(159)	(44.4)	(49.7)	(54.4)	(62.8)	(88.8)	(99.3)	(108.8)	(125.6)

See section 3.1.8 to convert factored resistance value to ASD value.

Table 12 — Hilti KWIK HUS in the soffit of uncracked lightweight concrete over metal deck^{1,2,3,4,5,6,7}



			Installation i	n lower flute			Installation i	n upper flute	
Nominal	Nominal	Tensio	n - фN _r	Shear	r - φV _r	Tensio	n - фN _r	Shear	· - φV _r
anchor diameter in.	embedment depth in. (mm)	f' = 20 MPa (2,900 psi) lb (kN)	f' _c = 30 MPa ((4,350 psi) lb (kN)	f' c = 20 MPa (2,900 psi) lb (kN)	f' = 30 MPa (4,350 psi) Ib (kN)	f' = 20 MPa (2,900 psi) lb (kN)	f' _c = 30 MPa (4,350 psi) lb (kN)	f' _c = 20 MPa (2,900 psi) lb (kN)	f' = 30 MPa (4,350 psi) lb (kN)
	1-5/8	820	1,005	925	925	650	795	2,175	2,175
	(41)	(3.6)	(4.5)	(4.1)	(4.1)	(2.9)	(3.5)	(9.7)	(9.7)
0.70	2-1/2	1,430	1,755	835	835	1,865	2,285	3,365	3,365
3/8	(64)	(6.4)	(7.8)	(3.7)	(3.7)	(8.3)	(10.2)	(15.0)	(15.0)
	3-1/4	2,505	3,070	1,990	1,990	n/o	n/o	n/o	2/2
	(83)	(11.1)	(13.7)	(8.9)	(8.9)	n/a	n/a	n/a	n/a
	2-1/4	835	1,020	885	885	890	1,090	4,335	4,335
	(57)	(3.7)	(4.5)	(3.9)	(3.9)	(4.0)	(4.8)	(19.3)	(19.3)
1/2	3	1,955	2,395	1,615	1,615	n/a	n/a	n/a	n/a
1/2	(76)	(8.7)	(10.7)	(7.2)	(7.2)	Πγα	Пуа	Tiya	
	4-1/4	3,425	4,195	1,985	1,985	n/a	n/a	n/a	n/a
	(108)	(15.2)	(18.7)	(8.8)	(8.8)	11/4	11/4	11/4	
	3-1/4	2,670	3,270	1,915	1,915	n/a	n/a	n/a	n/a
5/8	(83)	(11.9)	(14.5)	(8.5)	(8.5)	11/4	11/4	Tiya	
3/0	5	6,070	7,430	2,315	2,315	n/a	n/a	n/a	n/a
	(127)	(27.0)	(33.1)	(10.3)	(10.3)	11/4	11/4	ii/a	Πηα
3/4	4	2,670	3,270	2,080	2,080	n/a	n/a	n/a	n/a
3/4	(102)	(11.9)	(14.5)	(9.3)	(9.3)	11/4	n/a	II/a	II/a

See section 3.1.8 to convert design strength value to ASD value.

Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

Apply spacing, edge distance, and concrete thickness factors in tables 4 to 7 as necessary. Compare to the steel values in table 9. The lesser of the values is to be used for the design. 2

Tablular values are for normal-weight concrete only. For lightweight concrete multiply design strength by λ_a as follows:

for sand-lightweight, $\lambda_a=0.68$; for all-lightweight, $\lambda_a=0.60$ Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is 3 x h_{nom} (nominal embedment). Tabular values are lightweight concrete and no additional reduction factor is needed.

No additional reduction factors for spacing or edge distance need to be applied.

Comparison of the tabular values to the steel strength is not necessary. Tabular values control.

Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.



DESIGN INFORMATION IN MASONRY

Table 13 — Allowable tension loads for Hilti KWIK HUS installed in grout-filled masonry walls (lb)1,2,3,4,5

				Spacing			Edge distance	
Nominal anchor diameter	Nominal embedment ³ in.	Loads at c _{cr} and s _{cr}	Critical - s _{cr} ⁶ in.	Minimum - s _{min}	Load reduction factor at s _{min} 6	Critical - c _{cr} ⁷ in.	Minimum c _{min} ⁸ in.	Load reduction factor 7
	1-5/8	535	4	2	0.70			
3/8	2-1/2	895	6	4	0.80	4	4	1.00
	3-1/4	1,210	0	4	0.60			
	2-1/4	710	4	2				
1/2	3	1,110	8	4	0.60	4	4	1.00
	4-1/4	1,515	0	4				
E /0	3-1/4	1,155	10	4	0.60	10	4	1.00
5/8	5	1,735	10	4	0.60	10	4	1.00
2/4	4	1,680	12	4	0.60	12	4	1.00
3/4	6-1/4	2,035	12	4	0.00	12	4	1.00

Table 14 — Allowable shear loads for Hilti KWIK HUS installed in grout-filled masonry walls (lb)^{1,2,3,4,5}

				Spacing		Edge distance				
								Load reductio	n factor at c _{min}	
Nominal anchor diameter	Nominal embedment ³ in.	Loads at c _{cr} and s _{cr}	Critical - s _{cr} ⁶ in.	Minimum - s _{min} in.	Load reduction factor at s _{min} ⁷	Critical - c _{cr} ⁸ in.	Minimum c _{min} ⁸ in.		Load direction parallel to edge	
	1-5/8	1,140						0.61	1.00	
3/8	2-1/2	1,165	6	4	0.94	6	4	0.70	1.00	
	3-1/4	1,190						0.70	1.00	
	2-1/4	1,845						0.50	1.00	
1/2	3	2,055	8	4	0.88	8	4	0.45	0.94	
	4-1/4	2,745	1					0.40	0.89	
	3-1/4	3,040	10	4	0.00	10	4	0.36	0.82	
5/8	5	3,485	10	4	0.36	10	4	0.34	0.92	
0./4	4	3,040	10	4	0.00	10	4	0.36	0.82	
3/4	6-1/4	3,485	10	4	0.36	12	4	0.34	0.92	

- 1 All values are for anchors installed in fully-grouted masonry with minimum masonry prism strength of 1,500 psi. Concrete masonry units may be lightweight or normal-weight.
- 2 Anchors may not be installed within 1 inch in any direction of a vertical joint.
- 3 Embedment depth is measured from the outside face of the concrete masonry embedment.
- 4 Linear interpolation of load values between minimum spacing (s_{mir}) and critical spacing (s_c) and between minimum edge distance (c_{mir}) and critical edge distance (c_c) is permitted.

5 For combined loading:
$$\left(\frac{T_{applied}}{T_{allowable}}\right)^{5/3} + \left(\frac{V_{applied}}{V_{allowable}}\right)^{5/3} \le \frac{1}{2}$$

- 6 Anchor spacing s_{cr} is where full load values in the table may be used. Anchor-to-anchor spacing of less than s_{min} is not recommended. Spacing is measured from the center of one anchor to the center of an adjacent anchor.
- 7 Load reduction factors are multiplicative, both spacing and edge distance load reduction factors must be considered. Load values for anchors installed at less than c_{cr} or s_{cr} must be multiplied by the appropriate load reduction factor based on actual edge distance or anchor spacing.
- 8 Critical edge distance c_{cr} is where full load values in the table may be used. Edge distance spacing of less than c_{min} is not recommended. Edge distance is measured from the center of the anchor to the closest edge.

Table 15 — Hilti KWIK HUS allowable loads installed in top of grout-filled concrete masonry construction (lb)1.2

						Sh	ear
Nominal anchor diameter	Nominal embedment in.	Minimum edge distance in.	Minimum spacing in.	Minimum end distance in.	Tension	Perpendicular to edge of masonry wall	Parallel to edge of masonry wall
1/2	4-1/4	1-3/4	8	4	680	305	1,110
5/8	5	1-3/4	10	5	1,310	305	1,165

¹ All values are for anchors installed in fully-grouted masonry with minimum masonry prism strength of 1,500 psi. Concrete masonry units may be lightweight or normal-weight.

INSTALLATION INSTRUCTIONS

Installation Instructions For Use (IFU) are included with each product package. They can also be viewed or downloaded online at www.hilti.com. Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the IFU.

ORDERING INFORMATION¹







Description	Hole diameter	Anchor length See figure 1	Minimum embedment depth	Qty / Box
KH 3/8 x 2-1/8	3/8	2-1/8	1-5/8	50
KH 3/8 x 3	3/8	3	2-1/2	50
KH 3/8 x 3-1/2	3/8	3-1/2	2-1/2	50
KH 3/8 x 4	3/8	4	3-1/4	50
KH 3/8 x 5	3/8	5	3-1/4	30
KH 1/2 x 3	1/2	3	2-1/4	30
KH 1/2 x 3-1/2	1/2	3-1/2	3	25
KH 1/2 x 4	1/2	4	3	25
KH 1/2 x 4-1/2	1/2	4-1/2	4- 1/4	25
KH 1/2 x 5	1/2	5	4-1/4	25
KH 1/2 x 6	1/2	6	4-1/4	25
KH 5/8 x 4	5/8	4	3-1/4	15
KH 5/8 x 5-1/2	5/8	5-1/2	3-1/4	15
KH 5/8 x 6-1/2	5/8	6-1/2	3-1/4	15
KH 3/4 x 4-1/2	3/4	4-1/2	4	10
KH 3/4 x 5-1/2	3/4	5-1/2	4	10
KH 3/4 x 7	3/4	7	4	10
KH 3/4 x 9	3/4	9	4	10

1 All dimensions in inches.