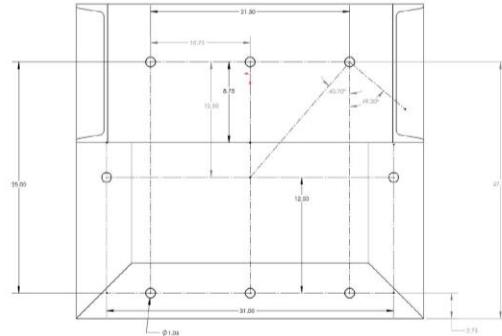
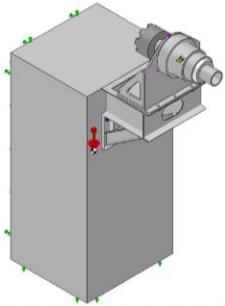
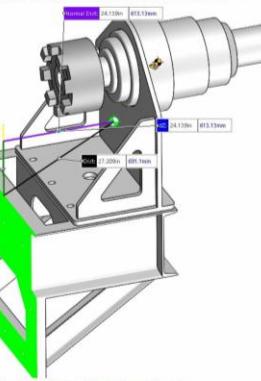


# Bolt Stress Calc & Design of Inchng Drive for M/C Shop

WO# 50281-Bolted bracket calculation



JUL-27-2025  
Referece: Machine Design-Bhandari Pa. 247



The bolts can be designed on the basis of principal stress theory or principal shear stress theory.

The principal stress  $\sigma_1$  is given by,

$$\sigma_1 = \frac{\sigma_t}{2} + \sqrt{\left(\frac{\sigma_t}{2}\right)^2 + \tau^2} \quad (7.13)$$

The principal shear stress is given by,

$$\tau_{\max} = \sqrt{\left(\frac{\sigma_t}{2}\right)^2 + \tau^2} \quad (7.14)$$

Note: bolts 7 & 8 not considered

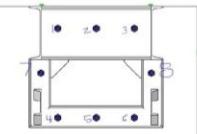
INPUTS

$V := 2800 \cdot \text{lb}$  Weight including base, reducer, reducer bracket and male coupling

$P := V$

$T := 1052688 \cdot \text{in} \cdot \text{lb}$  Maximum output torque

$B_{TSA} := .472 \text{ in}^2$  Bolt tensile stress area



$N_B := 6$  Number of bolts

$Y_s := 60000 \cdot \frac{\text{lb}}{\text{in}^2}$  Anchor bolt Yield Strength, considering A354-Grade BD

CALCULATION

Primary Shear Forces,  $P' = P'1, P'2, P'3, P'4, P'5, P'6$ ,

$$P' := \frac{V}{N_B} = 466.67 \text{ lb}$$

$P'_3 := P'$

Obtaining distances from center of bolt pattern to center of bolts  $r_1 = r_4 = r_3 = r_6$  and  $r_2 = r_5$

$$r_1 := \sqrt{(10.75 \cdot \text{in})^2 + (12.5 \cdot \text{in})^2} = 16.49 \text{ in}$$

$$r_2 := 12.5 \cdot \text{in}$$

$$r_7 := 15.5 \cdot \text{in}$$

From fig.1 we can deduct that bolts 3, 6, 1 and 4 would be under max. shear forces

$$P''_3 := \frac{T \cdot r_1}{4 \cdot (r_1^2) + 2 \cdot (r_2^2) + 2 \cdot (r_7^2)} = 9230.363 \text{ lb}$$

Resultant shear force on bolt 3 ( $P_s$ )

$$\Sigma F_y := P'_3 + ((P''_3) \cdot \cos(49 \cdot \text{deg})) = 6522.33 \text{ lb}$$

$$\Sigma F_x := P''_3 \cdot \sin(49 \cdot \text{deg}) = 6966.24 \text{ lb}$$

$$P_s := \sqrt{(\Sigma F_y)^2 + (\Sigma F_x)^2} = 9543.03 \text{ lb}$$

STRESS DUE TO TENSION CALCULATION

The moment  $V \times e$  tends to tilt the bracket about the lower edge, this way the top bolt row is taking maximum forces

$e := 24.25 \cdot \text{in}$  base, reducer, reducer bracket and male coupling COG to mounting face

$l_1 := 27.75 \cdot \text{in}$  Lower edge to upper bolt row distance

$l_2 := 15.25 \cdot \text{in}$  Lower edge to lower bolt row distance

$l_3 := 2.75 \cdot \text{in}$

$$P_3 := \frac{P \cdot e \cdot l_3}{3 \cdot (l_1^2 + l_3^2) + 2 \cdot (l_2^2)} = 66.74 \text{ lb}$$

Resisting forces in bolts 1 to 3

$$\sigma_t := \frac{P_3}{B_{TSA}} = 141.39 \frac{\text{lb}}{\text{in}^2}$$

Stress in bolt due to tension

$$\tau := \frac{P_s}{B_{TSA}} = 20218.27 \frac{\text{lb}}{\text{in}^2}$$

Stress in bolt due to shear

$$\tau_{\max} := \sqrt{\left(\frac{\sigma_t}{2}\right)^2 + \tau^2} = 20218.4 \frac{\text{lb}}{\text{in}^2}$$

Maximum shear stress in bolts

$$L_f := \frac{Y_s}{\tau_{\max}} = 2.97$$

Load factor top row bolts



Hydraulic motor w/ CB valve for metered rotation

**My contribution:** Designing the structural components, outsourcing of hydraulic components, design hose paths in assembly and analyse shear stress on hardware under supervision.