samba 公式推导

March 21, 2018

1. 二维控制方程

运动方程:

$$\frac{d(r,z)}{dt} = (u,v) \tag{1}$$

质量守恒:

$$\frac{dm}{dt} = 0 (2)$$

动量守恒方程:

$$\rho \frac{du}{dt} = \frac{\partial \sigma_{rr}}{\partial r} + \frac{\partial s_{rz}}{\partial z}$$

$$\rho \frac{dv}{dt} = \frac{\partial \sigma_{zz}}{\partial z} + \frac{\partial s_{rz}}{\partial r}$$
(3)

能量守恒方程:

$$\rho \frac{de}{dt} = \sigma_{rr} \frac{\partial u}{\partial r} + \sigma_{zz} \frac{\partial v}{\partial z} + s_{rz} \left(\frac{\partial u}{\partial z} + \frac{\partial v}{\partial r} \right)$$

$$= -p \frac{dV}{dt} + s_{rr} \frac{\partial u}{\partial r} + s_{zz} \frac{\partial v}{\partial z} + s_{rz} \left(\frac{\partial u}{\partial z} + \frac{\partial v}{\partial r} \right)$$

$$(4)$$

本构方程:

$$\frac{ds_{rr}}{dt} = 2\mu \left(\frac{\partial u}{\partial r} - \frac{1}{3} \nabla \cdot \vec{u} \right) + s_{rz} \left(\frac{\partial u}{\partial z} - \frac{\partial v}{\partial r} \right)
\frac{ds_{zz}}{dt} = 2\mu \left(\frac{\partial v}{\partial z} - \frac{1}{3} \nabla \cdot \vec{u} \right) - s_{rz} \left(\frac{\partial u}{\partial z} - \frac{\partial v}{\partial r} \right)
\frac{ds_{rz}}{dt} = \mu \left(\frac{\partial u}{\partial r} + \frac{\partial v}{\partial z} \right) + \frac{s_{rr} - s_{zz}}{2} \left(\frac{\partial u}{\partial z} - \frac{\partial v}{\partial r} \right)$$
(5)

2. 离散方法

2..1 时间离散: 预估校正方法

对于如下形式方程

$$\frac{\partial U}{\partial t} = F(U) \tag{6}$$

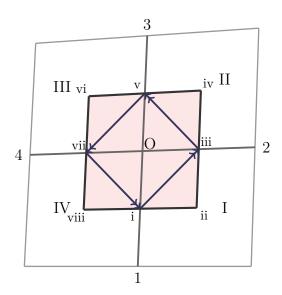


图 1: 控制单元示意图

预估步:

$$\frac{U^{n+\frac{1}{2}} - U^n}{\frac{1}{2}\Delta t} = F(U^n) \tag{7}$$

校正步:

$$\frac{U^{n+1} - U^n}{\Delta t} = F(U^{n+\frac{1}{2}}) \tag{8}$$

2...2 空间离散方法

2..2.1 运动方程离散

预估步:

$$\frac{(r,z)^{n+\frac{1}{2}} - (r,z)^n}{\frac{1}{2}\Delta t} = (u,v)^n$$
 (9)

和 Eq.(6) 不同, $(u,v)^{n+1/2}$ 不能直接由 $(r,z)^{n+1/2}$ 求出。这里需要由动量方程求得 $(u,v)^{n+1}$,然后取平均值

$$(u,v)^{n+\frac{1}{2}} = \frac{(u,v)^n + (u,v)^{n+1}}{2}$$
 (10)

校正步:

$$\frac{(r,z)^{n+1} - (r,z)^n}{\Delta t} = (u,v)^{n+\frac{1}{2}}$$
 (11)

2..2.2 动量方程离散

采用如图 2所示非结构四边形单元, Wilkins 在 1963 年首先通过有限体积方法得到 Wilkins 格式 [2]。点 i, ii, v, vii 分别为

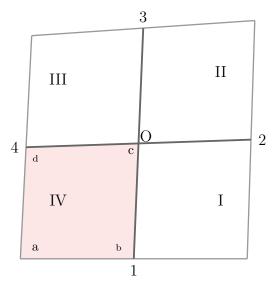


图 2: 控制单元示意图

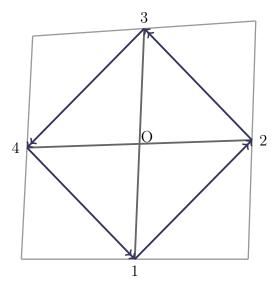


图 3: 控制单元示意图

线 O1, O2, O3, O4 的中点, ii, iv, vi, viii 分别为区域 I-IV 的几何中心。

对于动量离散方程 3, 在八边形面回路 $\Omega = i \rightarrow ii \rightarrow \cdots \rightarrow vii \rightarrow i$ 上积分:

$$\int_{\Omega} \rho \frac{du}{dt} d\Omega = \int_{\Omega} \frac{\partial \sigma_{rr}}{\partial r} + \frac{\partial s_{rz}}{\partial z} d\Omega$$
 (12)

$$\int_{\Omega} \rho \frac{dv}{dt} d\Omega = \int_{\Omega} \frac{\partial \sigma_{zz}}{\partial z} + \frac{\partial s_{rz}}{\partial r} d\Omega$$
 (13)

以方程 12为例, 左侧积分可以近似为

$$\int_{\Omega} \rho \frac{du}{dt} d\Omega = M \frac{du_o}{dt} \tag{14}$$

其中

$$M = \frac{1}{4} (A_I \rho_I + A_{II} \rho_{II} + A_{III} \rho_{III} + A_{IV} \rho_{IV})$$
 (15)

右侧积分根据 Green 公式:

$$\int_{\Omega} \operatorname{grad} f d\Omega = \oint_{\partial \Omega} f \overrightarrow{n} dl \tag{16}$$

有

$$\int_{\Omega} \frac{\partial \sigma_{rr}}{\partial r} + \frac{\partial s_{rz}}{\partial z} d\Omega = -\oint_{\partial \Omega} \sigma_{rr} dz + \oint_{\partial \Omega} s_{rz} dr$$
 (17)

由于线回路积分和所选回路无关,选择回路 $i \to iii \to v \to vii \to i$ 积分,以 $i \to iii$ 为例由于其平行且为 $\overline{12}$ 的一半,积分

$$\int_{vii}^{i} \sigma_{rr} dz \approx \frac{1}{2} \sigma_{zzI} (z_2 - z_1)$$
 (18)

同理可得

$$-\oint_{\partial\Omega}\sigma_{rr}dz + \oint_{\partial\Omega}s_{rz}dr = \frac{1}{2}\sum_{i=1}^{4}s_{rzi}(r_{i+1} - r_i) - \sigma_{rri}(z_{i+1} - z_i)$$
(19)

得到 wilkins 格式:

$$\frac{du_o}{dt} = \frac{1}{2M} \left[\sum_{i=1}^4 s_{rzi} (r_{i+1} - r_i) - \sigma_{rri} (z_{i+1} - z_i) \right]$$
(20)

该格式同样可以通过有限元方法得出 (Lascaux 1973 年) [1]。 控制体同样取如图 2,以 I 区为例,在该区通过虚功原理,可以 化作有限元的单元积分:

$$\int_{\Omega_I} \rho \frac{du}{dt} \phi_k d\Omega = \int_{\Omega_I} \left(\frac{\partial \sigma_{rr}}{\partial r} + \frac{\partial s_{rz}}{\partial z} \right) \phi_k d\Omega \tag{21}$$

其中

$$\phi_i = \frac{1}{4} (1 + \xi_i \xi) (1 + \eta_i \eta) \tag{22}$$

为基函数 , i = a, b, c, d 其中 $(\xi, \eta) = (-1, -1), (1, -1), (1, 1), (-1, 1)$

$$u = \sum_{i=a}^{d} u_i \phi_i$$

$$r = \sum_{i=a}^{d} r_i \phi_i$$

$$z = \sum_{i=a}^{d} z_i \phi_i$$
(23)

公式 21左侧可以化为:

$$\int_{\Omega_{I}} \rho \frac{du}{dt} \phi_{k} d\Omega = \int_{\Omega_{I}} \rho \sum_{i=a}^{d} \frac{du_{i}}{dt} \phi_{i} \phi_{k} dr dz$$

$$= \sum_{i=a}^{d} \frac{du_{i}}{dt} \int_{-1}^{1} \int_{-1}^{1} \rho \phi_{i} \phi_{k} J d\xi d\eta$$
(24)

其中

$$J = \left\| \begin{array}{cc} \frac{\partial r}{\partial \xi} & \frac{\partial r}{\partial \eta} \\ \frac{\partial z}{\partial \xi} & \frac{\partial z}{\partial \rho} \end{array} \right\| \tag{25}$$

右侧以第一项为例:

$$\int_{\Omega_{I}} \frac{\partial \sigma_{rr}}{\partial r} + \phi_{k} d\Omega =
\int_{\Omega_{I}} \frac{\partial (\sigma_{rr}\phi_{k})}{\partial r} d\Omega - \int_{\Omega_{I}} \frac{\partial \phi_{k}}{\partial r} \sigma_{rr} d\Omega
= - \int_{\partial\Omega_{I}} \sigma_{rr}\phi_{k} dz - \int_{\Omega_{I}} \frac{\partial \phi_{k}}{\partial r} \sigma_{rr} d\Omega$$

$$= - \int_{\partial\Omega_{I}} \sigma_{rr}\phi_{k} dz - \int_{\Omega_{I}} \frac{1}{J} \frac{\partial(z, \phi_{k})}{\partial(\xi, \eta)} \sigma_{rr} J d\xi d\eta
= - \int_{\partial\Omega_{I}} \sigma_{rr}\phi_{k} dz - \int_{-1}^{1} \int_{-1}^{1} \frac{\partial(z, \phi_{k})}{\partial(\xi, \eta)} \sigma_{rr} d\xi d\eta$$

2..2.3 能量方程离散

采用有限体积方法,和动量方程离散相似,以偏导数 $\frac{\partial u}{\partial r}$ 为例,通过 Green 积分可以化为:

$$\frac{\partial u}{\partial r} = -\frac{1}{A} \oint_{1 \to 2 \to 1} u dz$$

$$\approx -\frac{1}{A} (\frac{1}{2} (u_1 + u_2)(z_2 - z_1) + \frac{1}{2} (u_2 + u_3)(z_3 - z_2)$$

$$+ \frac{1}{2} (u_3 + u_4)(z_4 - z_3) + \frac{1}{2} (u_4 + u_1)(u_1 - u_4))$$

$$= -\frac{1}{A} ((u_1 - u_3)(z_2 - z_4) + (u_2 - u_4)(z_3 - z_1))$$
(27)

并将其记作 \bar{u}_r 。

能量方程空间离散为

$$\frac{dE}{dt} = -p^{n} \frac{dV}{dt} + V^{n} + s_{r} r^{n} \bar{u}_{r}^{n} + s_{z} z^{n} \bar{v}_{z}^{n} + s_{rz}^{n} (\bar{u}_{z}^{n} + \bar{v}_{r}^{n})$$
 (28)

2..2.4 本构方程离散

和能量方程离散类似,以 dsrr 为例

$$\frac{ds_{rr}}{dt} = 2\mu \left(\bar{u}_r^n - \frac{1}{3} (\bar{u}_r^n + \bar{v}_z^n) \right) + s_{rz}^n (\bar{u}_z^n - \bar{v}_r^n)$$
 (29)

参考文献

- [1] P Lascaux. Application of the finite elements method in two-dimensional hydrodynamics using the lagrange variables. Technical report, CEA Centre d'Etudes de Limeil.
- [2] Mark L Wilkins. Calculation of elastic-plastic flow. Technical report, California Univ Livermore Radiation Lab, 1963.