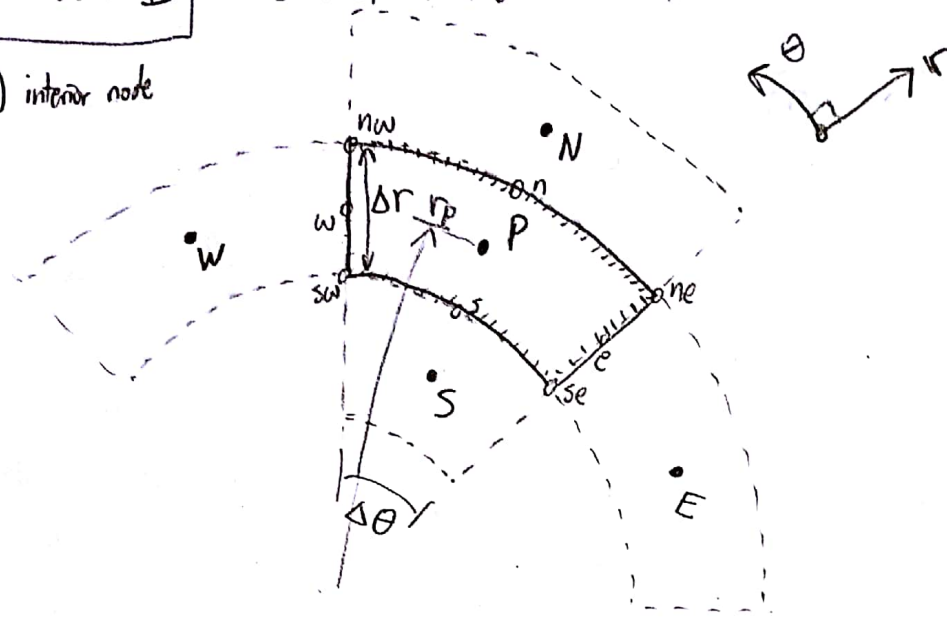


Problem 1

Control Volume formulation

a) interior node



Steady 2D heat conduction: $k \nabla^2 T + q = 0$

$$\nabla^2 T = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2}$$

$$\hookrightarrow k \nabla^2 T + q = 0 = \frac{k}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{k}{r^2} \frac{\partial^2 T}{\partial \theta^2} + q = 0$$

$$= k \frac{\partial^2 T}{\partial r^2} + \frac{k}{r} \frac{\partial T}{\partial r} + \frac{k}{r^2} \frac{\partial^2 T}{\partial \theta^2} + q = 0$$

Use FVM

First integrate the PDE over the volume which has P at the centroid

$$\int_V k \nabla^2 T dV + \int_V q dV = 0$$

Use divergence theorem to convert the First volume integral to a surface integral

$$\int_V k \nabla^2 T dV = \int_S k \nabla T \cdot \hat{n} dS$$

Problem 1 (cont.)

Now we have:

$$\int_S k \nabla T \cdot \hat{n} dS + \int_V q dV = 0.$$

Divide the surface integral into four distinct surfaces (n, s, e, w)

$$\int_{S_n} k \nabla T \cdot (\hat{u}_r) dS + \int_{S_s} k \nabla T \cdot (-\hat{u}_r) dS + \int_{S_e} k \nabla T \cdot (-\hat{u}_\theta) dS + \int_{S_w} k \nabla T \cdot (\hat{u}_\theta) dS + \int_V q dV = 0$$

Simplify by expanding $\nabla T = \frac{\partial T}{\partial r} \hat{u}_r + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{u}_\theta$ and evaluating dot products.

$$\int_{S_n} k \frac{\partial T}{\partial r} dS + \int_{S_s} -k \frac{\partial T}{\partial r} dS + \int_{S_e} -\frac{k}{r_e} \frac{\partial T}{\partial \theta} dS + \int_{S_w} \frac{k}{r_w} \frac{\partial T}{\partial \theta} dS + \int_V q dV = 0$$

Quadrature: use midpoint rule to approximate surface integrals and the volume integral (with 2nd order accuracy)

$$\approx k \left[\frac{\partial T}{\partial r} \Big|_n r_n \Delta \theta - \frac{\partial T}{\partial r} \Big|_s r_s \Delta \theta - \frac{k}{r_e} \frac{\partial T}{\partial \theta} \Delta r + \frac{k}{r_w} \frac{\partial T}{\partial \theta} \Delta r \right] + q_p \Delta V = 0$$

Extract common k and plug in $\Delta V = \Delta r \cdot r_p \Delta \theta \cdot (1) = r_p \Delta r \Delta \theta$, $r_e = r_w = r_p$

$$k \left[\frac{\partial T}{\partial r} \Big|_n r_n \Delta \theta - \frac{\partial T}{\partial r} \Big|_s r_s \Delta \theta - \frac{1}{r_p} \frac{\partial T}{\partial \theta} \Delta r + \frac{1}{r_p} \frac{\partial T}{\partial \theta} \Delta r \right] + q_p r_p \Delta r \Delta \theta = 0$$

Interpolation: use CDS2 to define $\frac{\partial T}{\partial r} \Big|_n, \frac{\partial T}{\partial r} \Big|_s, \frac{\partial T}{\partial \theta} \Big|_e, \frac{\partial T}{\partial \theta} \Big|_w$ in terms of cell-centered values (with 2nd-order accuracy)

$$\frac{\partial T}{\partial r} \Big|_n = \frac{T_N - T_P}{\Delta r} + \mathcal{O}((\Delta r)^2)$$

$$\frac{\partial T}{\partial r} \Big|_s = \frac{T_S - T_P}{\Delta r} + \mathcal{O}((\Delta r)^2)$$

$$\frac{\partial T}{\partial \theta} \Big|_e = \frac{T_E - T_P}{\Delta \theta} + \mathcal{O}((r_p \Delta \theta)^2)$$

$$\frac{\partial T}{\partial \theta} \Big|_w = \frac{T_W - T_P}{\Delta \theta} + \mathcal{O}((r_p \Delta \theta)^2)$$

Problem 1 (cont.) Substitute terms and drop higher-order terms $[O((\Delta r)^2), O((r_p \Delta \theta)^2)]$

$$k \left[\frac{T_N - T_P}{\Delta r} r_n \Delta \theta - \frac{T_S - T_P}{\Delta r} r_s \Delta \theta - \frac{T_E - T_P}{r_p \Delta \theta} \Delta r + \frac{T_W - T_P}{r_p \Delta \theta} \Delta r \right] + q_p r_p \Delta r \Delta \theta = 0$$

move term with q_p to RHS and multiply all terms by $r_p \Delta r \Delta \theta / k$

$$(T_N - T_P) r_n r_p (\Delta \theta)^2 - (T_S - T_P) r_s r_p (\Delta \theta)^2 - (T_E - T_P) (\Delta r)^2 + (T_W - T_P) (\Delta r)^2 = \frac{-q_p}{k} r_p^2 (\Delta r)^2 (\Delta \theta)^2$$

Rearrange in terms of coefficients A_N, A_S, A_P, A_E, A_W , substitute $r_n = r_p + \frac{\Delta r}{2}$ and $r_s = r_p - \frac{\Delta r}{2}$

$$\underbrace{\left[\left(r_p + \frac{\Delta r}{2} \right) r_p (\Delta \theta)^2 \right]}_{A_N} T_N + \underbrace{\left[\left(r_p - \frac{\Delta r}{2} \right) r_p (\Delta \theta)^2 \right]}_{A_S} T_S + \underbrace{\left[-(\Delta r) r_p (\Delta \theta)^2 \right]}_{A_P} T_P + \underbrace{\left[-(\Delta r)^2 \right]}_{A_E} T_E + \underbrace{\left[(\Delta r)^2 \right]}_{A_W} T_W = \underbrace{\left[\frac{-q_p}{k} (r_p \Delta r \Delta \theta)^2 \right]}_{Q_P}$$

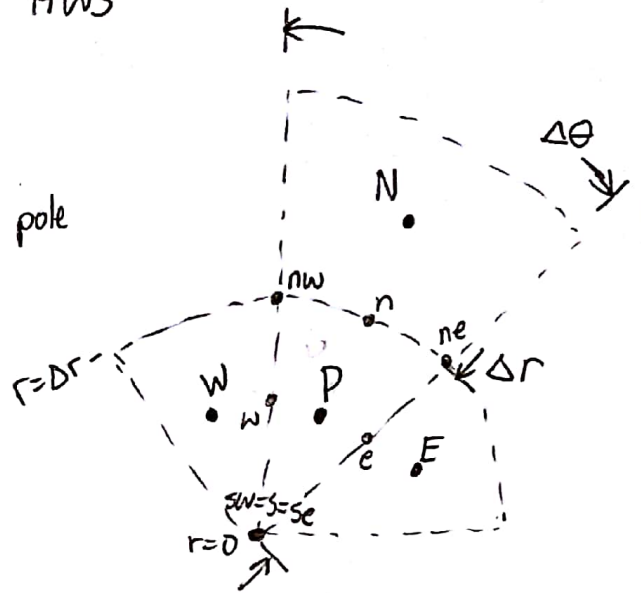
Problem 1 (cont.)

b) $C\psi$ in the inner ring, adjacent to pole

$$k \nabla^2 T + q = 0$$

Integrate over the volume

$$\int_V k \nabla^2 T dV + \int_V q dV = 0$$



Invoke Gauss' Divergence Theorem to convert first volume integral to surface integral

$$k \int_S \nabla T \cdot \hat{n} dS + \int_V q dV$$

Separate surface integral into the three discrete surfaces

$$\int_{S_n} \nabla T \cdot \hat{u}_r dS + \int_{S_e} \nabla T \cdot (-\hat{u}_\theta) dS + \int_{S_w} \nabla T \cdot (\hat{u}_\theta) dS + \frac{1}{k} \int_V q dV = 0$$

Evaluate dot products with $\nabla T = \frac{\partial T}{\partial r} \hat{u}_r + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{u}_\theta$

$$\int_{S_n} \frac{\partial T}{\partial r} dS + \int_{S_e} -\frac{1}{r} \frac{\partial T}{\partial \theta} dS + \int_{S_w} \frac{1}{r} \frac{\partial T}{\partial \theta} dS + \frac{1}{k} \int_V q dV = 0$$

Quadrature: approximate integrals with midpoint rule (2nd-order accurate)

$$\left. \frac{\partial T}{\partial r} \right|_n r_n \Delta \theta - \frac{1}{r_e} \left. \frac{\partial T}{\partial \theta} \right|_e \Delta r + \frac{1}{r_w} \left. \frac{\partial T}{\partial \theta} \right|_w \Delta r + \frac{1}{k} q_p \Delta r r_p \Delta \theta (1) = 0$$

Problem 1 (cont.)

Interpolation: approximate derivatives with COS2 (2nd-order accurate)

$$\left. \frac{\partial T}{\partial r} \right|_n = \frac{T_N - T_P}{\Delta r} + \mathcal{O}((\Delta r)^2) \quad \left. \frac{\partial T}{\partial \theta} \right|_e = \frac{T_E - T_P}{\Delta \theta} + \mathcal{O}((\Delta \theta)^2)$$

$$\left. \frac{\partial T}{\partial \theta} \right|_w = \frac{T_W - T_P}{\Delta \theta} + \mathcal{O}((\Delta \theta)^2)$$

Plug into quadrature equation; also substitute $r_n = r_p + \frac{\Delta r}{2}$, $r_e = r_p$, $r_w = r_p$

$$\frac{T_N - T_P}{\Delta r} (r_p + \frac{\Delta r}{2}) \Delta \theta - \frac{1}{r_p} \frac{T_E - T_P}{\Delta \theta} \Delta r + \frac{1}{r_p} \frac{T_W - T_P}{\Delta \theta} \Delta r = -\frac{1}{k} q_p r_p \Delta r \Delta \theta$$

Multiply all terms by $r_p \Delta r \Delta \theta$

$$(T_N - T_P) r_p (r_p + \frac{\Delta r}{2}) (\Delta \theta)^2 - (T_E - T_P) (\Delta r)^2 + (T_W - T_P) (\Delta r)^2 = -\frac{q_p}{k} (r_p \Delta r \Delta \theta)^2$$

Rearrange terms into coefficient form with A_N, A_P, A_E, A_W, Q_P :

$$\underbrace{\left[r_p (r_p + \frac{\Delta r}{2}) (\Delta \theta)^2 \right]}_{A_N} T_N + \underbrace{\left[-r_p (r_p + \frac{\Delta r}{2}) (\Delta \theta)^2 \right]}_{A_P} T_P + \underbrace{\left[-(\Delta r)^2 \right]}_{A_E} T_E + \underbrace{\left[(\Delta r)^2 \right]}_{A_W} T_W = \underbrace{\left[-\frac{1}{k} (r_p \Delta r \Delta \theta)^2 \right]}_{Q_P}$$


$A_S = 0$

(in this case, $r_p = \frac{\Delta r}{2}$)

Problem 1 (cont.)

c) $C \nVdash$ in the outer ring, adjacent to the boundary

Handle convection BC by looking at energy balance at boundary



$$\dot{q}_{conv}'' = \dot{q}_{cond}''$$

$$h(T_s - T_f) = k \left. \frac{\partial T}{\partial r} \right|_{r=R}$$

$$h[T(r) - T_f] = k \left. \frac{\partial T}{\partial r} \right|_R$$

This equation must be solved at the boundary

Start with steady 2D conduction equation $k \nabla^2 T + q = 0$

Integrate over the CV

$$\int_V \nabla^2 T \, dV + \int_V q \, dV = 0$$

Invoke Divergence Theorem for first integral

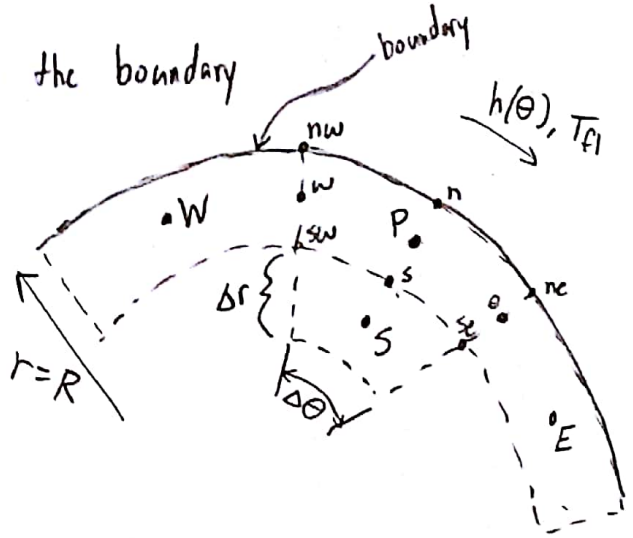
$$\int_S \nabla T \cdot \hat{n} dS + \frac{1}{k} \int_V q dV = 0$$

Separate surface integral into four parts (one for each surface)

$$\int_{S_n} \nabla T \cdot (\hat{u}_r) dS + \int_{S_3} \nabla T \cdot (-\hat{u}_r) dS + \int_{S_2} \nabla T \cdot (-\hat{u}_\theta) dS + \int_{S_w} \nabla T \cdot (\hat{u}_\theta) dS + \frac{1}{k} \int_V q dV = 0$$

Evaluate dot products

$$\int_{S_n} \frac{\partial T}{\partial r} dS + \int_{S_s} -\frac{\partial T}{\partial r} dS + \int_{S_c} \frac{-1}{r} \frac{\partial T}{\partial \theta} dS + \int_{S_w} \frac{1}{r} \frac{\partial T}{\partial \theta} dS + \frac{1}{k} \int_V dV = 0$$



Problem 1 (cont.) Quadrature: approximate integrals with midpoint rule (2nd-order accurate)

$$\left. \frac{\partial T}{\partial r} \right|_n R \Delta \theta + \left. \frac{\partial T}{\partial r} \right|_s (R - \Delta r) \Delta \theta + \frac{-1}{r_e} \left. \frac{\partial T}{\partial \theta} \right|_e \Delta r + \frac{1}{r_w} \left. \frac{\partial T}{\partial \theta} \right|_w \Delta r = -\frac{q_p}{k} r_p \Delta r \Delta \theta$$

Substitute $r_e = r_w = r_p = R - \frac{\Delta r}{2}$

$$\left. \frac{\partial T}{\partial r} \right|_n R \Delta \theta - \left. \frac{\partial T}{\partial r} \right|_s (R - \Delta r) \Delta \theta - \frac{1}{R - \frac{\Delta r}{2}} \left. \frac{\partial T}{\partial \theta} \right|_e \Delta r + \frac{1}{R - \frac{\Delta r}{2}} \left. \frac{\partial T}{\partial \theta} \right|_w \Delta r = -\frac{q_p}{k} (R - \frac{\Delta r}{2}) \Delta r \Delta \theta \quad (*)$$

Interpolation: use CDS2 to approximate derivatives at s, e, w faces (both 2nd-order accurate)
use BDS2 to approximate derivative at n face

$$\left. \frac{\partial T}{\partial r} \right|_s = \frac{T_s - T_p}{\Delta r} + \mathcal{O}((\Delta r)^2) \quad \left. \frac{\partial T}{\partial \theta} \right|_e = \frac{T_e - T_p}{\Delta \theta} + \mathcal{O}((\Delta \theta)^2) \quad \left. \frac{\partial T}{\partial \theta} \right|_w = \frac{T_w - T_p}{\Delta \theta} + \mathcal{O}((\Delta \theta)^2)$$

Derive BDS2: set $A \neq 0$ and $B \neq 0$, $C=0$, $D=0$

$$A T_{i-2} + B T_{i-1} = (A+B) T_i + (-2A-B) \Delta x \left. \frac{\partial T}{\partial x} \right|_i + (2A + \frac{1}{2}B) (\Delta x)^2 \left. \frac{\partial^2 T}{\partial x^2} \right|_i + (-\frac{4}{3}A - \frac{1}{6}B) (\Delta x)^3 \left. \frac{\partial^3 T}{\partial x^3} \right|_i + \text{HOTs}$$

$$\text{Set } 2A + \frac{1}{2}B = 0 \rightarrow B = -4A$$

$$A T_{i-2} - 4A T_{i-1} + 3T_i = 2A \Delta x \left. \frac{\partial T}{\partial x} \right|_i + (0) (\Delta x)^2 \left. \frac{\partial^2 T}{\partial x^2} \right|_i + \text{HOTs}$$

Divide by A and reorder

$$\left. \frac{\partial T}{\partial x} \right|_i = \frac{T_{i-2} - 4T_{i-1} + 3T_i}{2\Delta x} + \mathcal{O}((\Delta x)^2)$$

Apply to this problem for $\left. \frac{\partial T}{\partial r} \right|_n$

$$\left. \frac{\partial T}{\partial r} \right|_n = \frac{T_s - 4T_p + 3T_n}{\Delta r} + \mathcal{O}((\Delta r)^2)$$

Now we need to interpolate for T_s

$$T_s = \frac{T_p + T_s}{2}$$

$$\rightarrow \left. \frac{\partial T}{\partial r} \right|_n \approx \frac{\frac{T_p + T_s}{2} - 4T_p + 3T_n}{\Delta r}$$

Problem 1 (cont.) Now use the BC to solve for T_n

$$\frac{h}{k} [T_n - T_f] = \frac{-\frac{7}{2}T_p + \frac{1}{2}T_s + 3T_n}{\Delta r} = \frac{h}{k} T_n - \frac{h}{k} T_f = \frac{-7T_p + T_s}{2\Delta r} + \frac{3T_n}{\Delta r}$$

$$\frac{h}{k} T_n - \frac{3}{\Delta r} T_n = \frac{-7T_p + T_s}{2\Delta r} + \frac{h}{k} T_f$$

$$T_n = \frac{\left(\frac{-7T_p + T_s}{2\Delta r} + \frac{h}{k} T_f \right)}{\left(\frac{h\Delta r - 3k}{k\Delta r} \right)} = \frac{\frac{k}{2}(T_s - 7T_p) + h\Delta r T_f}{h\Delta r - 3k}$$

$$\left. \frac{\partial T}{\partial r} \right|_n = \frac{-7}{2\Delta r} T_p + \frac{1}{2\Delta r} T_s + \frac{3}{\Delta r} \left[\frac{\frac{k}{2}(T_s - 7T_p) + h\Delta r T_f}{h\Delta r - 3k} \right]$$

$$\left. \frac{\partial T}{\partial r} \right|_n = \frac{-7}{2\Delta r} T_p + \frac{1}{2\Delta r} T_s + \frac{3}{\Delta r} \frac{k}{2} \frac{T_s}{h\Delta r - 3k} - \frac{21}{\Delta r} \frac{k}{2} \frac{T_p}{h\Delta r - 3k} + \frac{3h}{h\Delta r - 3k} T_f$$

$$\left. \frac{\partial T}{\partial r} \right|_n = T_p \underbrace{\left[\frac{-7}{2\Delta r} - \frac{21k}{2\Delta r(h\Delta r - 3k)} \right]}_{C_1} + T_s \underbrace{\left[\frac{1}{2\Delta r} + \frac{3k}{2\Delta r(h\Delta r - 3k)} \right]}_{C_2} + T_f \underbrace{\left[\frac{3h}{h\Delta r - 3k} \right]}_{C_3}$$

$$\left. \frac{\partial T}{\partial r} \right|_n = C_1 T_p + C_2 T_s + C_3 T_f$$

Substitute derivative approximations into original equation (*)

$$[C_1 T_p + C_2 T_s + C_3 T_f] R \Delta \theta - \frac{T_s - T_p}{\Delta r} (R - \Delta r) \Delta \theta - \frac{1}{R - \frac{\Delta r}{2}} \frac{T_E - T_p}{\Delta \theta} \Delta r + \frac{1}{R - \frac{\Delta r}{2}} \frac{T_W - T_p}{\Delta \theta} \Delta r = \underbrace{\frac{-q_p}{k} (R - \frac{\Delta r}{2}) \Delta r \Delta \theta}_{(RHS)_a}$$

Start re-arranging to eventually find A_s, A_p, A_E, A_W, Q_p

$$T_p \left[C_1 + \frac{(R - \Delta r) \Delta \theta}{\Delta r} + \frac{\Delta r}{(R - \frac{\Delta r}{2}) \Delta \theta} - \frac{\Delta r}{(R - \frac{\Delta r}{2}) \Delta \theta} \right] + T_s \left[C_2 - \frac{(R - \Delta r) \Delta \theta}{\Delta r} \right] + T_E \left[\frac{-\Delta r}{(R - \frac{\Delta r}{2}) \Delta \theta} \right] + T_W \left[\frac{\Delta r}{(R - \frac{\Delta r}{2}) \Delta \theta} \right] + R \Delta \theta C_3 T_f = (RHS)_a$$

Problem 1 (cont.)

The full coefficients are:

$$\left[\frac{-7}{2\Delta r} - \frac{21k}{2\Delta r(h\Delta r - 3k)} + \frac{(R - \Delta r)\Delta\theta}{\Delta r} \right] = A_P$$

$$\left[\frac{1}{2\Delta r} + \frac{3k}{2\Delta r(h\Delta r - 3k)} - \frac{(R - \Delta r)\Delta\theta}{\Delta r} \right] = A_S$$

$$0 = A_N$$

$$\left[\frac{-\Delta r}{(R - \frac{\Delta r}{2})\Delta\theta} \right] = A_E$$

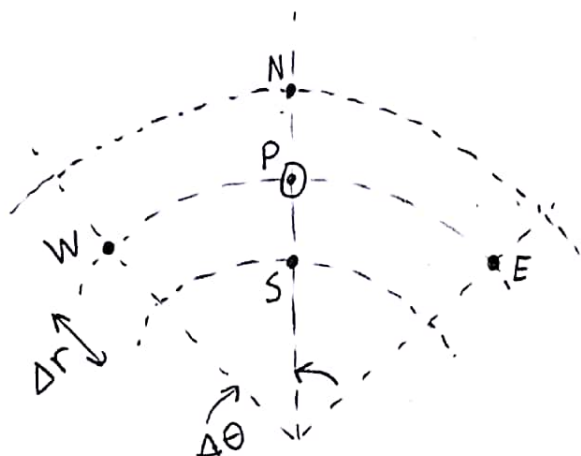
$$\left[\frac{\Delta r}{(R - \frac{\Delta r}{2})\Delta\theta} \right] = A_W$$

$$\left[\frac{-q_p}{k} (R - \frac{\Delta r}{2})\Delta r\Delta\theta - \frac{3hR\Delta\theta T_{fluid}}{h\Delta r - 3k} \right] = Q_P$$

$$A_P T_P + A_S T_S + A_E T_E + A_W T_W = Q_P$$

Problem 2

FDM for internal node



Find approximation to

$$k \nabla^2 T + q = 0$$

using Taylor Series expansions

PDE is $k \nabla^2 T + q = 0 \rightarrow \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} = \frac{-q}{k}$

Use CDS2 for all derivatives (2nd-order accurate)

$$\left. \frac{\partial T}{\partial r} \right|_P = \frac{T_N - T_S}{2 \Delta r}$$

$$\left. \frac{\partial^2 T}{\partial r^2} \right|_P = \frac{T_N - 2T_P + T_S}{(\Delta r)^2}$$

$$\left. \frac{\partial^2 T}{\partial \theta^2} \right|_P = \frac{T_W - 2T_P + T_E}{(\Delta \theta)^2}$$

$$\begin{aligned} & - \frac{1}{6} (\Delta r)^2 \left. \frac{d^3 T}{dx^3} \right|_P + \text{HOTs} \\ & - \frac{1}{12} (\Delta r)^2 \left. \frac{d^4 T}{dr^4} \right|_P + \text{HOTs} \\ & - \frac{1}{12} (\Delta \theta)^2 \left. \frac{d^4 T}{d\theta^4} \right|_P + \text{HOTs} \end{aligned}$$

Plug into PDE, evaluate at point P

Leading-order TE terms

$$\frac{T_N - 2T_P + T_S}{(\Delta r)^2} + \frac{1}{r_P} \frac{T_N - T_S}{2 \Delta r} + \frac{1}{r_P^2} \frac{T_W - 2T_P + T_E}{(\Delta \theta)^2} = \frac{-q}{k}$$

Multiply all terms by $(r_P \Delta r \Delta \theta)^2$

$$(T_N - 2T_P + T_S)(r_P \Delta \theta)^2 + \frac{1}{2} (T_N - T_S) r_P \Delta r (\Delta \theta)^2 + (T_W - 2T_P + T_E)(\Delta r)^2 = \frac{-q}{k} (r_P \Delta r \Delta \theta)^2$$

Problem 2 (cont.) Now rearrange to show coefficients

$$\left[(r_p \Delta \theta)^2 + \frac{1}{2} r_p \Delta r (\Delta \theta)^2 \right] T_N + \left[(r_p \Delta \theta)^2 - \frac{1}{2} r_p \Delta r (\Delta \theta)^2 \right] T_S + \left[-2(r_p \Delta \theta)^2 - 2(\Delta r)^2 \right] T_P + \left[(\Delta r)^2 \right] T_E + \left[(\Delta r)^2 \right] T_W = \left[\frac{-q}{k} (r_p \Delta r \Delta \theta)^2 \right]$$

Simplify expressions

$$\underbrace{\left[\left(r_p + \frac{\Delta r}{2} \right) r_p (\Delta \theta)^2 \right]}_{A_N} T_N + \underbrace{\left[\left(r_p - \frac{\Delta r}{2} \right) r_p (\Delta \theta)^2 \right]}_{A_S} T_S + \underbrace{\left[-2 \left\{ (r_p \Delta \theta)^2 + (\Delta r)^2 \right\} \right]}_{A_P} T_P + \underbrace{\left[(\Delta r)^2 \right]}_{A_E} T_E + \underbrace{\left[(\Delta r)^2 \right]}_{A_W} T_W = \underbrace{\left[\frac{-q}{k} (r_p \Delta r \Delta \theta)^2 \right]}_{Q_P}$$

Problem 3 FVM vs FDM

The result for FDM is almost identical to the FVM result for an interior volume. The only difference is the A_P coefficient. Both results have the same A_N , A_S , A_E , A_W , and Q_P . They both form linear matrix equations. They are both second-order accurate. In applying boundary conditions, the FVM requires an expression for the temperature on a surface of a control volume, while the FDM requires an expression for temperature on a node itself. The FVM has more flexibility with boundary conditions, as corner points with discontinuous BCs can be handled, while only one value can be used at a corner node in FDM.