

## 1 Airplane Discretization

In this question we will explore briefly a simplified linear model of an airplane control model. First let's define the variables we will be working with, in reference with figure 1:

- (i)  $\alpha$  = Angle of Attack (angle the plane makes with the direction of wind)
- (ii)  $\theta$  = Pitch Angle (angle of the plane with respect to the horizontal)
- (iii)  $u$  = Elevator angle (used to control the aircraft's pitch)

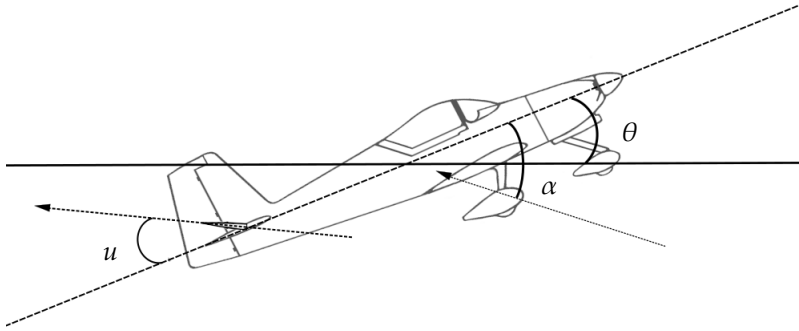


Figure 1: Simplified Airplane model

Now, consider the following (simplified) continuous time system:

$$\frac{d}{dt}\alpha = 5\alpha - \frac{d}{dt}\theta + c_1\delta \quad (1)$$

$$\frac{d^2}{dt^2}\theta = -\alpha + \frac{d}{dt}\theta + c_2\delta \quad (2)$$

- a) For the system of differential equations given, **write the matrix differential equation as**

$$\frac{d}{dt}\vec{x} = A\vec{x} + B\delta$$

- b) Now, assume for some specific component values we get the following differential equation:

$$\frac{d}{dt}\vec{x}(t) = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \vec{x}(t) + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u(t). \quad (3)$$

Unfortunately, we are unable to measure our state vector continuously. Suppose that we sample the system with some sampling interval  $T$ . Let us discretize the above system. Assume that we use piecewise constant voltage inputs  $u(t) = u[k]$  for  $t \in [kT, (k+1)T)$ .

Calculate a discrete-time system for Equation (3)'s continuous-time vector system in the form:

$$\vec{x}[k+1] = A_d\vec{x}[k] + \vec{b}_d[k].$$

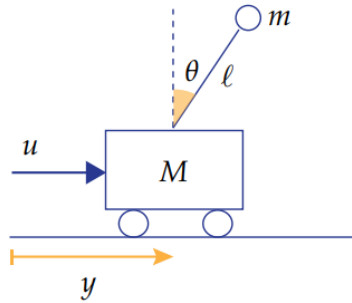
## 2 Inverted Pendulum on a Rolling Cart

Recall the inverted pendulum depicted below from Homework 6 problem 1, which is placed on a rolling cart and whose equations of motion are given by:

$$\ddot{y} = \frac{1}{\frac{M}{m} + \sin^2 \theta} \left( \frac{u}{m} + \dot{\theta}^2 \ell \sin \theta - g \sin \theta \cos \theta \right)$$

$$\ddot{\theta} = \frac{1}{\ell \left( \frac{M}{m} + \sin^2 \theta \right)} \left( -\frac{u}{m} \cos \theta - \dot{\theta}^2 \ell \cos \theta \sin \theta + \frac{M+m}{m} g \sin \theta \right).$$

where we use  $\dot{x}$  to denote the time derivative of  $x$ ; that is,  $\dot{y} = \frac{dy}{dt}$ ,  $\dot{\theta} = \frac{d\theta}{dt}$ ,  $\ddot{y} = \frac{d^2y}{dt^2}$  and  $\ddot{\theta} = \frac{d^2\theta}{dt^2}$ .



- a) Recall the result of our linearized model from Homework 6, problem 1c:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \approx \underbrace{\begin{bmatrix} 0 & 1 & 0 \\ \frac{M+m}{lM}g & 0 & 0 \\ -\frac{m}{M}g & 0 & 0 \end{bmatrix}}_A \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ -\frac{1}{lM} \\ \frac{1}{M} \end{bmatrix}}_B u.$$

Show that the linearized model is controllable.

- b) Suppose  $M = 1$ ,  $m = 0.1$ ,  $l = 1$ , and  $g = 10$ , and design a state feedback controller,

$$u(t) = -k_1 \theta(t) - k_2 \dot{\theta}(t) - k_3 \dot{y}(t),$$

such that the eigenvalues of  $A - BK$  (the “closed-loop eigenvalues”) are  $\lambda_1 = \lambda_2 = \lambda_3 = -1$ .

- c) Suppose we set  $k_2 = k_3 = 0$  and vary only  $k_1$ ; that is, the controller uses only  $\theta(t)$  for feedback. Does there exist a  $k_1$  value such that all closed-loop eigenvalues have negative real parts?

### 3 Minimum Norm Control

Suppose we had a linear discrete-time system with the following dynamics

$$\vec{x}[t+1] = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t) \quad (4)$$

Given the initial state  $\vec{x}[0] = \vec{0}$ , we would like to reach a target state  $\vec{x}_t = \begin{bmatrix} 5 \\ 0 \end{bmatrix}$ .

- a) Show that we can reach the state  $\vec{x}_t$  in a finite number of time-steps
- b) What sequence of control inputs can we give to reach the state  $\vec{x}_t$  in two time-steps?
- c) While we can theoretically reach  $\vec{x}_t$  in two time-steps, we notice that it is too expensive to move our system this quickly. Set up an optimization problem of the form below to reach  $\vec{x}_t$  in five time-steps with minimum energy.

$$\min_{\vec{w} \in \mathbb{R}^5} \|\vec{w}\|^2 \quad \text{subject to } H\vec{w} = \vec{y} \quad (5)$$

- d) What is the solution to the optimization problem from the previous part? Give the optimal solution  $\vec{w}^*$ .
- e) Try solving the minimum norm problem for 2 steps all the way up to 10 steps and compare the norms of each solution.