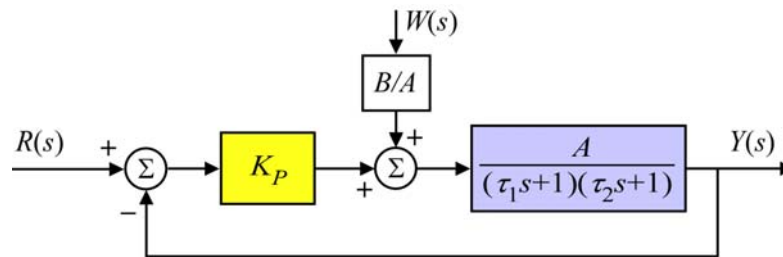




1. *P-Control: output of the controller is \_\_\_\_\_ to the **error** between the reference input,  $r$  and the measured output,  $y$ .*
2. *The block diagram for the system with P-controller is*



3. *The controller output is  $u = K_P e$ , where  $K_P$  is the proportional \_\_\_\_\_.*
4. *The transfer function from the reference input,  $r$  to the system output,  $y$  is*

$$\frac{Y}{R}(s) = \frac{\frac{K_P A}{(\tau_1 s + 1)(\tau_2 s + 1)}}{1 + \frac{K_P A}{(\tau_1 s + 1)(\tau_2 s + 1)}} = \frac{K_P A}{(\tau_1 s + 1)(\tau_2 s + 1) + K_P A}$$

5. *The transfer function from the disturbance,  $w$  to the system output,  $y$  is*

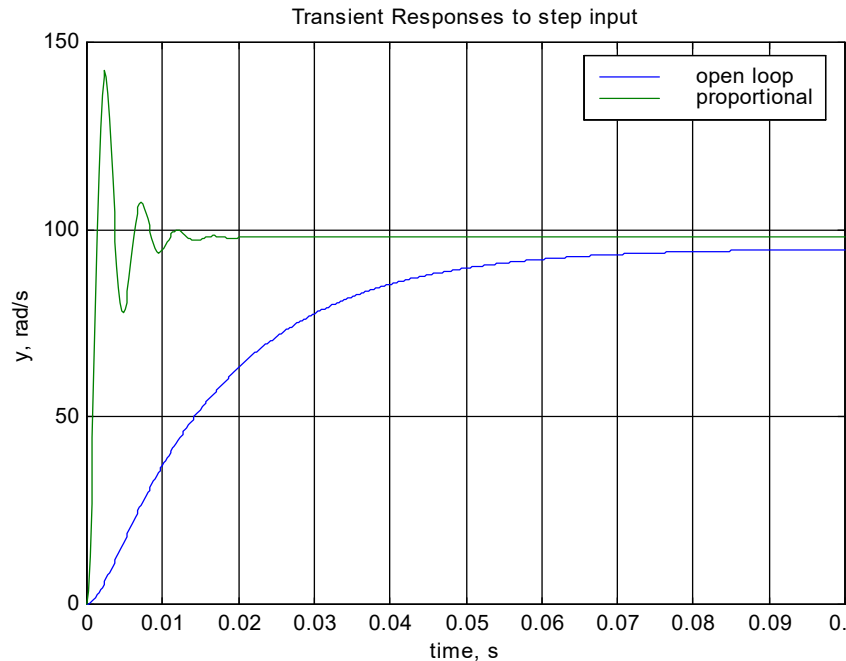
$$\frac{Y}{W}(s) = \frac{\frac{A}{(\tau_1 s + 1)(\tau_2 s + 1)}}{1 + \frac{K_P A}{(\tau_1 s + 1)(\tau_2 s + 1)}} \cdot \frac{B}{A} = \frac{B}{(\tau_1 s + 1)(\tau_2 s + 1) + K_P A}$$

6. *Example problem: Let  $K_P = 5$  with  $w = -0.1$  ( $W(s) = -0.1/s$ ),  $r = 100$  ( $R(s) = 100/s$ ),  $\tau_1 = 1/60$ ,  $\tau_2 = 1/600$ , and  $A = 10$ .*

$$Y(s) = \frac{5000}{s((\tau_1 s + 1)(\tau_2 s + 1) + 50)} + \frac{-5}{s((\tau_1 s + 1)(\tau_2 s + 1) + 50)}$$

$$= \frac{4995}{s((\tau_1 s + 1)(\tau_2 s + 1) + 50)}$$

$$y_{ss} = \lim_{s \rightarrow 0} sY(s) = \underline{\hspace{2cm}}$$



1. Proportional control \_\_\_\_\_ the rise time of the system (As the gain  $K_P$  is increased).
2. As a result, the transient response is \_\_\_\_\_.  $\rightarrow$  overshoot is increased.
3. Notice that there is still some \_\_\_\_\_ in the response.
4. The steady state error with respect to a step input can be eliminated with the addition of \_\_\_\_\_ to a proportional controlled system.

1. Integral control: output of the controller is equal to the \_\_\_\_\_ **of the error** between the reference input,  $r$  and the measured output,  $y$ .
2. The controller output is  $u = K_I \int e dt$ , where  $K_I$  is the integral gain.  $K_I$  can also be written as  $K_I = \frac{K_P}{T_I}$ , where  $T_I$  is the integral or reset time. The Laplace transform of the integral controller is

$$U(s) = \underline{\hspace{2cm}}$$

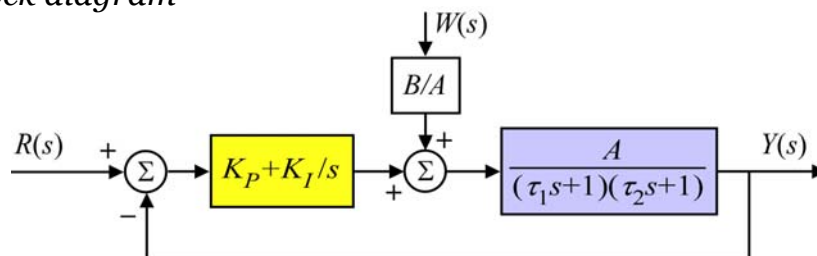
3. Integral control by itself tends to make systems \_\_\_\_\_, thus we use it with a proportional controller → **Proportional Integral (PI) Controller**.

$$u = K_P e + K_I \int e dt = K_P e + \frac{K_P}{T_I} \int e dt$$

4. The Laplace transform of the PI controller is

$$U(s) = \left( K_P + \frac{K_I}{s} \right) E(s) = K_P \left( 1 + \frac{1}{T_I s} \right) E(s)$$

1. Block diagram



2. Transfer function between the system output,  $y$  and the reference input,  $r$  is

$$\frac{Y}{R}(s) = \frac{\left( K_P + \frac{K_I}{s} \right) A}{1 + \frac{\left( K_P + \frac{K_I}{s} \right) A}{(\tau_1 s + 1)(\tau_2 s + 1)}} = \frac{\left( K_P + \frac{K_I}{s} \right) A}{(\tau_1 s + 1)(\tau_2 s + 1) + \left( K_P + \frac{K_I}{s} \right) A} \cdot \frac{s}{s}$$

## 3. Transfer function (cont'd)

$$\frac{Y}{R}(s) = \frac{(K_P s + K_I)A}{s(\tau_1 s + 1)(\tau_2 s + 1) + (K_P s + K_I)A}$$

4. The transfer function between the system output,  $y$  and the disturbance,  $w$  is

$$\frac{Y}{W}(s) = \frac{\frac{A}{(\tau_1 s + 1)(\tau_2 s + 1)}}{1 + \frac{\left(K_P + \frac{K_I}{s}\right)A}{(\tau_1 s + 1)(\tau_2 s + 1)}} \cdot \frac{B}{A} = \frac{B}{(\tau_1 s + 1)(\tau_2 s + 1) + \left(K_P + \frac{K_I}{s}\right)A} \cdot \frac{s}{s}$$

$$\frac{Y}{W}(s) = \frac{Bs}{s(\tau_1 s + 1)(\tau_2 s + 1) + (K_P s + K_I)A}$$

5. Example problem:  $K_P = 5$ ,  $K_I = 5/0.1 = 500$ ,  $w = -0.1$ ,  $r = 100$ .

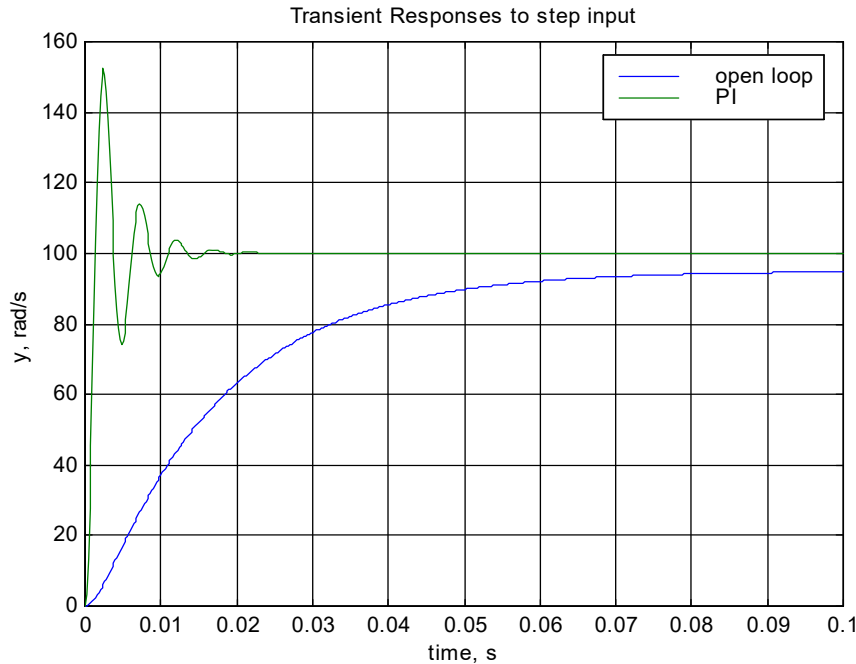
$$Y(s) = \frac{(AK_P r + Bw)s + K_I Ar}{s(s(\tau_1 s + 1)(\tau_2 s + 1) + (K_P s + K_I)A)}$$

$$y_{ss} = \lim_{s \rightarrow 0} sY(s) = \frac{K_I Ar}{K_I A} = r$$

- Therefore, the additional integral control removes the effect of the disturbance.

## 6. Comments on PI control

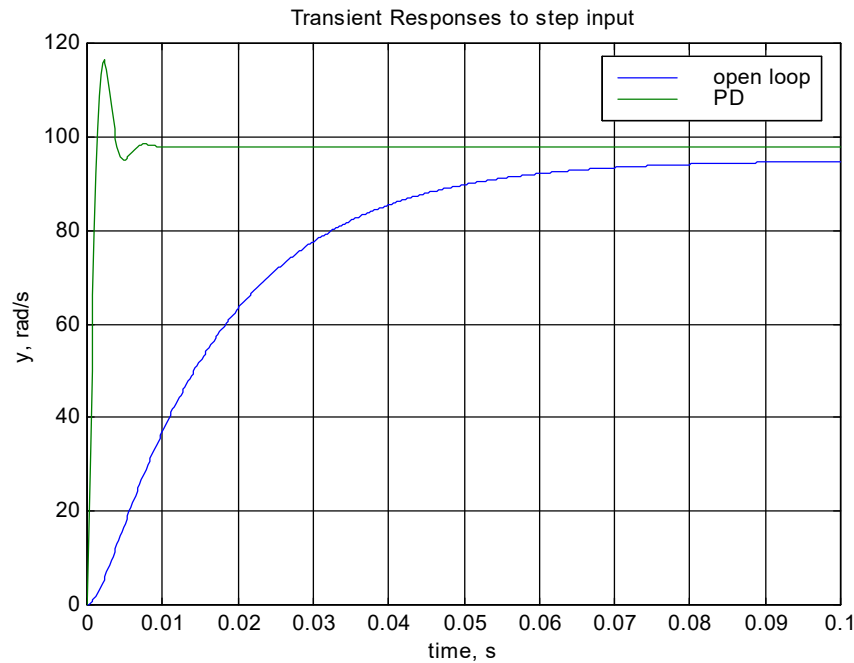
- 1) The PI controller \_\_\_\_\_ the steady state error (for step inputs).
- 2) However, it adds more instability to system.
- 3) Adding \_\_\_\_\_ to a PI controller fixes the instability problem. → PID Control



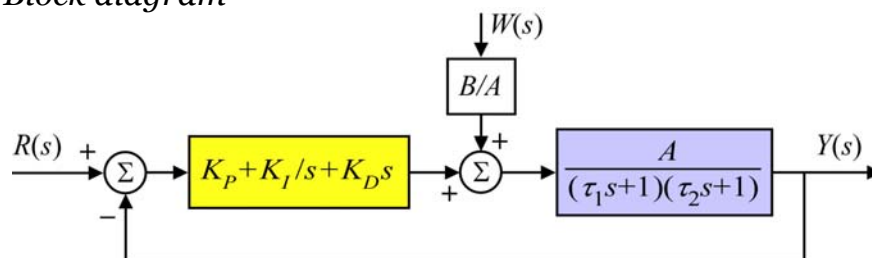
1. *Derivative control: output of the controller is equal to the derivative of the error between the reference input and the system output.*
2. *The controller output is  $u = K_D \frac{de}{dt}$ , where  $K_D$  is the derivative gain.  $K_D$  can also be written as  $K_D = K_P T_D$ , where  $T_D$  is the derivative time. The Laplace transform of the derivative controller is  $U(s) =$  \_\_\_\_\_*

☐ We use derivative control to add stability to P/PI controllers.

3. *Proportional Derivative (PD) control:*
  - 1) It adds stability by \_\_\_\_\_.
  - 2) However, it does not remove \_\_\_\_\_.
  - 3) Since its output is dependent on the current rate of change of the error, PD control shows \_\_\_\_\_.



## 1. Block diagram

2. Transfer function between the system output,  $y$  and the reference input,  $r$  is

$$\begin{aligned} \frac{Y}{R}(s) &= \frac{\left(K_D s + K_P + \frac{K_I}{s}\right)A}{(\tau_1 s + 1)(\tau_1 s + 1) + \left(K_D s + K_P + \frac{K_I}{s}\right)A} \\ &= \frac{(K_D s^2 + K_P s + K_I)A}{s(\tau_1 s + 1)(\tau_2 s + 1) + (K_D s^2 + K_P s + K_I)A} \end{aligned}$$

3. The transfer function between the system output,  $y$  and the disturbance,  $w$  is

$$\frac{Y}{W}(s) = \frac{\frac{A}{(\tau_1 s + 1)(\tau_2 s + 1)}}{1 + \frac{\left(K_D s + K_P + \frac{K_I}{s}\right)A}{(\tau_1 s + 1)(\tau_2 s + 1)}} \cdot \frac{B}{A} = \frac{B}{(\tau_1 s + 1)(\tau_2 s + 1) + \left(K_D s + K_P + \frac{K_I}{s}\right)A}$$

$$= \frac{Bs}{s(\tau_1 s + 1)(\tau_2 s + 1) + (K_D s^2 + K_P s + K_I)A}$$

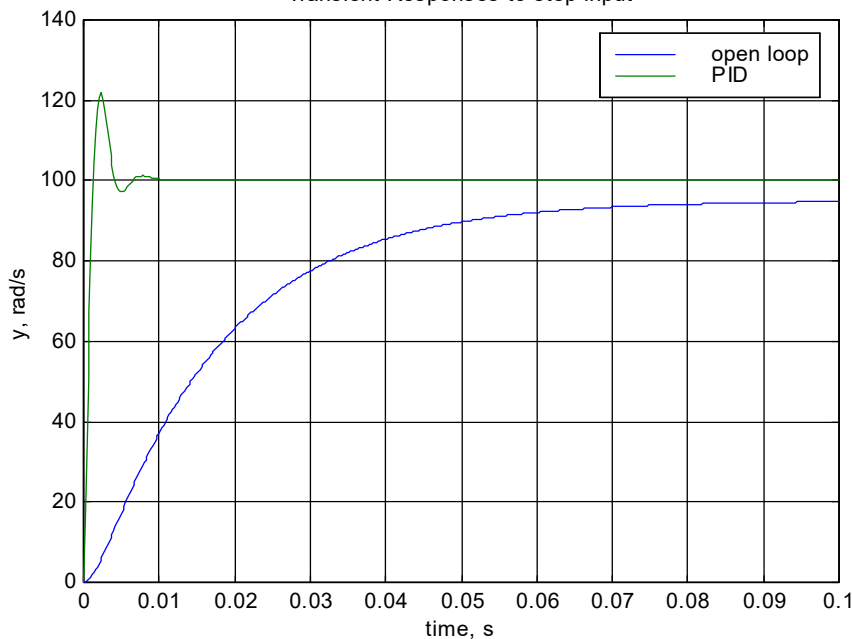
4. The steady-state value is

$$y_{ss} = \lim_{s \rightarrow 0} sY(s) = \underline{\hspace{2cm}}$$

- Therefore, the steady-state response becomes exactly the same as the reference input. → SSE is completely eliminated.

$$K_I = 500, K_P = 5, K_D = 5(0.0004) = 0.002, w = -0.1, r = 100$$

Transient Responses to step input





1. The steady-state error can be **completely eliminated** due to the integral control.
2. The transient response is improved due to the derivative control  
→ Overshoot is reduced.
3. Combined, the three controls (**Proportional**, **Integral**, and **Derivative**) form the classical **PID controller**, which is widely used in the process industries.
4. Now, it remains to find the appropriate values for the three gains,  $K_p$ ,  $K_i$ , and  $K_d$ . → **PID tuning**.
5. High derivative gain can \_\_\_\_\_ to the system.

```
clear;

% System responses to controllers
tau1=1/60; tau2=1/600; t=[0:.0002:.1];
W=.1; A=10; B=50; R=100;

% open loop case
num1=R-W*B;
den1=[tau1*tau2 tau1+tau2 1];
yol=step(num1,den1,t);

% proportional control
Kp=5;
num2=R*Kp*A-W*B;
den2=[tau1*tau2 tau1+tau2 1+Kp*A];
yp=step(num2,den2,t);

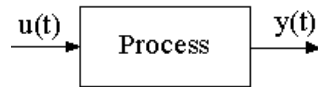
% proportional/integral control
Ti=.01;
Ki=Kp/Ti;
num3=[R*A*Kp-W*B R*A*Ki];
den3=[tau1*tau2 tau1+tau2 1+Kp*A Ki*A];
ypi=step(num3,den3,t);

% PID control
Td=.0004;
Kd=Kp*Td;
num4=[R*A*Kd R*A*Kp-W*B R*A*Ki];
den4=[tau1*tau2 tau1+tau2+Kd*A 1+Kp*A Ki*A];
ypid=step(num4,den4,t);

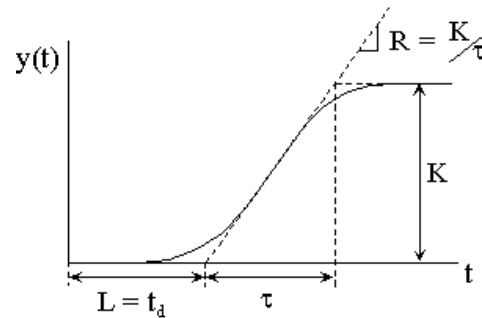
% PD control
num5=[R*A*Kd R*A*Kp-W*B];
den5=[tau1*tau2 tau1+tau2+Kd*A 1+Kp*A];
ypd=step(num5,den5,t);

% plotting data
plot(t,yol,t,ypid)
%plot(t,yol,t,yp,t,ypi,t,ypid,t,ypd)
grid
title('Transient Responses to step input')
xlabel('time, s')
ylabel('y, rad/s')
legend('open loop','PID')
```

1. A method for selecting the PID control parameters based on experiments on the process and thus bypass the need for a complete dynamic model. There are two widely-used methods
2. Transient-response method



$u(t)$  is a step input



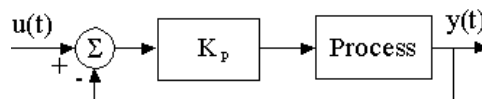
- 1) Step response of many process control systems exhibits a process reaction curve that can be approximated by  $\frac{Y}{U}(s) = \frac{Ke^{-t_d s}}{\tau s + 1}$ .
- 2) This process is characterized by two parameters:
  - a. \_\_\_\_\_,  $R$  (slope of the tangent line)
  - b. \_\_\_\_\_,  $L$  (intersection with time axis)

- 3) In order to achieve a damping of about  $\zeta = 0.21$ , the parameters are selected according to this table:

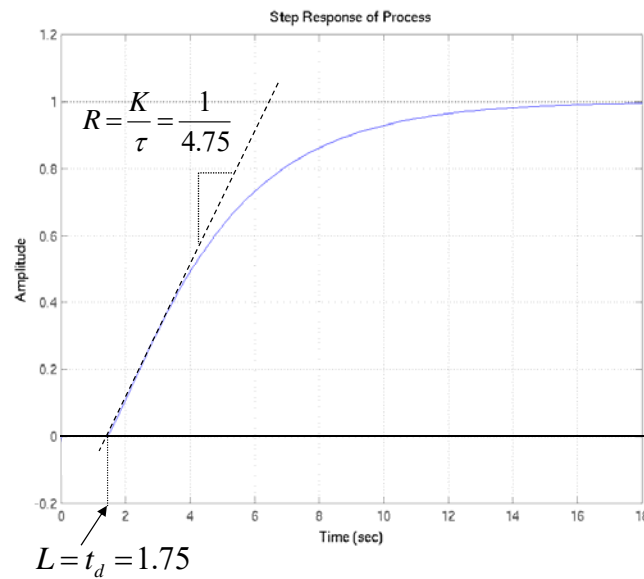
	$K$	$T_I$	$T_d$
P	$1/RL$		
PI	$.9/RL$	$L/.3$	
PID	$1.2/RL$	$2L$	$.5L$

## 2. Stability-limit method

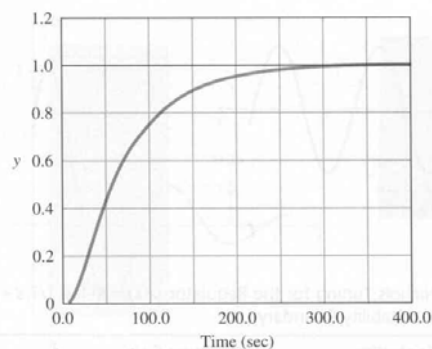
- 1) Using a proportional controller, the gain is slowly increased until the system becomes \_\_\_\_\_. At this point the gain,  $K_u$ , and the period of the system at its marginally stable point,  $P_u$  are recorded.
- 2) Using these two parameters, the PID parameters are selected according to the following table.



	$K$	$T_I$	$T_d$
P	$.5 K_u$		
PI	$.45 K_u$	$P_u/1.2$	
PID	$.6 K_u$	$P_u/2$	$P_u/8$



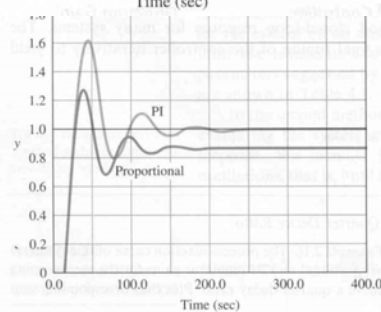
Can be read directly from the step response of a process with a time delay.



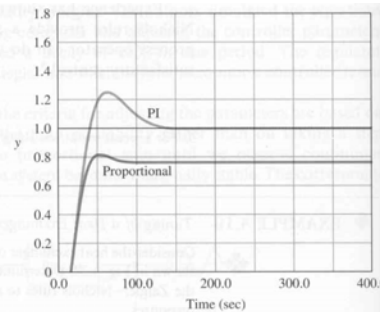
From the process reaction curve,  
 $R = 1/90$  and  $L = 13$  sec. Then, using

	K	$T_I$
P	$1/RL$	
PI	$.9/RL$	$L/.3$

$K = 6.92$  for P-control and  $K = 6.22$   
 and  $T_I = 43.3$  for PI-control.

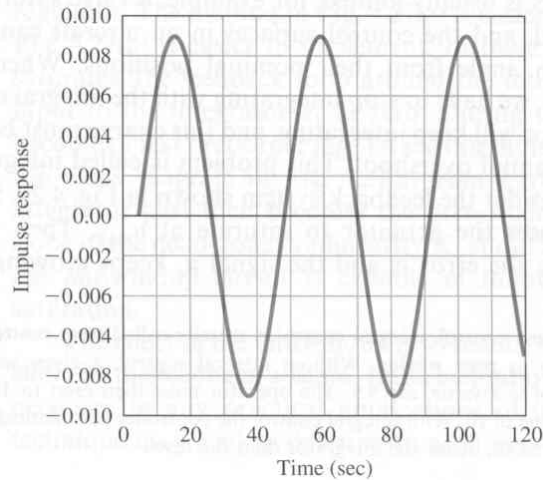


Too much oscillation



Improved responses  
 by reducing  $K$  by a factor of 2

Proportional feedback is applied to the system. When the gain,  $K_u = 15.3$ , the system showed non-decaying oscillation in response to a short pulse.



The gain was  $K_u = 15.3$  and the period was measured at  $P_u = 42$  sec. Then, using

	K	$T_I$
P	$.5K_u$	
PI	$.45K_u$	$(P_u/1.2)$

$K = 7.65$  for P-control and  $K = 6.885$  and  $T_I = 35$  for PI-control.