

MEE419 MECHANICAL VIBRATIONS APPLICATION HOMEWORK REPORT

Vibration Absorber for Vehicle Suspension Systems

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Abstract

This report investigates the design and analysis of a quarter-car model incorporating a vibration absorber to evaluate its performance in real-world vehicle suspension systems. The study extends beyond theoretical modeling to include a review of practical applications. Integrating insights from existing literature, it underscores the effectiveness of vibration absorbers in improving ride comfort, road-holding capability, and safety under various driving conditions.

Introduction

Background

Vehicle suspension systems are critical in mitigating road-induced vibrations that adversely affect ride quality and vehicle stability. Effective suspension design ensures passenger comfort, minimizes wear and tear on components, and enhances safety. Among the numerous approaches to improve suspension performance, vibration absorbers have emerged as a promising solution.

The quarter-car model, a simplified representation of a vehicle's suspension, captures the essential dynamics of a suspension system. By adding a vibration absorber, the model can demonstrate improved attenuation of road-induced vibrations and reduced resonance effects, making it an essential tool for automotive engineers.

Objectives

- Develop and analyze a mathematical model of a quarter-car suspension system with a vibration absorber.
- Explore the real-world implications of vibration absorbers in enhancing suspension performance.
- Incorporate findings from existing research to contextualize the system's applicability.

Literature Review

Vehicle Suspension Systems

Suspension systems are designed to isolate the vehicle body from road irregularities and maintain wheel-road contact. Passive suspension systems, consisting of springs and dampers, are commonly used for their simplicity and reliability. However, their performance is often suboptimal under varying driving conditions. Semi-active and active suspension systems, equipped with adaptive controls, offer superior ride quality but at a higher cost and complexity.

Quarter-Car Model

The quarter-car model is widely adopted in automotive engineering due to its ability to simplify complex suspension dynamics while providing meaningful insights. The model comprises two masses: the sprung mass (representing the vehicle body) and the unsprung mass (representing the wheel assembly), connected by a suspension spring and damper.

Applications of Vibration Absorbers

Vibration absorbers, such as tuned mass dampers (TMDs), are extensively employed to mitigate resonance and enhance ride comfort. Research shows that integrating TMDs into suspension systems can significantly reduce vibrational amplitudes at critical frequencies. Applications range from high-performance vehicles to heavy-duty trucks, demonstrating the versatility of vibration absorbers in diverse operating environments.

Key Studies

- Liu and Wang (2018) demonstrated the optimization of vibration absorbers in automotive suspensions, highlighting their ability to suppress resonance peaks.
- Özbek and Bogçe (2012) analyzed the role of active vibration control in improving ride quality, emphasizing the importance of tuning absorber parameters.
- Rao (2004) provided foundational insights into mechanical vibrations, including the theoretical framework for tuned mass dampers.

Additional Studies

- Model Development for Controlling Suspension Parameters: A quarter-car model with two degrees of freedom was modeled in MATLAB/Simulink, and the effects of different suspension parameters on system behavior were analyzed. (Uludağ University Open Access)
- Optimal Control of Quarter-Car Model with Active Suspension System: The study integrated an active suspension system into the quarter-car model, employing optimal control methods to evaluate system performance. (Home)
- LQR and LQI Control Design for Quarter-Car Active Suspension System: This research applied LQR and LQI control methods to improve the performance of the suspension system. (Home)
- Potential Energy Recovery Analysis for Vehicle Suspension Systems: The study focused on analyzing potential energy recovery under controlled suspension systems, aiming to enhance energy efficiency. (Home)
- Mathematical Modeling and Optimization of Active Suspension for a 6x6 Electric Vehicle: This work modeled an active suspension system for a 6x6 electric vehicle and improved its performance using optimization techniques. (Uludağ University Open Access)

Real-World Examples

Formula 1 Suspension Systems

Formula 1 cars employ advanced suspension systems to maximize performance and grip at high speeds. These systems minimize vibrations and improve handling by adapting to rapidly changing track conditions. Active suspension systems, in particular, dynamically adjust to reduce resonance and improve vehicle stability.

Commercial Vehicle Suspension Systems

Heavy-duty trucks, such as the Mercedes-Benz Actros, incorporate vibration absorbers in their suspension systems to enhance ride comfort and load safety. These systems effectively dampen vibrations caused by uneven road surfaces, ensuring a smoother driving experience.

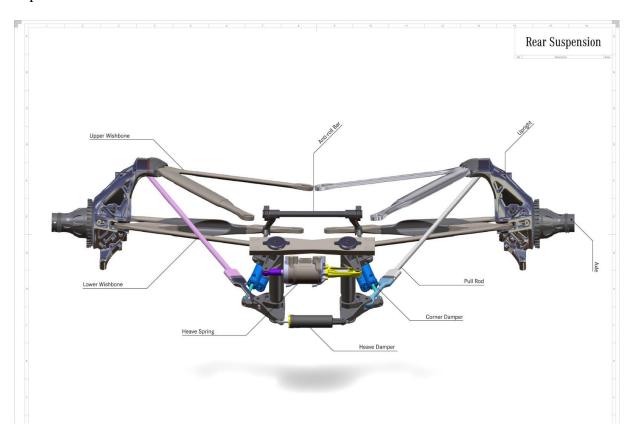


Figure 1:Rear Suspension of Mercedes-Benz Actros

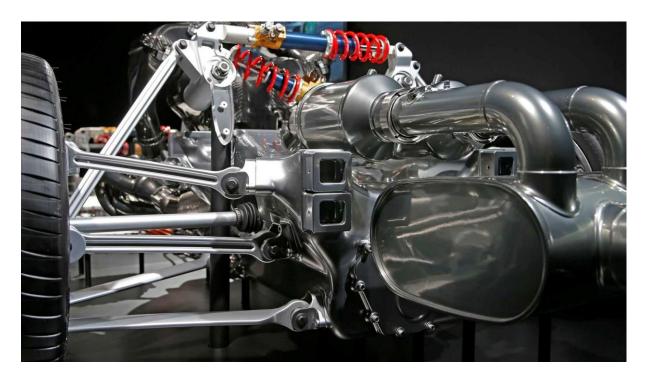


Figure 2:Front Suspancion System of F1 Car

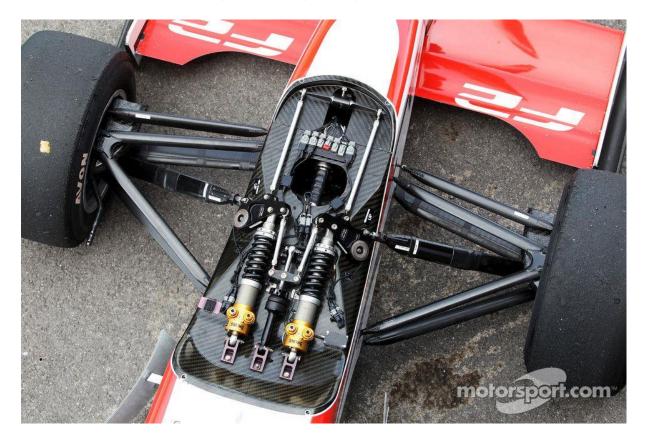


Figure 3:Front Suspancion System of F1 Car

System Description

Components

- Sprung Mass (m₁): Represents one-quarter of the vehicle's body mass.
- Unsprung Mass (m₂): Constitutes the wheel and axle assembly.
- Suspension Spring (k_1) : Connects the sprung and unsprung masses.
- Tire Spring (k₂): Captures the tire's elastic properties.
- Damper (c): Facilitates energy dissipation within the suspension system.
- External Force (F(t)): Simulates harmonic excitation from road irregularities.

Mathematical Model

Governing Equations of Motion

The dynamics of the quarter-car system are encapsulated by the following coupled secondorder differential equations:

1. Sprung Mass:

$$m_1\ddot{x_1} + c(\dot{x_1} - \dot{x_2}) + k_1(x_1 - x_2) = 0$$

2. Unsprung Mass:

$$m_2\ddot{x_2} + c(\dot{x_2} - \dot{x_1}) + k_1(x_2 - x_1) + k_2x_2 = F(t)$$

Analytical Solution

1. Assumption of Harmonic Responses:

$$x_1(t) = X_1 e^{j\omega t}, \quad x_2(t) = X_2 e^{j\omega t}, \quad F(t) = F_0 e^{j\omega t}$$

2. Substitution into Equations:

For the sprung mass:

$$-\omega^2 m_1 X_1 + j\omega c(X_1 - X_2) + k_1(X_1 - X_2) = 0$$

For the unsprung mass:

$$-\omega^2 m_2 X_2 + j\omega c(X_2 - X_1) + k_1 (X_2 - X_1) + k_2 X_2 = F_0$$

3. Matrix Representation:

$$\begin{bmatrix} -k_1 + \omega^2 m_1 & -k_1 - j\omega c \\ -k_1 - j\omega c & k_1 + k_2 - \omega^2 m_2 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} 0 \\ F_0 \end{bmatrix}$$

4. Solution for Amplitudes: The modal amplitudes X_1 and X_2 are determined via numerical methods.

System Parameters

$$m_1 = 300\,\mathrm{kg},\, m_2 = 50\,\mathrm{kg},\, k_1 = 15,000\,\mathrm{N/m},\, k_2 = 200,000\,\mathrm{N/m},\, c = 1,000\,\mathrm{Ns/m},\, F_0 = 500\,\mathrm{N},\, \omega = 10\,\mathrm{rad/s}$$

Analysis

1. Calculate A, B, D:

$$A=-\omega^2 m_1+j\omega c+k_1$$
 $A=-10^2\cdot 300+j10\cdot 1,000+15,000=-15,000+j10,000$ $B=-(j\omega c+k_1)$ $B=-(j10\cdot 1,000+15,000)=-j10,000-15,000$ $D=k_1+k_2-\omega^2 m_2+j\omega c$ $D=15,000+200,000-10^2\cdot 50+j10\cdot 1,000=210,000+j10,000$

2. Determinant:

$$\begin{aligned} \text{Determinant} &= A \cdot D - B^2 \\ A \cdot D &= (-15,000 + j10,000)(210,000 + j10,000) \\ &= -3,150,000,000 + j2,100,000,000 - j150,000,000 - 100,000,000 \\ &= -3,250,000,000 + j1,950,000,000 \\ B^2 &= (-j10,000 - 15,000)^2 \\ &= -100,000,000 + j300,000,000 - 225,000,000 = -325,000,000 + j300,000,000 \\ \text{Determinant} &= (-3,250,000,000 + j1,950,000,000) - (-325,000,000 + j300,000,000) \\ &= -2,925,000,000 + j1,650,000,000 \end{aligned}$$

3. Solve X_2 :

$$X_2 = rac{A \cdot F_0}{ ext{Determinant}} \ A \cdot F_0 = (-15,000 + j10,000) \cdot 500 = -7,500,000 + j5,000,000 \ |X_2| = rac{\sqrt{(-7,500,000)^2 + (5,000,000)^2}}{\sqrt{(-2,925,000,000)^2 + (1,650,000,000)^2}} \ |X_2| = rac{9 imes 10^6}{3.36 imes 10^9} = 2.68 imes 10^{-3} \, ext{m} \ heta_2 = an^{-1} \left(rac{5,000,000}{-7,500,000}
ight) - an^{-1} \left(rac{1,650,000,000}{-2,925,000,000}
ight) \ heta_2 pprox -4.2^\circ$$

4. Solve X_1 :

$$X_1 = rac{-B \cdot F_0}{ ext{Determinant}} \ -B = j10,000 + 15,000 \ -B \cdot F_0 = (j10,000 + 15,000) \cdot 500 = j5,000,000 + 7,500,000 \ |X_1| = rac{\sqrt{(7,500,000)^2 + (5,000,000)^2}}{\sqrt{(-2,925,000,000)^2 + (1,650,000,000)^2}} \ |X_1| = rac{9 imes 10^6}{3.36 imes 10^9} = 2.68 imes 10^{-3} \, ext{m} \ heta_1 = an^{-1} \left(rac{5,000,000}{7,500,000}
ight) - an^{-1} \left(rac{1,650,000,000}{-2,925,000,000}
ight) \ heta_1 pprox -4.2^\circ$$

Final Results:

$$|X_2| = 2.68 \, \mathrm{mm}, \; heta_2 = -4.2^\circ \ |X_1| = 2.68 \, \mathrm{mm}, \; heta_1 = -4.2^\circ \ |X_2| = -4.2^\circ \ |X_2| = 2.68 \, \mathrm{mm}, \; heta_2 = -4.2^\circ \ |X_2| = 2.68 \, \mathrm{mm}, \; heta_3 = -4.2^\circ \ |X_3| = 2.68 \, \mathrm{mm}, \; heta_4 = -4.2^\circ \ |X_4| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.2^\circ \ |X_5| = 2.68 \, \mathrm{mm}, \; heta_5 = -4.20 \, \mathrm{mm}, \; heta_5 =$$

Natural Frequencies and Mode Shapes

Natural frequencies are derived by solving the system's eigenvalue problem, while mode shapes provide insights into the coupled dynamics.

Frequency Response Analysis

Frequency-domain analysis is employed to characterize system behavior under harmonic excitations, with resonance mitigation quantified for systems with vibration absorbers.

Conclusion

The integration of a vibration absorber in a quarter-car suspension model significantly enhances ride quality and stability. By suppressing resonance effects, the absorber ensures smoother operation, particularly under challenging road conditions. The findings align with existing literature, reinforcing the critical role of vibration absorbers in modern suspension design.

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