



### 5. Root Locus Techniques

# Sketching the Root Locus Transient Response Design via Gain Adjustment

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#### Introduction



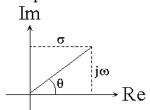
- 1. Control system problem
- 2. What is Root Locus?
  - A graphical presentation of the closed-loop poles as a system parameter is varied.
  - 2) Provides a qualitative description of a control system's performance.
  - 3) Allows control design for systems of order higher than 2.
  - 4) Gives a graphical representation of a system's \_\_\_\_\_

## A

#### **Complex Numbers**



1) Any complex number, *s* described in Cartesian coordinates can be graphically represented by a vector. It can also be represented in polar or exponential form.

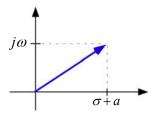


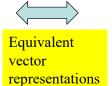
$$s = \sigma + j\omega \implies M \angle \theta \text{ or } M e^{j\theta}$$
  
where  $M =$ 

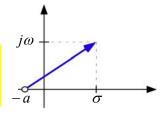
$$\theta$$
 =

2) If the complex number is substituted in a complex function F(s), another complex number will result.

If 
$$F(s) = s + a$$
 with  $s = \sigma + j\omega$   $\Rightarrow$   $F(s) = \sigma + a + j\omega$ 







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#### **Complex Functions**

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☐ General complex functions can be represented as

$$F(s) = \frac{\prod_{i=1}^{m} (s + z_i)}{\prod_{j=1}^{n} (s + p_j)} = \frac{\prod \text{ numerator's complex factors}}{\prod \text{ denominator's complex factors}} = \frac{\prod ()}{\prod ()}$$

Since each complex factor can be represented by a vector, the magnitude, M of F(s) at any point, s, is

$$M = \frac{\prod \text{ zero lengths}}{\prod \text{ pole lengths}} = \frac{\prod\limits_{i=1}^{m} \left| (s + z_i) \right|}{\prod\limits_{j=1}^{n} \left| (s + p_j) \right|}$$

and the angle,  $\theta$  of F(s) at any point, s is

$$\theta = \sum_{i=1}^{m} \text{ angles of zeros } -\sum_{i=1}^{n} \text{ angles of poles}$$

$$= \sum_{i=1}^{m} \angle(s + z_i) - \sum_{i=1}^{n} \angle(s + p_i).$$

☐ Thus,



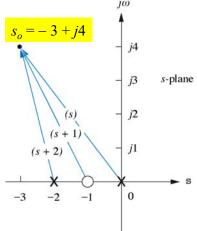
#### **Example 1: Complex Functions**



Given

$$F(s) = \frac{s+1}{s(s+2)}$$

find F(s) at the point  $s_o = -3 + j4$ .



$$M_{z1} = |s_o + 1| = |-3 + j4 + 1| = \sqrt{(-2)^2 + 4^2} = \sqrt{20}$$

$$M_{p1} = |s_o + 0| = |-3 + j4 + 0| = \sqrt{9 + 16} = 5$$

s-plane 
$$M_{p2} = |s_o + 2| = |-3 + j4 + (2)| = \sqrt{(-1)^2 + 4^2} = \sqrt{17}$$

$$\theta_{z_1} = \tan^{-1} \left( \frac{4}{2} \right) = 116.57^{\circ}$$

$$\theta_{p_1} = \tan^{-1} \left( \frac{4}{3} \right) = 126.87^{\circ}$$

$$\theta_{p_2} = \tan^{-1} \left( \frac{4}{1} \right) = 104.04^{\circ}$$

$$F(s_o) = \frac{\sqrt{20}}{5\sqrt{17}} \angle$$

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#### **Root Locus Motivating Example (1/3)**

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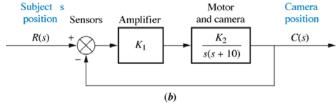
#### CameraMan® Camera System

Automatically follows a subject who wears infrared sensors on front and back (the front sensor is also a microphone); tracking commands and audio are relayed to CameraMan via a radio frequency link from a unit worn by the subject.



K	Pole 1	Pole 2		
0	-10	0		
5	-9.47	-0.53		
10	-8.87	-1.13		
15	-8.16	-1.84		

Table 8.1 Pole location as a function of gain for the system





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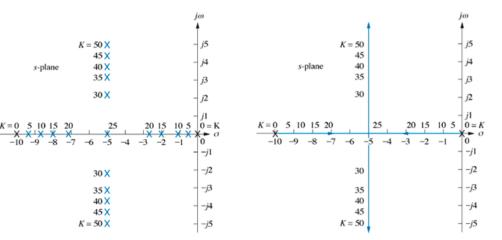
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#### **Root Locus Motivating Example (2/3)**



- As the gain, K increases, the closed-loop pole, which is at -10 for K = 0, moves toward the \_\_\_\_\_ and the closed-loop pole, which is at 0 for K = 0 moves toward the \_\_\_\_\_.
- They meet at \_\_\_\_\_, break away from the real axis, and move into the complex plane. One closed-loop pole moves upward while the other moves downward.





#### **Root Locus Motivating Example (3/3)**



- 1. It is this representation of the \_\_\_\_\_\_as the gain is varied that we call a root locus.
- 2. For this course, the discussion is limited to positive gain, or  $K \ge 0$ .

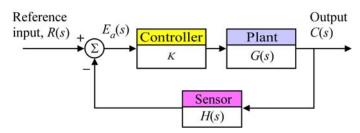
- 3. The root locus shows the changes in the **transient response** as the gain, *K* varies.
- 4. The poles are real for gains less than 25. Thus, the system is
- 5. At a gain of 25, the poles are real and multiple and hence \_\_\_\_\_damped.
- 6. For gains above 25, the system is \_\_\_\_\_\_.
- 7. Regardless of the value of gain, the settling time for the system remains the same under all conditions of underdamped responses.
- 8. As the gain is increased, the damping ratio diminishes and the percent overshoot increases.
- 9. The damped frequency of oscillation, which is equal to the imaginary part of the pole, also increases with an increase in gain, resulting in a reduction of the peak time.
- 10. Since the root locus never crosses over into the right half-plane, the system is \_\_\_\_\_\_.



#### **Root Locus Formulation (1/3)**



1. Feedback control system with a proportional controller.



2. The closed-loop transfer function for the control system is

$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)}$$

3. The closed-loop poles are found by solving the characteristic equation, i.e.,

or equivalently,

$$KG(s)H(s) = -1 = 1\angle(2k+1)180^{\circ}, \ k = 0, \pm 1, \pm 2, \cdots$$

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#### **Root Locus Formulation (2/3)**

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- 4. Thus, the two criteria that the closed-loop poles must meet are
  - Magnitude criterion

$$|KG(s)H(s)| =$$

Angle criterion

$$\angle KG(s)H(s) =$$

5. If the system transfer function can be factored as

$$GH = \frac{(s+z_1)(s+z_2)...(s+z_m)}{(s+p_1)(s+p_2)...(s+p_n)}$$

then.

then,  

$$1 + KG(s)H(s) = 0 \implies 1 + \frac{K(s + z_1)(s + z_2)...(s + z_m)}{(s + p_1)(s + p_2)...(s + p_n)} = 0$$

$$(s + p_1)(s + p_2)...(s + p_n) + K(s + z_1)(s + z_2)...(s + z_m) = 0$$

□ Thus, the closed-loop poles will change as K varies from 0 to  $\infty$ .



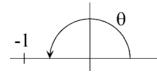
#### **Root Locus Formulation (3/3)**



- 6. By the Root Locus method, one can find what the locations (locus) of the closed loop poles when K increases from 0 to  $\infty$ . This method also provides information on the transient behavior and system stability.
- \_\_\_\_\_ **Criterion** is first used to When drawing Root Locus, the 7. find the values of *s* that satisfies the characteristic equation.

For 
$$G(s)H(s) = \frac{(s+z_1)(s+z_2)...(s+z_m)}{(s+p_1)(s+p_2)...(s+p_n)}$$

$$\angle KG(s)H(s) = \sum \theta_i = (\theta_{z_1} + \theta_{z_2} + \cdots) - (\theta_{p_1} + \theta_{p_2} + \cdots) = (2k+1)180^{\circ}$$



 $\theta$  must be an \_\_\_\_ multiple of 180°

8. Then, the particular value of K for each of s can be found by using the **Criterion** as follows.

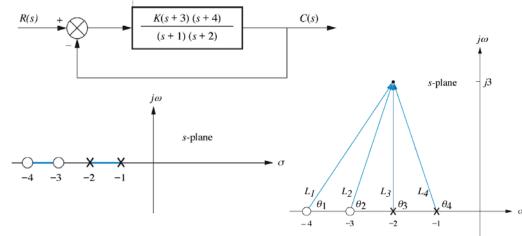


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### **Example 2: Root Locus Formulation (1/2)**ALABAMA

For the following system, check whether points  $s_1 = -2 + j3$  and  $s_2 = -2 + j3$  $-2 + i(\sqrt{2}/2)$  are on the root locus of the closed-loop system.



Solution

$$KGH = \frac{K(s+3)(s+4)}{(s+1)(s+2)} \implies T(s) = \frac{K(s+3)(s+4)}{(1+K)s^2 + (3+7K)s + (2+12K)}$$



## Example 2: Root Locus Formulation (2/2)



☐ If the point  $s_1 = -2 + j3$  is a closed-loop pole, it must satisfy the angle criterion.

$$\angle KG(s_1)H(s_1) = \theta_{z_1} + \theta_{z_2} - (\theta_{p_1} + \theta_{p_1})$$

$$= 56.31^{\circ} + 71.57^{\circ} - 90^{\circ} - 180.43^{\circ} = -70.55^{\circ}$$

Therefore,  $s_1$  is not on the root locus.

The sum of the angles for  $s_2 = -2 + j(\sqrt{2}/2)$  is

$$\angle KG(s_2)H(s_2) = \theta_{z_1} + \theta_{z_2} - (\theta_{p_1} + \theta_{p_1})$$

$$= 19.47^{\circ} + 35.26^{\circ} - 90^{\circ} - 144.74^{\circ} = -180.0^{\circ}$$

Therefore,  $s_2$  satisfies the Angle Criterion and is a point on the root locus for some value of gain, K.

 $\Box$  The value of gain, K for  $s_2$  can be found by using the Magnitude criterion.

$$K = \frac{1}{|G(s_2)H(s_2)|} = \underline{\hspace{1cm}}$$

Thus,  $s_2 = -2 + j(\sqrt{2/2})$  is a point on the root locus for a gain of \_\_\_\_\_.

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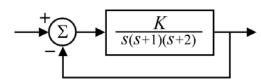
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#### **Root Locus Sketching (1/9)**

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☐ Consider drawing Root Locus for the following system.



 $lue{}$  **Step 1**: Locate the OL poles and zeros.

$$\begin{array}{c|c} & \operatorname{Im}(s) \\ & & \\ \hline & \\ -2 & -1 \end{array} \longrightarrow \operatorname{Re}(s)$$

■ **Rule**: If there are *n* poles and *m* zeros in the OL transfer function, the branches of the locus start at the \_\_\_\_\_\_ of the **OL transfer function**. As the gain *K* increases to infinity, *m* of these branches approach the zeros of the OL transfer function.

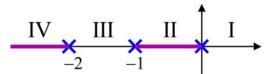
OL transfer function = 
$$\frac{(s + z_1)(s + z_2)...(s + z_m)}{(s + p_1)(s + p_2)...(s + p_n)}$$



#### **Root Locus Sketching (2/9)**



- □ **Step 2**: Determine branches of the Root Locus on the real axis.
- □ **Rule**: The loci are on the real axis to the \_\_\_\_\_ of an \_\_\_\_ number of poles and zeros.



Branch	I	II	III	IV
Sum of angles	0	180°	360°	540°

• Sum of all the angles to test points in branches II and IV are odd multiples of 180°, and by the angle criterion, they are on the RL.

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#### **Root Locus Sketching (3/9)**

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- ☐ **Step 3**: Determine asymptotes.
- ☐ **Rule**: The root locus approaches \_\_\_\_\_ as asymptotes as the locus approaches infinity.
  - a. Number of asymptotes →

where n = # of OL poles

$$m =$$
# of OL zeros

For the current example: \_\_\_\_\_

b. Angles of asymptotes

$$\theta_k = \frac{(2k+1)180^{\circ}}{n-m}$$
, where  $k = 0, 1, 2, \dots$ 

For the current example, k = 0, 1, 2 because of 3 asymptotes.

$$\theta_1 = \frac{(1)180^{\circ}}{n-m} = 60^{\circ}, \ \theta_2 = \frac{(2+1)180^{\circ}}{n-m} = 180^{\circ}, \ \theta_3 = \frac{(5)180^{\circ}}{n-m} = 300^{\circ}$$



#### **Root Locus Sketching (4/9)**



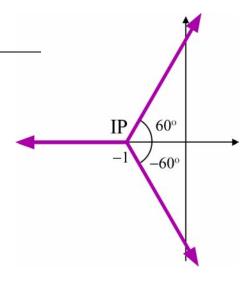
c. Intersection Point (IP) of asymptotes

$$\alpha = \frac{\sum poles - \sum zeros}{n - m}$$

It doesn't matter whether the poles and zeros are real or complex

For the current example

$$\alpha =$$



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## A

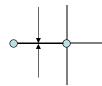
#### **Root Locus Sketching (5/9)**

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☐ **Step 4**: Determine break away/ break in points.



breakaway point



break-in point



not a break point

- ☐ Rule:
  - **a. Breakaway point** on the real axis occurs when the value of K is a \_\_\_\_\_ with respect to the values of K on either side.
  - **b. Break-in point** on the real axis occurs when the value of *K* is a \_\_\_\_\_ with respect to the values of *K* on either side.
- ☐ Thus, one first needs to find the maximum and minimum by using the derivative

and the solutions of the equation are the breakaway and break-in points.



#### **Root Locus Sketching (6/9)**



☐ For the current example, the denominator is given by

$$1 + GH = 0 = 1 + \frac{K}{s(s+1)(s+2)} = 0$$

and the characteristic equation is

From 
$$K = -s(s+1)(s+2) = -(s^3 + 3s^2 + 2s)$$
,  

$$\frac{dK}{ds} = 0 = \implies s = -0.45, -1.7$$

Since -1.7 is not on the RL, -0.45 is the breakaway point in this example.

□ Although −1.7 is an extremum point, since it is not on the valid branch, the point is not on the RL. As can be seen from this example, the derivative condition is a **necessary**, **but not sufficient** condition to indicate a break point.

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#### **Root Locus Sketching (7/9)**



□ **Step 5**: Determine departure and arrival angles.

The departure and arrival angles can be found by applying the Angle Criterion which states that

$$\underbrace{(\psi_1 + \psi_2 + \dots + \psi_m)}_{-} - \underbrace{(\phi_1 + \phi_2 + \dots + \phi_n)}_{-} = (2k+1)180^{\circ}$$

Angles from the zeros Angles from the poles to a test point to a test point

□ Rule:

**a. Departure angle** of a Root Locus from a pole can be found from

$$\phi_d = (\psi_1 + \psi_2 + \dots + \psi_m) - (\phi_1 + \phi_2 + \dots + \phi_n) - (2k+1)180^\circ$$

Angles from the zeros Angles from the poles to the **pole** of interest to the **pole** of interest

b. Arrival angle: of a Root Locus to a zero can be found

$$\psi_d = -\underbrace{(\psi_1 + \psi_2 + \dots + \psi_m)} + \underbrace{(\phi_1 + \phi_2 + \dots + \phi_n)} + (2k+1)180^\circ$$

Angles from the zeros Angles from the poles to the **zero** of interest to the **zero** of interest



#### **Root Locus Sketching (8/9)**



□ **Step 6**: Determine the frequency and gain at imaginary-axis crossing.

Method 1: The Routh-Hurwitz criterion can be used to find both the frequency and gain for which the Root Locus crosses the imaginary axis.

Method 2: Simply substitute \_\_\_\_\_ in the characteristic equation and set both the real and imaginary parts equal to zero.

**□** Example:

The characteristic equation:  $s^3 + 3s^2 + 2s + K = 0$ Then, by substituting \_\_\_\_\_ into the char. eq., one gets

$$\Rightarrow (K_{cr} - 3\omega^2) + (2\omega - \omega^3)j = 0$$

$$\Rightarrow K_{cr} = 3\omega^2 \text{ and } 2\omega = \omega^3$$

$$\Rightarrow \omega = \sqrt{2} \text{ and } K_{cr} = 3(\sqrt{2})^2 = 6$$

Thus, the Root Locus crosses at  $s = \pm j\sqrt{2}$  when K = 6.

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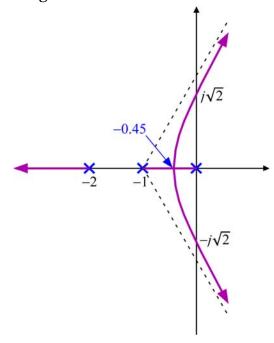
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#### **Root Locus Sketching (9/9)**

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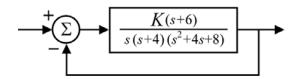
☐ The resulting Root Locus





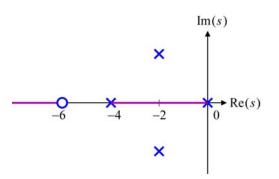
#### **Root Locus Sketching Example #1 (1/4)**





Zeros: -6Poles:  $0, -4, -2 \pm i2$ 

Steps 1,2



Step 3 n = 4, m = 1Number of asymptotes = For k = 0, 1, 2:

$$\theta_1 = 60, \ \theta_2 = 180, \ \theta_3 = 300$$

$$\alpha = \frac{-4 + (-2 + 2j) + (-2 - 2j) + 6}{3}$$
$$= -\frac{2}{3}$$

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## Root Locus Sketching Example #1 (2/4) THE UNIVERSITY OF ALABAMA

Steps 4:

$$\frac{K(s+6)}{s(s+4)(s^2+4s+8)} = -1 \longrightarrow K =$$

$$\frac{dK}{ds} = 0 \implies s = -3.08, -7.30 \text{ (real roots)}$$

(they are both on the root locus!)

Notice that we are only interested in the numerator because the denominator can't make dK/ds = 0

$$K = \frac{N(s)}{D(s)} \implies \frac{dK}{ds} = \frac{1}{2}$$

$$0 = D(s)N'(s) - N(s)D'(s)$$



#### **Root Locus Sketching Example #1 (3/4)**



$$N(s) = -(s^4 + 8s^3 + 24s^2 + 32s)$$
  $D(s) = s + 6$ 

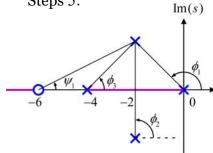
$$D(s) = s + 6$$

$$N'(s) = -(4s^3 + 24s^2 + 48s + 32)$$
  $D'(s) = 1$ 

$$D'(s) = 1$$

The roots of D(s)N'(s) - N(s)D'(s) = 0 can be found using Matlab:

Steps 5:



 $\phi_1 = 135^\circ$ ,  $\phi_2 = 90^\circ$ ,  $\phi_3 = 45^\circ$ 

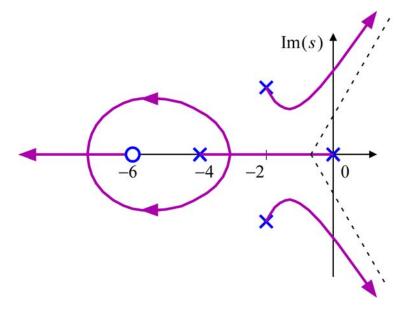
$$\psi_1 = \tan^{-1}(2/4) = 26.6^{\circ}$$

$$\phi_d = \sum \psi - \sum \phi - (2k+1)180^\circ$$

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#### **Root Locus Sketching Example #1 (4/4)** ALABAMA

Step 6: sketch



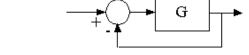


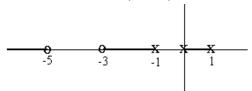
#### **Root Locus Sketching Examples (1/5)**



☐ Show the minimum calculations needed for R.L. of the unity feedback system.

1. 
$$G(s) = \frac{K(s+3)(s+5)}{s(s^2-1)}$$





3 poles, 2 zeros - so there is only one asymptote

# of asymptotes = 3 - 2 = 1

For 1 asymptote k = 0.

$$\theta_k = \frac{(2k+1)180^\circ}{1} = \frac{(2(0)+1)180^\circ}{1} = 180^\circ$$

You don't need to do a calc of the break-in/breakaway points.

No poles off of the real axis, so no departure angle calcs.

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#### **Root Locus Sketching Examples (2/5)**

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When the gain K is increased, the poles enter the stable region.

Find for which value of *K*, the system becomes stable.

Substitute  $s=j\omega$  in the characteristic equation and set both the real and imaginary parts equal to zero.

Char. Eq.: 
$$s(s^2 - 1) + K(s + 3)(s + 5) = s^3 - s + K(s^2 + 8s + 15)$$

$$(j\omega)^3 - j\omega + K((j\omega)^2 + 8j\omega + 15) = -j\omega^3 - j\omega + K(15 - \omega^2 + 8j\omega) = 0$$

$$\Rightarrow (15K - K\omega^2) + (8K\omega - \omega - \omega^3)j = 0$$

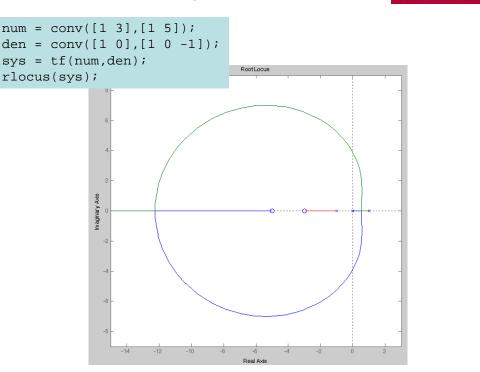
$$\Rightarrow \omega =$$
 and  $K =$ 

Thus, the Root Locus crosses at  $s = \pm j$  when K = \_\_\_\_.



### **Root Locus Sketching Examples (3/5)**







#### **Root Locus Sketching Examples (4/5)**



$$2. \quad G(s) = \frac{K}{s^2(s+p)}$$

3. Poles at 
$$0, -2, -3 \pm 2j$$



#### **Root Locus Sketching Examples (5/5)**



4. 
$$G(s) = \frac{K(s+2)^2}{s(s-2)(s+4)}$$

$$5. \quad G(s) = \frac{K}{s(s+4)^3}$$

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#### **Generalized Root Locus (1/2)**



- ☐ Using the same Root Locus technique, we can obtain a root locus for variations of system parameters other than the forward-path gain, *K*.
- ☐ For example: We can obtain a root locus for variations of the value of \_\_\_\_ in the following system.

$$R(s) \xrightarrow{+} 10 C(s) KG(s)H(s) = \frac{10}{(s+2)(s+p1)}$$

The problem is that p1 is not a \_\_\_\_\_ of the function, as the gain K.

- The solution to this problem is to create an equivalent system where p1 appears as the \_\_\_\_\_\_, *i.e.*, we effectively want to create an equivalent system whose denominator is 1 + p1G(s)H(s).
- $\Box$  For the example system, the CL transfer function is

$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)} = \frac{10}{s^2 + (p1+2)s + 2p1 + 10}$$



#### **Generalized Root Locus (2/2)**



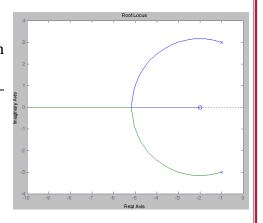
- $\Box$  By isolating p1, we have  $T(s) = \frac{10}{s^2 + 2s + 10 + p1(s + 2)}$ .
- Now, by dividing numerator and denominator by the term not included with p1,  $s^2 + 2s + 10$ , we obtain,

$$T(s) =$$

☐ We have reached a system for which

$$KG(s)H(s) =$$

and the root locus can now be sketched as a function of p1.



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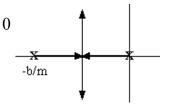
#### **Generalized Root Locus: Example 1**

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- Given the <u>closed</u> loop expression:  $\frac{Y}{R}(s) = \frac{1}{ms^2 + bs + k_1}$
- $\square$  We must express the <u>denominator</u> as , where K is the variable being varied.
- $\Box$  If we vary  $k_1$ , we must isolate it first.

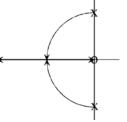
$$(ms^{2} + bs) + k_{1} = 0 \implies 1 + \frac{k_{1}}{ms^{2} + bs} = 0$$

$$\Rightarrow 1 + \frac{k_{1}}{\underbrace{ms^{2} + bs}} = 0$$



If we vary b,  $ms^{2} + k_{1} + bs = 0 \implies 1 + \frac{bs}{ms^{2} + k_{1}} = 0$  bs

$$\Rightarrow 1 + \frac{bs}{ms^2 + k_1} = 0$$

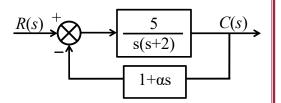




### Generalized Root Locus: Example 2 (1/2) THE UNIVERSITY OF ALABAMA



- Given the system to the right, plot the root locus for a system as  $\alpha$  goes from 0 to  $\infty$ .
  - \* Notice that  $\alpha$  cannot be simply multiplied by a transfer function.



Get the closed loop transfer function *C/R* in the form 1.

$$\frac{C}{R}(s) = \frac{G(s)}{1 + G(s)H(s)} \quad \text{or in our} \quad \frac{C}{R}(s) = \frac{\frac{5}{s(s+2)}}{1 + \frac{5(1+\alpha s)}{s(s+2)}}$$

- \* Note that you don't need to simplify the TF.
- Set the denominator equal to zero and isolate the variable in question. 2.

$$1 + \frac{5(1+\alpha s)}{s(s+2)} = 0 \Longrightarrow$$

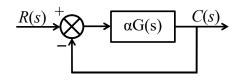
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### Generalized Root Locus: Example 2 (2/2) ALABAMA

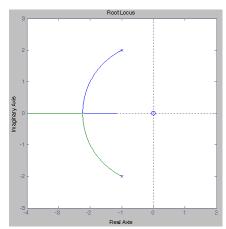
Write in the form 1 + KG(s) = 0 where *K* is the variable that goes from 3. zero to infinity.

$$1 + \frac{\alpha 5s}{s^2 + 2s + 5} = 0$$
 \* Notice that this is in the correct form and now  $K = \alpha$  in this example.

Plot the root locus. Notice that there is a new open loop transfer 4. function G(s). Our system now looks like:



$$G(s) =$$





#### **Selecting the Gain from the Root Locus**



Root locus is a plot of all possible root locations to the Closed-Loop characteristic equation or equivalently to the following equation:

$$1 + KG(s) = 0$$

- The two criteria that all the points on a RL must meet are
  - Magnitude criterion

$$|KG(s)| = 1$$

**Angle criterion** 

$$\angle KG(s) = (2k+1)180^{\circ}$$

Once the RL is obtained using the **angle criterion**, the gain value, K for each point on the RL can be found by using the **magnitude** criterion.

$$|KG(s)| = 1$$
  $\Rightarrow$   $K = \frac{1}{|G(s)|} (K > 0)$ 

K can be found numerically or graphically. 

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#### **Gain Selection- Method #1 (1/2)**

Q: When the OL transfer function is given as

$$G(s) = \frac{1}{s(s^2 + 8s + 32)} = \frac{1}{s(s^2 + 8s + 16 + 32 - 16)}$$
$$= \frac{1}{s((s+4)^2 + 16)} = \frac{1}{s(s+4+4j)(s+4-4j)},$$

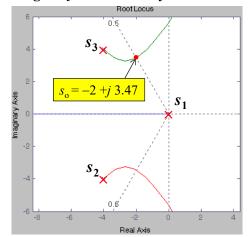
determine the CL gain, *K* needed to give  $\zeta = 0.5$  to the system.

- From the RL graph, one can find that the line of  $\zeta = 0.5$ crosses the root locus at
- The distance from each of the poles to  $s_0$  is:  $|s_o - s_1|, |s_o - s_2|, |s_o - s_3|$

where 
$$s_1 = 0$$
  
 $s_2 = -4 - 4j$ 

$$s_{2}^{1} = -4 - 4j$$

$$s_{3} = -4 + 4j$$





#### Gain Selection- Method #1 (2/2)



 $\Box$  The OL transfer function evaluated at  $s_0$  is:

$$G(s_o) = \frac{1}{s_o(s_o - s_2)(s_o - s_3)}$$

 $\square$  Now, using the magnitude criterion, the gain K can be calculated as

$$K = \frac{1}{|G(s_o)|} = |s_o||s_o - s_2||s_o - s_3| = |s_o||s_o + (4+4j)||s_o + (4-4j)|$$

$$= |-2 + 3.47j||-2 + 3.47j + 4 + 4j||-2 + 3.47j + 4 - 4j|$$

$$= |-2 + 3.47j||2 + 7.47j||2 - 0.53j|$$

$$=$$

$$=$$

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#### **Gain Selection- Method #2**



- ☐ This method works only for a third-order system.
- $\begin{array}{c|c} \hline K \\ \hline s(s^2+8s+32) \\ \hline \end{array}$
- ☐ For a third-order system shown,

$$\frac{Y}{R}(s) = \frac{K}{s(s^2 + 8s + 32) + K} = \frac{K}{s^3 + 8s^2 + 32s + K}$$

 $\hfill \Box$  Characteristic polynomial is:

$$D_c(s) = s^3 + 8s^2 + 32s + K$$

- This polynomial is compared with the standard cubic equation term by term.  $D_c(s) =$
- $= s^{3} + (2\zeta\omega_{n} + p)s^{2} + (2\zeta\omega_{n}p + \omega_{n}^{2})s + \omega_{n}^{2}p$   $\square \text{ We get the following three equations}$

 $8 = 2\zeta\omega_n + p, \ 32 = 2\zeta\omega_n p + \omega_n^2, \ K = \omega_n^2 p$ 

and the fourth equation is the design specification,  $\zeta = 0.5$ .

 $\square$  By solving the four equations simultaneously, one can get

$$p = 4$$
,  $\omega_n = 4$ ,  $K = 64$ 

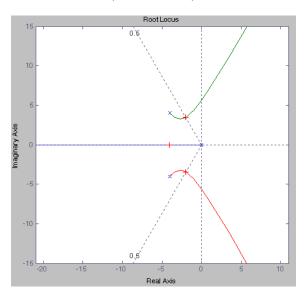


#### **Gain Selection- Method #3 (1/2)**



 $\Box$  Using Matlab, we can find the value of gain K that gives

$$G(s) = \frac{K}{s(s^2 + 8s + 32)}, \quad \zeta = 0.50$$



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#### **Gain Selection- Method #3 (2/2)**



☐ Matlab code:

```
clear; clf
                             % numerator
num=1;
den=[1 8 32 0];
                             % denominator
sys=tf(num,den);
rlocus(sys);
                             % draw root locus
zeta=.5;
wn=0;
                            % place grid line at zeta = 0.5
sgrid(zeta,wn);
                           % find value of K on the root locus
[K,p]=rlocfind(sys)
                            % point p at gain K is also found
pause
[sys2]=feedback(K*sys,1,-1) % closed loop system using gain K
step(sys2)
                             % system
```

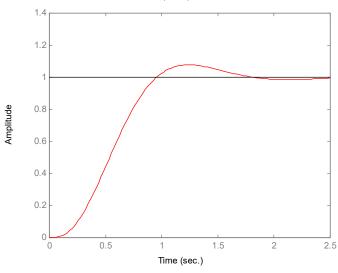


### **Gain Selection- Step Response**



$$G(s) = \frac{K}{s(s^2 + 8s + 32)}$$
 with  $\zeta = 0.50$ 





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