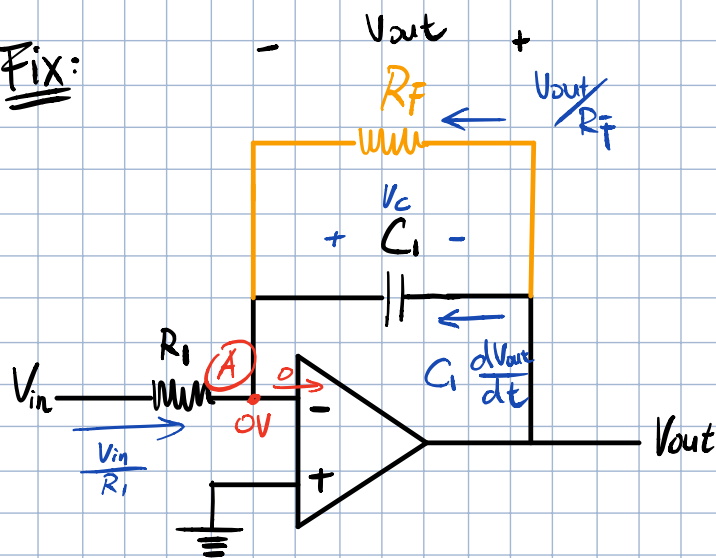
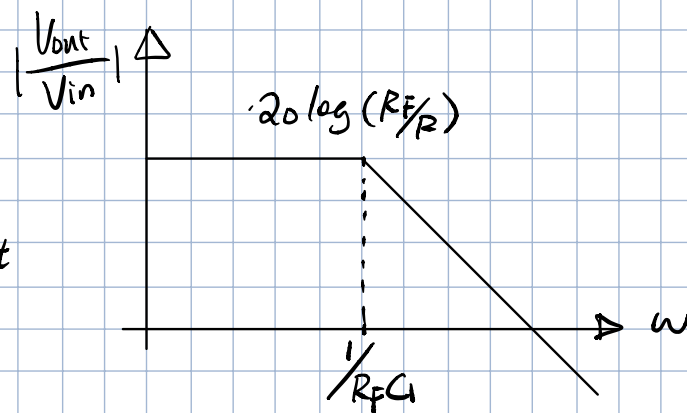


Fix:



$$\frac{V_{out}}{V_{in}} = - \frac{R_f // \frac{1}{j\omega C_f}}{R_i} = - \frac{R_f/R_i}{1 + j\omega R_f C_f}$$

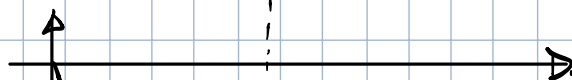
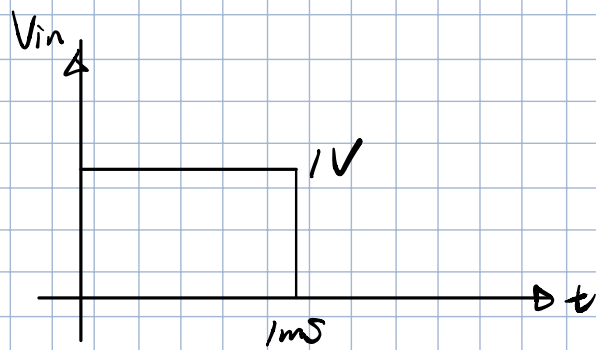
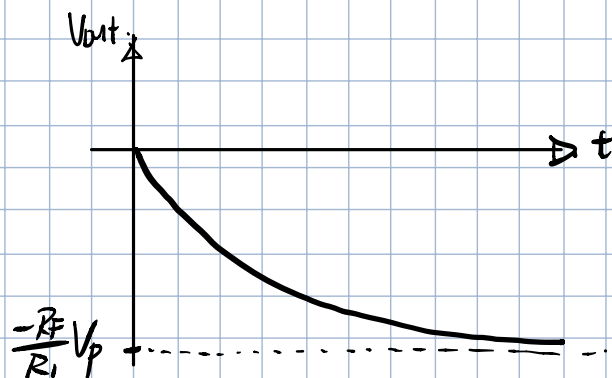
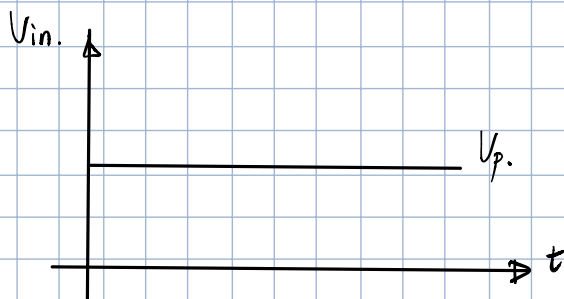


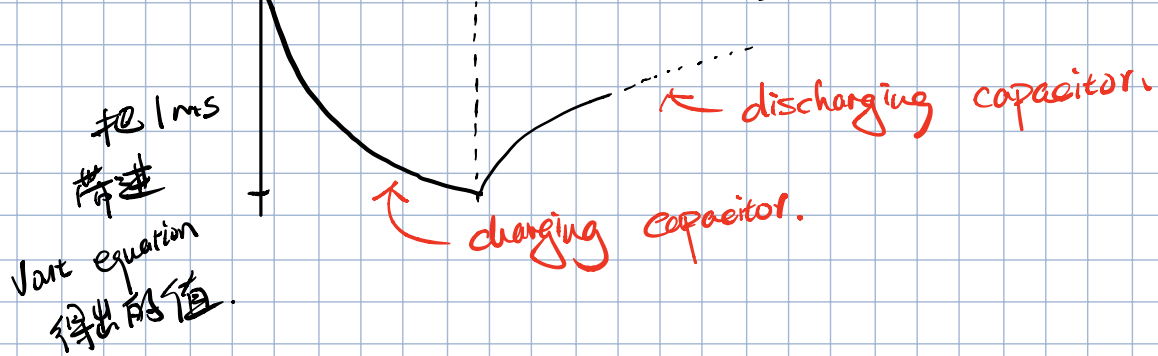
KCL @ Node (A):

$$\frac{V_{in}}{R_i} + \frac{V_{out}}{R_f} + C_f \frac{dV_{out}}{dt} = 0$$

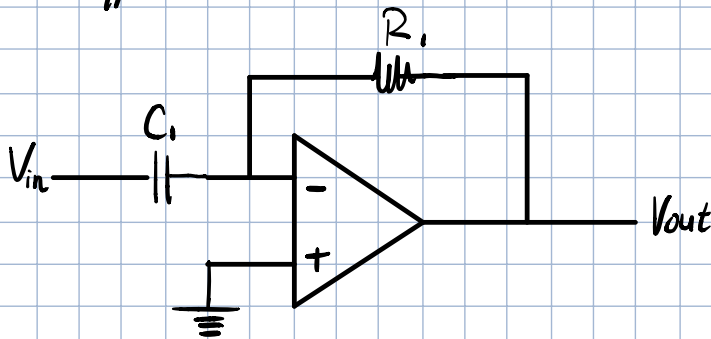
$$\underline{R_f C_f \frac{dV_{out}}{dt} + V_{out} = - \frac{R_f}{R_i} V_{in}} \quad \text{1st order D.E.}$$

$$V_{out} = - \frac{R_f}{R_i} V_p (1 - e^{-t/R_f C_f})$$



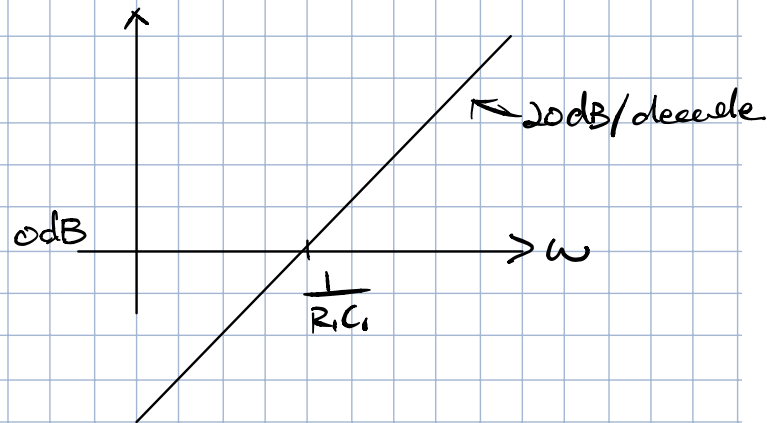


Differentiator.

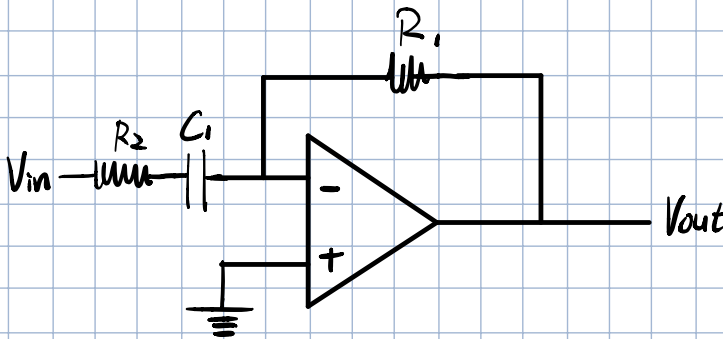


$$\frac{V_{out}}{V_{in}} = \frac{-R_1}{\frac{1}{j\omega C_1}} = -j\omega R_1 C_1$$

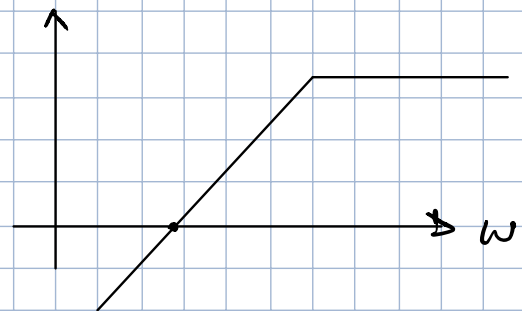
transfer function $\left| \frac{V_{out}}{V_{in}} \right| = \omega R_1 C_1$



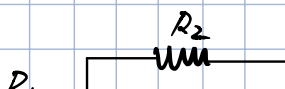
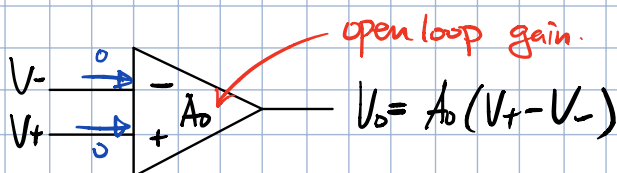
drawbacks: amplify noise @ high freq.



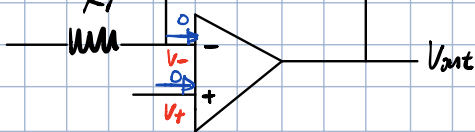
$$\frac{V_{out}}{V_{in}} = -\frac{R_1}{R_2 + \frac{1}{j\omega C_1}} = \frac{-sR_1C_1}{1 + sR_2C_1}$$



Summary of op-amp



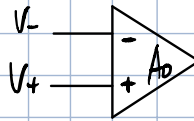
closed loop amplifier w/ negative feedback



$$V_- = V_+$$

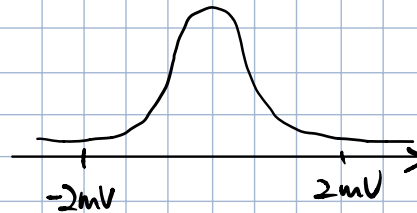
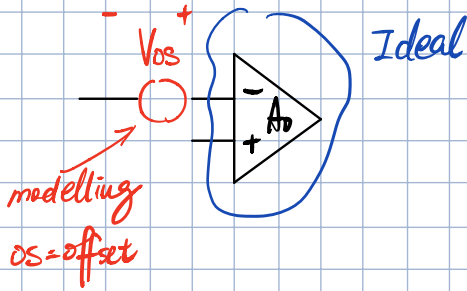
Op-Amp Imperfection.

① DC offset

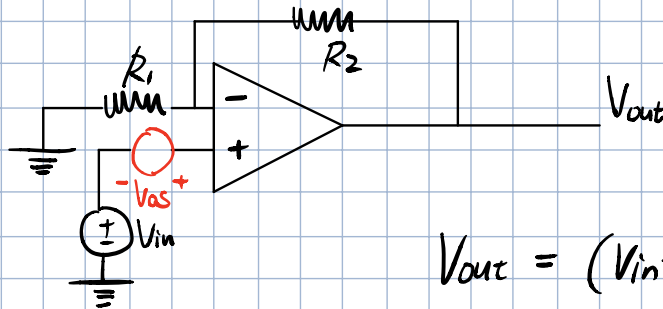


$$V_{out} = A_0(V_+ - V_-)$$

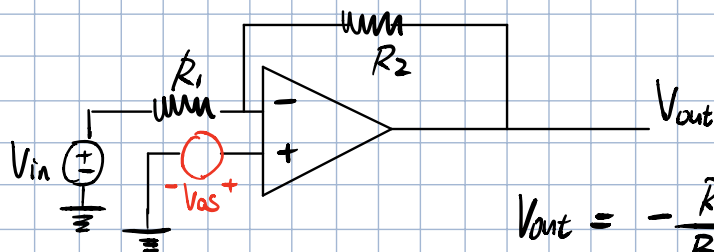
perfect op-amp: if $V_+ = V_- = 0$, $V_{out} = 0$



Effect of DC offset:



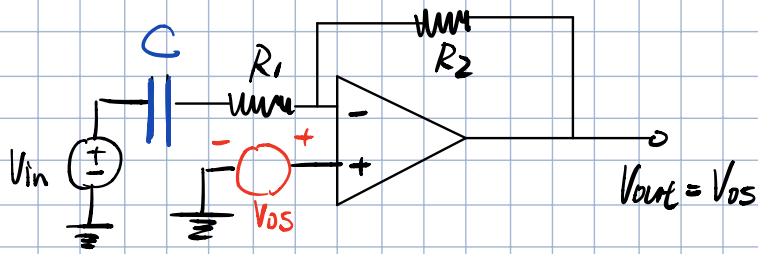
$$V_{out} = (V_{in} + V_{os}) \left(1 + \frac{R_2}{R_1}\right)$$



$$V_{out} = \underbrace{-\frac{R_2}{R_1} V_{in}}_{V_{os} \text{ turned off}} + \underbrace{V_{os} \left(1 + \frac{R_2}{R_1}\right)}_{V_{in} \text{ turned off}}$$

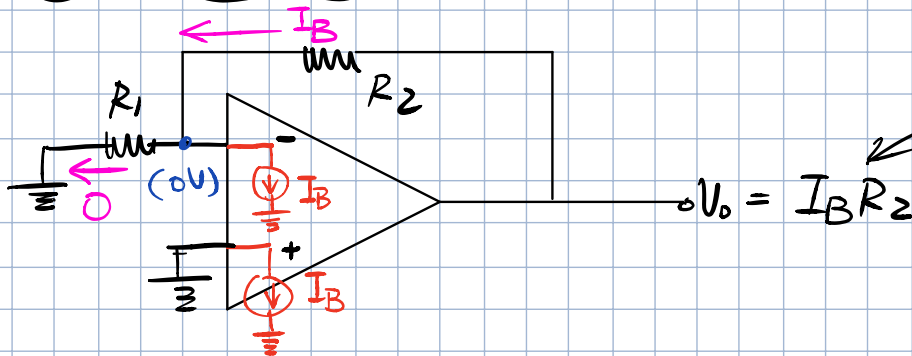
In both cases presented above, V_{os} is amplified. ☹️

Some relief for AC circuit.



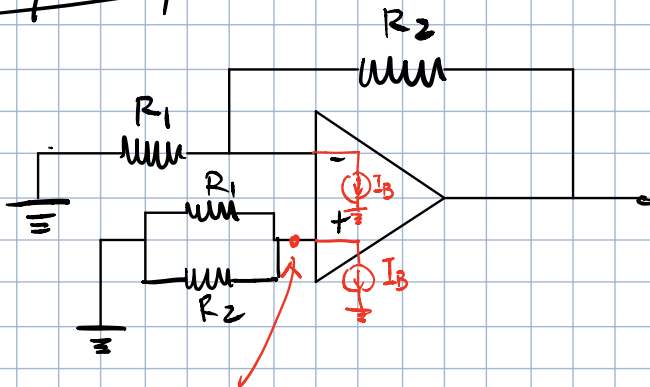
Capacitor is used to pass AC signal while blocking DC signal (V_{os})

2) Input Bias Current



non-zero voltage.

quick fix:



$$V_{out} = I_B R_2 - I_B \frac{R_1 R_2}{R_1 + R_2} \left(1 + \frac{R_2}{R_1} \right)$$

$$= 0$$

$$-I_B (R_1 // R_2) = -I_B \frac{R_1 R_2}{R_1 + R_2}$$