ADER 构造过程

November 5, 2018

ADER 基本思想

对于黎曼问题:

$$\partial_t U + \partial_x F(U) = 0$$

$$U(x,0) = \begin{cases} U_L(x), x < x_{i+1/2} \\ U_R(x), x > x_{i+1/2} \end{cases}$$
(1)

根据泰勒展开,在拉格朗日体系下,可以得到 τ 时刻近似为

$$U(x_{i+1/2},\tau) = U(x_{i+1/2},0+) + \sum_{k=1}^{r-1} \left[\frac{d^k}{dt^k} U(x,t)(x_{i+1/2},0+) \right] \frac{\tau^k}{k!}$$
(2)

其中 $U(x_{i+1/2},0+)$ 是通过 $U_L(x_{i+1/2})$ 和 $U_L(x_{i-1/2})$ 构造的黎曼解求得的 Godunov 状态。式中全导数可以通过如下形式得到,

$$\frac{d}{dt} = \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} \tag{3}$$

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高阶全导数

因此可以给出一到二阶高阶全导数形式如下

$$\frac{dU}{dt} = \frac{\partial U}{\partial t} + u \frac{\partial U}{\partial x} \tag{4}$$

$$\frac{d^{2}U}{dt^{2}} = \frac{d}{dt} \left(\frac{\partial U}{\partial t} + u \frac{\partial U}{\partial x} \right)
= \frac{\partial^{2}U}{\partial t^{2}} + \frac{\partial u}{\partial t} \frac{\partial U}{\partial x} + 2u \frac{\partial^{2}U}{\partial x \partial t} + u \frac{\partial u}{\partial x} \frac{\partial U}{\partial x} + u^{2} \frac{\partial^{2}U}{\partial x^{2}}$$
(5)

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高阶时间导数

高阶时间导数求法:

$$\frac{\partial U}{\partial t} = -A \frac{\partial U}{\partial x}
\frac{\partial^{2} U}{\partial x \partial t} = -\frac{\partial A}{\partial x} \frac{\partial U}{\partial x} - A \frac{\partial^{2} U}{\partial x^{2}}
\frac{\partial^{2} U}{\partial t^{2}} = -\frac{\partial A}{\partial t} \frac{\partial U}{\partial x} - A \frac{\partial^{2} U}{\partial x \partial t}
\frac{\partial^{3} U}{\partial x^{2} \partial t} = -\frac{\partial^{2} A}{\partial x^{2}} \frac{\partial U}{\partial x} - 2 \frac{\partial A}{\partial x} \frac{\partial^{2} U}{\partial x^{2}} - A \frac{\partial U^{3}}{\partial x^{3}}
\frac{\partial^{3} U}{\partial x \partial t^{2}} = -\frac{\partial^{2} A}{\partial x \partial t} \frac{\partial U}{\partial x} - \frac{\partial A}{\partial x} \frac{\partial^{2} U}{\partial x \partial t} - \frac{A}{\partial t} \frac{\partial U^{2}}{\partial x^{2}} - A \frac{\partial^{3} U}{\partial x^{2} \partial t}
\frac{\partial^{3} U}{\partial t^{3}} = -\frac{\partial^{2} A}{\partial t^{2}} \frac{\partial U}{\partial x} - \frac{\partial A}{\partial t} \frac{\partial^{2} U}{\partial x \partial t} - \frac{A}{\partial t} \frac{\partial U^{2}}{\partial x \partial t} - A \frac{\partial^{3} U}{\partial x \partial t^{2}}$$
(6)

高阶空间导数和广义黎曼解

通过广义黎曼解, 界面上空间导数发展方程为

$$\frac{\partial U_{x}^{(k)}}{\partial \tau} + A(U(x_{i+1/2}(0+), 0+)) \frac{\partial U_{x}^{(k)}}{\partial x} = 0$$

$$U_{x}^{(k)}(x_{i+1/2}, 0) = \begin{cases}
P_{L}^{(k)}(x_{i+1/2}), & \text{if } x < x_{i+1/2}, \\
P_{R}^{(k)}(x_{i+1/2}), & \text{if } x > x_{i+1/2},
\end{cases}$$
(7)

其中 A 为 Jacob 矩阵, $A = \frac{\partial F}{\partial U}$, $P_{L(R)}^{(k)} = \frac{\partial^k U_{L(R)}(x)}{\partial x^k}$ 通过广义黎曼求解器可以得到更高阶空间导数。

这里 $A(U(x_{i+1/2}(0+),0+))$ 为冻结矩阵,则可以通过如 HLL 构造

$$U^{(k)}(x_{i+1/2},0) = \frac{s_R U_R^{(k)} - s_L U_L^{(k)} + A U_L^{(k)} - A U_R^{(k)}}{s_R - s_L}$$
(8)

其中 $s_L(R)$ 通过 U_L 和 U_R 构造。

有限体积离散

在拉氏框架下,网格点随时间运动方程为

$$\frac{dx(t)}{dt} = u(x, t) \tag{9}$$

对黎曼问题

$$\begin{cases} \frac{\partial U}{\partial t} + \frac{\partial F}{\partial x} = 0\\ \partial_t s_{xx} + u \partial_x s_{xx} - \frac{4}{3} \partial_x u = 0\\ Q(x, t = 0) = \begin{cases} Q_L, & \text{if } x < 0\\ Q_R, & \text{if } x > 0 \end{cases} \end{cases}$$
(10)

其中 $U = (\rho, \rho u, \rho E)$, $F = (\rho u, \rho u^2 + p - s_{xx}, (\rho E + p - s_{xx})u)$, $Q = (\rho, \rho u, \rho E)$ 。

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有限体积离散

三阶 WENO 格式下二阶空间导数构造方法

We take the $U_L^{(1)}$ as an example, the same to U_L , we use two stencils $S(i-1,i)=c_{11}U_{i-1}+c_{12}U_i$ and $S(i,i+1)=c_{21}U_i+c_{22}U_{i+1}$ to construct the $U_{i+1/2}^{(1)}$,

In an uniform mesh, the coefficients c_{11} and c_{12} are constructed as

$$\frac{c_{11}U_{i-1} + c_{12}U_i - (c_{11}U_{i-2} + c_{12}U_{i-1})}{\Delta x^2} = \frac{\partial^2 U_i}{\partial x^2} + O(\Delta x)$$
(11)

We get $c_{11}=-1$ and $c_{12}=1$, in a similar process, we can get $c_{21}=-1$ and $c_{22}=1$, so

$$q_1 = U_{i-1} - U_i$$

 $q_2 = U_i - U_{i+1}$ (12)

Using $\mathit{S}(\mathit{i}-1,\mathit{i},\mathit{i}+1)$ we can construct a 2nd order approximation of $\mathit{U}_\mathit{L}^{(1)}$

$$U_{i+1/2}^{(1)L} = \omega_1 q_1 + \omega_2 q_2 \tag{13}$$

where $\omega_i=rac{lpha_k}{lpha_1+lpha_2}$ and $lpha_k=rac{d_k}{(eta_k+arepsilon)^p}$, d_k is the linear weights of q_1 and q_2 can be solved as

$$\frac{d_1 q_1 + d_2 q_2}{\Delta x^2} = \frac{\partial^2 U_i}{\partial x^2} + O(\Delta x^2)$$
 (14)

Then we get $d_1=\frac{1}{4}$ and $d_2=\frac{3}{4}$. And the smoothness indicatros are

$$\beta_1 = q_1^2, \beta_2 = q_2^2 \tag{15}$$

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守恒方程有限体积离散

基于格林公式可以写作

$$\oint_{\partial\omega} (Udx - Fdt) = 0 \tag{17}$$

展开有

$$\int_{x_{i-1}^{n+1}/2}^{x_{i+1}^{n+1}/2} U dx - \int_{x_{i-1}^{n}/2}^{x_{i+1}^{n}/2} U dx + \int_{x_{i-1}^{n}/2}^{x_{i-1}^{n}/2} U dx - \int_{x_{i+1}^{n}/2}^{x_{i+1}^{n}/2} U dx - \left(\int_{t^{n}}^{t^{n+1}} F(x_{i-1/2}, t) dt - \int_{t^{n}}^{t^{n+1}} F(x_{i+1/2}, t) dt \right) = 0$$
 (18)

将 Eq.(9) 带入有,

$$\int_{\substack{x_{i-1}^{n+1} \\ x_{i-1/2}^{n+1}}}^{x_{i+1/2}^{n+1}} U dx - \int_{\substack{x_{i-1/2}^{n} \\ x_{i-1/2}^{n}}}^{x_{i+1/2}^{n}} U dx - \begin{bmatrix} \int_{t^{n}}^{t^{n+1}} F(x_{i-1/2}, t) - u(x_{i-1/2}, t) U dt \\ - \int_{t^{n}}^{t^{n+1}} F(x_{i+1/2}, t) - u(x_{i+1/2}, t) U dt \end{bmatrix} = 0$$
 (19)

定义

$$f = F - uU \tag{20}$$

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有

$$\int_{x_{i-1/2}^{n+1/2}}^{x_{i+1/2}^{n+1}} U dx - \int_{x_{i-1/2}^{n}}^{x_{i+1/2}^{n}} U dx - \left[\int_{t^{n}}^{t^{n+1}} f(x_{i-1/2}, t) U dt - \int_{t^{n}}^{t^{n+1}} f(x_{i+1/2}, t) U dt \right] = 0$$
 (21)

令单元平均值

$$\bar{U}_{i}^{n} = \frac{1}{\Delta x^{n}} \int_{x_{i-1/2}^{n+1}}^{x_{i+1/2}^{n+1}} U(x, t^{n}) dx$$
 (22)

其中 $\Delta x^n = x_{i+1/2}^n - x_{i-1/2}^n$ 。 因此 Eq.(21) 变为

$$\bar{U}_i^{n+1} \Delta x_i^{n+1} - \bar{U}_i^{n} \Delta x_i^{n} - (F_{i-1/2} - F_{i+1/2}) = 0$$
 (23)

其中

$$F_{i+1/2} = \int_{t^n}^{t^{n+1}} f(x_{i+1/2}, t) dt$$
 (24)



Constitute equation

In the Lagrangian frame, the equation of the constitute model can be written as

$$\frac{\mathrm{d}\mathsf{s}_{\mathsf{XX}}}{\mathrm{d}\mathsf{t}} = \frac{4\mu}{3} \frac{\partial \mathsf{u}}{\partial \mathsf{x}} \tag{25}$$

For the cell-centered Lagrangian scheme, the geometrical conservation law is very important, that is,

$$\frac{\dot{V}}{V} = \frac{\partial u}{\partial x} \tag{26}$$

should be satisfied. In the one-dimensional case, the volume of the cell $\emph{I}_\emph{i}$ is evaluated by

$$V_i(t) = x_{i+1/2}(t) - x_{i-1/2}(t)$$
(27)

Taking the material derivative on the both sides of Eq.27, we have

$$\dot{V}_i(t) = u_{i+1/2}(t) - u_{i+1/2}(t)$$
(28)

We can get

$$\frac{\partial u}{\partial t} = \frac{\dot{V}_i(t)}{V_i} = \frac{u_{i+1/2}(t) - u_{i-1/2}(t)}{x_{i+1/2} - x_{i-1/2}}$$
(29)

Then, The semi-discrete formulation for Eq.25 has the following form:

$$\frac{ds_{xx}}{dt} = \frac{4\mu}{3} \frac{u_{i+1/2} - u_{i-1/2}}{\Delta x_i}$$
 (30)

ADER 构造过程

高斯积分

对于 $F_{i+1/2}$ 采用高斯积分

$$F_{i+1/2} = \int_{t^n}^{t^{n+1}} f(x_{i+1/2}, t) dt = \sum_{g=1}^{\alpha} \omega_g f(U(x_{i+1/2(t_g)}, t_g)) \Delta t$$
 (31)

其中 α 为高斯点个数, ω_g 为 g 点加权值。



Gaussian quadrature

In numerical analysis, a quadrature rule is an approximation of the definite integral of a function, usually stated as a weighted sum of function values at specified points within the domain of integration. An n-point Gaussian quadrature rule named after Carl Friedrich Gauss, is a quadrature rule constructed to yield an exact result for polynomials of degree 2n-1 or less by a suitable choice of the nodes x_i and weightes w_i for i=1, n. The most common domain of integration for such a rule is taken as [-1,1], so the rule is stated as

$$\int_{-1}^{1} f(x) dx \approx \sum_{i=0}^{n} \omega_{i} f(x_{i})$$
(32)

which is exact for polynomials of degree 2n-1 or less. This exact rule is known as the Gauss-Legendre quadrature rule.

Guass-Legendre quadrature

For the simplest integration problem stated above, i.e., f(x) is well-approximated by polynomials on [-1,1], the associated orthogonal polynomials are Legrendre-polynomials, denoted by $P_n(x)$. The i-th Gauss node, x_i is the i-th root of P_n and the weights are given by the formula (Abramowitz Stegun 1972, p.887)

$$\omega_i = \frac{2}{(1 - x_i^2)[P'_n(x_i)]^2}$$
 (33)

Some lower-order quadrature rules are tabulated below

Number of points, n	Points, x_i ,	Weights, ω_i
1	0	2
2	$\pm \frac{1}{\sqrt{3}}$	1
3	$0 \ (\pm \sqrt{\frac{3}{5}})$	$\frac{8}{9} \left(\frac{5}{9} \right)$
4	$\pm\sqrt{rac{3}{7}-rac{2}{7}\sqrt{rac{6}{5}}}$ ($\pm\sqrt{rac{3}{7}+rac{2}{7}\sqrt{rac{6}{5}}}$)	$\frac{18-\sqrt{30}}{36} \left(\begin{array}{c} \frac{18+\sqrt{30}}{36} \end{array} \right)$

Change of interval

An integral over [a,b] must be changed into an integral over [-1,1] before applying the Gaussian quadrature rule. This change of interval can be done in the fllowing way

$$\int_{a}^{b} f(x)dx = \frac{b-a}{2} \int_{-1}^{1} f(\frac{b-a}{2}x + \frac{a+b}{2})dx$$
 (34)

对于区域 $[0, \tau]$

求解流程

$$\begin{aligned} x_{i+1/2}^{n+1} &= x_{i+1/2}^{n} + \sum_{g=1}^{2} u(x_{i+1/2}, t_g) \omega_g \Delta t \\ \Delta x_{i}^{n+1} &= x_{i+1/2}^{n+1} - x_{i-1/2}^{n+1} \\ \Delta x_{i}^{n+1} &\overline{U}_{i}^{n+1} &= \Delta x_{i}^{n} \overline{U}_{i}^{n} + F_{i+1/2} - F_{i-1/2} \\ \overline{\$}_{xx_{i}}^{n+1} &= \overline{\$}_{xx_{i}}^{n} + \frac{\Theta_{i+1/2} - \Theta_{i-1/2}}{\Delta x^{n}} \\ \overline{\$}_{xx_{i}}^{n+1} &= \Gamma(\overline{\$}_{xx_{i}}^{n})^{n+1} = \Gamma(\overline{\$}_{xx_{i}}^{n+1}) \end{aligned}$$
(35)

其中

$$F_{i+1/2} = \sum_{g=1}^{2} f(U(x_{i+1/2}), t_g) \omega_g \Delta t$$

$$\Theta_{i+1/2} = \sum_{g=1}^{2} \frac{4}{3} \mu u(x_{i+1/2}, t_g) \omega_g \Delta t$$
(36)

通过泰勒展开

$$U(x_{i+1/2}, \tau) = U(x_{i+1/2}, 0) + \sum_{k=1}^{n-1} \frac{d^k U}{dt^k} \frac{\tau^n}{n!}$$
(37)



求解流程

其中全导数

$$\frac{dU}{dt} = \frac{\partial U}{\partial t} + u \frac{\partial U}{\partial x}
\frac{d^2 U}{dt^2} = \frac{d}{dt} \left(\frac{\partial U}{\partial t} + u \frac{\partial U}{\partial x} \right)
= \frac{\partial^2 U}{\partial t^2} + \frac{\partial u}{\partial t} \frac{\partial U}{\partial x} + 2u \frac{\partial^2 U}{\partial x \partial t} + u \frac{\partial u}{\partial x} \frac{\partial U}{\partial x} + u^2 \frac{\partial^2 U}{\partial x^2}$$
(38)

时间导数又可以转化为空间导数

$$\frac{\partial U}{\partial t} = -A \frac{\partial U}{\partial x}
\frac{\partial^2 U}{\partial x \partial t} = -\frac{\partial A}{\partial x} \frac{\partial U}{\partial x} - A \frac{\partial^2 U}{\partial x^2}
\frac{\partial^2 U}{\partial t^2} = -\frac{\partial A}{\partial t} \frac{\partial U}{\partial x} - A \frac{\partial^2 U}{\partial x \partial t}$$
(39)

最终需要构造高阶空间导数。根据重构如 WENO3 可以构造二阶精度的 $U_L(x_{i+1/2},0)$ 和 $U_R(x_{i+1/2},0)$ 同样可以构造一阶精度的 $U_L^{(1)}(x_{i+1/2},0)$ 和 $U_R^{(1)}(x_{i+1/2},0)$ 。 WENO5 可以构造四阶的 $U_{L(R)}(x_{i+1/2},0)$. . . 一阶精度的 $U_{L(R)}^{(3)}(x_{i+1/2},0)$ 。 通过黎曼求解器可以根据 $U_{L(R)}(x_{i+1/2},0)$,同样的通过广义黎曼求解器可以根据 $U_{L(R)}^{(k)}(x_{i+1/2},0)$ 得到 $U^{(k)}(x_{i+1/2},0)$

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A 和 dA

$$A = \begin{pmatrix} 0 & 1 & 0 & 0 \\ -u^2 + \frac{\partial p}{\partial \rho} + \Gamma(\frac{u^2}{2} - e) & u(2 - \Gamma) & \Gamma & -1 \\ (\Gamma(\frac{u^2}{2} - e) - e + \frac{\sigma_X}{\rho} + \frac{\partial p}{\partial \rho})u & -\Gamma u^2 - \frac{\sigma_X}{\rho} + e & (1 + \Gamma)u & -u \\ \frac{4}{3}\mu\frac{\mu}{\rho} & 0 & u \end{pmatrix}$$
(40)

where,
$${\it e}={\it E}-\frac{u^2}{2}$$
 , $\Gamma=\frac{\Gamma_0\rho_0}{\rho}$, $\sigma_{\it X}=-p+{\it s}_{\it XX},\;\frac{\partial p}{\partial \rho}={\it a}_0^2\it f'(\eta)$

$$dA(1,1) = 0$$
 $dA(1,2) = 0$ $dA(1,3) = 0$ $dA(1,4) = 0$

$$\mathit{dA}(2,1) = -2\mathit{udu} + \mathit{a}_0^2\mathit{f}''(\eta)\frac{\mathit{d}\rho}{\rho_0} + \mathit{d}\Gamma(\frac{\mathit{u}^2}{2} - \mathit{e}) + \Gamma(\mathit{udu} - \mathit{de})$$

$$dA(2,2) = du(2 - \Gamma) - ud\Gamma$$

$$dA(2,3) = d\Gamma$$

$$dA(2,4) = 0$$

$$\mathrm{d}\mathrm{A}(3,1) = (\Gamma(\frac{u^2}{2} - \mathrm{e}) - \mathrm{e} + \frac{\sigma_{\mathrm{X}}}{\rho} + \frac{\partial \rho}{\partial \rho})\mathrm{d}\mathrm{u} + (\mathrm{d}\Gamma(\frac{u^2}{2} - \mathrm{e}) + \Gamma(\mathrm{u}\mathrm{d}\mathrm{u} - \mathrm{d}\mathrm{e}) - \mathrm{d}\mathrm{e} + \frac{\mathrm{d}\sigma_{\mathrm{X}}}{\rho} - \frac{\sigma_{\mathrm{X}}\mathrm{d}\rho}{\rho^2} + \mathrm{a}_0^2 f'(\eta) \frac{\mathrm{d}\rho}{\rho_0})\mathrm{u}$$

$$dA(3,2) = -d\Gamma u^2 - 2u\Gamma - \frac{d\sigma_x}{\rho} + \frac{\sigma_x d\rho}{\rho^2} + de$$

$$dA(3,3) = (1 + \Gamma)du + d\Gamma u$$

$$dA(3,4) = -du$$

$$dA(4,1) = \frac{4}{3}\mu \frac{du}{\rho} - \frac{4}{3}\mu \frac{ud\rho}{\rho^2}$$

$$dA(4,2) = \frac{4}{3}\mu \frac{d\rho}{\rho^2}$$

$$dA(4,3) = 0$$

$$dA(4,4) = du$$

 $\Gamma_{i,j} = \frac{1}{2} \left(\frac{1}{2} \right)^{-1} \left(\frac{1}{2} \right$

where $\textit{de} = \textit{dE} - \textit{udu}, \textit{d}\Gamma = -\frac{\Gamma_0 \, \rho_0 \, \textit{d}\rho}{\rho^2}$, $\textit{d}\sigma_{\rm X} = -\textit{d}p + \textit{d}s_{\rm XX}$



ADER 构造过程

sub-cell WENO-3 construct

First, define sub-cell points The sub-cell points $x_i^{(k)}$, $k=1,\ldots,2r-1$ in I_i are given by

$$x_i^{(k)} = x_{i-1/2} + \frac{k-1}{2r-3} \Delta x \tag{42}$$

For third-order scheme there are is no need of sub-cell points, $x_i^{(1)} = x_{(i-1/2)}, x_i^2 = x_{(i+1/2)}$. Step 2 Reconstruct (2r-2) point-wise values of u Using p_{WENO}^{2r-1} to get $u_i^{(k)}$

$$\rho_{WENO}^{2r-1} = \sum_{k=0}^{r-1} \omega_k q_k^r(x, \bar{u}_{i-r+1+k}, \cdots, \bar{u}_{i+k})$$
(43)

$$u_i^{(k)} = u(x_i^{(k)}) + e_i^{(k)} (\Delta x)^{2r-1}$$
(44)

Step 3, Construct $p_i(x)$ Ansatz $p_i(x)$ of u in I_i as follows

$$p_{i}(x) = \sum_{l=0}^{2r-2} a_{l} \left(\frac{x - x_{i-1/2}}{\Delta x}\right)^{l}$$
 (45)

By the equation

$$\begin{cases} p_i(x_i^{(l)}) = u_i^{(l)}, & l = 0, \dots, 2r - 2 \\ \frac{1}{\Delta x} \int_L p_i(x) dx = \bar{u}_i \end{cases}$$
(46)

For the third-order WENO scheme

$$U_i^{(1)} = U_{(i-1/2)}$$
 $U_i^{(2)} = U_{(i+1/2)}$
(47)

$$a_{0} = U_{i}^{(1)}$$

$$a_{1} = 6\bar{U} - 2U_{i}^{(2)} - 4U_{i}^{(1)}$$

$$a_{2} = 3(U_{i}^{(1)} + U_{i}^{(2)} - 2\bar{U})$$

$$(48)$$



For each cell I_j , we have two stencils $S_j=(x_{j-\frac{3}{2}},x_{j-\frac{1}{2}},x_{j+\frac{1}{2}})$ and $S_{j+1}=(x_{j-\frac{1}{2}},x_{j+\frac{1}{2}},x_{j+\frac{3}{2}})$ corresponding to $I_j=[x_{j-\frac{1}{2}},x_{j+\frac{1}{2}}]$. On these two stencils, we obtain two interpolations

$$p'_{j}(x) = u_{j} + \frac{\bar{u}_{j} - \bar{u}_{j-1}}{h}(x - x_{j}), p'_{j+1}(x) = \bar{u}_{j} + \frac{\bar{u}_{j+1} - \bar{u}_{j}}{h}(x - x_{j})$$
(49)

with the smoothness indicators $\mathit{IS}_j = (\bar{u}_j - \bar{u}_{j-1})^2$ and $\mathit{IS}_{j+1} = (\bar{u}_{j+1} - \bar{u}_j)^2$ Then we can get the left-hand reconstruction

$$R_{j}(x) = \frac{\alpha_{0}}{\alpha_{0} + \alpha_{1}} \rho_{j}'(x) + \frac{\alpha_{1}}{\alpha_{0} + \alpha_{1}} \rho_{j+1}'(x)$$
 (50)

where $\alpha_0 = C_0/(\varepsilon + lS_j)^2$, $\alpha_1 = C_1/(\varepsilon + lS_{j+1})$, C_0 and C_1 are the optimal weight of u at position x, given by solving

$$q^{3}(x, \bar{u}_{i-1}, \bar{u}_{i}, \bar{u}_{i+1}) = \sum_{k=0}^{1} C_{0} q_{0}(x, \bar{u}_{i-1+k}, \bar{u}_{i+k})$$
(51)

For convenient to understand, here we set $\beta = (x - x_i)/\Delta x$, C_0 and C_1 are

$$C_0 = 1 - \frac{\beta_a}{\beta} C_1 = \frac{\beta_a}{\beta} \tag{52}$$

where $\beta_a = 3\beta^2 + 3\beta - \frac{1}{4}$.

The we can get the subcell approximation of u in I_i as

$$p_{j}(x) = \sum_{l=0}^{2} a_{l} \left(\frac{x - x_{j+1/2}}{\Delta x}\right)^{l}$$
 (53)

where

$$a_0 = U_i^{(1)}$$

$$a_1 = 6\bar{U} - 2U_i^{(2)} - 4U_i^{(1)}$$

$$a_2 = 3(U_i^{(1)} + U_i^{(2)} - 2\bar{U})$$
(54)

and $u_i^{(1)} = R_j(x_{i-1/2}), u_i^{(2)} = R_j(x_{i+1/2}).$ So

$$\frac{\partial p_{j}}{\partial x}(x) = \frac{s_{1}}{\Delta x} + \frac{2s_{2}(x - x_{i-1/2})}{\Delta x^{2}}$$

$$\frac{\partial^{2} p_{j}}{\partial x^{2}}(x) = \frac{2s_{2}}{\Delta x^{2}}$$
(55)



For each cell I_j , we have two stencils $S_j=(x_{j-\frac{3}{3}},x_{j-\frac{1}{3}},x_{j+\frac{1}{3}})$ and $S_{j+1}=(x_{j-\frac{1}{3}},x_{j+\frac{1}{3}},x_{j+\frac{3}{3}})$ corresponding to $I_j = [x_{j-\frac{1}{\alpha}}, x_{j+\frac{1}{\alpha}}]$. On these two stencils, we obtain two interpolations

$$p'_{j}(x) = u_{j} + \frac{\bar{u}_{j} - \bar{u}_{j-1}}{h}(x - x_{j})$$
(56)

and

$$p'_{j+1}(x) = \bar{u}_j + \frac{\bar{u}_{j+1} - \bar{u}_j}{h}(x - x_j)$$
(57)

with the smoothness indicators $S_j=(\bar{u}_j-\bar{u}_{j-1})^2$ and $S_{j+1}=(\bar{u}_{j+1}-\bar{u}_j)^2$ Then we can get the left-hand reconstruction

$$u_{L}(x) = \frac{\alpha_{0}}{\alpha_{0} + \alpha_{1}} p'_{j}(x) + \frac{\alpha_{1}}{\alpha_{0} + \alpha_{1}} p'_{j+1}(x)$$
(58)

where $\alpha_0 = \mathcal{C}_0/(\varepsilon + \mathit{IS}_j)^2$, $\alpha_1 = \mathcal{C}_1/(\varepsilon + \mathit{IS}_{j+1})$, \mathcal{C}_0 and \mathcal{C}_1 are the optimal weight of u at position x , given by solving

$$q^{3}(x, \bar{u}_{i-1}, \bar{u}_{i}, \bar{u}_{i+1}) = \sum_{k=0}^{1} C_{0} q_{0}(x, \bar{u}_{i-1+k}, \bar{u}_{i+k})$$
(59)

For convenient to understand, here we set $\beta=(x-x_i)/\Delta x$, C_0 and C_1 are

$$C_0 = 1 - \frac{\beta_a}{\beta} C_1 = \frac{\beta_a}{\beta} \tag{60}$$

where $\beta_a = 3\beta^2 + 3\beta - \frac{1}{4}$.

The we can get the subcell approximation of u in I_i as

$$p_{j}(x) = \sum_{l=0}^{2} a_{l} \left(\frac{x - x_{j+1/2}}{\Delta x}\right)^{l} \tag{61}$$