



EECS 16B

Designing Information Devices and Systems II

Lecture 25

Prof. Yi Ma

Department of Electrical Engineering and Computer Sciences, UC Berkeley,
yima@eecs.berkeley.edu

Outline

- Principal Component Analysis (Statistics)
 - Least Squares versus Principal Components
- Linearization of Nonlinear Systems

Principal Component Analysis (Statistics)

$$U = [U_\ell, U_{m-\ell}] \in \mathbb{R}^{m \times m} \text{ orthogonal} \quad \|A\|_F^2 = \|UU^\top A\|_F^2 = \|U_\ell U_\ell^\top A\|_F^2 + \|U_{m-\ell} U_{m-\ell}^\top A\|_F^2$$

$$\underbrace{\max_{U_\ell} \|U_\ell U_\ell^\top A\|_F^2}_{A = \{\vec{a}_1, \vec{a}_2, \dots, \vec{a}_n\}} \Leftrightarrow \underbrace{\min_{U_\ell} \|A - U_\ell U_\ell^\top A\|_F^2}_{\sum \vec{a}_i = 0} \Leftrightarrow \min_{U_{m-\ell}} \|U_{m-\ell} U_{m-\ell}^\top A\|_F^2$$

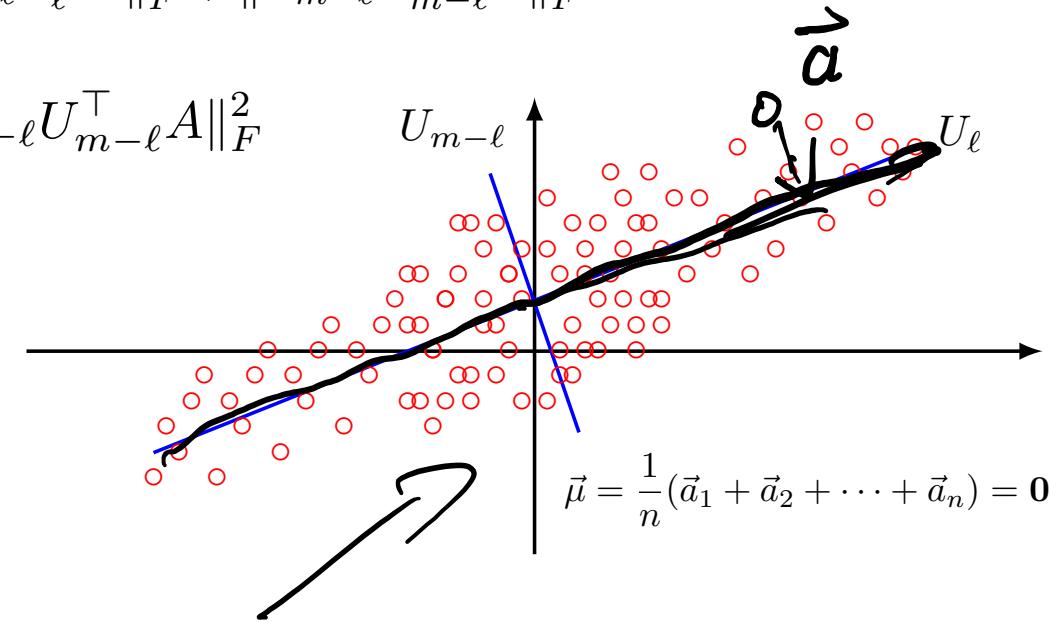
$$A = [\vec{a}_1, \vec{a}_2, \dots, \vec{a}_n] \quad \sum \vec{a}_i = 0$$

$UU^\top A \leftarrow$ preserve most info.

$\|\vec{a}_i - U_\ell U_\ell^\top \vec{a}_i\|$ minimized.

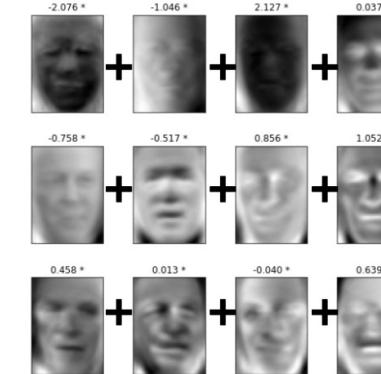
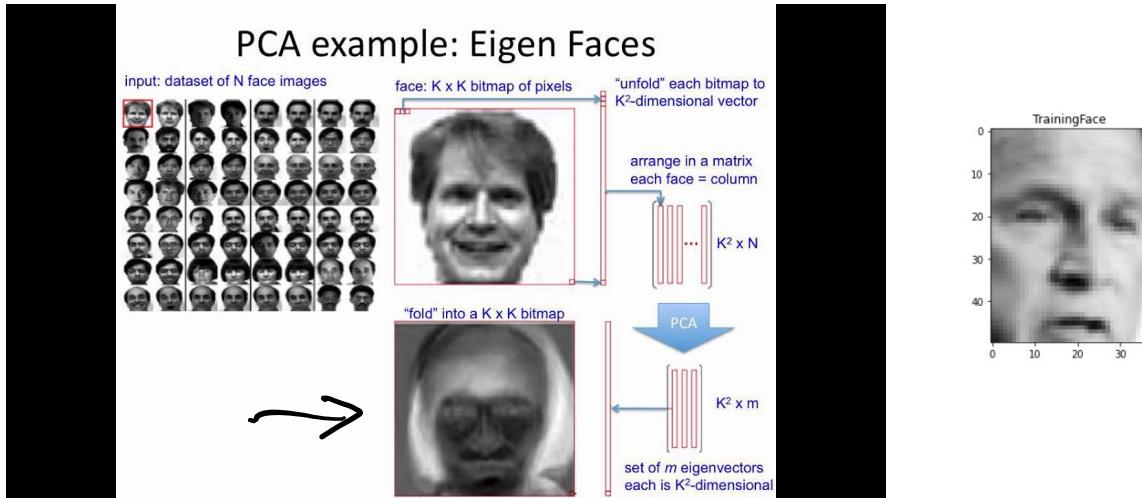
$$U_\ell ? \|U_\ell U_\ell^\top \vec{a} - \vec{a}\| \quad \text{small}$$

$$U_\ell \vec{w} = \underbrace{w_1 \vec{u}_1 + \dots + w_{12} \vec{u}_{12}}_{\vec{w} \in \mathbb{R}^{\ell=12}}$$



Applications of PCA

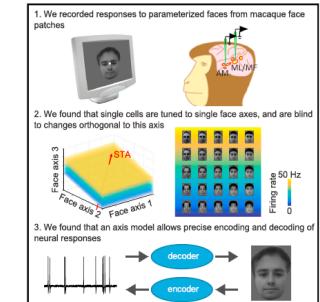
- Eigenfaces [Turk & Pentland 1991]:



Cell

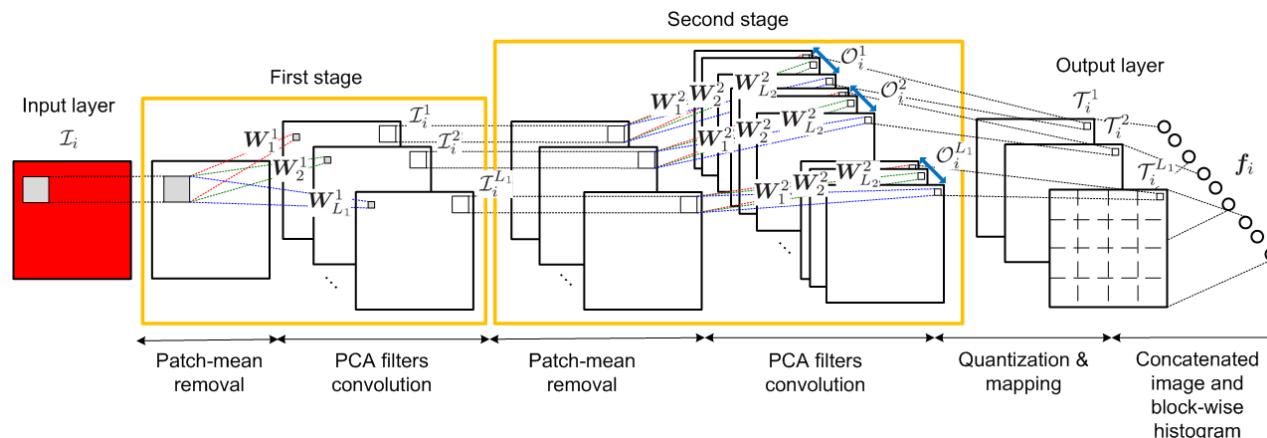
The Code for Facial Identity in the Primate Brain

Graphical Abstract



- Facial images can be linearly reconstructed using responses of ~200 face cells
- Face cells display flat tuning along dimensions orthogonal to the axis being coded
- The axis model is more efficient, robust, and flexible than the exemplar model
- Face patches ML/MF and AM carry complementary information about faces

- PCANet [Chan & Ma et. al. 2015]:



Recognition rates (%) on FERET dataset.

Probe sets	<i>F_b</i>	<i>F_c</i>	<i>Dup-I</i>	<i>Dup-II</i>	Avg.
LBP [18]	93.00	51.00	61.00	50.00	63.75
DMMA [25]	98.10	98.50	81.60	83.20	89.60
P-LBP [21]	98.00	98.00	90.00	85.00	92.75
POEM [26]	99.60	99.50	88.80	85.00	93.20
G-LQP [27]	99.90	100	93.20	91.00	96.03
LGBP-LGXP [28]	99.00	99.00	94.00	93.00	96.25
sPOEM+POD [29]	99.70	100	94.90	94.00	97.15
GOM [30]	99.90	100	95.70	93.10	97.18
PCANet-1 (Trn. CD)	99.33	99.48	88.92	84.19	92.98
PCANet-2 (Trn. CD)	99.67	99.48	95.84	94.02	97.25
PCANet-1	99.50	98.97	89.89	86.75	93.78
PCANet-2	99.58	100	95.43	94.02	97.26

Least Squares (Regression) versus PCA

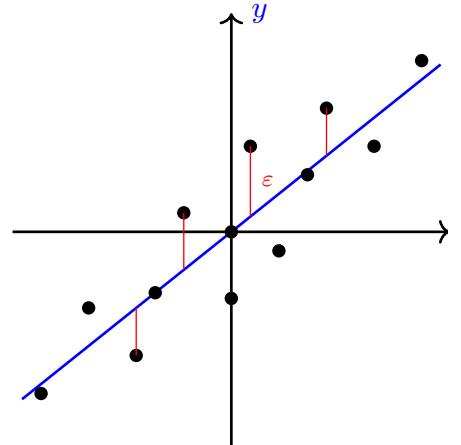
$$A = \begin{bmatrix} x_1 & x_2 & \dots & x_n \\ y_1 & y_2 & \dots & y_n \end{bmatrix} \quad \vec{x}^T \quad \vec{y}^T$$

$$y = \alpha x + \eta? \quad \leftarrow \text{regression}$$

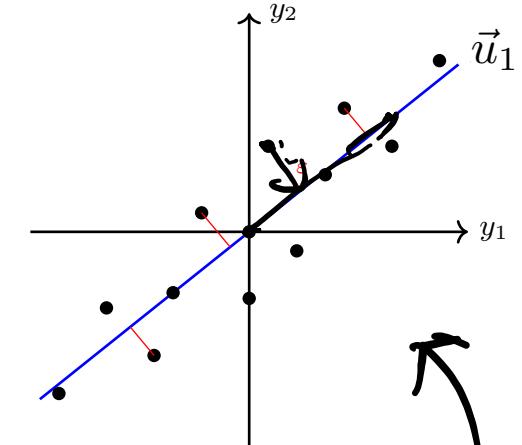
$$\| \vec{y} - \alpha \vec{x} \|_2^2$$

$$A = \begin{bmatrix} y_{11} & y_{12} & \dots & y_{1n} \\ y_{21} & y_{22} & \dots & y_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ y_{m1} & y_{m2} & \dots & y_{mn} \end{bmatrix} \rightarrow \| \vec{u}_i^T A \|_2^2 \quad \text{maximized}$$

Prediction versus Correlation



Supervised



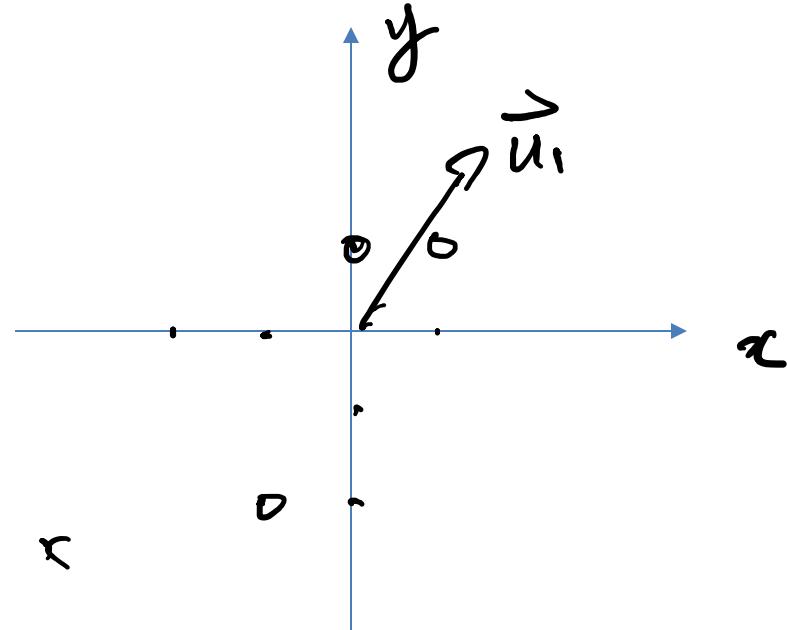
versus Unsupervised

Least Squares (Regression) versus PCA

Example: $A = \begin{bmatrix} -1 & 0 & 1 \\ -2 & 1 & 1 \end{bmatrix} = \left\{ \begin{bmatrix} \vec{x}^T \\ \vec{y}^T \end{bmatrix} \right\}$

$$\min ||\vec{y} - \alpha \vec{x}||_2^2 \rightarrow \alpha = \frac{\vec{x}^T \vec{y}}{(\vec{x}^T \vec{x})}$$
$$= \frac{\frac{3}{2}}{\frac{3}{2}} = 1.5$$
$$y = \frac{3}{2}x$$

Prediction versus Correlation

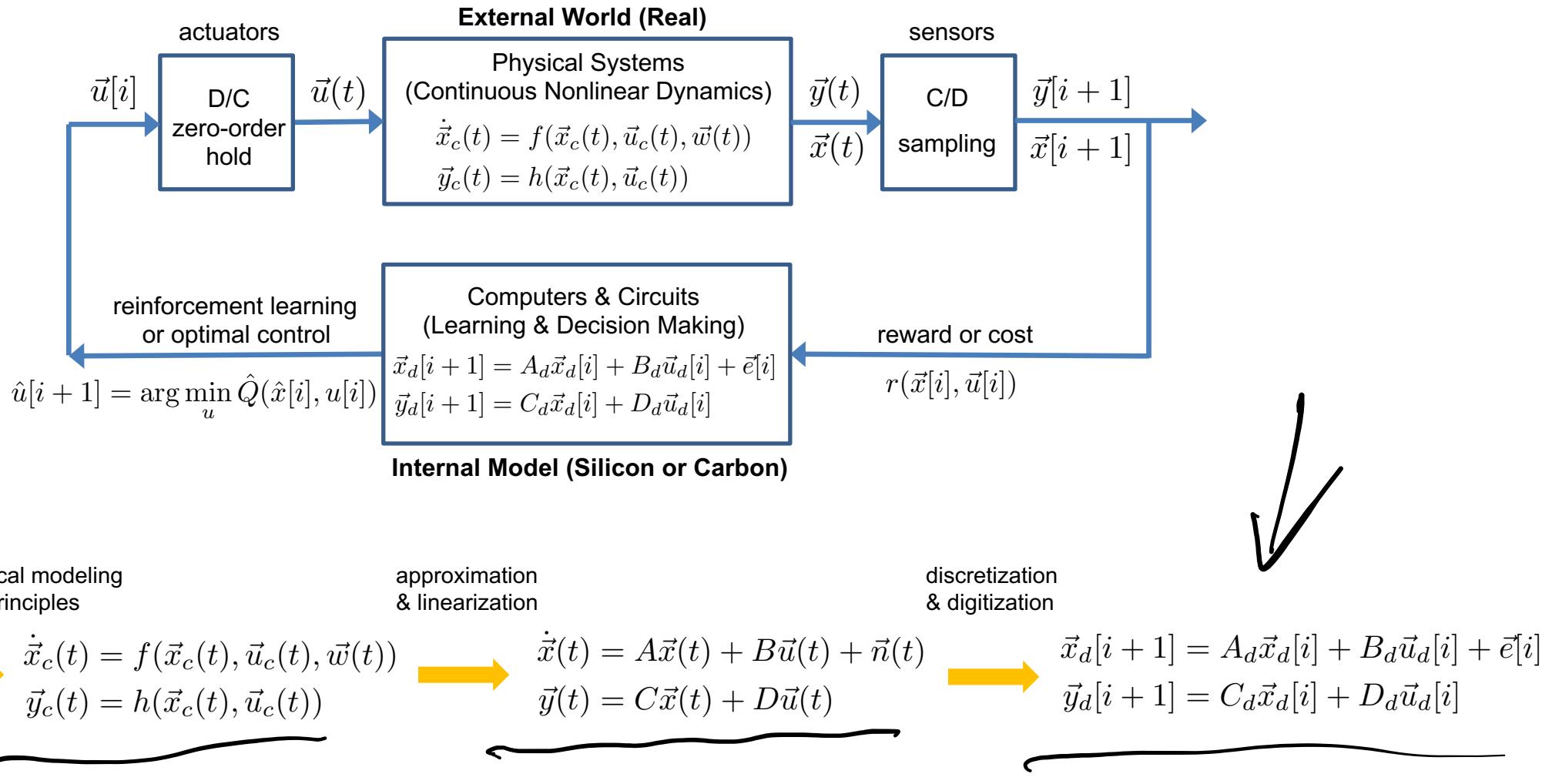


$$A A^T = \begin{bmatrix} 2 & 3 \\ 3 & 6 \end{bmatrix} \leftarrow \vec{u}_1 = \begin{bmatrix} 0.47 \\ 0.88 \end{bmatrix}$$

$$\text{slope} = \frac{0.88}{0.47} \approx 1.87.$$

System Modeling & Control

All autonomous intelligent (AI) systems rely on **closed-loop** learning and control:



Linear versus Nonlinear Systems

Objectives: Identification (learning), Analysis (stability), Control (closed-loop feedback)

Continuous Time

Linear Control Systems

$$\frac{d\vec{x}(t)}{dt} = A\vec{x}(t) + B\vec{u}(t) \leftarrow \vec{x}[i+1] = A\vec{x}[i] + B\vec{u}[i]$$

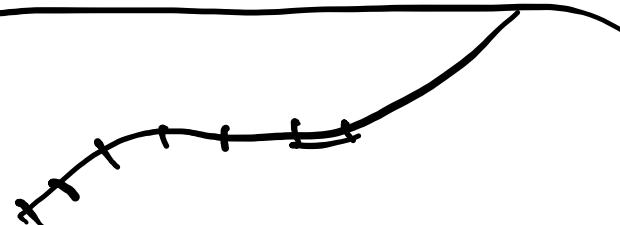


Nonlinear Control Systems

$$\frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}(t), \vec{u}(t)) \leftarrow \vec{x}[i+1] = \vec{f}(\vec{x}[i], \vec{u}[i])$$

Autonomous Systems

$$\frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}(t))$$



$$\vec{u}(t) \approx g(\vec{x}(t))$$

$$\frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}(t), g(\vec{x}(t)))$$

$$F = ma$$

Nonlinear Systems: Examples

Diagram of a simple pendulum of length l . The angle θ is measured from the vertical dashed line. Gravity mg acts vertically downwards. The forces are resolved into components along the string and perpendicular to it.

$$m\ell \frac{d^2\theta(t)}{dt^2} = -k\ell \frac{d\theta(t)}{dt} - mg \sin \theta(t)$$

$$x_1(t) = \theta(t)$$

$$x_2(t) = \frac{d\theta(t)}{dt}$$

$$\left[\begin{array}{c} \frac{dx_1(t)}{dt} \\ \frac{dx_2(t)}{dt} \end{array} \right] = \left[\begin{array}{c} x_2(t) \\ -\frac{g}{l} \sin x_1(t) - \frac{k}{m} x_2(t) \end{array} \right]$$

$$\frac{d\vec{x}(t)}{dt} = f(x_1(t), x_2(t)) \in \mathbb{R}^2$$

$$ma = F$$

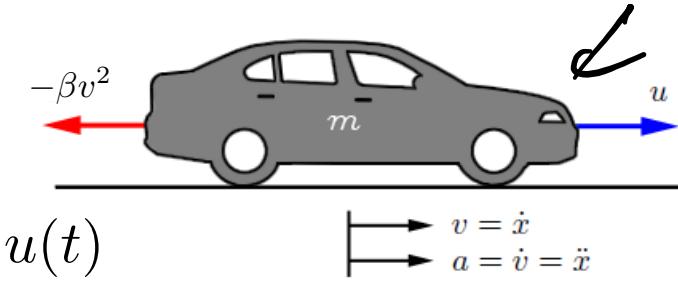
$$m \frac{v(t)}{dt} = -\beta v(t)^2 + u(t)$$

drag

$$x(t) = v(t)$$

$$\frac{dx(t)}{dt} = -\frac{\beta}{m} x(t)^2 + \frac{1}{m} u(t)$$

$$= f(x(t), u(t)) \in \mathbb{R}^1$$



Nonlinear Autonomous Systems: Equilibrium Points

$$\frac{d\vec{x}(t)}{dt} = \underline{\vec{f}(\vec{x}(t))} \in \mathbb{R}^n$$

if $\vec{f}(\vec{x}^*) = \vec{0} \in \mathbb{R}^n$, we call
 \vec{x}^* equilibrium pts.

$$\vec{x}(t) = \vec{x}^* \quad \frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}^*) = \vec{0}$$

$$\vec{x}[i+1] = \vec{f}(\vec{x}[i]) \in \mathbb{R}^n$$

$$\vec{x}[i+1] = \vec{f}(\vec{x}[i]) = \vec{x}[i]$$

an equilibrium pt. \vec{x}^* is
such that

$$\vec{f}(\vec{x}^*) = \vec{x}^*$$

fixed pt.

Nonlinear Autonomous Systems: Linearization

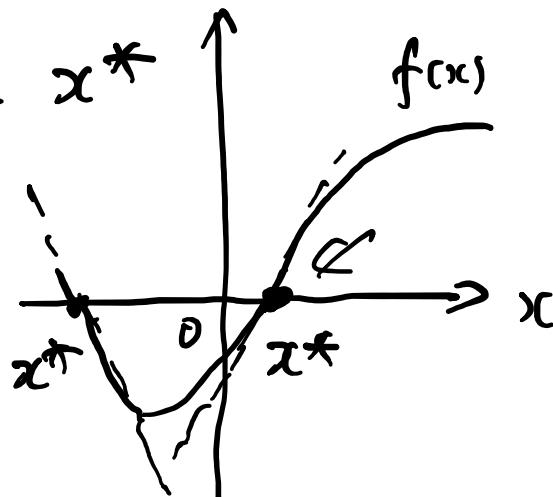
Scalar case: $\frac{dx(t)}{dt} = f(x(t))$

at an equilibrium pt. x^*

$$f(x^*) = 0$$

around one x^*

$$\textcircled{1} \quad f(x) = \underbrace{f(x^*)}_{0} + \boxed{f'(x^*)} \underbrace{(x - x^*)}_{\delta(t)} + \text{h.o.t.}$$



$$\rightarrow \delta(t) = \frac{x(t) - x^*}{\delta(t)}$$

$$\boxed{\frac{d\delta(t)}{dt}} = \frac{d(x(t) - x^*)}{dt} = \frac{dx(t)}{dt} = \boxed{f'(x^*) \delta(t)}$$

Vector case: $\frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}(t)) \in \mathbb{R}^n$

around some equilibrium point \vec{x}^* : $\vec{f}(\vec{x}^*) = 0$

$$\vec{\delta}(t) = \vec{x}(t) - \vec{x}^*$$

$$\frac{d\vec{\delta}(t)}{dt} = \vec{f}(\vec{x}(t))$$

$$= \boxed{\nabla_{\vec{x}} \vec{f} \Big|_{\vec{x}^*}} \vec{\delta}(t)$$

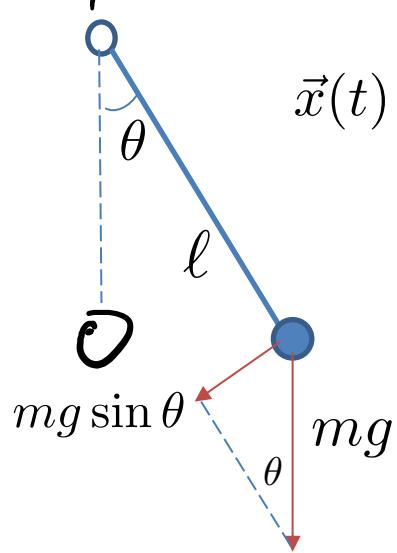
$$\frac{\partial \vec{f}}{\partial \vec{x}} \Big|_{\vec{x}^*} = \vec{\nabla}_{\vec{x}} \vec{f}(\vec{x}^*)$$

$$\vec{f}: \vec{x} \in \mathbb{R}^n \rightarrow \mathbb{R}^n \quad \begin{bmatrix} f_1(x_1, \dots, x_n) \\ \vdots \\ f_n(x_1, \dots, x_n) \end{bmatrix} = \vec{f}(\vec{x})$$

$$\frac{\partial \vec{f}}{\partial \vec{x}} \Big|_{\vec{x}^*} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1}, \dots, \frac{\partial f_1}{\partial x_n} \\ \vdots \\ \frac{\partial f_n}{\partial x_1}, \dots, \frac{\partial f_n}{\partial x_n} \end{bmatrix} \Big|_{\vec{x}^*} = \frac{\nabla_{\vec{x}} f(\vec{x}^*)}{\nabla_{\vec{x}} f(\vec{x}^*)}$$



Nonlinear Autonomous Systems: Example



$$\vec{x}(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} \theta(t) \\ \frac{d\theta(t)}{dt} \end{bmatrix} \in \mathbb{R}^2 \quad \left\{ \begin{array}{l} \frac{dx_1(t)}{dt} = x_2(t) \\ \frac{dx_2(t)}{dt} = -\frac{g}{l} \sin(x_1(t)) - \frac{k}{m} x_2(t) \end{array} \right. \quad \begin{array}{l} = f_1(x_1(t), x_2(t)) \\ = \underline{f_2(x_1(t), x_2(t))} \end{array}$$

① equilibrium pt.
 $\vec{f}(\vec{x}^*) = 0$

$$f_1(x_1, x_2) = 0 \Rightarrow x_2 = 0$$

$$f_2(x_1, x_2) = -\frac{g}{l} \sin x_1 = 0 \Rightarrow x_1 = \frac{\pi}{2}$$

\vec{x}^* $(0, 0)$ points
 $(\pi, 0)$ of interest

Nonlinear Autonomous Systems: Example

Diagram of a simple pendulum of length ℓ with mass m . The angle θ is measured from the vertical dashed line. The forces acting on the mass are the weight mg and the tension $mg \cos \theta$.

$$\vec{x}(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} \theta(t) \\ \frac{d\theta(t)}{dt} \end{bmatrix}$$

$$\vec{\delta}(t) = \vec{x}(t) - \vec{x}^*$$

$$\frac{d\vec{\delta}(t)}{dt} = \frac{d\vec{x}(t)}{dt} = \underbrace{\vec{f}(\vec{x}(t))}_{\vec{f}(\vec{x}^*) + J_{\vec{x}} \vec{f}'(\vec{x}) \Big|_{\vec{x}^*}} = \underbrace{\vec{f}(\vec{x}^*)}_{\text{constant}} + J_{\vec{x}} \vec{f}'(\vec{x}) \Big|_{\vec{x}^*} \vec{\delta}(t)$$

$$J_{\vec{x}} \vec{f}'(\vec{x}) \Big|_{(x_1^*, x_2^*)} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(x_1^*, x_2^*) & \frac{\partial f_1}{\partial x_2}(x_1^*, x_2^*) \\ \frac{\partial f_2}{\partial x_1}(x_1^*, x_2^*) & \frac{\partial f_2}{\partial x_2}(x_1^*, x_2^*) \end{bmatrix} \in \mathbb{R}^{2 \times 2}$$

① $\vec{x}^* = (0, 0)$, $J_{\vec{x}} \vec{f}' \Big|_{\vec{x}^*} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{\ell} \cdot 1 & \frac{k}{m} \end{bmatrix} A_1$

② $\vec{x}^* = (\pi, 0)$, $J_{\vec{x}} \vec{f}' \Big|_{\vec{x}^*} = \begin{bmatrix} 0 & 1 \\ +\frac{g}{\ell} \cdot 1 & -\frac{k}{m} \end{bmatrix} A_2$

$$\checkmark A_1? \quad \text{tr}(A_1) < 0 \quad \det(A_1) = \frac{g}{e} > 0 \quad (\lambda - d_1)(\lambda - d_2) \\ = \lambda^2 - \underline{(\lambda_1 + \lambda_2)}\lambda + \underline{\lambda_1 \lambda_2}$$

$$A_2? \quad \text{tr}(A_2) < 0, \quad \det(A_2) = \frac{-g}{e} < 0 \quad \lambda I - A = \underbrace{\begin{bmatrix} \lambda - a_{11} & -a_{12} \\ -a_{21} & \lambda - a_{22} \end{bmatrix}}$$

$$\det(\lambda I - A) =$$

$$= \lambda^2 - \boxed{(\lambda_{11} + \lambda_{22})}\lambda + \frac{(a_{11}a_{22} - a_{12}a_{21})}{\det(A)}$$

$$\text{tr}(A)$$

$$< 0$$

$$\frac{\det(A)}{> 0}$$

Nonlinear Control Systems: Operating Points

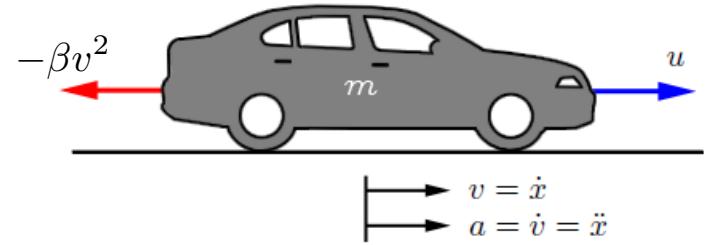
$$\frac{d\vec{x}(t)}{dt} = \vec{f}(\vec{x}(t), \vec{u}(t)) \in \mathbb{R}^n$$

$$\vec{x}[i + 1] = \vec{f}(\vec{x}[i], \vec{u}[i]) \in \mathbb{R}^n$$

Nonlinear Control Systems: Linearization

Scalar case: $\frac{dx(t)}{dt} = f(x(t), u(t))$

Nonlinear Control Systems: Example



$$\frac{dx(t)}{dt} = -\frac{\beta}{m}x(t)^2 + \frac{1}{m}u(t) = f(x(t), u(t))$$

$$m \frac{v(t)}{dt} = -\beta v(t)^2 + u(t)$$