
EECS 16B
Spring 2022
Lecture 25
4/19/2022

LECTURE 25 - Linearization continued

Given nonlinear system $\frac{d}{dt}\vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t))$, where

$$x(t) \in \mathbb{R}^n, u(t) \in \mathbb{R}^m, \vec{f}(\vec{x}, \vec{u}) = \begin{bmatrix} f_1(x_1, \dots, x_n, u_1, \dots, u_m) \\ \vdots \\ f_n(x_1, \dots, x_n, u_1, \dots, u_m) \end{bmatrix}, \vec{f}(\vec{x}^*, \vec{u}^*) = 0.$$

Linearized model at operating point (\vec{x}^*, \vec{u}^*) is :

$$\boxed{\frac{d}{dt} \delta \vec{x}(t) = A \delta \vec{x}(t) + B \delta \vec{u}(t)}$$

where, $\delta \vec{x}(t) = \vec{x}(t) - \vec{x}^*$, $\delta \vec{u}(t) = \vec{u}(t) - \vec{u}^*$,

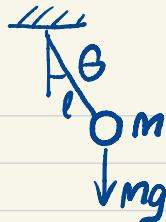
$$A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) & \dots & \frac{\partial f_1}{\partial x_n}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \\ \vdots & & \vdots \\ \frac{\partial f_n}{\partial x_1}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) & \dots & \frac{\partial f_n}{\partial x_n}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \end{bmatrix},$$

$$B = \begin{bmatrix} \frac{\partial f_1}{\partial u_1}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) & \dots & \frac{\partial f_1}{\partial u_m}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \\ \vdots & & \vdots \\ \frac{\partial f_n}{\partial u_1}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) & \dots & \frac{\partial f_n}{\partial u_m}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \end{bmatrix}.$$

(i, j) entry of A and B given by :

$$\left\{ \begin{array}{l} A(i, j) = \frac{\partial f_i}{\partial x_j}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \\ B(i, j) = \frac{\partial f_i}{\partial u_j}(x_1^*, \dots, x_n^*, u_1^*, \dots, u_m^*) \end{array} \right.$$

Example 1:



$$x_1(t) := \theta(t)$$

$$x_2(t) := \frac{d\theta}{dt}(t)$$

$$\frac{d}{dt} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} x_2(t) \\ -\frac{k}{m}x_2(t) - \frac{g}{l}\sin(x_1(t)) \end{bmatrix}$$

$$f_1(x_1, x_2) = x_2$$

$$f_1(x_1(t), x_2(t))$$

$$f_2(x_1, x_2) = -\frac{k}{m}x_2 - \frac{g}{l}\sin x_1$$

$$f_2(x_1(t), x_2(t))$$

Downward pointing equilibrium: $(x_1, x_2) = (0, 0)$

Upward " " " $(x_1, x_2) = (\pi, 0)$

$$\vec{J}_{\vec{x}} \vec{f}(\vec{x}) = \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(x_1, x_2) & \frac{\partial f_1}{\partial x_2}(x_1, x_2) \\ \frac{\partial f_2}{\partial x_1}(x_1, x_2) & \frac{\partial f_2}{\partial x_2}(x_1, x_2) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{l}\cos x_1 & -\frac{k}{m} \end{bmatrix}$$

$$A = \vec{J}_{\vec{x}} \vec{f}(\vec{x}^*) \quad A_{\text{down}} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{l} & \frac{k}{m} \end{bmatrix} = \vec{J}_{\vec{x}} \vec{f}(0, 0)$$

$$A_{\text{up}} = \begin{bmatrix} 0 & 1 \\ \frac{g}{l} & -\frac{k}{m} \end{bmatrix} = \vec{J}_{\vec{x}} \vec{f}(\pi, 0)$$

Stability Criteria (continuous-time) for $A \in \mathbb{R}^{2 \times 2}$:

$$A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \quad \lambda I - A = \begin{bmatrix} \lambda - a_{11} & -a_{12} \\ -a_{21} & \lambda - a_{22} \end{bmatrix}$$

$$\det(\lambda I - A) = (\lambda - a_{11})(\lambda - a_{22}) - a_{12}a_{21} = \underbrace{\lambda^2 - (a_{11} + a_{22})\lambda}_{-\text{tr}(A)} + \underbrace{(a_{11}a_{22} - a_{12}a_{21})}_{\det(A)}$$

Recall trace of A : $\text{tr}(A) = a_{11} + a_{12}$

$-\text{tr}(A)$ $\det(A)$

$$\lambda_1 = \frac{\text{tr}(A) - \sqrt{\text{tr}(A)^2 - 4\det(A)}}{2} \quad \lambda_2 = \frac{\text{tr}(A) + \sqrt{\text{tr}(A)^2 - 4\det(A)}}{2}$$

(i) $\det(A) \leq 0 \Rightarrow \text{unstable}$

because $\sqrt{\text{tr}(A)^2 - 4\det(A)} \geq \sqrt{\text{tr}(A)^2} = |\text{tr}(A)|$

therefore $\lambda_2 \geq \frac{\text{tr}(A) + |\text{tr}(A)|}{2} \geq 0$

(ii) $\text{tr}(A) \geq 0 \Rightarrow \text{unstable}$

- If $\text{tr}(A)^2 - 4\det(A) < 0$ then $\sqrt{\text{tr}(A)^2 - 4\det(A)}$ imaginary and $\text{Re}(\lambda_1) = \text{Re}(\lambda_2) = \frac{\text{tr}(A)}{2} \geq 0$.
- If $\text{tr}(A)^2 - 4\det(A) \geq 0$ then $\sqrt{\text{tr}(A)^2 - 4\det(A)} \geq 0$ and $\lambda_2 > \frac{\text{tr}(A)}{2} \geq 0$.

(iii) $\det(A) > 0$ and $\text{tr}(A) < 0 \Rightarrow \text{stable}$

- If $\text{tr}(A)^2 - 4\det(A) < 0$ then $\sqrt{\text{tr}(A)^2 - 4\det(A)}$ imaginary and $\text{Re}(\lambda_1) = \text{Re}(\lambda_2) = \frac{\text{tr}(A)}{2} < 0$.
- If $\text{tr}(A)^2 - 4\det(A) \geq 0$, then $\sqrt{\text{tr}(A)^2 - 4\det(A)} \in [0, |\text{tr}(A)|]$ where the upper bound follows from $\det(A) > 0$. Thus, $\lambda_1 = \frac{\text{tr}(A) - \sqrt{\cdot}}{2} \leq \frac{\text{tr}(A)}{2} < 0$, $\lambda_2 = \frac{\text{tr}(A) + \sqrt{\cdot}}{2} < \frac{\text{tr}(A) + |\text{tr}(A)|}{2} \leq 0$.

Combining (i)-(iii): stable if and only if $\det(A) > 0$ and $\text{tr}(A) < 0$.

$$A_{\text{down}} = \begin{bmatrix} 0 & \frac{1}{L} \\ -\frac{g}{L} & -\frac{k}{m} \end{bmatrix}$$

$$\text{tr}(A_{\text{down}}) = -\frac{k}{m} < 0 \quad \checkmark$$

$$\det(A_{\text{down}}) = \frac{g}{L} > 0 \quad \checkmark$$

stable

$$A_{\text{up}} = \begin{bmatrix} 0 & \frac{1}{L} \\ \frac{g}{L} & -\frac{k}{m} \end{bmatrix}$$

$$\text{tr}(A_{\text{up}}) = -\frac{k}{m} < 0 \quad \checkmark$$

$$\det(A_{\text{up}}) = -\frac{g}{L} < 0 \quad \times$$

unstable

Look at evals of A_{up} for more insight:

$$\det(\lambda I - A_{up}) = \det\begin{pmatrix} \lambda & -1 \\ -\frac{g}{l} & \lambda + \frac{k}{m} \end{pmatrix} = \lambda^2 + \frac{k}{m}\lambda - \frac{g}{l}$$

$$\lambda_{1,2} = \frac{-\frac{k}{m} \mp \sqrt{\left(\frac{k}{m}\right)^2 + 4\frac{g}{l}}}{2}$$

$$\lambda_2 = \frac{-\frac{k}{m} + \sqrt{\left(\frac{k}{m}\right)^2 + 4\frac{g}{l}}}{2} > 0 \text{ since } \sqrt{\left(\frac{k}{m}\right)^2 + 4\frac{g}{l}} > \left(\frac{k}{m}\right)^2 = \frac{k}{m}$$

Note: λ_2 becomes more positive (therefore instability more severe) when l is smaller. Try balancing a shorter stick in your hand!

Linearization in Discrete Time :

$$\vec{x}[i+1] = \vec{f}(\vec{x}[i], \vec{u}[i]) \quad (1)$$

$$\vec{x}^* = \vec{f}(\vec{x}^*, \vec{u}^*)$$

$$\vec{f}(\vec{x}, \vec{u}) \approx \underbrace{\vec{f}(\vec{x}^*, \vec{u}^*)}_{\vec{x}^*} + A\underbrace{(\vec{x} - \vec{x}^*)}_{\delta \vec{x}} + B\underbrace{(\vec{u} - \vec{u}^*)}_{\delta \vec{u}} \quad (2)$$

where A and B are obtained as in page 1.

Linearization: replace \vec{f} in (1) with approximation in (2):

$$\vec{x}[i+1] = \vec{x}^* + A \delta \vec{x}[i] + B \delta \vec{u}[i]$$

$$\underbrace{\vec{x}[i+1] - \vec{x}^*}_{= \delta \vec{x}[i+1]} = A \delta \vec{x}[i] + B \delta \vec{u}[i]$$

Example 2: Population growth model

$$x[i+1] = r x[i]$$

$\underbrace{}$
population of a species in
generation i

Assume $r > 1 \Rightarrow$ exponential, unbounded growth.

Unrealistic because resources run out when x gets large.

A more realistic model where cst. r is replaced with x -dependent growth rate $r(1 - \frac{x}{N})$:

$$x[i+1] = r \left(1 - \frac{x[i]}{N}\right) x[i] \quad \text{nonlinear}$$

$\underbrace{}_{f(x[i])}$

$$f(x) = r \left(1 - \frac{x}{N}\right)x = rx - \frac{r}{N}x^2, \quad f'(x) = r - \frac{2r}{N}x \quad (3)$$

Equilibrium (discrete time): $x = f(x)$

$$x = r \left(1 - \frac{x}{N}\right)x$$

$$x \left(1 - r + \frac{r}{N}x\right) = 0$$

Two roots: $x=0$ (extinct) $x = \frac{N}{r} (r-1) > 0$
since $r > 1$

Linearized model:

i) around $x^* = 0$: $\delta x[i+1] = \underbrace{f'(0)}_{=r \text{ from (3)}} \delta x[i]$

$r > 1 \Rightarrow$ unstable

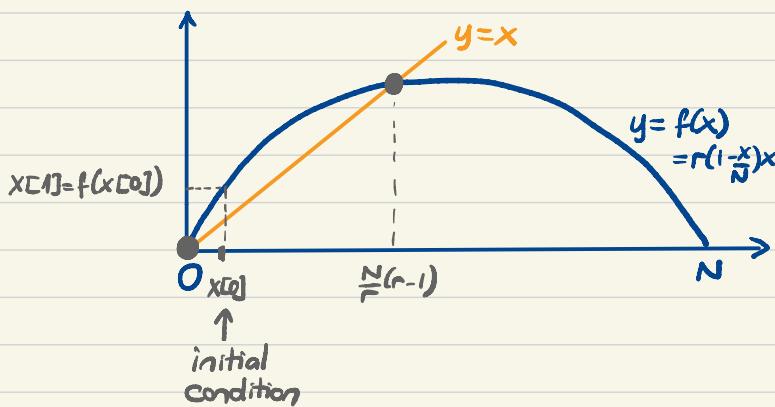
(ii) around $x^* = \frac{N}{r}(r-1)$:

$$f'(\frac{N}{r}(r-1)) = r - \frac{2r}{N} \left(\frac{N}{r}(r-1) \right) = r - 2r + 2 = 2 - r$$

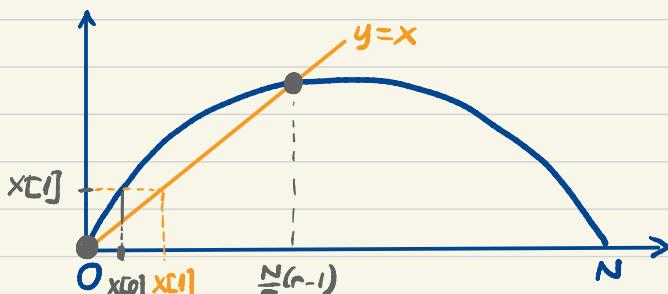
$$\delta x[i-1] = \underbrace{(2-r)}_{\in (-1, 1) \text{ for stability}} \delta x[i]$$

i.e., $r \in (1, 3)$

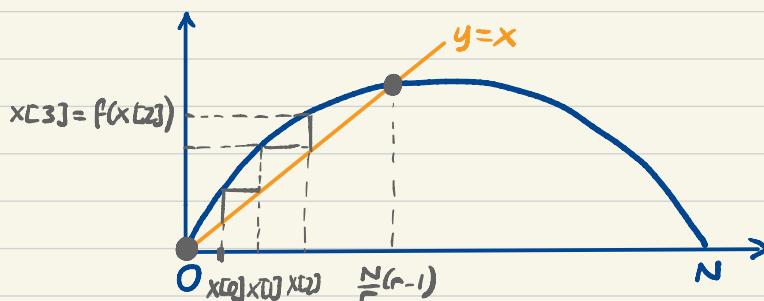
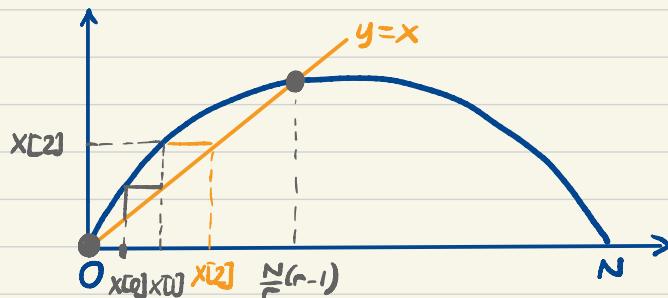
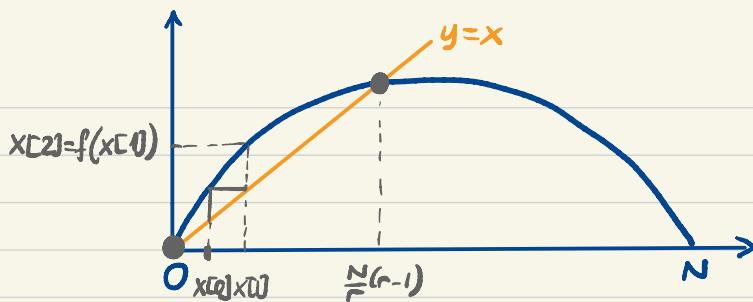
"Cobweb diagrams": graphical method to visualize how solutions of scalar discrete-time equations evolve (beyond scope for this course but kinda fun):



intersections of $y=f(x)$ and $y=x$ are equilibrium points b/c $f(x)=x$ at those points

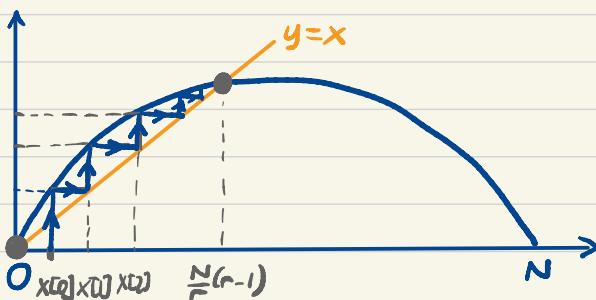


used $y=x$ axis to bring value $x[1]$ from vertical to horizontal axis



Continuing in this manner, you can see that the solution from $x[0]$ evolves as shown below, indicating convergence to

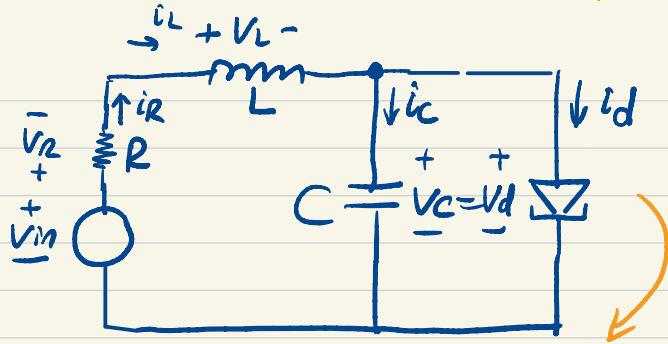
$$x^* = \frac{N(r-1)}{r}.$$



Examples above didn't have inputs. Ex. 3 below has V_{in} as input.

Example 3:

tunnel diode circuit



KCL:

$$(3) \quad i_R = i_L = i_C + i_d$$

KVL:

$$(4) \quad V_{in} = V_R + V_L + V_C$$

$$(5) \quad V_d = V_C$$



tunnel diode voltage-current characteristic

$$\vec{X} = \begin{bmatrix} V_C \\ i_L \end{bmatrix}$$

$$C \frac{dV_C}{dt} = i_C(t) \stackrel{(3)}{=} i_L(t) - i_d(t) = i_L(t) - g(V_d(t)) \stackrel{(5)}{=} i_L(t) - g(V_C(t))$$

$$L \frac{di_L}{dt} = V_L(t) \stackrel{(4)}{=} V_{in}(t) - V_R(t) - V_C(t)$$

$$= V_{in}(t) - R i_R(t) - V_C(t)$$

$$\stackrel{(3)}{=} V_{in}(t) - R i_L(t) - V_C(t)$$

Variables in orange above are neither state nor input variables. We use the substitutions indicated above each equation to make sure the right hand side depends only on $\vec{X} = \begin{bmatrix} V_C \\ i_L \end{bmatrix}$ and $u = V_{in}$, so we get a model of the form

$$\frac{d}{dt} \vec{X}(t) = \vec{f}(\vec{X}(t), u(t)).$$

$$\frac{d}{dt} V_C(t) = \frac{1}{C} i_L(t) - \frac{1}{C} g(V_C(t))$$

$$\frac{d}{dt} i_L(t) = \frac{1}{L} V_{in}(t) - \frac{R}{L} i_L(t) - \frac{1}{L} V_C(t)$$

Can't write in matrix/vector form because of nonlinearity $g(\cdot)$.