

EFFECTIVE PARAMETERS OF FERROELECTRIC DIELECTRIC MIXTURES

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ABSTRACT

We investigate the homogenized parameters of ferroelectric-dielectric composites under a static electric field. A numerical model that takes into account the coupling between the electrostatic problem and the electric field dependent permittivity of the ferroelectric material is used.

CONTEXT

Ferroelectric materials play a crucial role in reconfigurable microwave devices, with typical applications including antenna beam steering, phase shifters, tunable power splitters, filters, voltage controlled oscillators and matching networks [1], and the key requirements are large tunability and low losses. These materials have high permittivity values even at microwave frequencies, which can be an issue in some practical applications. Thus it has been considered to mix ferroelectrics to low-index and low-loss non-tunable dielectrics in order to reduce both permittivity values and losses, or to use porous ceramics [2, 3].

METHOD

Ferroelectric permittivity

Landau potential given by $F(P, E) = F_0 + aP^2/2 + bP^4/4 + cP^6/6 - EP$, where E is the applied electric field and P is the polarization [4, 5]

$$\epsilon^f(E) = \left[\frac{\partial^2 F(P, E)}{\partial P^2} \right]^{-1} = \frac{\epsilon^f(0)}{1 + \alpha P_0^2 + \beta P_0^4}, \quad (1)$$

Anisotropy

$$\epsilon^f(E) = \begin{pmatrix} \epsilon_{xx}^f(E_x) & 0 & 0 \\ 0 & \epsilon_{yy}^f(E_y) & 0 \\ 0 & 0 & \epsilon_{zz}^f(E_z) \end{pmatrix} \quad (2)$$

Electrostatic model

Gauss' law for the potential V :

$$\nabla \cdot (\epsilon \nabla V) = 0 \quad (3)$$

Homogenization

Two scale convergence homogenization [6, 7], TE case: solutions ψ_j of two annex problems

$$\nabla \cdot [\xi \nabla (\psi_j + r_j)] = 0, \quad (4)$$

where $r = (x, y)^T$ and $\xi = \epsilon^T / \det(\epsilon)$. The homogenized tensor $\tilde{\xi}$ is obtained with:

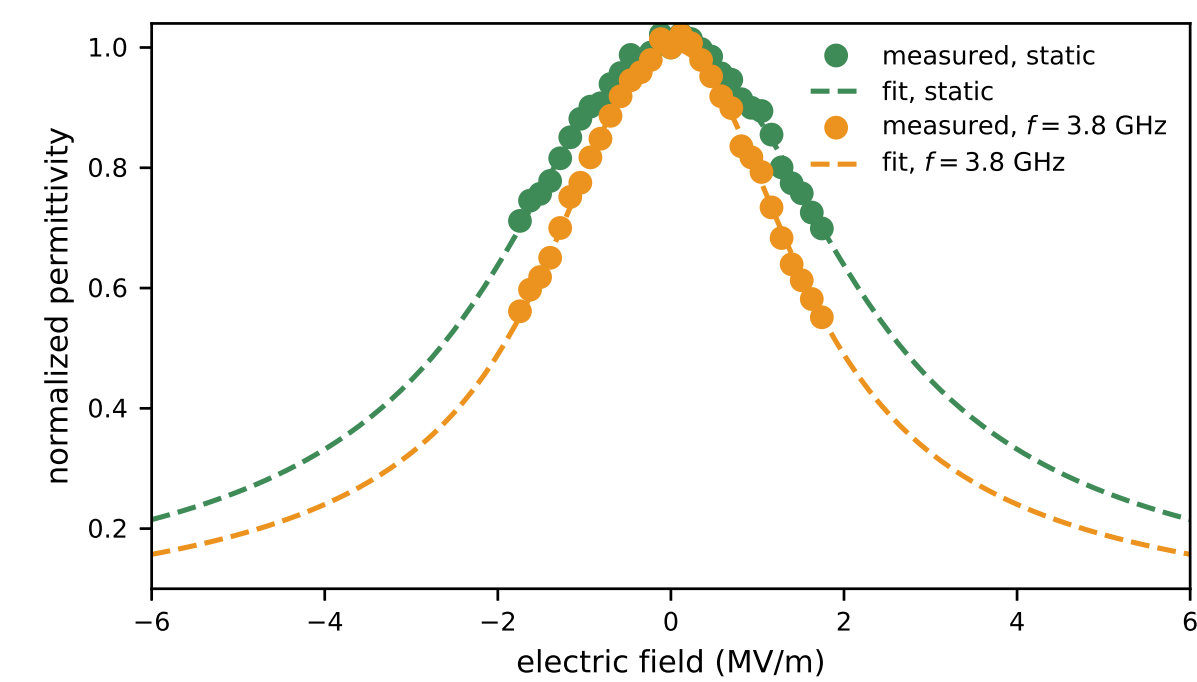
$$\tilde{\xi} = \langle \xi \rangle + \phi, \quad (5)$$

where $\langle \cdot \rangle$ denotes the mean value over the unit cell.

Correction terms $\phi_{ij} = \langle \xi \nabla \psi_i \rangle_j$.

Open source numerical implementation

Equations (3) and (4) are solved with a Finite Element Method using the freewares Gmsh [8] and GetDP [9] driven by a Python package.

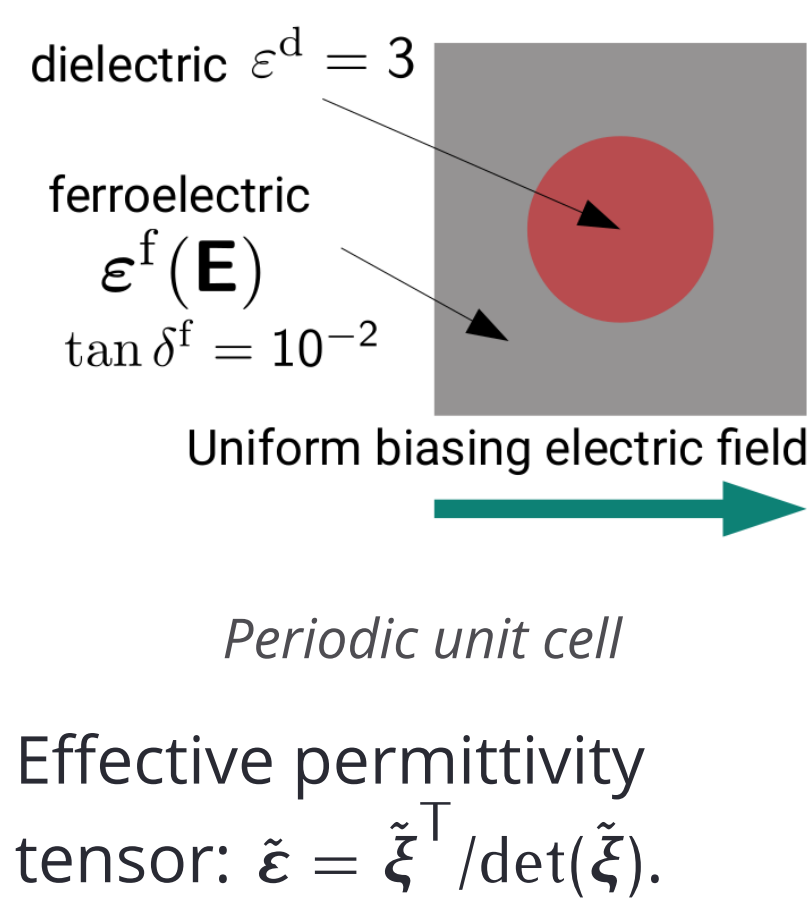


Variation of the ferroelectric permittivity as a function of the applied electric field.

case	$\epsilon^f(0)$	α ($\mu\text{m}^2/\text{V}^2$)	β ($\mu\text{m}^4/\text{V}^4$)
static	3050	0.120	0.024
$f = 3.8 \text{ GHz}$	165	0.240	0.079

Coupled problem

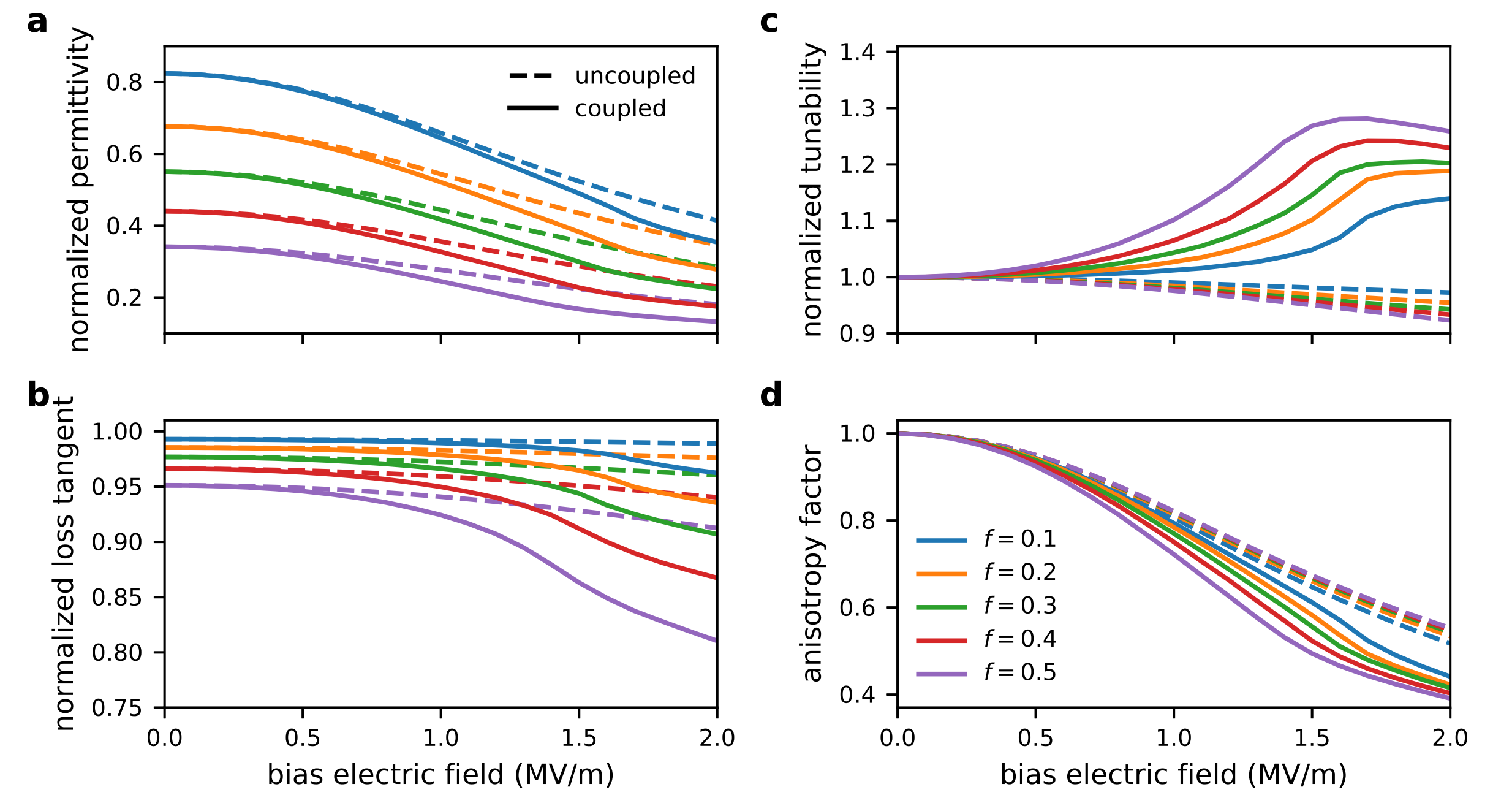
The electric field $E = -\nabla V$ derived from the solution of Eq. (3) depends on the permittivity distribution, which itself depends on the electric field through Eq. (1).



RESULTS

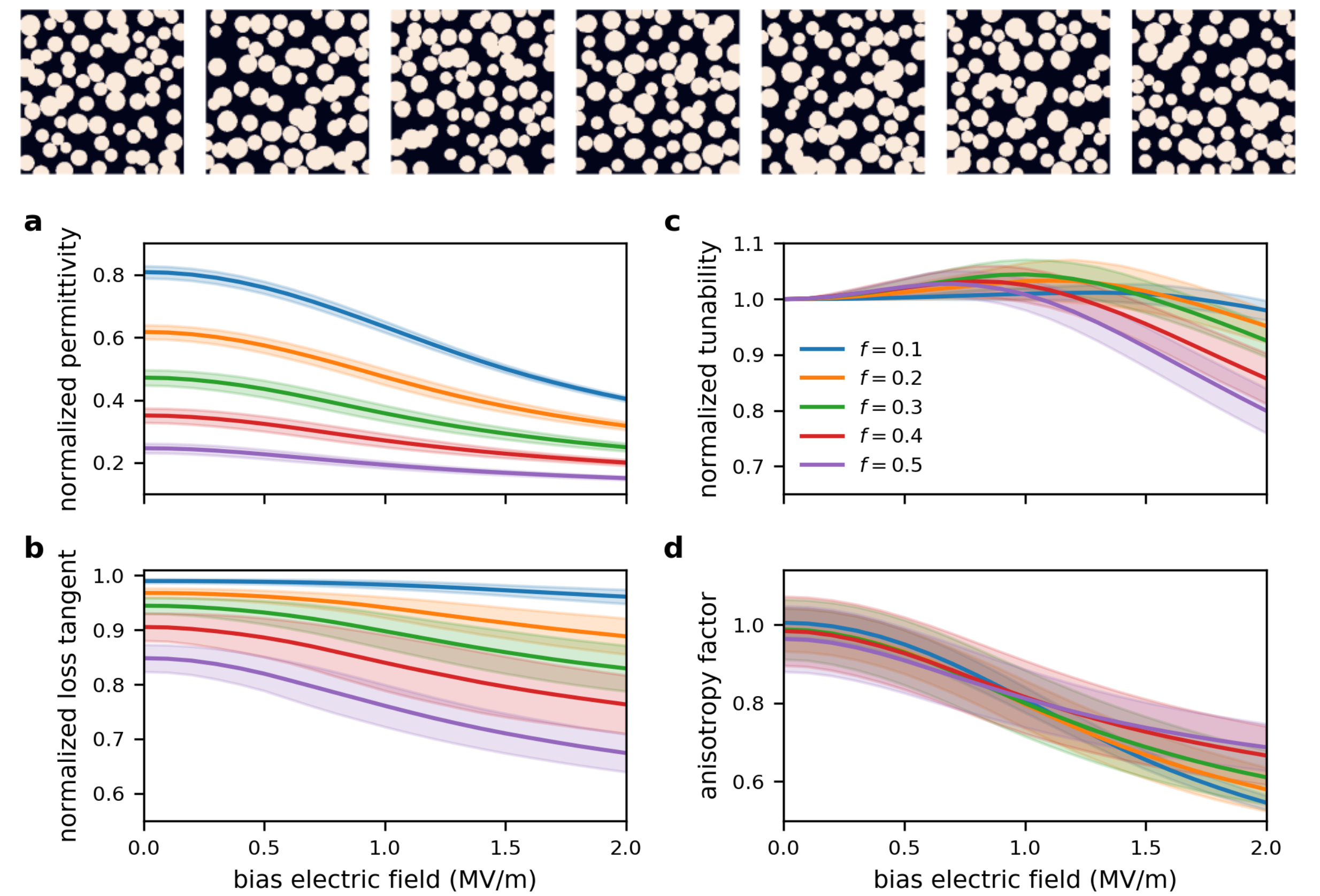
Effective parameters

Tunability $n = \epsilon_{xx}(0)/\epsilon_{xx}(E)$, anisotropy factor $a = \epsilon_{xx}(E)/\epsilon_{yy}(E)$



Effective parameters of the 2D metamaterials as a function of the applied electric field for various filling fraction of dielectric. (a): normalized permittivity, (b): normalized loss tangent, (c): normalized tunability and (d): anisotropy factor. The solid lines correspond to the coupled model and the dashed lines to the uncoupled model. Values are normalized with respect to the bulk properties.

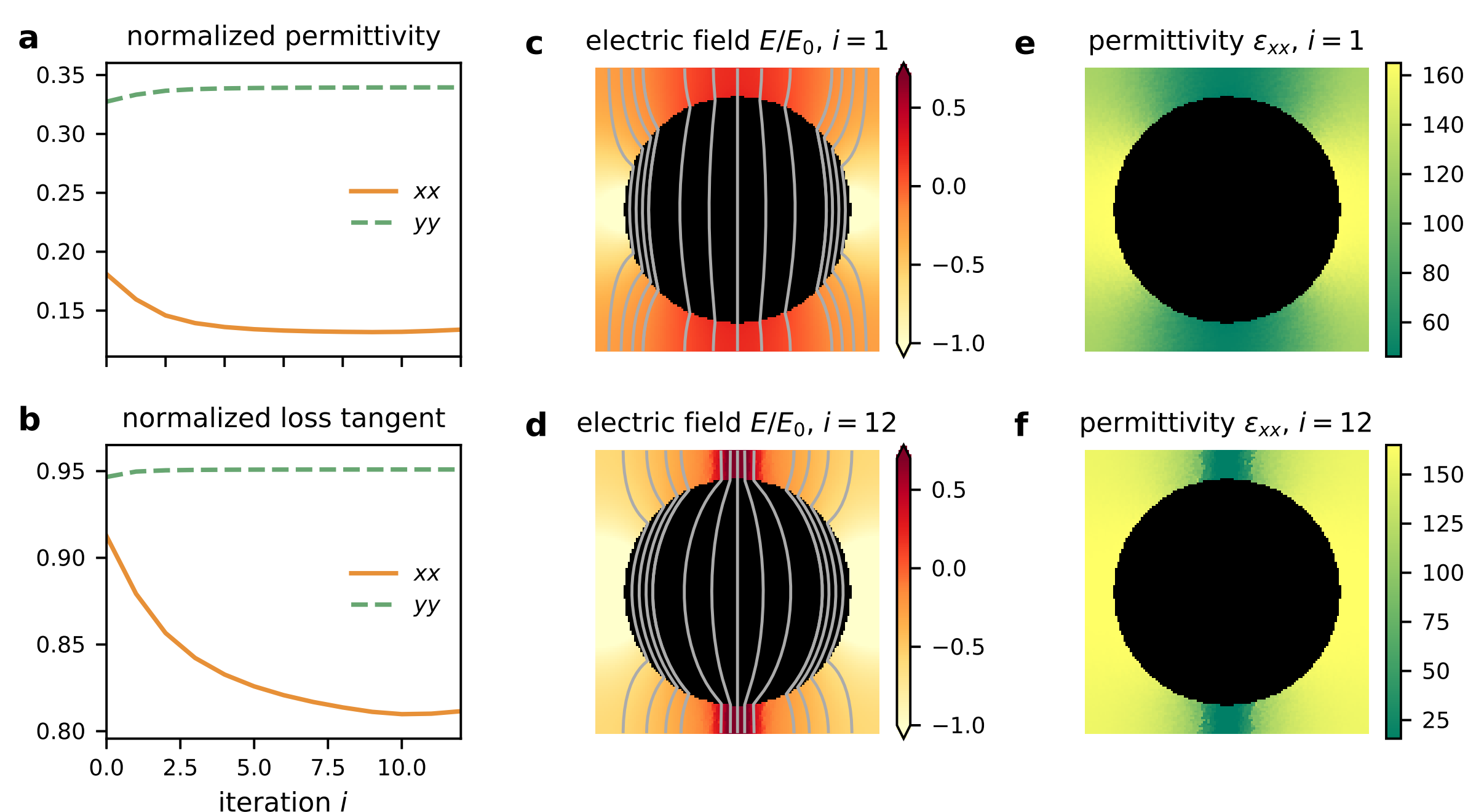
Pseudo-random case



Effective parameters of the pseudo-random composites as a function of the applied electric field for various filling fraction of dielectric, when the coupling is taken into account. (a): normalized permittivity, (b): normalized loss tangent, (c): normalized tunability and (d): anisotropy factor. The solid lines represent the average values over the 21 samples and the lighter error bands show a confidence interval corresponding to the standard deviation.

RESULTS

Periodic case



Convergence of the coupled problem. Real part (a) and loss tangent (b) of the components of the homogenized permittivity tensor as a function of iteration step i . The distribution of the normalized electric field (colour map: magnitude in logarithmic scale, lines: equipotential contours) and of the xx component of the permittivity tensor are shown for $i = 1$ (c and d) and $i = 12$ (e and f).

REFERENCES

- [1] A. K. Tagantsev et al. "Ferroelectric Materials for Microwave Tunable Applications". *J. Electroceram.* **11**:1-2 (2018), pp. 5–66.
- [2] V. O. Sherman et al. "Ferroelectric-dielectric tunable composites". *Journal of Applied Physics* **99**:7 (2006), p. 074104.
- [3] L. Padurariu et al. "Tailoring non-linear dielectric properties by local field engineering in anisotropic porous ferroelectric structures". *Appl. Phys. Lett.* **100**:25 (June 2012), p. 252905.
- [4] L. D. Landau et al. *Electrodynamics of continuous media*. **8**. elsevier, 2013.
- [5] K. Zhou et al. "Dielectric response and tunability of a dielectric-paraelectric composite". *Applied Physics Letters* **93**:10 (2008), p. 102908.
- [6] G. Allaire. "Homogenization and Two-Scale Convergence". *SIAM Journal on Mathematical Analysis* **23**:6 (1992), pp. 1482–1518.
- [7] S. Guenneau et al. "Homogenization of Three-Dimensional Finite Photonic Crystals". *Journal of Electromagnetic Waves and Applications* **14**:4 (2000), pp. 529–530.
- [8] C. Geuzaine et al. "Gmsh: A 3-D finite element mesh generator with built-in pre- and post-processing facilities". *International Journal for Numerical Methods in Engineering* **79**:11 (2009), pp. 1309–1331.
- [9] P. Dular et al. "A general environment for the treatment of discrete problems and its application to the finite element method". *IEEE Transactions on Magnetics* **34**:5 (Sept. 1998), pp. 3395–3398.

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