PHY 321 HW 5

a) as force depends only on position. We'll check it the cost is zero,

$$\overrightarrow{\nabla} \times \overrightarrow{F} = \begin{bmatrix} \overrightarrow{i} & \overrightarrow{j} & \overrightarrow{k} \\ \overrightarrow{j} & \overrightarrow{j} & \overrightarrow{j} \\ \overrightarrow{k} & 0 & 0 \end{bmatrix} = \overrightarrow{\partial_z} F_x \widehat{j} = \overrightarrow{\partial_z} F_x \widehat{k} = O_{\widehat{j}} - O_{\widehat{j}} = 0$$

Yes, the fire a conservative. This implies that the work done by this Force in the electron between 2 points is independent of the path taken, and the holk done arend a closed outh is zero.

$$\int_{-\frac{\pi}{b}}^{x} \int_{-\frac{\pi}{b}}^{x} \int_{-$$

$$mv^2 = \frac{F_3b}{T} \left(\omega_3 \left(\frac{2\pi \lambda}{b} \right) - 1 \right)$$

$$mv^{2} = \frac{F_{3}b}{\pi} \left(\omega_{3} \left(\frac{2\pi x}{b} \right) - 1 \right)$$

$$V(x) = \sqrt{\frac{F_{3}b}{m\pi}} \left(\omega_{3} \left(\frac{2\pi x}{b} \right) - 1 \right)$$

$$U(r) = -\int_{0}^{\infty} \vec{F}(x) \cdot d\vec{k} = \left(-\frac{F_{b}b}{2\pi} \left(\cos\left(\frac{2\pi x}{b} \right) - 1 \right) = U(x) \right)$$

4= FL naximum are at multiples of 16

zeros are at multiples of b

Analysis on next page.



Equilibrium points are every maximum and minimum. Maxes are unstable because any movement mad decrease the potential, while result in increasing kitche energy, and Forther decreasing Attential. Mint are stable E.P. 's because any magnet results in an increasing in an increasing energy.

311 -> B)

a) Fest acting on line of motion.



We start with P(t+dt) = (m+dm)(v+ds) - dm(v-vex) = mv + mdv + dmvex that the without Fert

with first, dp = P(t+1t) - P(t) = mdv + anvex where QP = First dt

=> Fext of = mdv + dn Vex

dividing by et = Fest: mdv + dn vex: mdv + Vex - dn

> Fext = mv + mva

regularity gles mu = -muex + Fext

b) IF Fext & scart, then this became mi = -mvex - mg

m=-k = m=m,-kt = mi=kvex-mg

or (mo-kt) = + kvex - (mo-kt) g

mi=kvex-mg = i= k vex-g = du=(kvex-glat=(m-kt vex-g)dt

where we will du = Strong - g) at

=> v= -vex en/k++mo/ = gt = -vex en/-m/-en/mo/-gt

= |v= Vex ln | mo | -gt



PHY 321 HW 5 PS 2

C) from 3.7 M= 2×106 kg, Matter 2 mix = 1×106 kg. Vex=3000 MJ. V== 2 min = 1×106 kg. Vex=3000 MJ. V== 2 min scandy

If there wil 10 grandy: U= 3000 en (2) = [2079.44 M/J = 10 scandy

If -MVex was less than -mg, than the force of staining would be larger than the thrust force, and the rocket wouldn't lift off until enough mass/weight would be lost from the exhaust. Your overall F=mq=0 since your contact force with the ground would equal whatever extra graintanood force is left. Eventually, reducing mass could cause mg to be smaller, and the rocket could take off.

3) 3.13) we have $v(t) = V_{ex} \ln \left| \frac{m_0}{m} \right| - gt = V_{ex} \ln \left| \frac{m_0}{m_0 - kt} \right| - gt$ Takes rate gives $y(t) = V_{ex} \cdot \int \ln \left| \frac{m_0}{m_0 - kt} \right| dt - \frac{1}{2}gt^2$

Sen | m-kt | at = Sen(w) -k. ak = -k Sen(w) du = -k (u·(en(u)-1)

your extitation of the

 $\int en \left| \frac{m_0}{m_0 - kt} \right| dt = - \left[t \left(en \left(\frac{m_0 - kt}{n_0} \right) \cdot \frac{m_0}{k} - 1 \right] = t - \frac{m_0}{k} ln \left(\frac{m_0}{n_0} \right) \right]$ $= t + \frac{m_0}{k} ln \left(\frac{m_0}{n_0} \right) = t - \frac{m_0}{k} ln \left(\frac{m_0}{n_0} \right)$

Plussy back in a JCE1= Vex (+- men(m))- = gt2 = Vext - vexm en(m)- = st

= (mo) = vext - 19t2 - muck en (mo)

9 fres 120 kends, $\frac{m}{n} = 2$, $k = \frac{M_0 - M}{t} = \frac{166}{120} = 8333, 3\bar{j}$ $4(6) = 3000.120 - \frac{1}{2}.9.81.120^2 - \frac{106.3000}{10\%20} ln(2) = 369,000 - 79632 - 249533$ $4(120) \approx 39835$

12 after 2 minutes, [y/120] = 39,835 m

3.14)
$$\vec{f} = -b\vec{v}$$
 $m\vec{v} = -mv_{ex} + f^{ext} = -mv_{ex} - bv$
 $m = m - kt$
 $m = kv_{ex} - bv$
 $m - kt$
 $m - kt$

$$\exists \begin{array}{l} \frac{1}{k} \ln \left| \frac{m_0}{m} \right| = \frac{1}{b} \ln \left| \frac{k v_{ex}}{k v_{ex} - b v} \right|$$

$$\ln \left| \frac{k v_{ex}}{k v_{ex} - b v} \right| = \frac{b}{k} \ln \left| \frac{m_0}{m} \right|$$

$$\frac{k v_{ex}}{k v_{ex} - b v} = \frac{m_0}{k} \frac{k v_{ex}}{k v_{ex} - b v} = \frac{m_0}{k} \frac{k v_{ex}}{k v_{ex} - b v}$$

$$\Rightarrow k v_{ex} - b v = k v_{ex} \left(\frac{m_0}{m_0} \right)^{k/k}$$

$$v = \frac{k v_{ex}}{b} - \frac{k v_{ex}}{b} \left(\frac{m_0}{m_0} \right)^{k/k}$$

$$\Rightarrow v = \frac{k}{b} v_{ex} \left(1 - \left(\frac{m_0}{m_0} \right)^{k/k} \right)$$

MY 321 HW 5 093

4) 3,20) M, M2 at R, R2. Let M, and M2 be composed of n and p point we know $R_1 = M_1 \stackrel{?}{=} M_2 \stackrel{?}{=} M_2 \stackrel{?}{=} M_2 \stackrel{?}{=} M_2 \stackrel{?}{=} M_2 \stackrel{?}{=} M_3 \stackrel{?}{=} M_3 \stackrel{?}{=} M_3 \stackrel{?}{=} M_3 \stackrel{?}{=} M_4 \stackrel{?}{=} M_2 \stackrel{?}{=} M_3 \stackrel{?}{=} M_3$ he know the total center of Mail R= (Ma) = E Mara $= \left[\underbrace{\underset{q=1}{\overset{\wedge}{\otimes}}}_{M_{\alpha}} M_{\alpha} + \underbrace{\underset{q=n+1}{\overset{\wedge}{\otimes}}}_{M_{\alpha}} M_{\alpha} \right] \cdot \left[\underbrace{\underset{q=1}{\overset{\wedge}{\otimes}}}_{M_{\alpha}} M_{\alpha} + \underbrace{\underset{q=n+1}{\overset{\wedge}{\otimes}}}_{M_{\alpha}} M_{\alpha} \right]$ $= \left[M_{1} + M_{2} \right] \cdot \left[M_{1} R_{1} + M_{2} R_{2} \right]$ => (R = M, R, +M2R2)

5) a) I Au = 1.5×10" M. Mo= 2×1030 kg. MELIN = 6×1027

INDIANTE X=1 Av. 7:0. Assume almost exceller Motion.

For SMOME dix = For Men dix - For Men dix - For Men dix - For Men dix - Men dix - For Me

ox $r = \sqrt{x^2 + y^2} + remake$. $F_{x} = \frac{-6M_0 M_E}{r^2} \omega x \theta = \frac{-6M_0 M_E}{r^2} x^{2}$ F = -6 Mone 1140 = -6 Mone y

4 First-order capiel effectful equations: \(\frac{dv_x}{at} = \frac{-6M0}{r^3} \times \frac{dv_y}{at} = \frac{-6M0}{r^5} \times di = Vx

Now he need to get make these dimension/011.

assuming eiterlas state, $V = \frac{M_{E}V^{2}}{year} = \frac{6M_{O}M_{E}}{7} = \frac{6M_{O}M_{E}}{7} = \frac{7}{6M_{O}} = \frac{1}{2}C$ assuming eiterlas state, $V = \frac{2\pi r}{year} = \frac{2\pi \cdot 1AV}{year} = \frac{7}{9} \left(\frac{AV}{V}\right)^{3}$

usity step length h.

b) wing ever) method, this discretized as,

$$V_{x,i+1} = V_{x,i} - h \frac{y_{\pi^2}}{r_{i}^3} \times;$$

$$X_{i+1} = X_i + h V_{x,i} \leftarrow$$

$$V_{y_{i+1}} = V_{y_{i}} - h \frac{y_{\pi^2}}{r_{i}^3} y_{i}$$

$$y_{i+1} = y_{i} + h V_{y_{i}} \leftarrow$$

or Uxing and Uxing if ever-cromes method



Values velocity-verlet method:
$$\begin{array}{lll}
X_{i+1} = X_i + ot V_i + \frac{ot^2}{2} a_i \\
V_{i+1} = V_i + \frac{ot}{2} (a_{i+1} + a_i) & \text{wher } a_{i+1} \text{ degends only on } X_{i+1}
\end{array}$$

Note, then sam equation work for y or & direction, just replace for example & with y, I with by, and as was ay.

