Continuous-time LTI Impulse Response and Convolution

ECEN 380 Section 001

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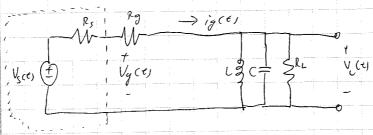
Objective: The purpose of this lab is to help us better understand

LTI systems and the principles of convolution and impulse vesponse

We will under stand the mathematics to model LCCDES and how they

apply to analog circuits. We will build a croson speaker

Task 1:



function generator

By using KCL, wasce: ic(+) + ip(+) + i(+) - ig(+)

Using the equation for current for L, Re, and C, and then differentiating the equation, we get: $(\frac{d^2}{dt^2}V_L(t) + \frac{1}{R_f}\frac{d}{dt}V_L(t) + \frac{1}{L}V_L(t) = \frac{d}{dt}ig(t)$

Divide by C: de Vices + 1 of Vices + 1 Vices = 1 d igces

We find that 2, = RC 2= CL

We are using the values $R_1 = 8-9$ L = 2.78 m/H C = 4.83 n/H Q = 4.83 n/H $Q = 4.83 \text{ n$ = 27.447 X10

$$R_1 = -\frac{\lambda_1}{2} + \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

$$R_2 = -\frac{\lambda_1}{2} - \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

$$R_3 = -\frac{\lambda_1}{2} + \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

$$R_4 = -\frac{\lambda_1}{2} + \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

$$R_5 = -\frac{\lambda_1}{2} + \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

$$R_7 = -\frac{\lambda_1}{2} + \sqrt{\left(\frac{\lambda_1}{2}\right)^2 - \lambda_2}$$

= -2.87752 = -25879997

$$X(e) = \frac{1}{c} \frac{dx}{dc} i_j(e)$$
 $i_g(e) = \frac{V_s(e)}{R_{s+R_g}}$

$$\times (t) = \frac{1}{C} \frac{d}{dt} \frac{V_s(t)}{R_{s+R_g}}$$

$$y(t) = V_c(t)$$
 $\partial_1 = \frac{1}{r_c}$ $\partial_2 = \frac{1}{cL}$

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 $h_{c}(\epsilon) = h_{i}(t) + h_{z}(t)$, $h_{c}(\epsilon)$ is the impulse response for a generic x(t) Task [

 $=\int_{0}^{t}\frac{e^{-rt}+P_{2}(t-r)}{e^{-rt}}dr=\frac{1}{r_{1}-r_{2}}e^{-r_{1}}\frac{1}{r_{1}-r_{2}}\left[\frac{\rho_{1}+\rho_{2}t}{r_{1}-r_{2}}+\frac{1}{r_{1}-r_{2}}\left[\frac{\rho_{1}+\rho_{2}t}{r_{1}-r_{2}}+\frac{1}{r_{1}-r_{2}}\right]\frac{1}{r_{1}-r_{2}}e^{-r_{1}-r_{2}}$

they

 $X(t) = \frac{1}{c} \frac{d}{dt} \frac{v_s(t)}{v_s + v_g}$ $h(t) = \frac{1}{\rho_1 - r_2} \left[\rho_1 e^{\rho_1 t} - \rho_2 e^{\rho_2 t} \right] \frac{1}{c} \frac{1}{\rho_s + r_g}$

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 $\frac{\mathbb{P}_{1}}{\mathbb{Z}R_{L}C} + \sqrt{\frac{1}{\mathbb{Z}R_{L}C}} - \frac{1}{\mathbb{Z}L} = \frac{-1}{\mathbb{Z}R_{L}C} + \sqrt{\frac{1}{\mathbb{Z}R_{L}C^{2}}} - \frac{1}{\mathbb{Z}L}$

 $P_{2} = \frac{-1}{2R,C} \quad \left(\frac{1}{4R_{c}^{2}c^{2}} - \frac{1}{CC} \right)$

 $\frac{1}{p_1 - p_2} \left[e^{p_1 \epsilon} - e^{p_1 \epsilon} \right] u(\epsilon) = h_c(\epsilon)$

For 8 IZ = R, X = 1 = 12940 > W = 1375 so it's overdamped

For $R_{c}=33$ $\Delta = \frac{1}{2R_{c}}=3136$ $>W_{o}$ soit's overdanged for $R_{c}=100$ $\Delta = \frac{1}{2R_{c}}=1035$ < W_{o} so it's underdanged.

It looks like a RLC natural response because the capacitine and the inductance were designed with a 82 load in mind.

R = 8 ohms

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R = 33 ohms

6000

4000

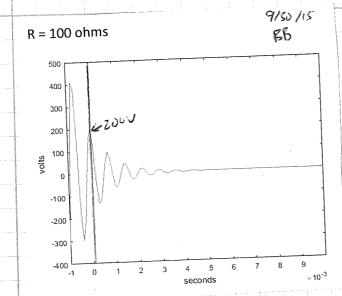
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Task 1



```
r = 8;
rs = 50;
rg = r*10;
1 = 2.78e-3;
c = 4.83e-6;
t = -1:1e-4:10e-3;
p1 = (-1/(2*r*c)) + sqrt((1/(4*r^2*c^2)) -
1/(c*1));
p2 = (-1/(2*r*c)) - sqrt((1/(4*r^2*c^2)) -
1/(c*l));
h_t = (1/(c*(p1-
p2) * (rs+rg))) * (p1*exp(p1*t)-
p2*exp(p2*t));
figure(1);
plot(t, h t);
xlim([-1e-3 1e-2]);
xlabel('seconds');
ylabel('volts');
```

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1) sing the motlab code above, we plotted the impulse vesponse of the RLC circuit with R=8,33,100.

We are building the circuit described from task 1. We used L= 2.78 mH, C= 4.83 MF TASK Z

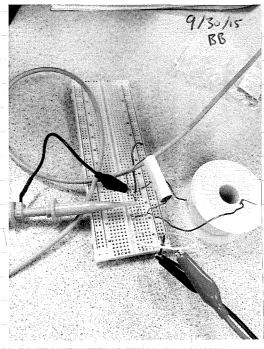
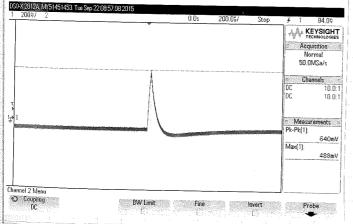


Photo of our circuit

Using the oscilluscope and a pulse from the function generator, we obtained the waveforms below. They represent the voltage drops across the load vesistor. We took the calculated values and divided them by the actor

R = 8.2 ohms

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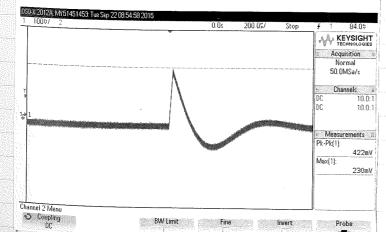


Measured whe to obtain the scaling factor. Scaling factor:

1600V = 3200

R = 33 ohms

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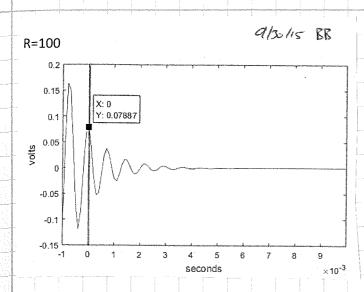


Scaling factor: 550v : 2391

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R=

Task 2



Calculated Measured
0.07887 V 0.09 V

The calculated MATLAB plots matched up fairly closely with the measured response. The errors could have been caused by several things, including: differences in actual values of the inductor and capacitor. We did not measure what the exact value of them. We just used the printed value and did not take into account the tolerance. It could also have been the noise from the 0-scope.

Using the h(t) = (P, Pz)(rs+rg) (P, e P, t), we did the TASK 3

Convolution with 2 rect function.

K= C.(P,-P2)(rstry) for tet. Jok Pie Pretail de

= K[e,(t+) P2(t+)]| = K[e,t-e,t]

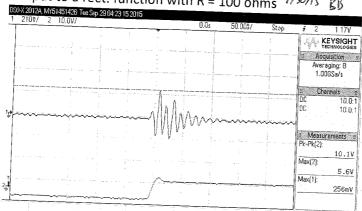
for t>to Jok P. (e-to) P. e Price- v) Cz = K[e, (e-v)] | hosto

We used the function generator to generate a vect function and vecorded the output. Output to a rect. function with R = 33 ohms

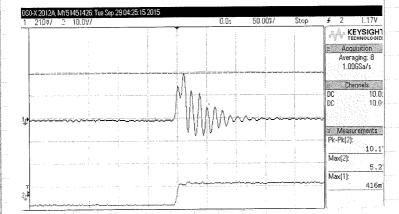
| DSOX 2012A M/514/51428 Tue Sep 2904/2005/2015 | Troth / 2 10.007 | D.0s | 50.002/ Stop | 5 2 1.17V | TECHNOLOGIES | Acquisition | Averaging | 8 1.00053a/s | 1. Channels | D.C. 10.0:1 | D.C. 10.17 | Max/2; | 5.8V | 5.8

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Output to a rect. function with R = 100 ohms 9/30/15 gß



Output to a rect. function with R = 8 ohms $9/3 \cdot 1/5$ BB



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Convolution Code:

```
r = 8;
rs = 50;
rg = r*10;
1 = 2.78e-3;
c = 4.83e-6;
t = -1:1e-4:10e-3;
scaleFactor = 2500;
h_t = ((1/(c*(p1-p2)*(rs+rg)))*(p1*exp(p1*t)-
p2*exp(p2*t))) / scaleFactor;
t_0 = 1e-3;
t1 = t - t_0;
constant = 1/(c*(p1-p2)*(rs+rg));
funct1 = constant*(-exp(p1*(t)) +
\exp(p2*(t))).*(t<t_0);
funct2 = constant*(-exp(p1*(t)) + exp(p2*(t)) +
\exp(p1*(t1))-\exp(p2*(t1))).*(t>=t_0);
Convolved = (funct1 + funct2).*(t>0).*10;
figure(1);
plot(t, Convolved);
xlim([-1e-3 1e-2]);
xlabel('seconds');
ylabel('volts');
```

We wrote MATLAB code to compute the consolution based on our integracion. The plots (an bee seen on the next page

-0.4 Con 0. 0.

-0.0

-0.1

-0.2

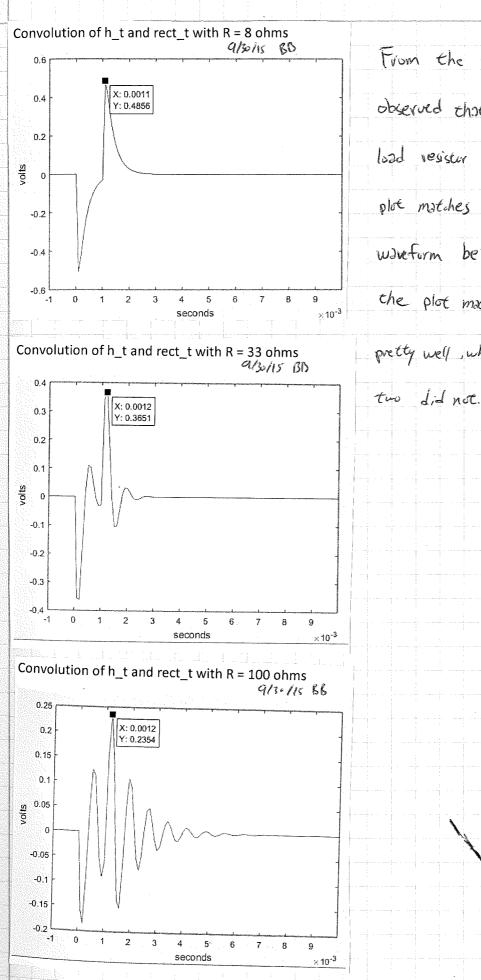
-0.

-0.:

Con

Con

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From the plots, we observed that when the load resistor is higher, the plot matches the measured waveform better. For R = 100.00 the plot matched the measurement pretty well, while the other

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Task 3
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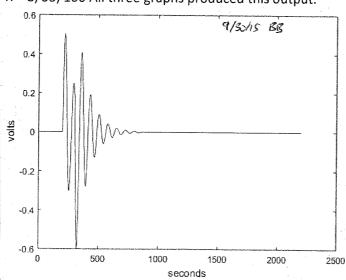
Matlab Code with conv funct.

```
r = 33;
rs = 50;
rg = r*10;
1 = 2.78e-3;
c = 4.83e-6;
t = -.001:1e-5:10e-3;
scaleFactor = 2500;
p2 = (-1/(2*r*c)) + sqrt((1/(4*r^2*c^2)) -
1/(c*1));
p1 = (-1/(2*r*c)) - sqrt((1/(4*r^2*c^2)) -
1/(c*1));
h_t = ((1/(c*(p1-
p2) * (rs+rg))) * (p1*exp(p1.*t)-
p2*exp(p2.*t))) / scaleFactor.* (t >= 0);
t_0 = 1e-3;
rect_t = double(t>=0 & t <= t_0);
x = conv(rect_t, h_out);
figure(1);
plot(x);
xlabel('seconds');
ylabel('volts');
```

Above is the MATLAB Code to plot the convolution of h(t) and rece(t). Using the MATLAB function conv.

Below is the plot

R = 8, 33, 100 All three graphs produced this output.



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cz (+).

Conclusion

In this 126 we will able to derive the impulse response mathematically as well as measure it based on the circuit that we built. The graphs looked fairly similar except for the selling factor. This is due to the Q.F.G. not being able to generate and infinite pulse. We were able to calculate the scaling factor and vedraw the graphs in MATA MATCAB. This yielded plots that were much closer to the measured graph We were then able to to a convolution convolve h(t) with vector, to predict the artest. We then used the T.G. to create a vert function and measure the output The Using MATLAB to do the complution bosed on our calculations unided similar graphs for the output for LOW St, but less similar graphs for tesser resistance. Then using the conv function in MITTARS we plot the untput again.

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