

High peak power Ti:sapphire lasers

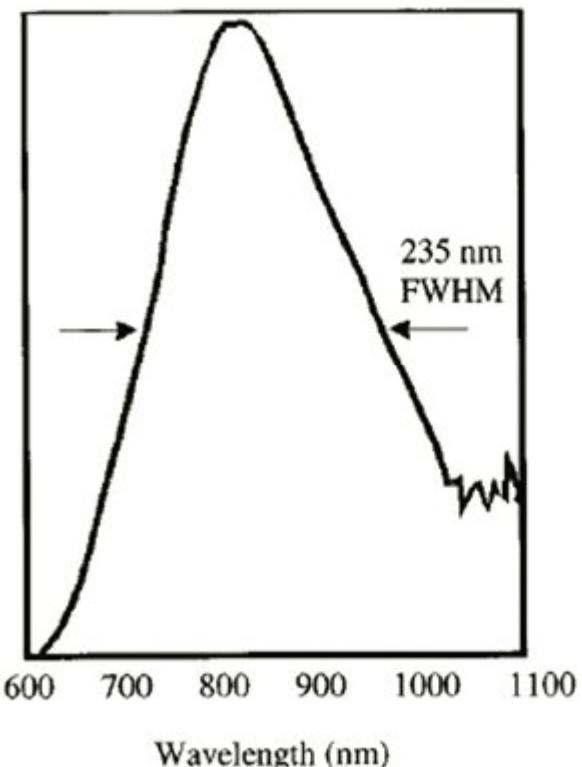
Mikhail P. Kalashnikov



*Max-Born-Institut für Nichtlineare Optik und Kurzzeitspektroskopie
Berlin, Germany*

Properties of Ti:Sapphire

- very high damage threshold ($8\text{-}10 \text{ J/cm}^2$)
- high saturation fluence $\sim 0.9 \text{ J/cm}^2$
- high thermal conductivity
- suitable peak gain cross section of $\sigma = 2.7 \cdot 10^{-19} \text{ cm}^2$

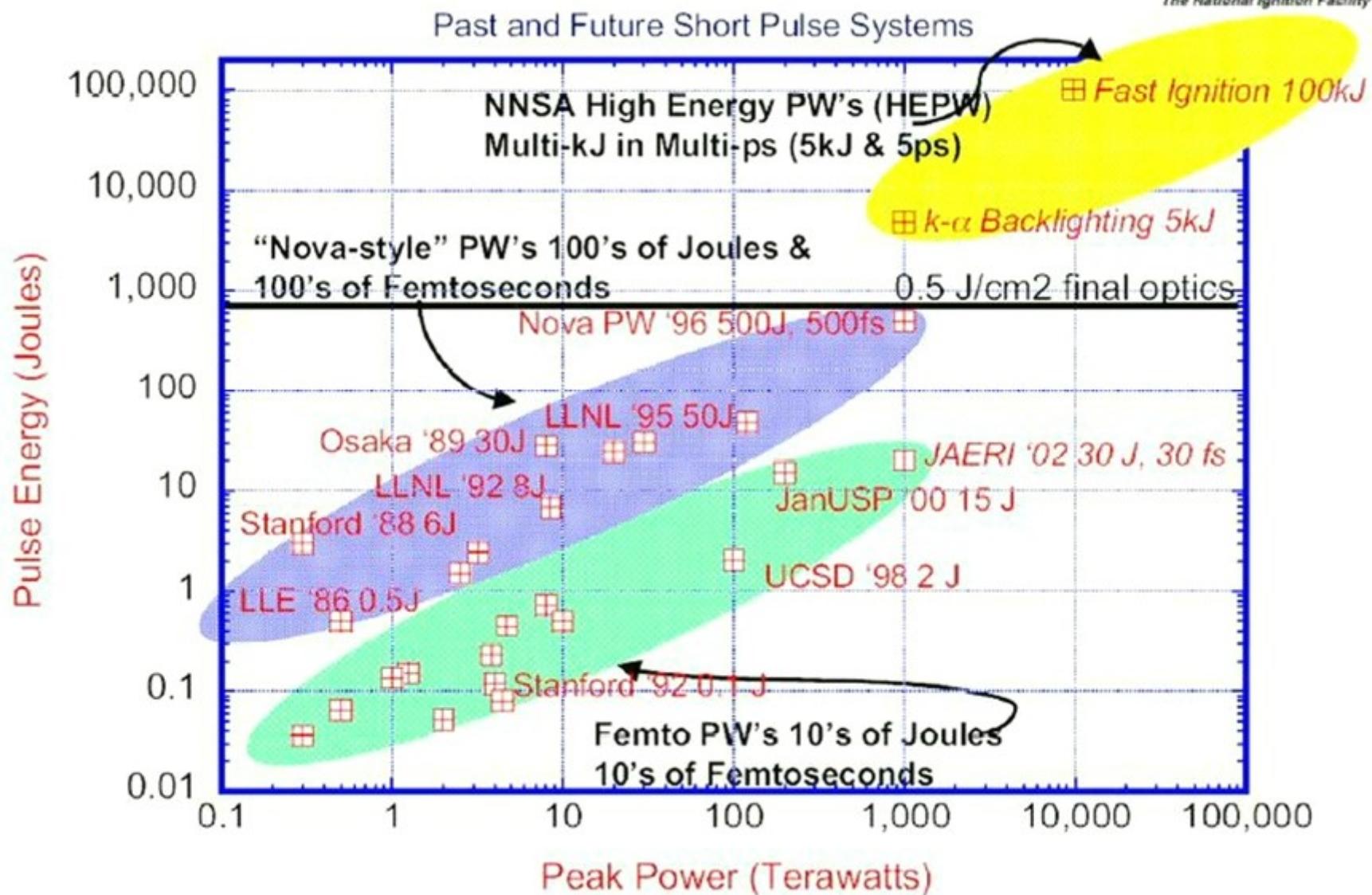


Maximum absorption at $\sim 500 \text{ nm}$, thus pumped by 2ω of YAG lasers at $\lambda \approx 532 \text{ nm}$

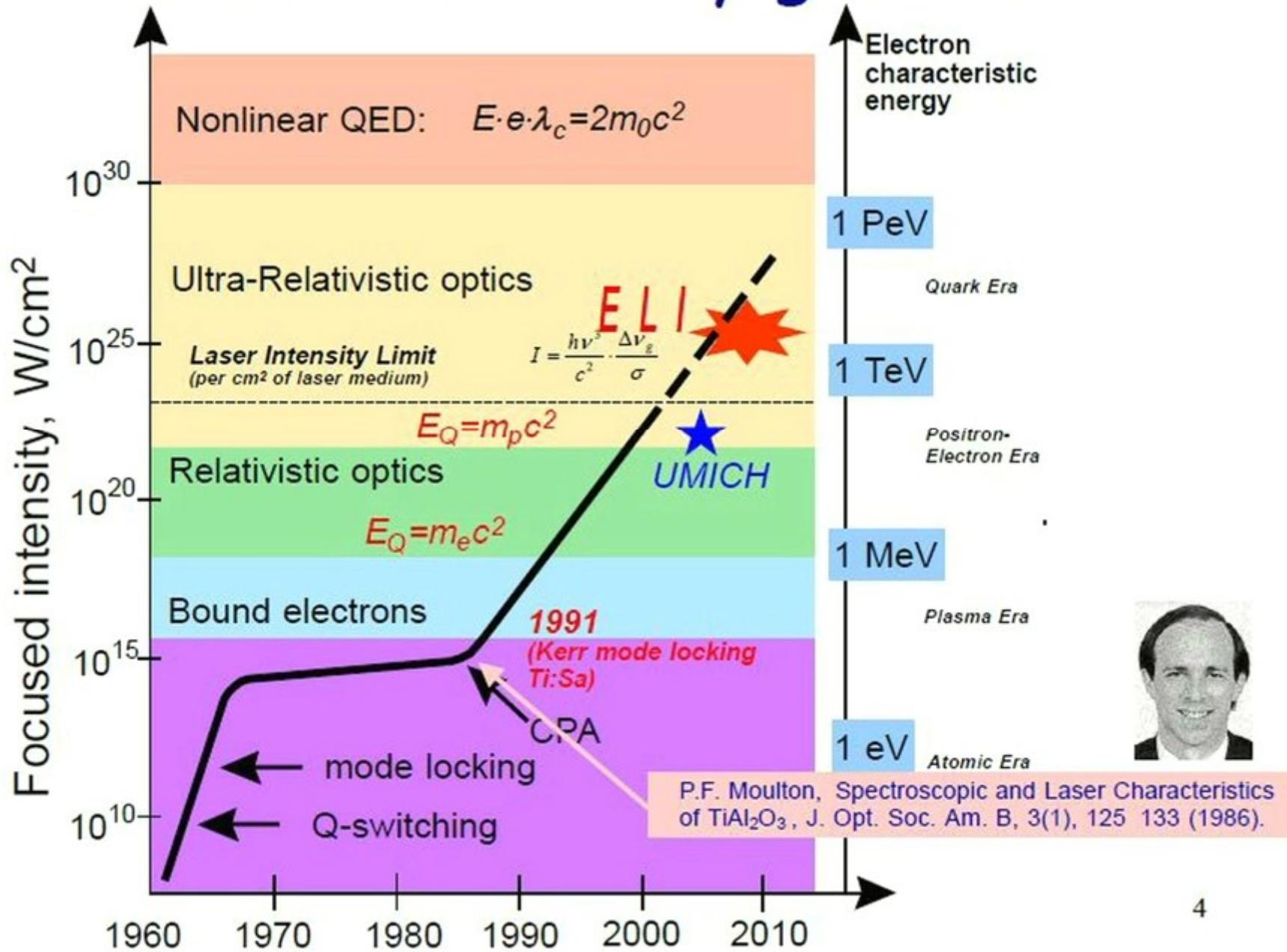
Three Classes of Petawatt Lasers



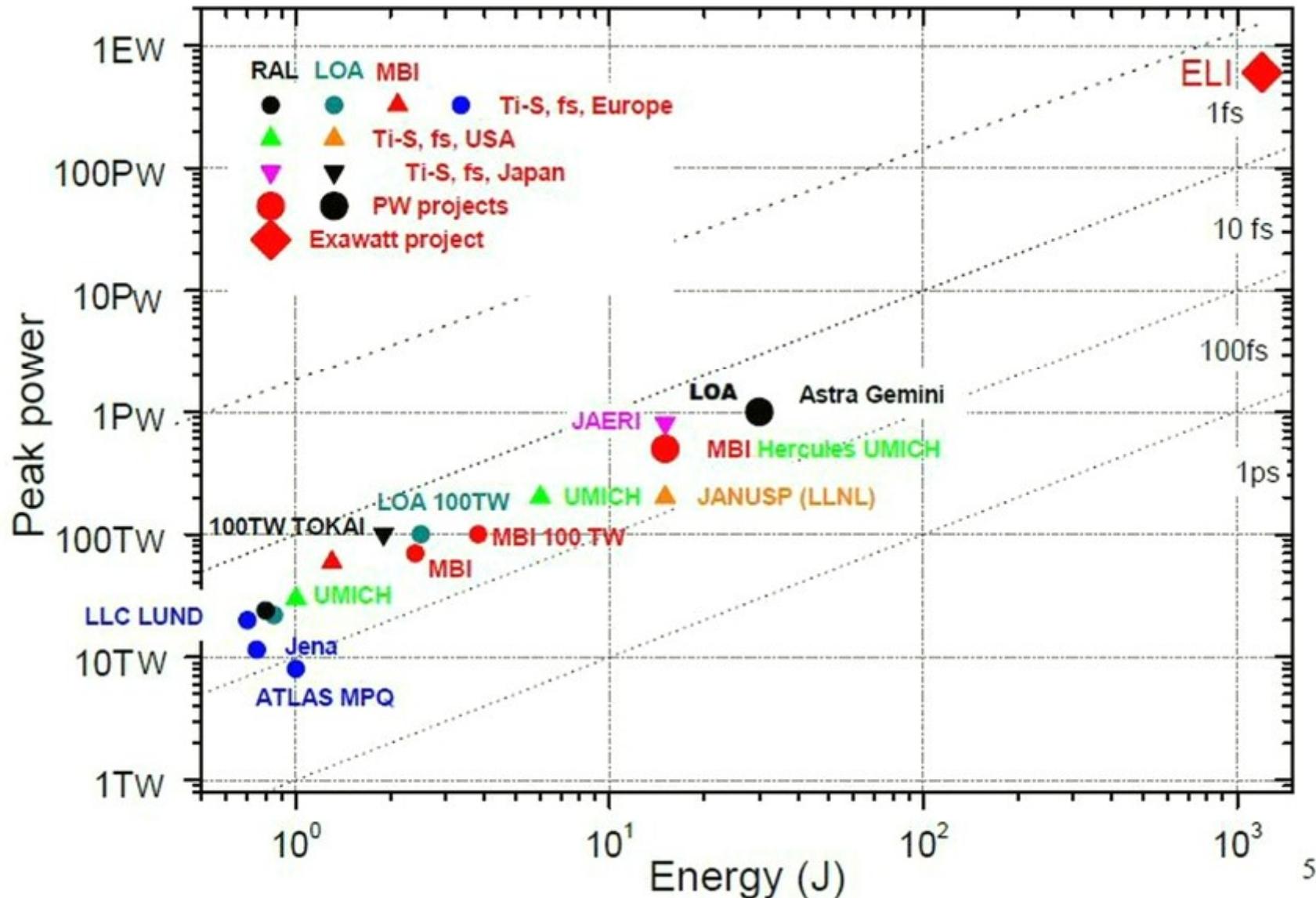
The National Ignition Facility



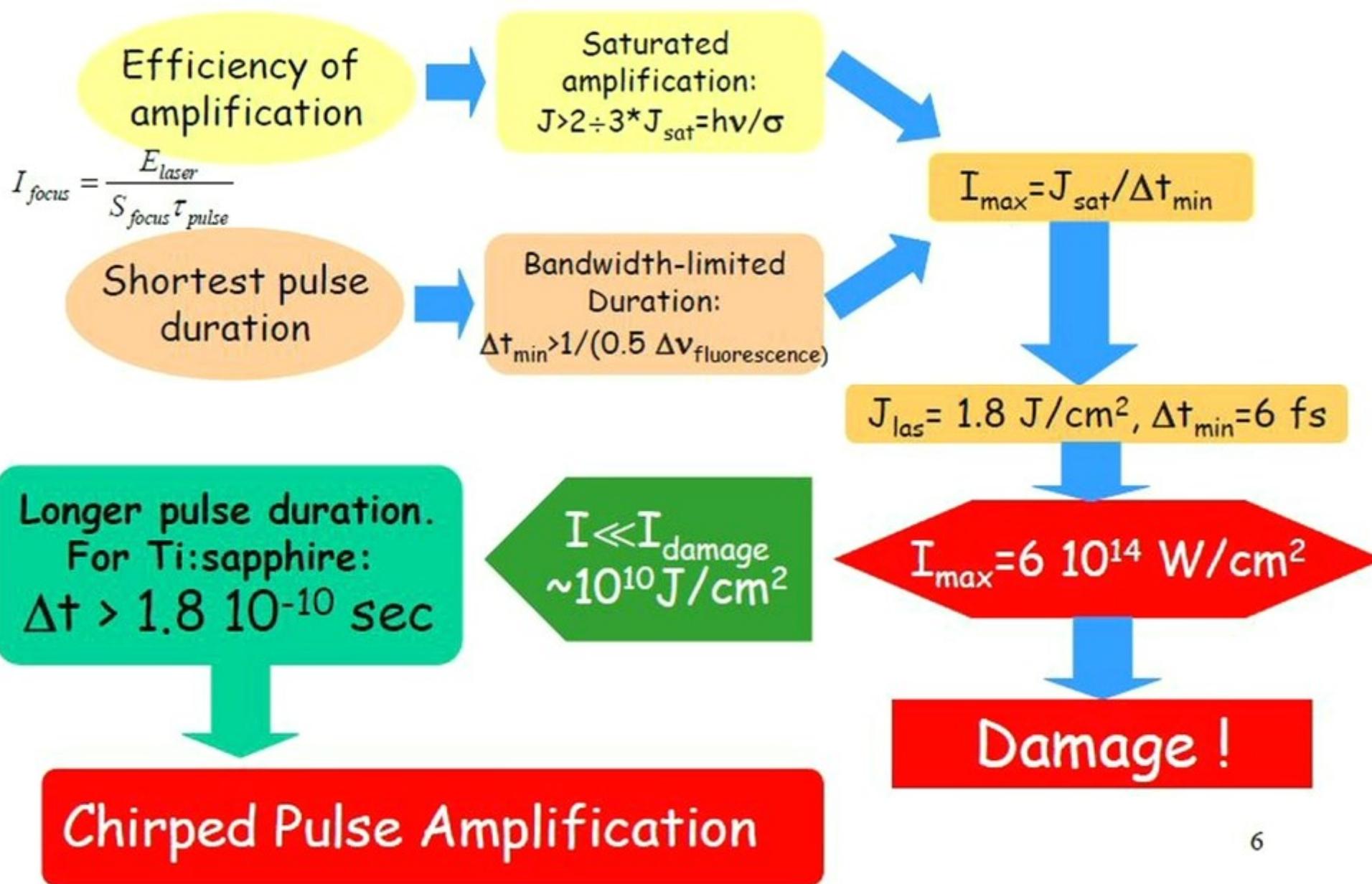
Laser Intensity growth



World Ti:sapphire high power lasers



Chirped pulse amplification



Pulse chirping

Passing through dispersive medium the pulse gets stretched:

Undispersed Gaussian pulse

after traveling through a positively dispersing medium, M

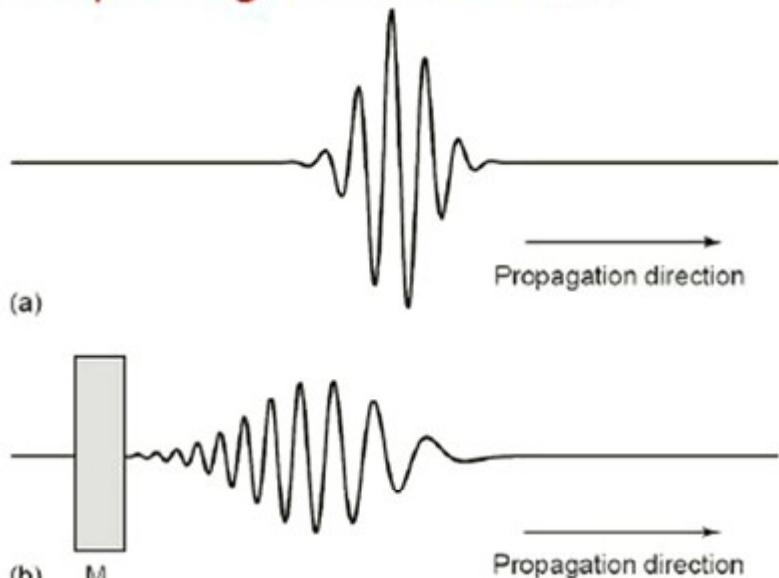
$$\tilde{E}(\omega) = \sqrt{S(\omega)} \exp[-i\varphi(\omega)]$$

↑ Spectrum ↑ Spectral phase

$$\varphi(w) = \varphi(w_0) + (w - w_0)\varphi'(w_0) + \frac{1}{2}(w - w_0)^2\varphi''(w_0)$$

$$+ \frac{1}{6}(w - w_0)^3\varphi'''(w_0) + \frac{1}{24}(w - w_0)^4\varphi''''(w_0) + \dots$$

$$\frac{\tau_{\text{out}}}{\tau_{\text{in}}} = 1 + \frac{\varphi''^2}{\tau_{\text{in}}^4} 16(\ln 2)^2$$



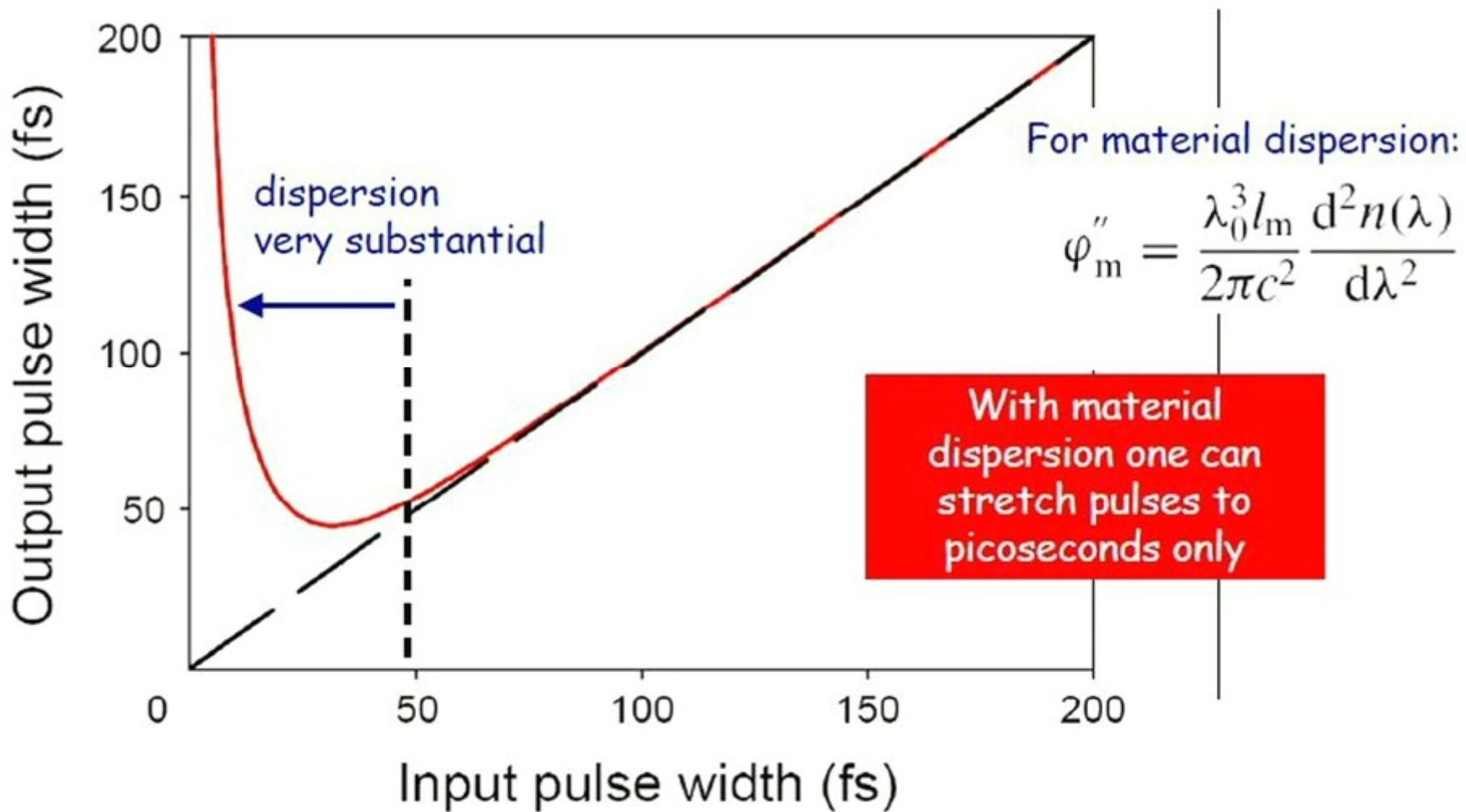
The instantaneous frequency:

$$\omega(t) = \omega_0 - d\phi/dt$$

$\varphi'(w_0)$ is the group delay,
 $\varphi''(w_0)$ the group velocity dispersion (GVD)

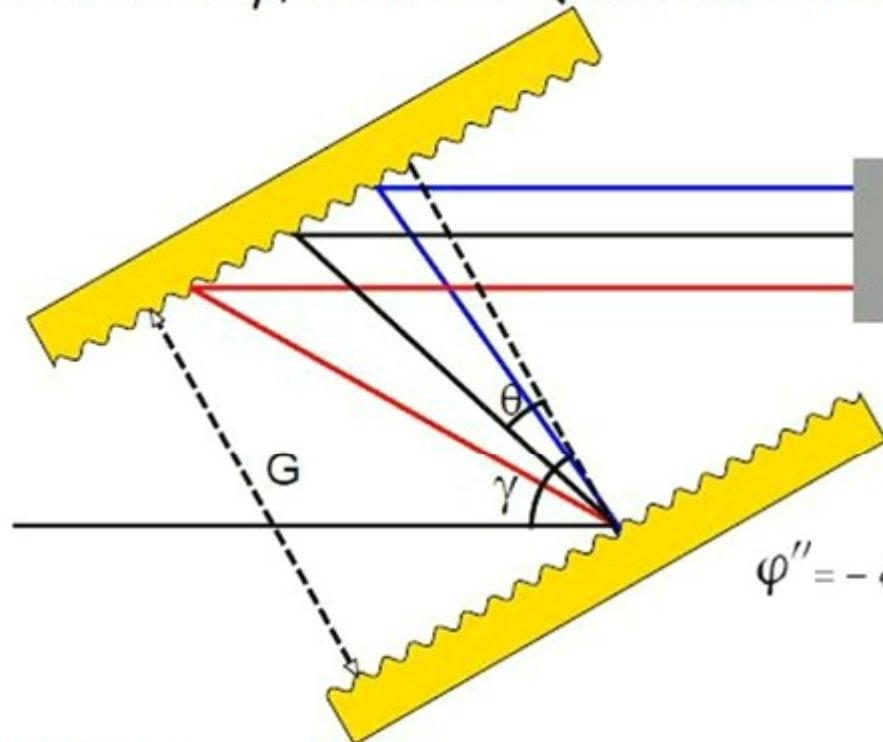
$\varphi'''(w_0)$ and $\varphi''''(w_0)$ -
are TOD and FOD

Dispersion of 10 mm BK7



Pulse stretching (diffraction gratings)

E. B. Treacy, IEEE J. Quantum Electron. QE-5, 454 (1969)



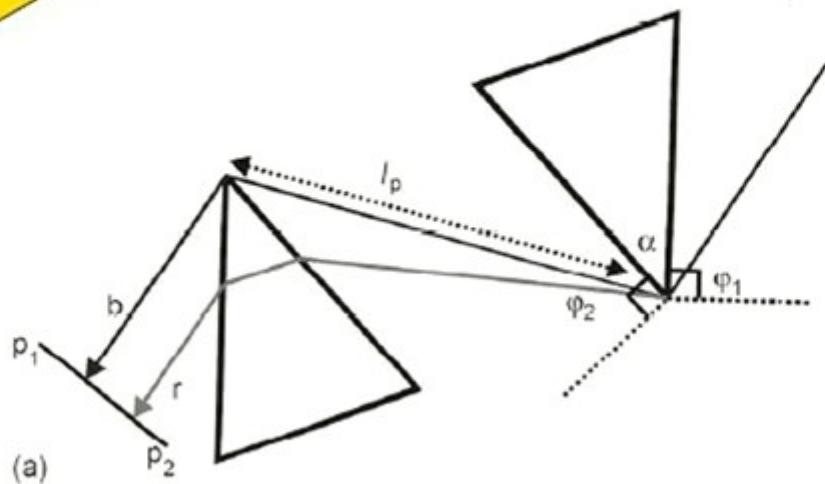
Diffraction gratings
compressor

$$\varphi' = -\frac{m^2 \lambda^3}{2\pi c^2 d^2 \cos^2 \theta} b, \quad b = -\frac{G}{\cos \theta(\lambda_0)}.$$

$$\varphi'' = -\phi_2 \frac{\lambda}{2\pi c} \left[1 + \frac{m\lambda}{d} \frac{\sin \theta}{\cos^2 \theta} \right]$$

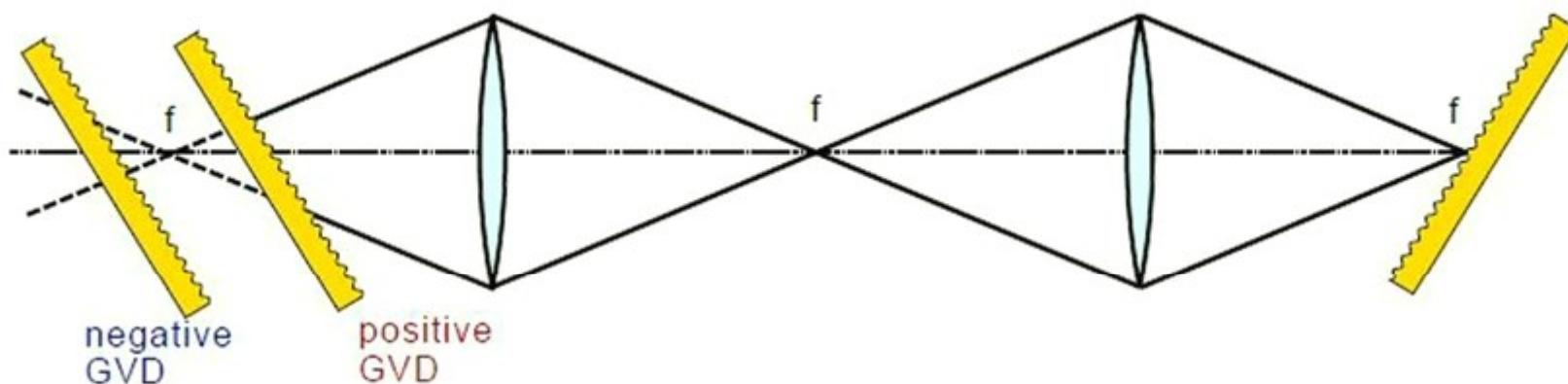
$$\varphi''' = -\phi_3 \frac{3\lambda^2}{4\pi^2 c^2} \left\{ 4 + 8 \frac{m\lambda}{d} \frac{\sin \theta}{\cos^2 \theta} + \frac{\lambda^2}{d^2} [1 + \tan^2 \theta (6 + 5 \tan^2 \theta)] \right\}$$

Efficiency ~ 74%
possible



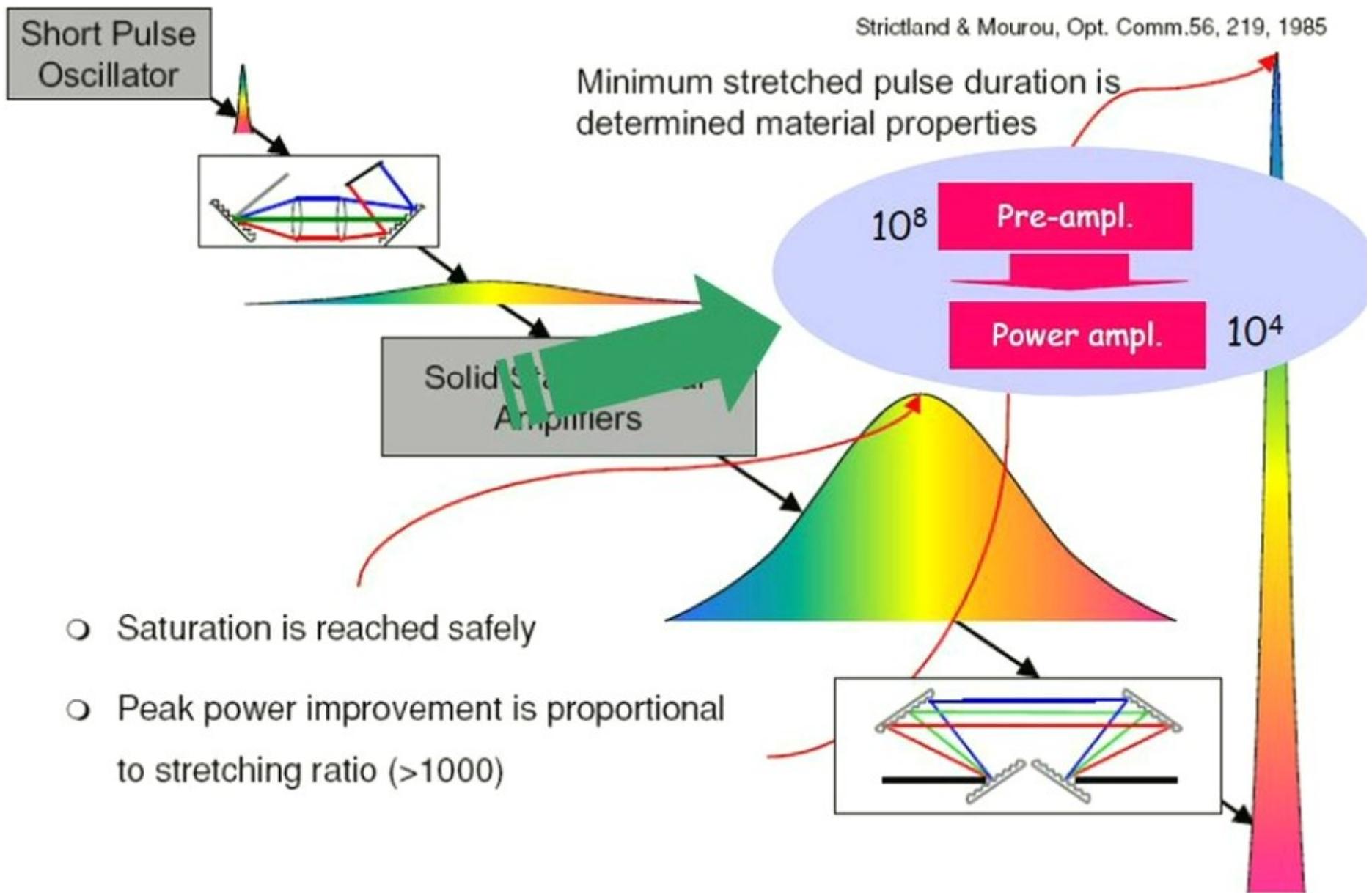
stretcher

O. E. Martinez, J. Opt. Soc. Am. B 3, 929 (1986)

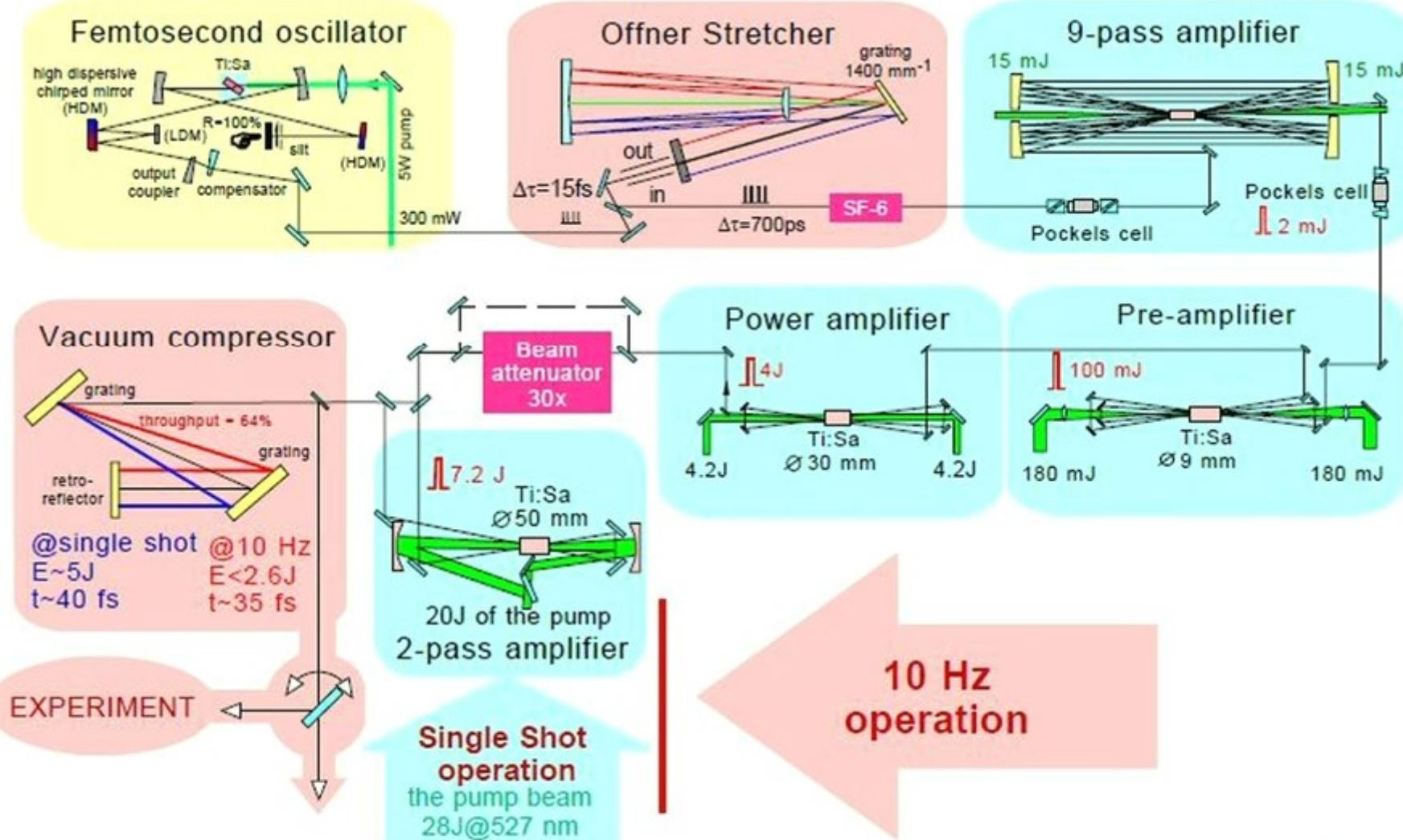


Matching between the Martinez and Treacy grating pair arrangements. The input grating is imaged by a telescope of magnification 1, to form a "virtual" grating parallel to the second grating. The distance b between the two gratings, real and virtual, can be continuously adjusted from positive to negative

Chirped Pulse Amplification

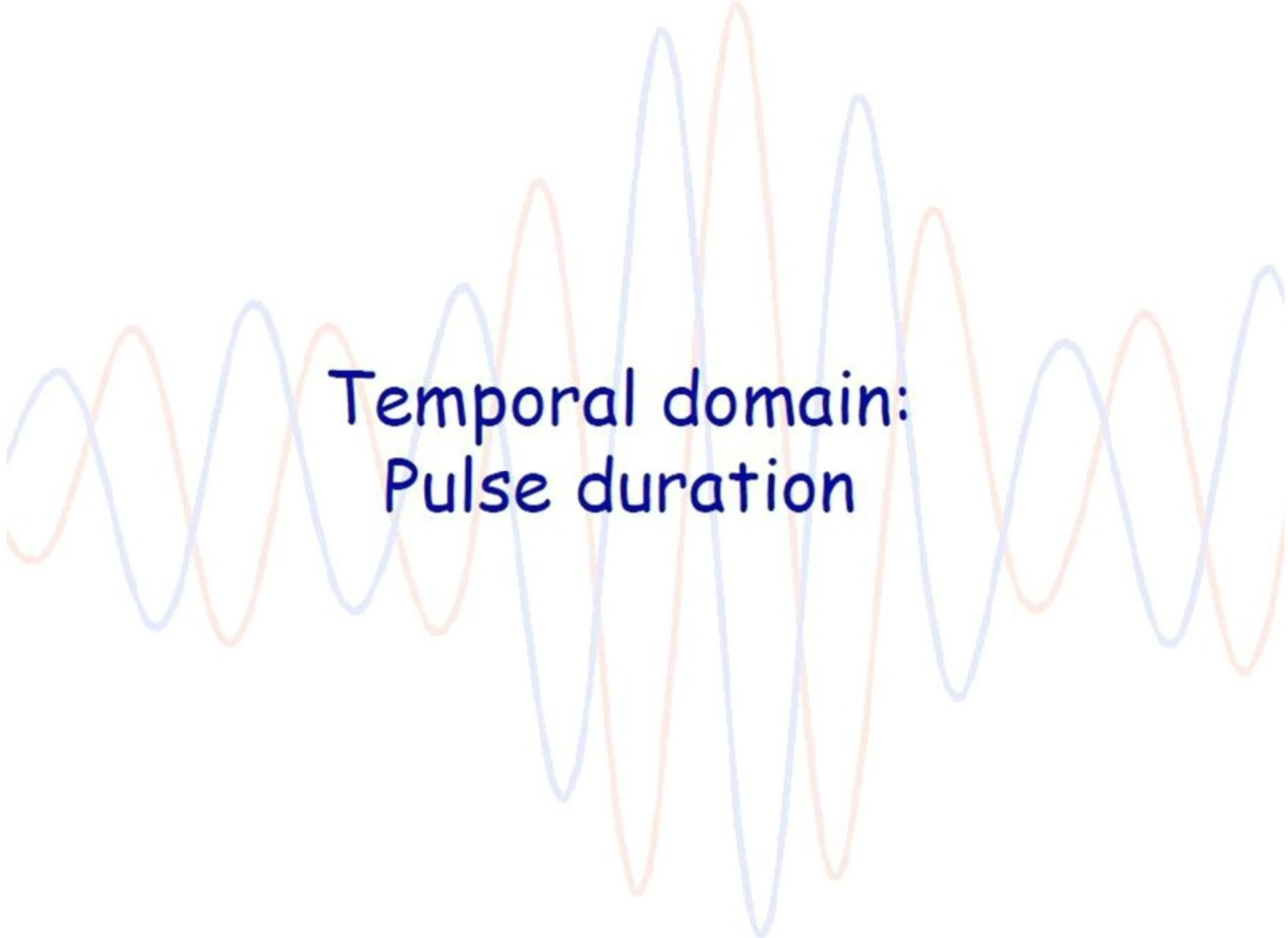


100 TW MBI Ti:Sa laser



MBI 100TW Ti:sapphire laser





Temporal domain:
Pulse duration

Errors of recompression

To reach short recompressed pulses one needs to compensate for the spectral phase:

$$\phi_{\text{str}}(\omega) + \phi_{\text{comp}}(\omega) + \phi_{\text{med}}(\omega) = 0$$

Typically in Ti:sapphire lasers the stretching starts from 10–15 fs and the stretching factor reaches the value of

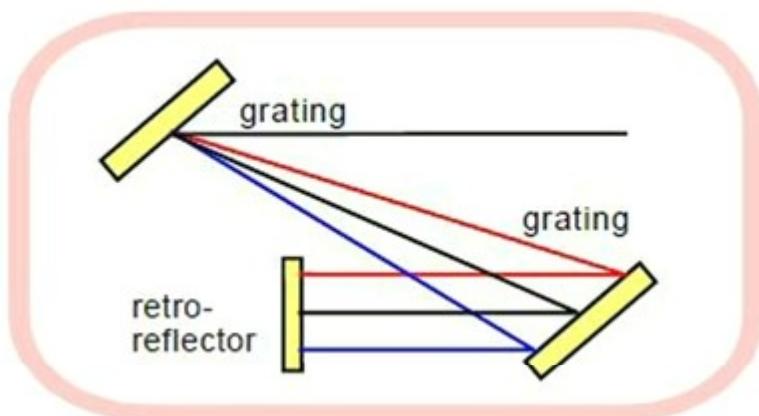
$$\tau_{\text{str}}/\tau_{\text{Ti}} = 5 \cdot 10^4$$

In this case:

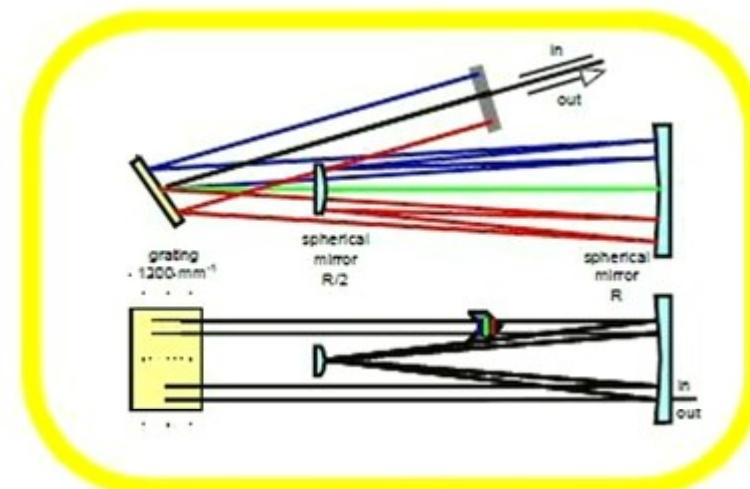
- one needs to consider spectral phase including 4th order of dispersion
- diffraction gratings have only 3 variable parameters:
 - angle of incidence
 - grating constant
 - spacing between the gratings
- different materials need to be taken into account

Compressor and stretchers

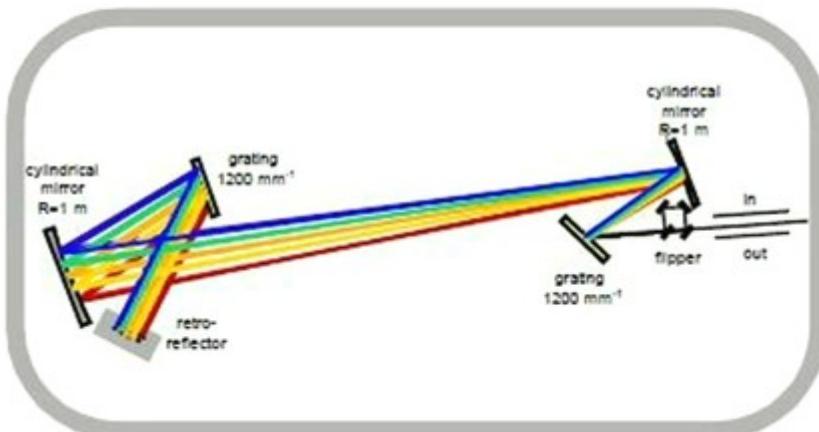
Compressor



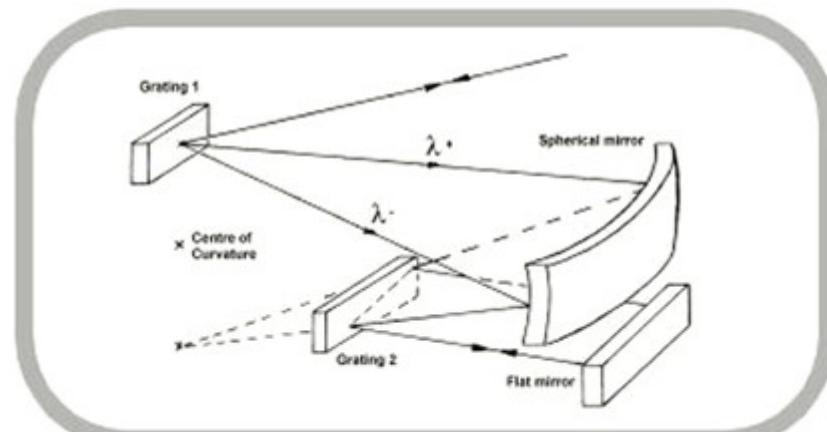
Öffner



Aberrational



RAL



Errors of recompression

Most important errors of the stretcher and compressor:

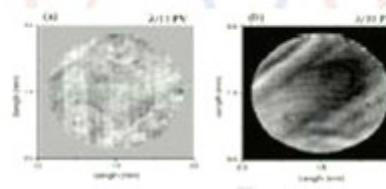
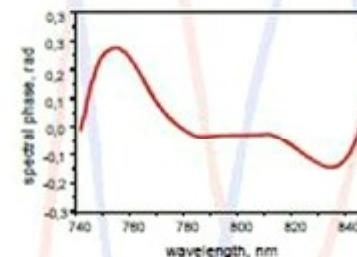
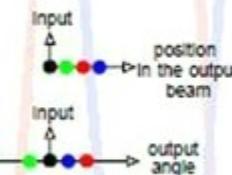
- variation of group delay over beam aperture and spatially varying dispersion

residual spectral phase

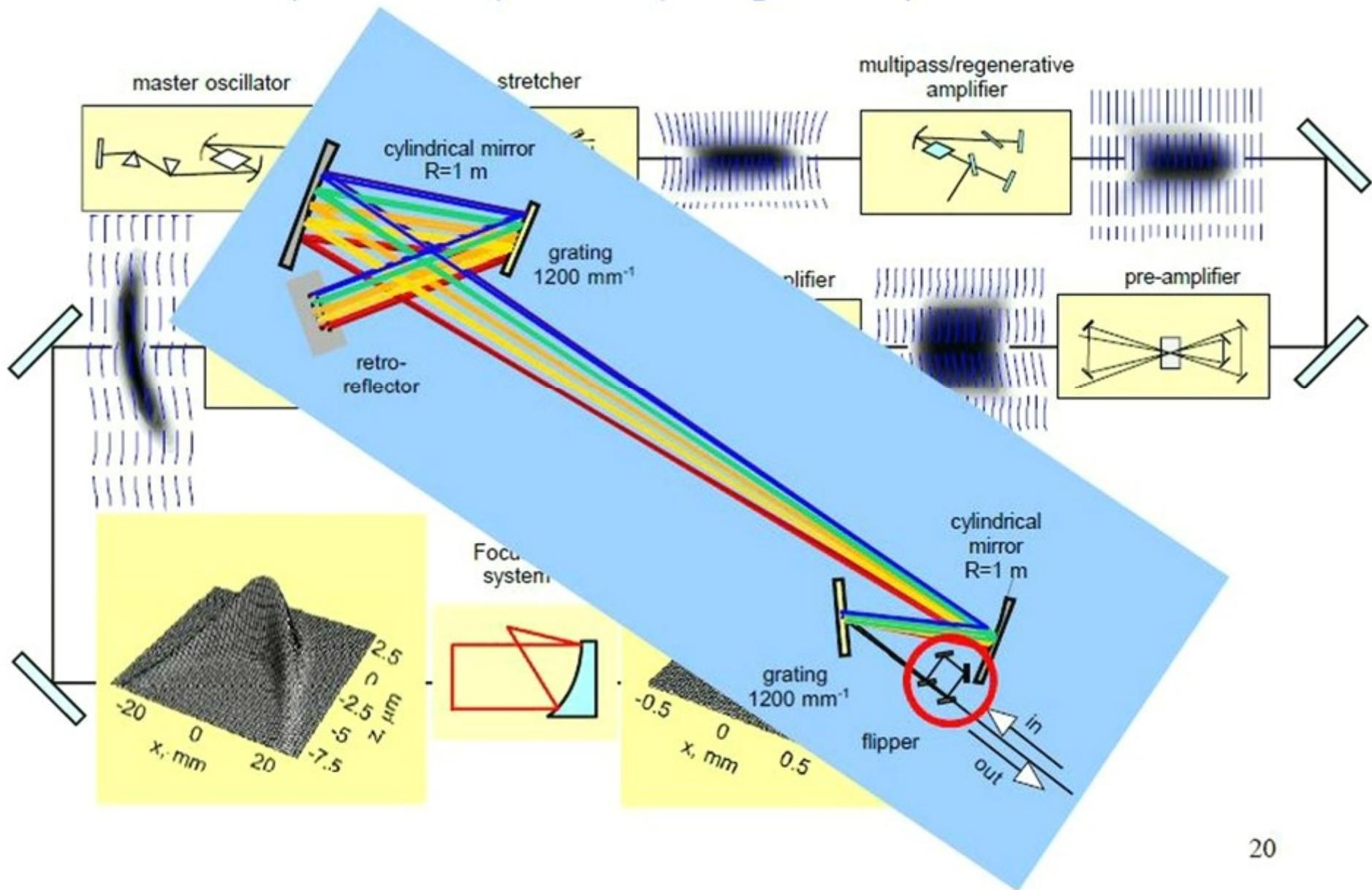
spatial and angular chirp

- spectral clipping

- spectral phase 'noise'



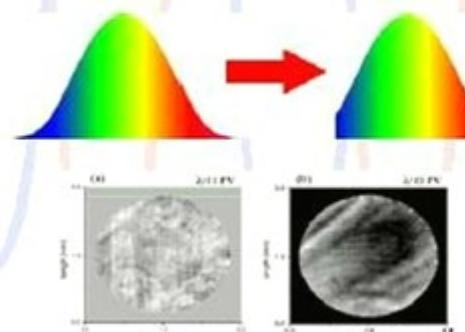
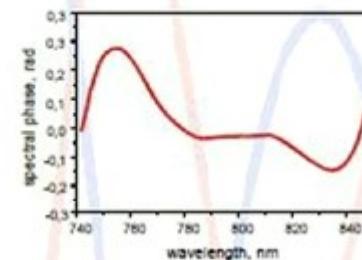
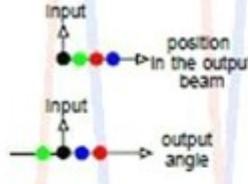
Spatially varying dispersion



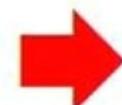
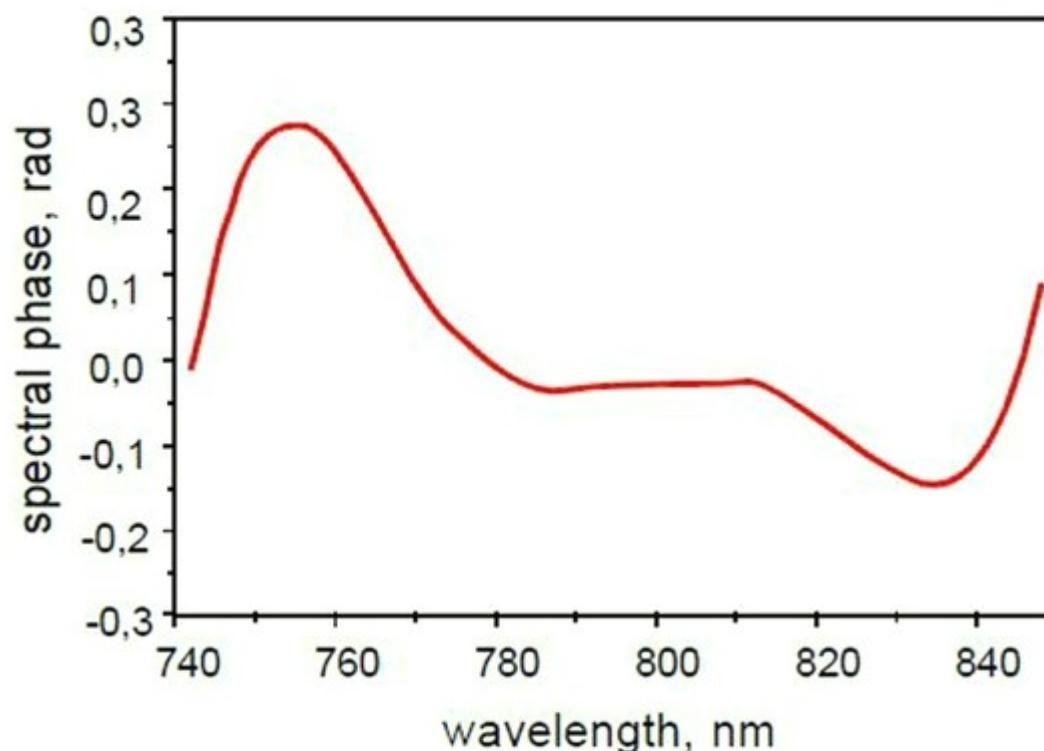
Errors of recompression

Most important errors of the stretcher and compressor:

- group delay over beam aperture and spatially varying dispersion
- residual spectral phase
- spatial and angular chirp
- spectral clipping
- spectral phase 'noise'



Residual phase

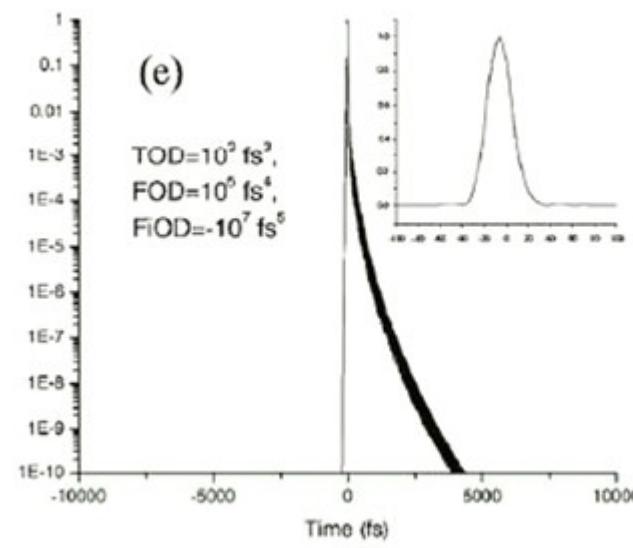
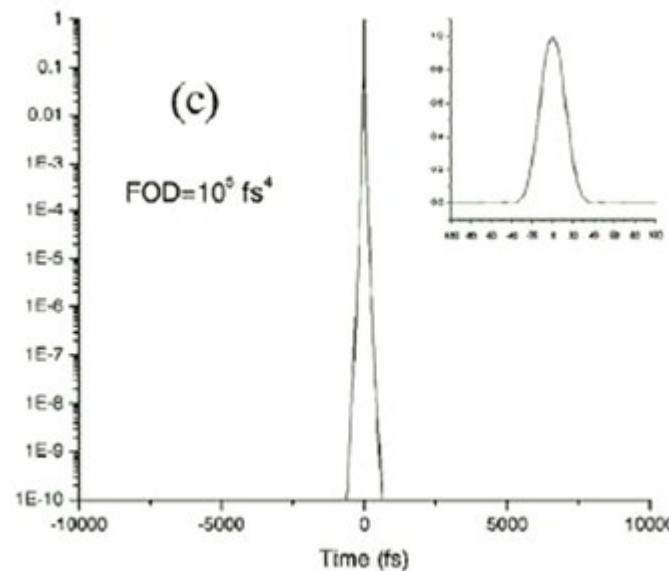
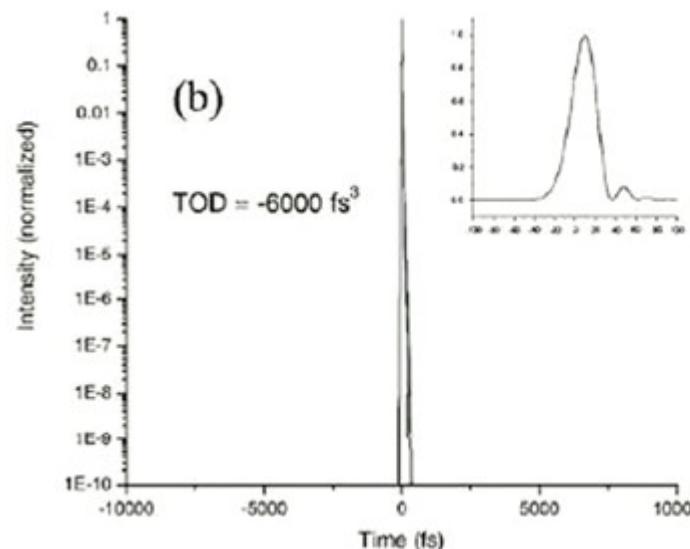
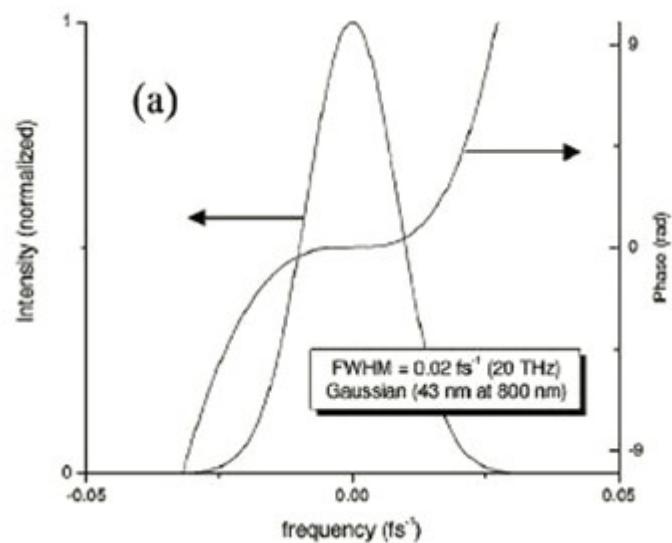


Reshaping of
the pulse

High orders of dispersion (FOD) and higher are usually compensated by:

- using diffraction gratings with different constants in the stretcher and compressor
- adding materials
- stretcher geometry

Influence of spectral phase



K.-H. HONG, B. HOU, J.A. NEES, E. POWER, G.A. MOUROU, Generation and measurement of $>10^8$ intensity contrast ratio in a relativistic kHz chirped-pulse amplified laser, Appl. Phys. B 81, 447-457 (2005)

Dazzler

acousto-optic programmable dispersive filter (AOPDF)

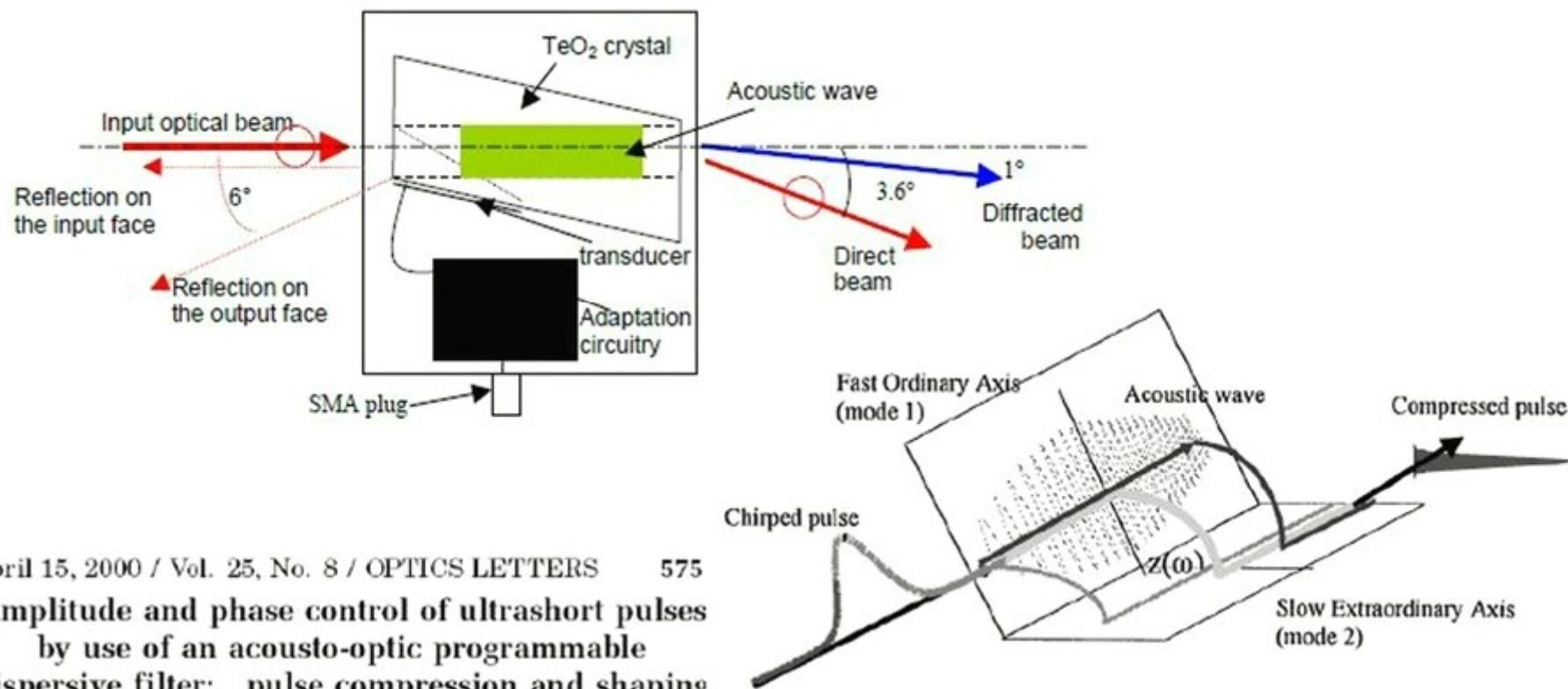


Fig. 1. Schematic of the AOPDF.

April 15, 2000 / Vol. 25, No. 8 / OPTICS LETTERS 575
**Amplitude and phase control of ultrashort pulses
 by use of an acousto-optic programmable
 dispersive filter: pulse compression and shaping**

F. Verluse and V. Laude

Laboratoire Central de Recherches, Thomson-CSF, Domaine de Corbeville, F-91494 Orsay Cedex, France, and
 Laboratoire pour l'Utilisation des Lasers Intenses, Ecole Polytechnique, 91128 Palaiseau Cedex, France

Z. Cheng and Ch. Spielmann

Photonics Institute, Vienna University of Technology, Gußhausstraße 27-29/387, A-1040 Vienna, Austria

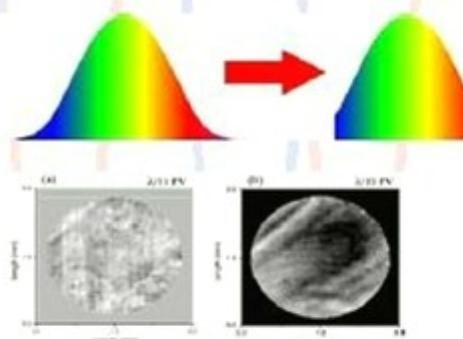
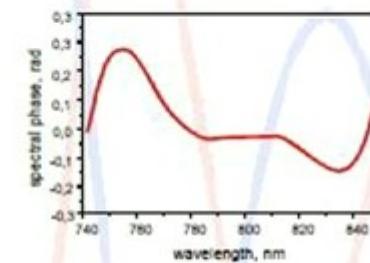
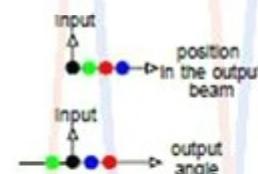
P. Tournois

Fastlite, Xtec, Ecole Polytechnique, 91128 Palaiseau Cedex, France

Errors of recompression

Most important errors of the stretcher and compressor:

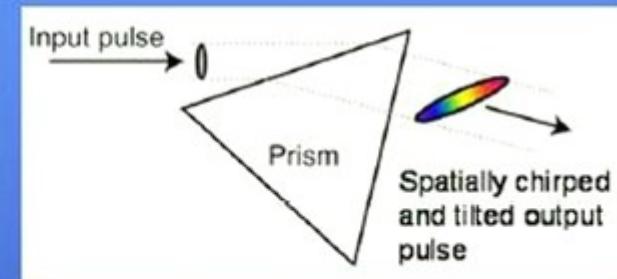
- group delay over beam aperture and spatially varying dispersion
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- spectral phase 'noise'



What causes angular dispersion in a CPA laser?

Prism pair in the oscillator

- Slightly different apex angle
- Non-parallel refractive surfaces

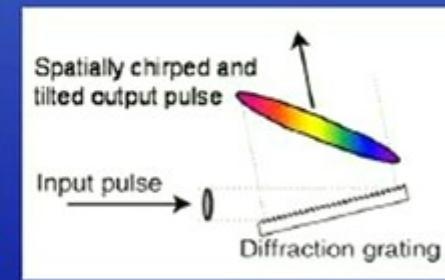


Slightly wedged optical components

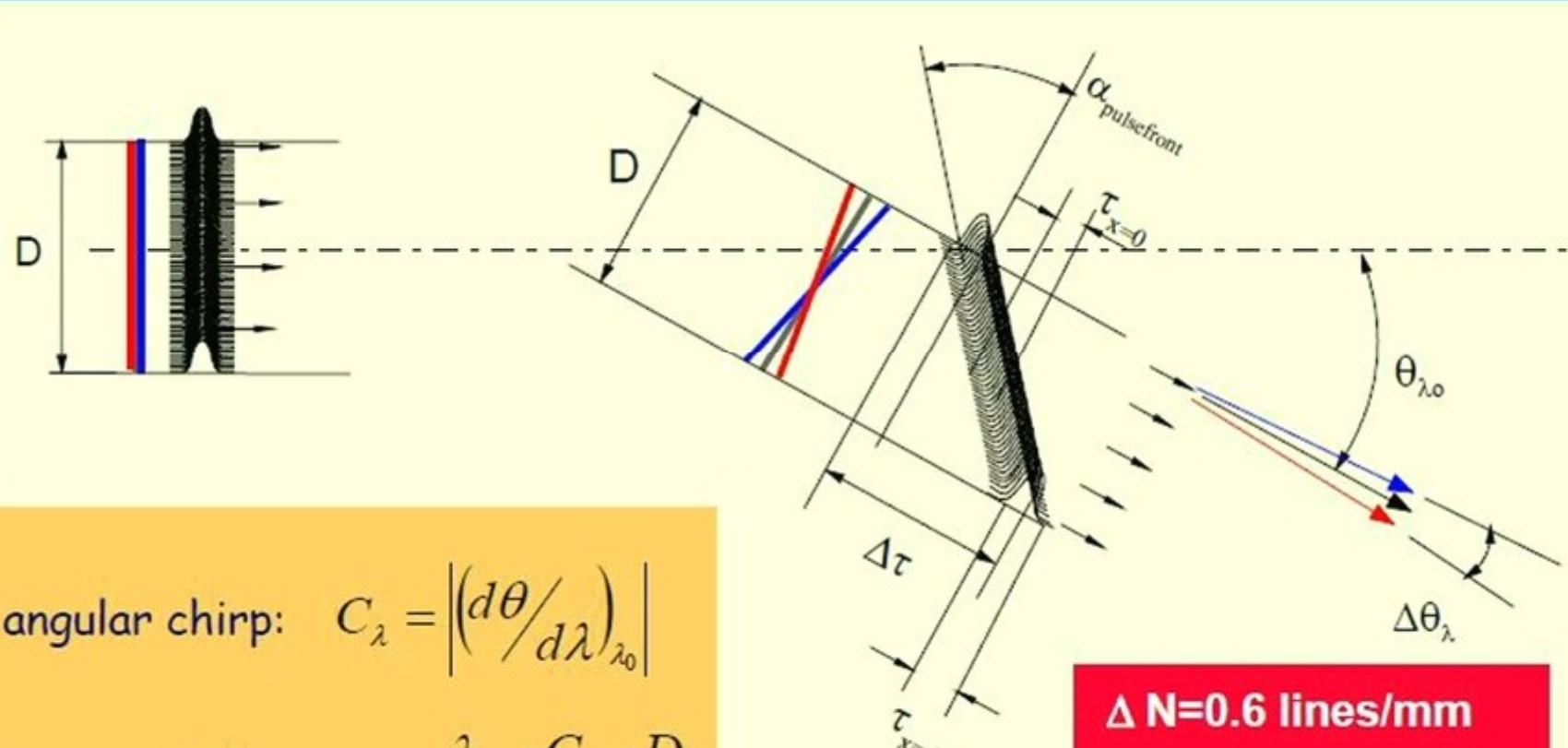
- Non-precise set-up of the output coupler (osc.)
- Surfaces of the Ti:S crystals (osc., ampl.)

Grating nonparallelism in the stretcher/compressor

Diffraction gratings with slightly different constant



Tilt of the recompressed pulse front coming from the angular chirp



$$\text{angular chirp: } C_\lambda = \left| \left(\frac{d\theta}{d\lambda} \right)_{\lambda_0} \right|$$

$$\text{temporal tilt: } \Delta\tau = \frac{\lambda_0 \cdot C_\lambda \cdot D}{c}$$

$\Delta N = 0.6 \text{ lines/mm}$

$\Delta\Theta_{\lambda_{780-840}} = 0.2 \text{ mrad}$

$\Theta_{\lambda_0} = 2.76 \text{ mrad}$

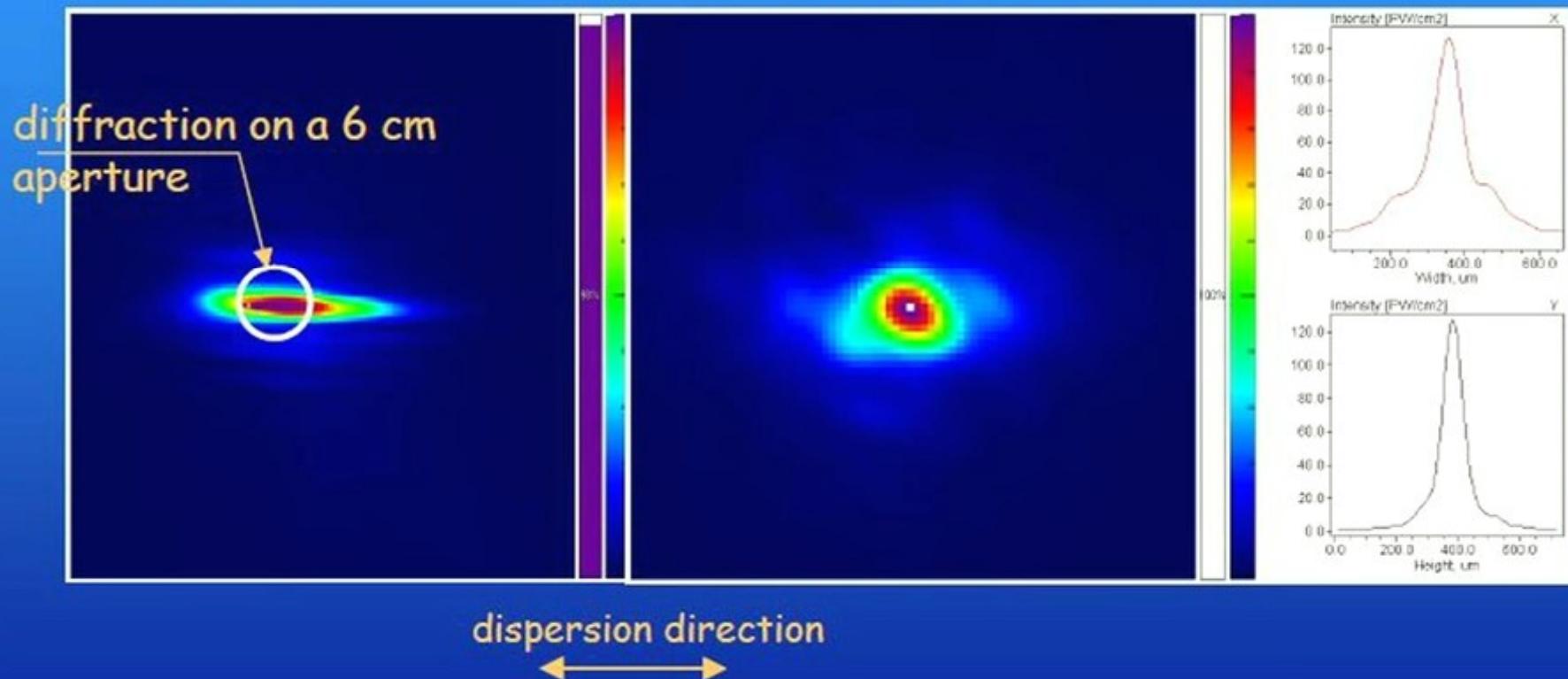
$\Delta\tau = 530 \text{ fs}$

Far-field distribution

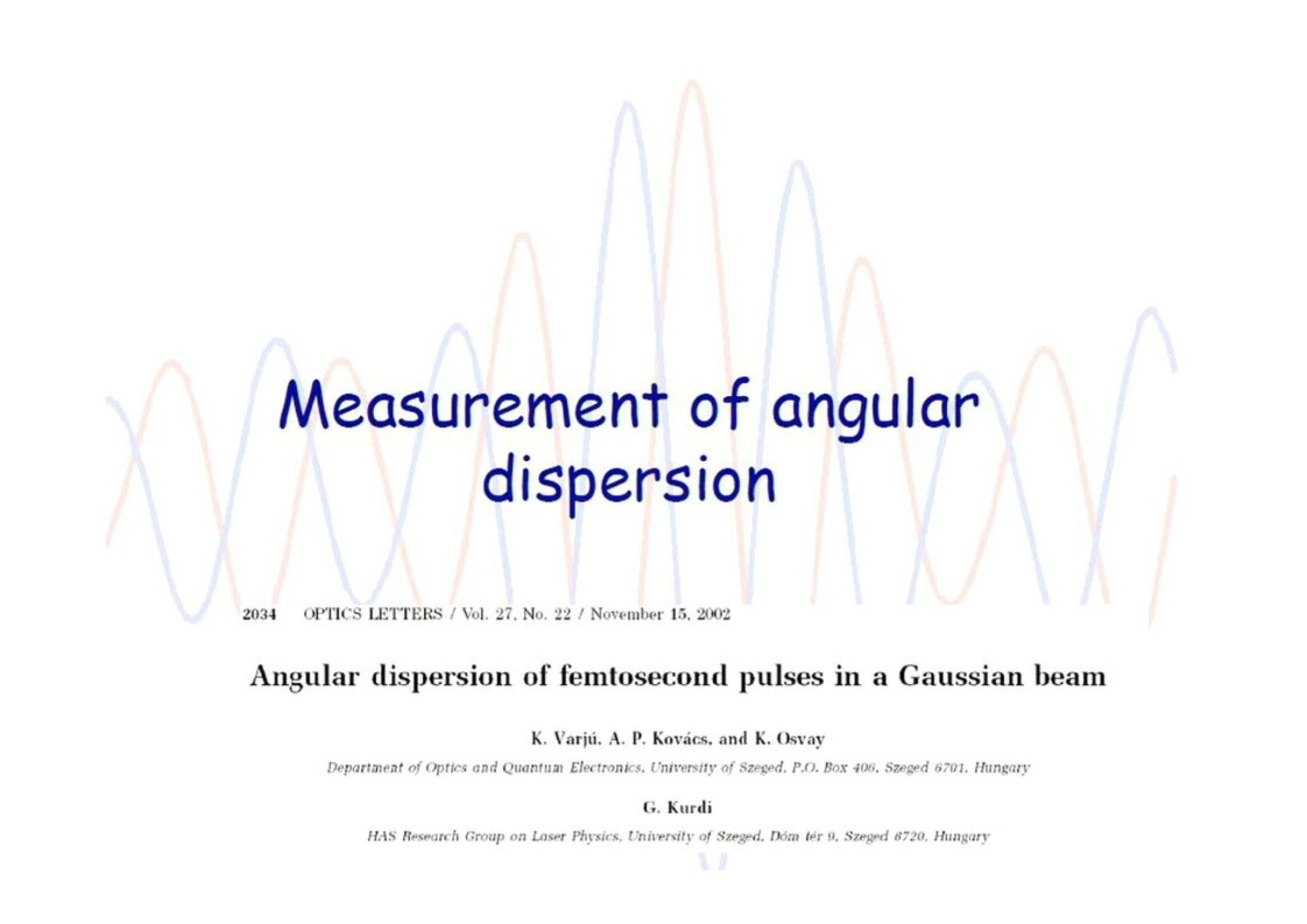
The diffraction gratings have different constants ($\Delta N = 0.6$ lines/mm).

before

after correction



Diffraction gratings are not parallel to each other



Measurement of angular dispersion

2034 OPTICS LETTERS / Vol. 27, No. 22 / November 15, 2002

Angular dispersion of femtosecond pulses in a Gaussian beam

K. Varjú, A. P. Kovács, and K. Osvay

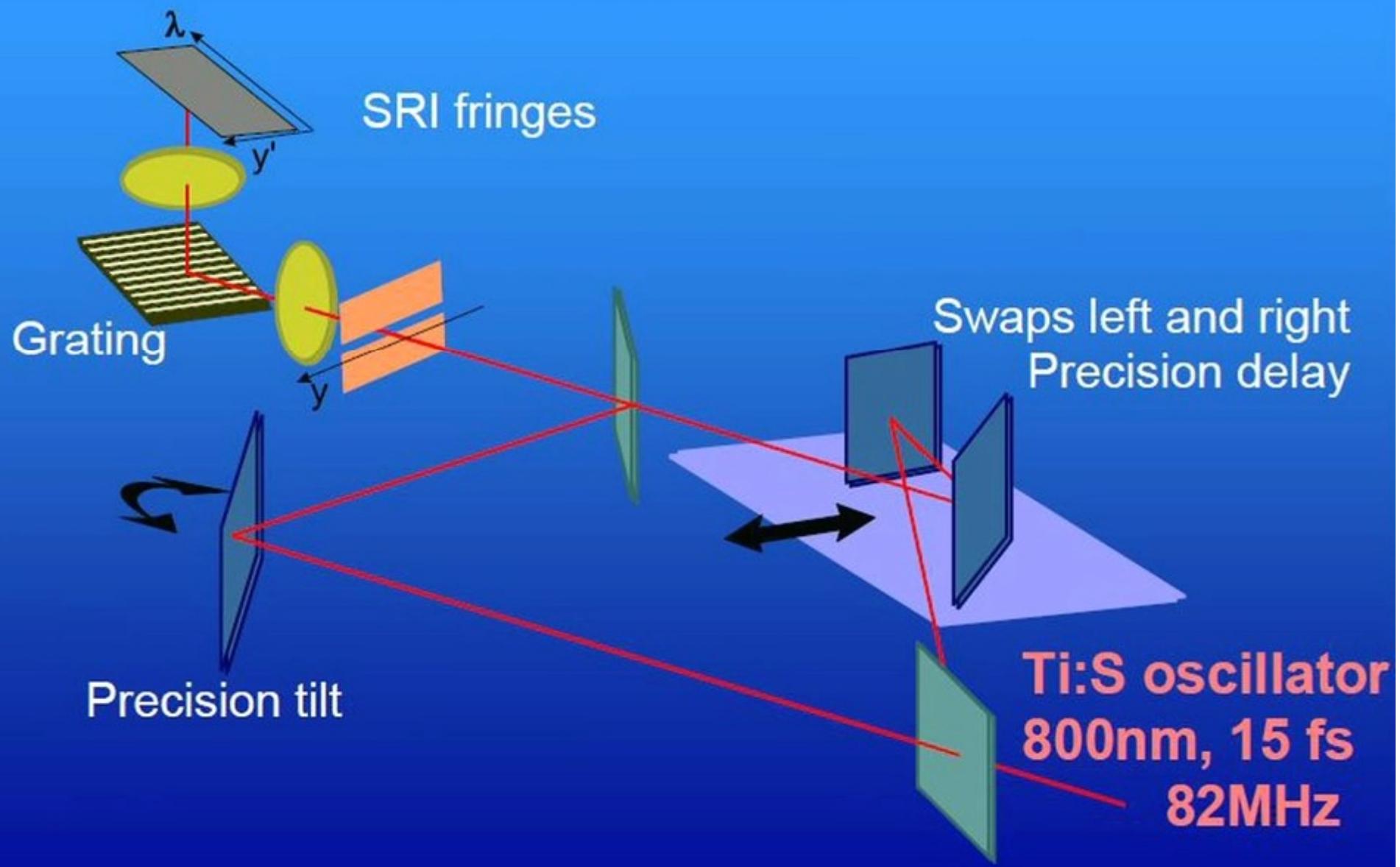
Department of Optics and Quantum Electronics, University of Szeged, P.O. Box 406, Szeged 6701, Hungary

G. Kurdi

HAS Research Group on Laser Physics, University of Szeged, Dóm tér 9, Szeged 6720, Hungary

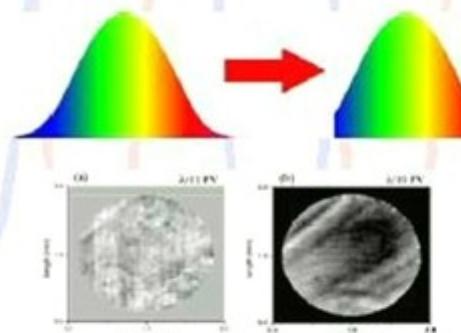
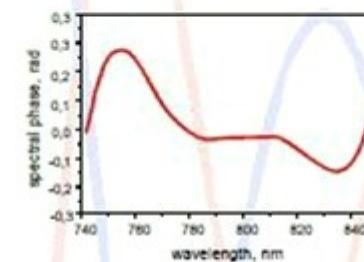
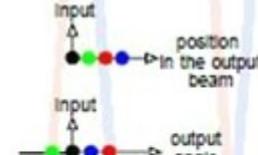


Experimental setup: Mach-Zender interferometer

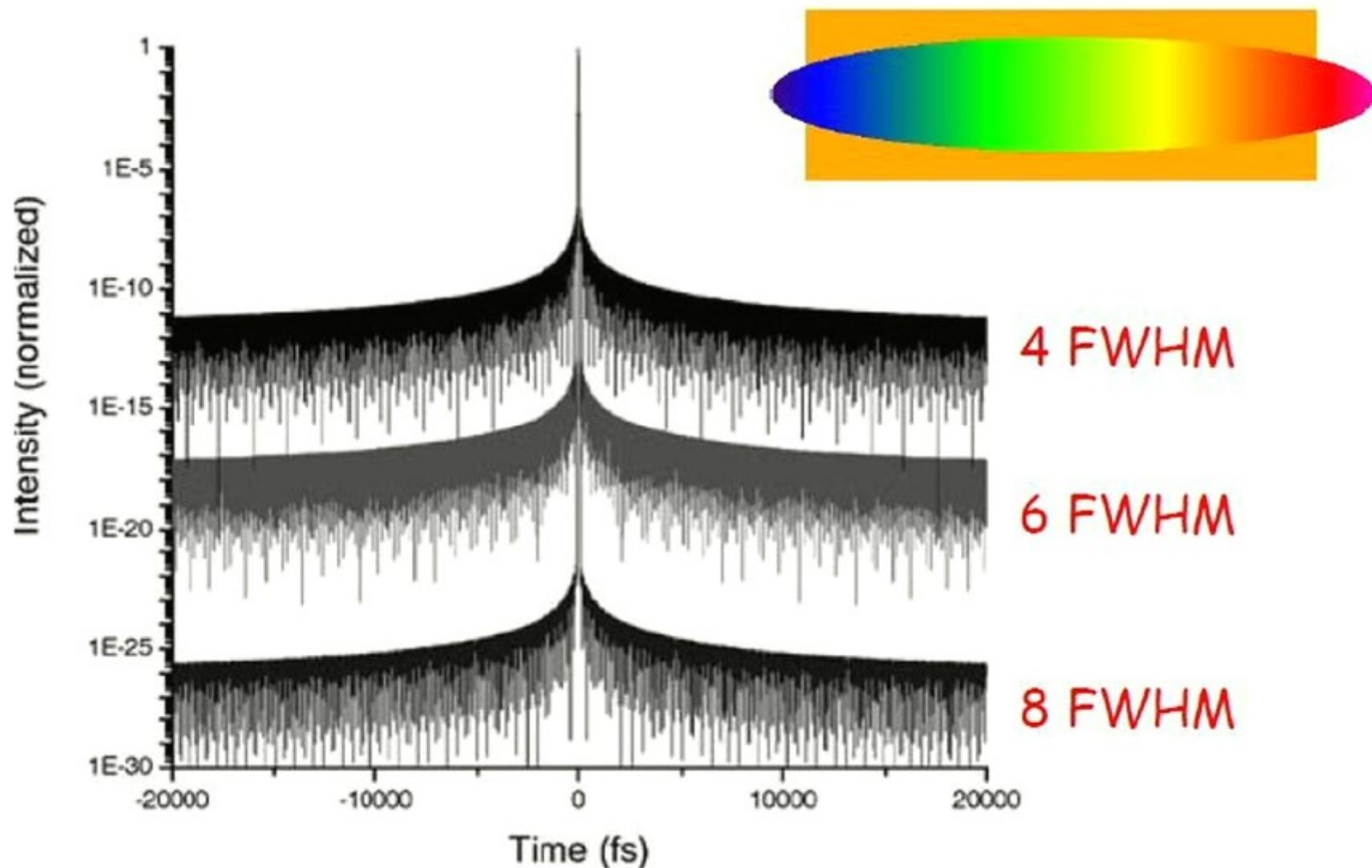


Errors of recompression

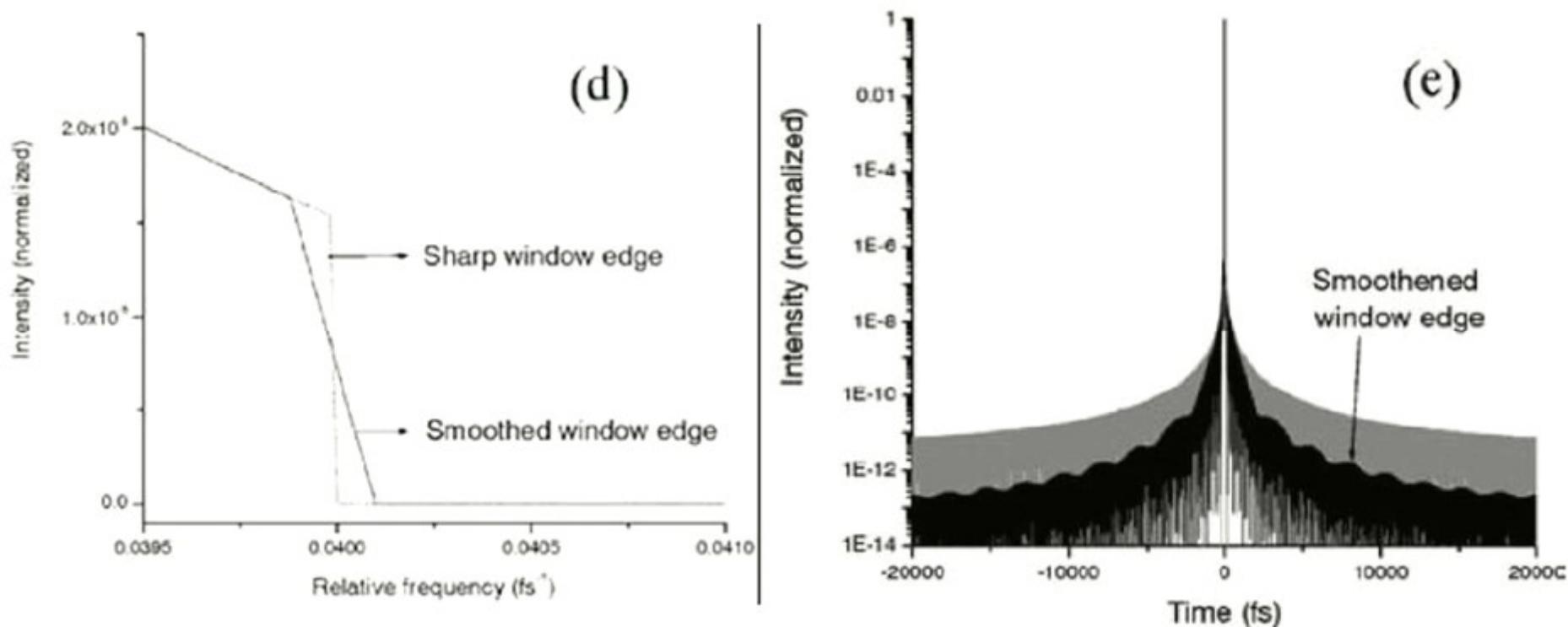
- group delay over beam aperture and spatially varying dispersion
- residual spectral phase
- spatial and angular chirp
- spectral clipping
- spectral phase 'noise'



Spectral clipping



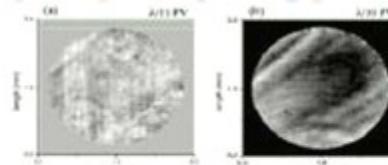
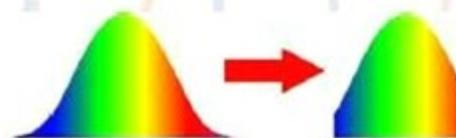
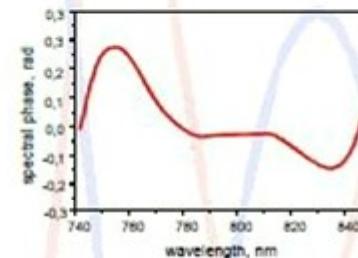
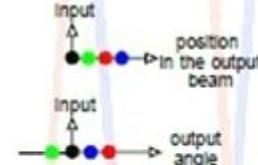
Influence of the spectral edge sharpness



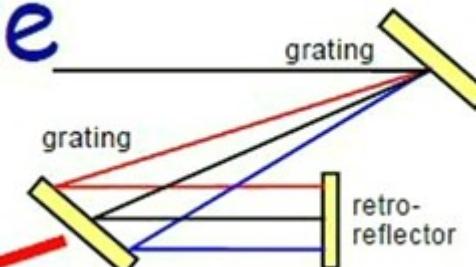
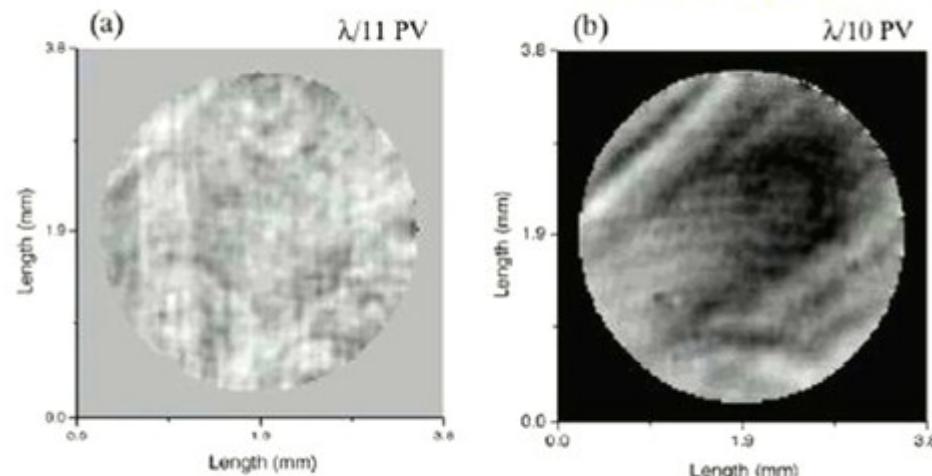
The spectral window edges with different sharpness and resulting temporal structures

Errors of recompression

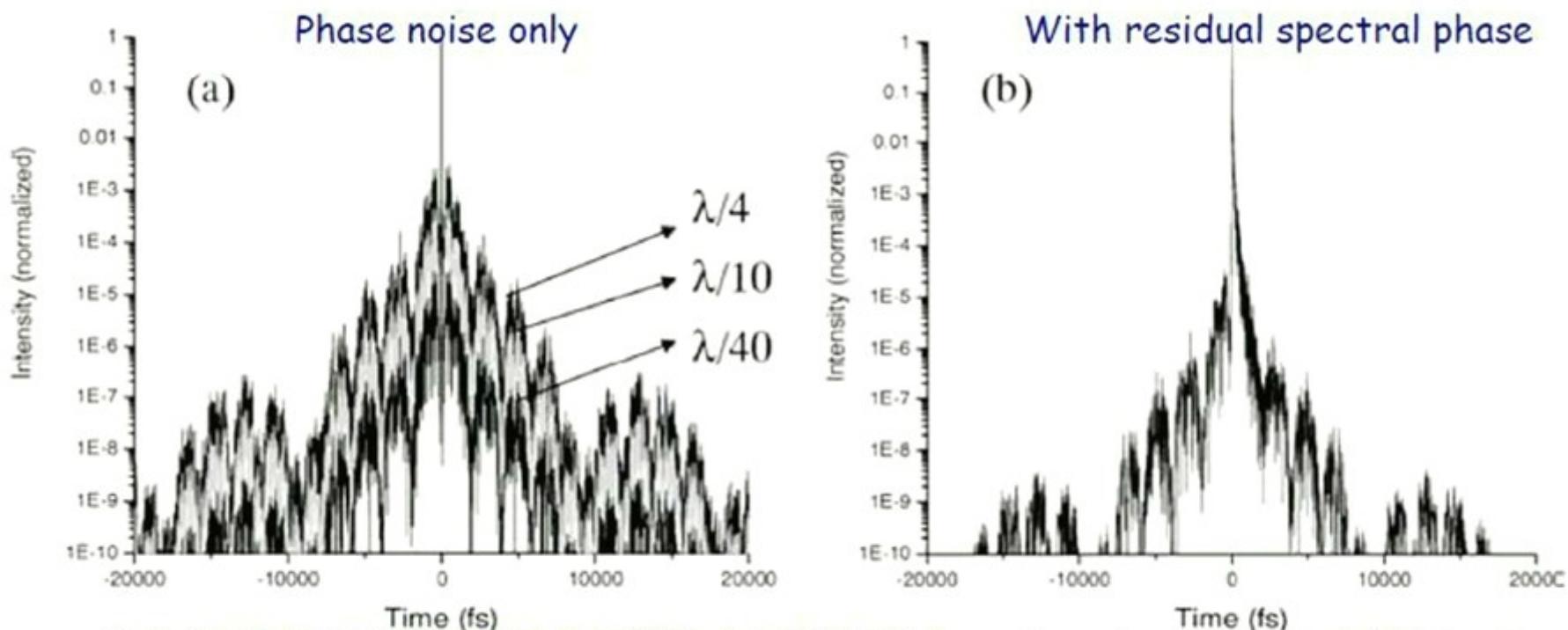
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Phase noise



Optical elements in the compressor, stretcher, diffraction gratings



K.-H. HONG, B. HOU, J.A. NEES, E. POWER, G.A. MOUROU, Generation and measurement of $>10^8$ intensity contrast ratio in a relativistic kHz chirped-pulse amplified laser, Appl. Phys. B 81, 447-457 (2005)

Specific for CPA

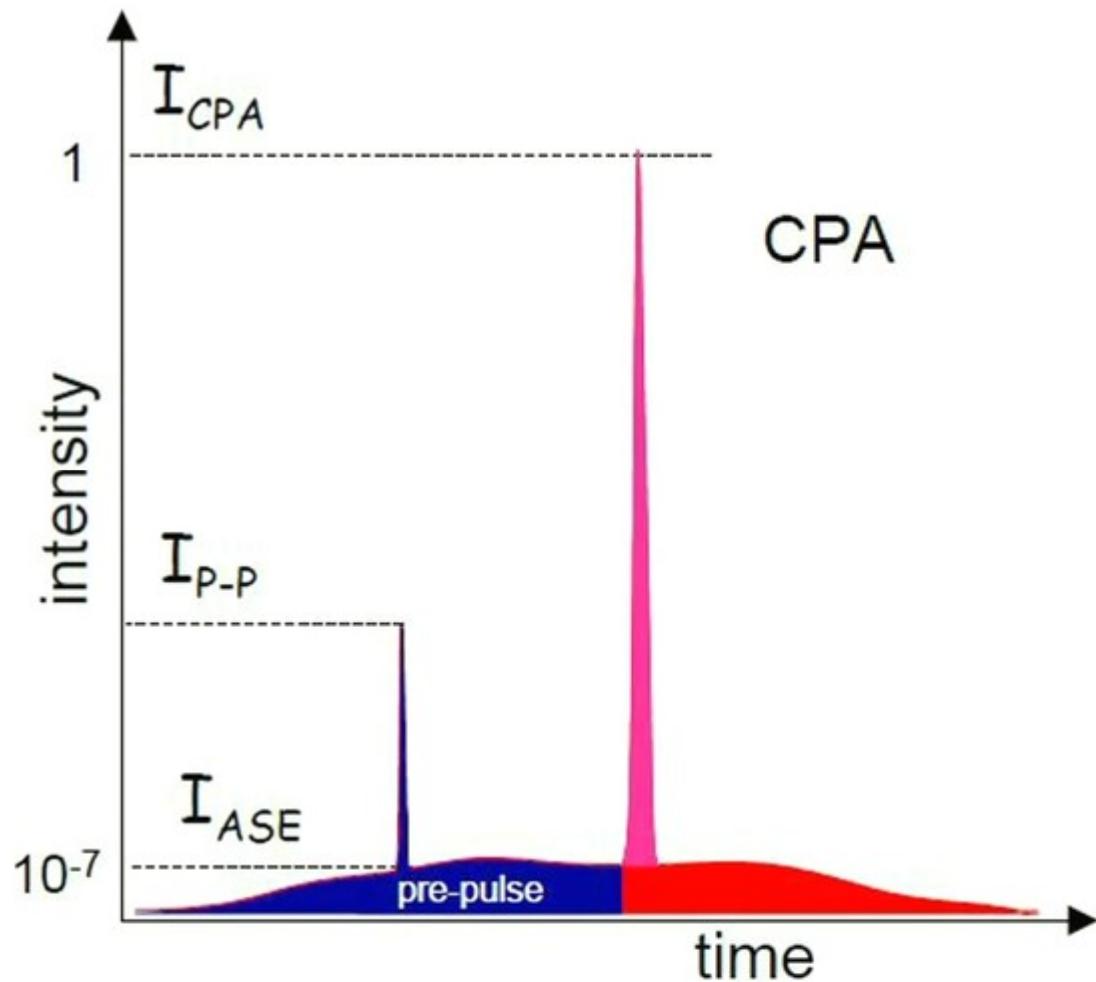
Energy contrast:

$$K_E = \int I_{CPA} dt / \int I_{ASE} dt$$

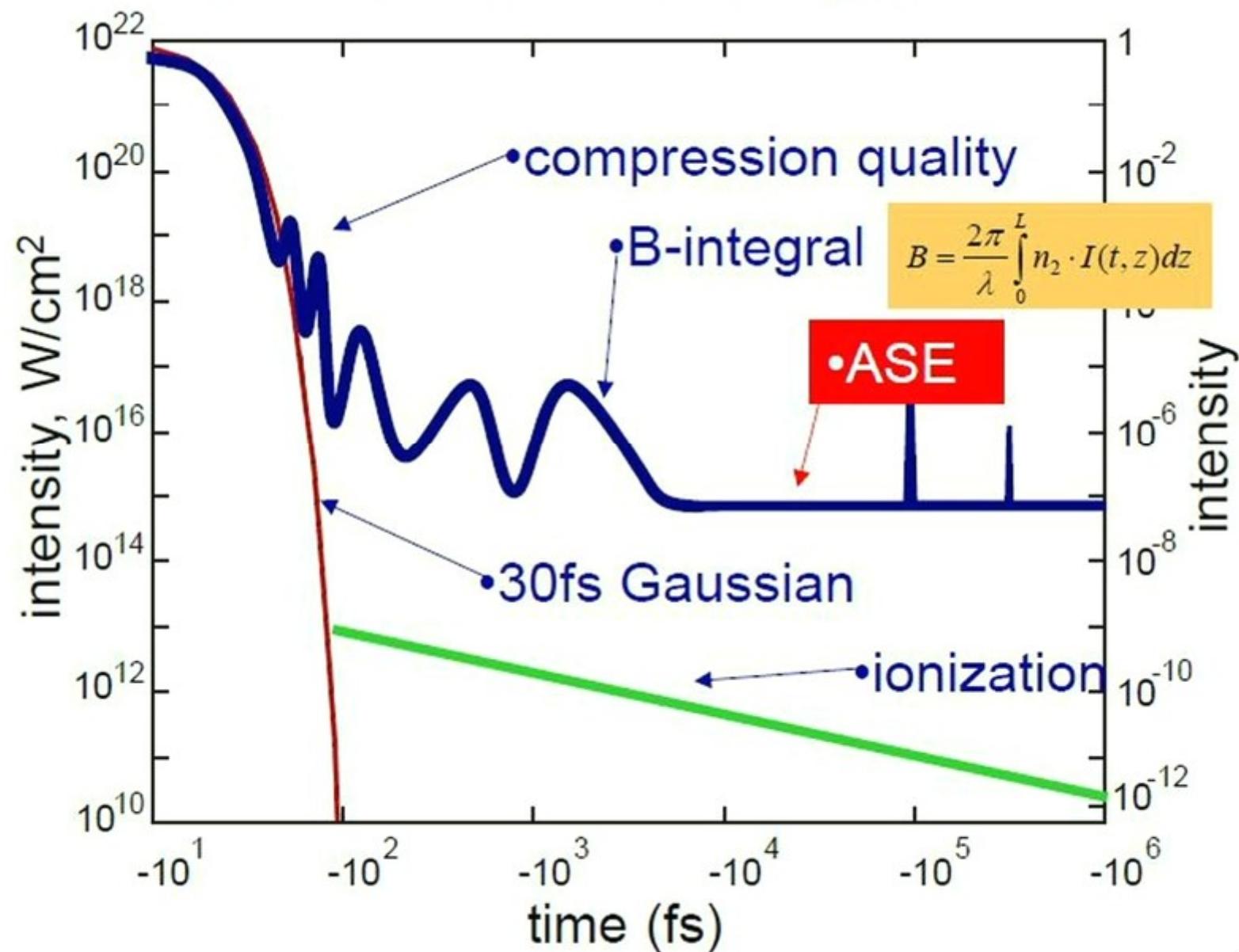
Intensity contrast:

$$K_I = I_{CPA} / I_{ASE}$$

At a fixed ASE-level shortening of the pulse not only increases the laser power, but leads also to higher contrast.

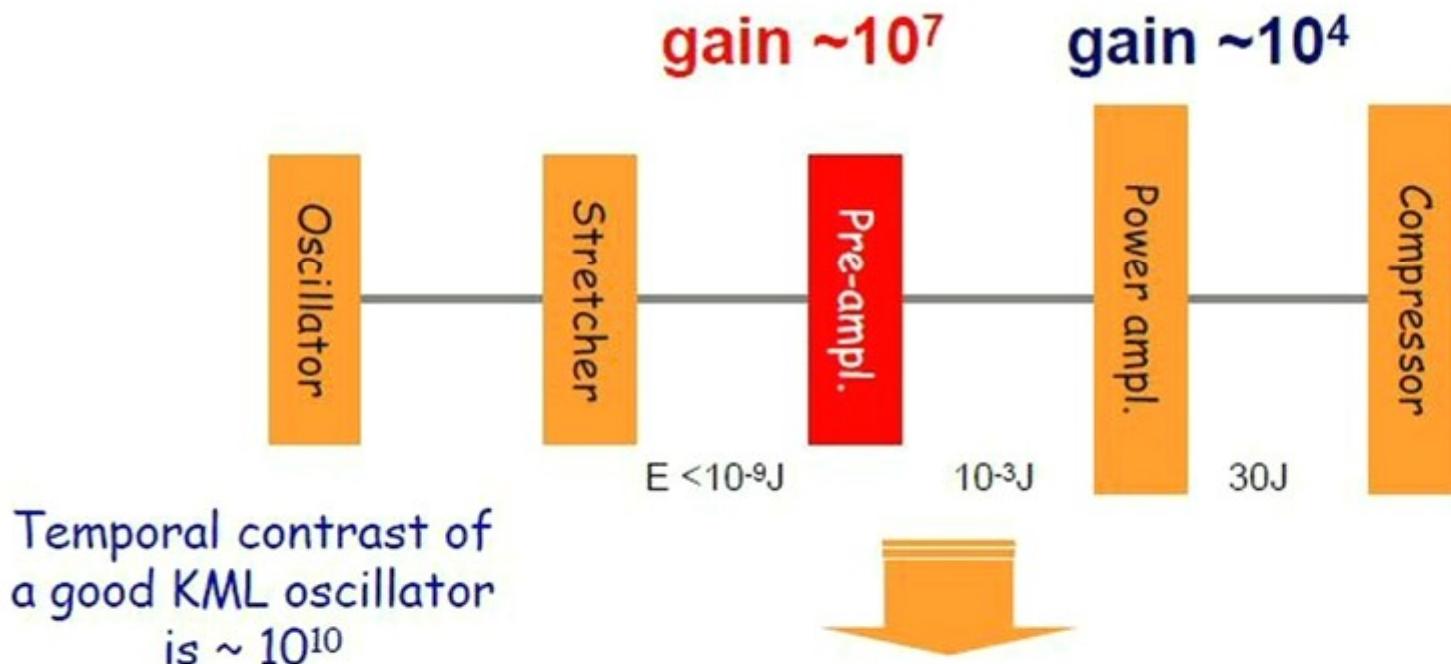


Time domain of laser - solid target interaction



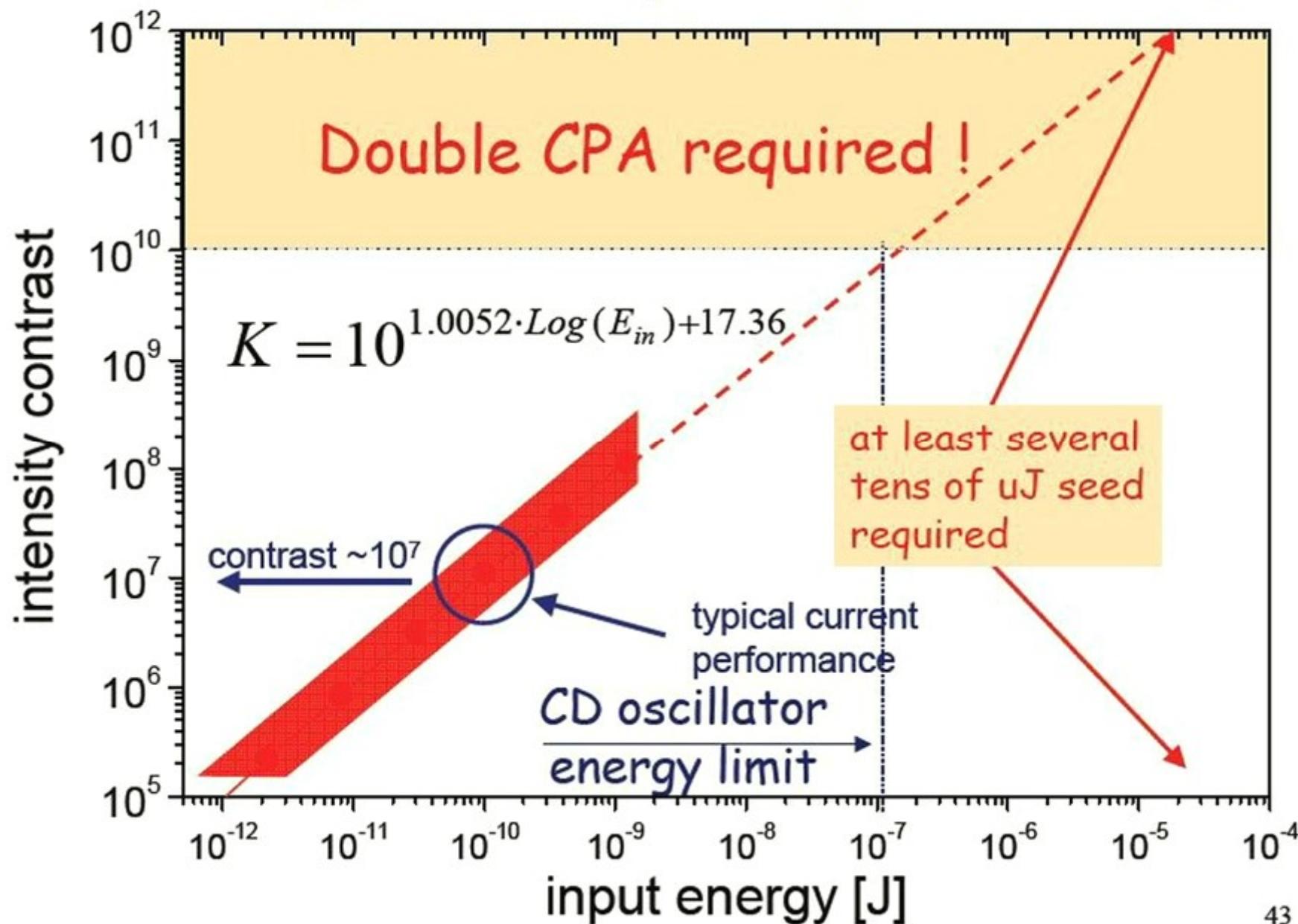
Typical CPA Ti:sapphire laser architecture

$$\text{The ASE brightness is given by: } B_{ASE} = \frac{F_{SAT} \Delta v}{4\pi\tau_{FL} \Delta v_{FL}} \cdot (G_{ASE} - 1)$$

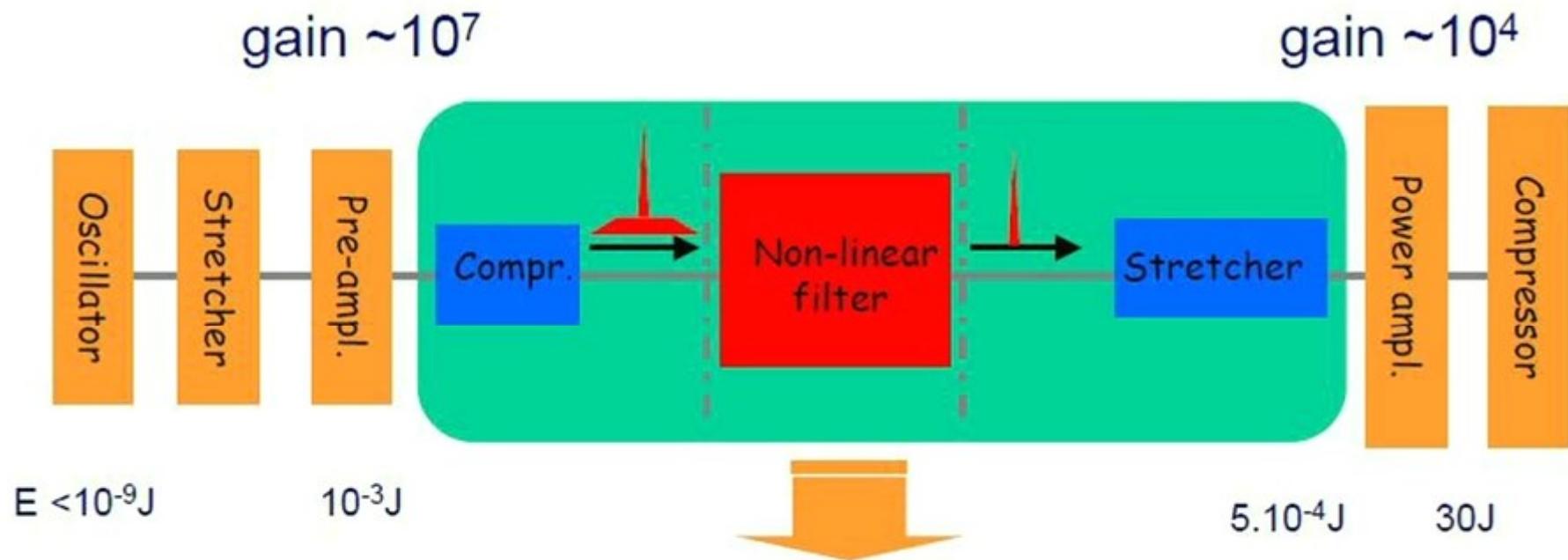


The contrast is almost fully determined by the laser front end.

Scaling to a PW power (10^{22} W/cm^2)

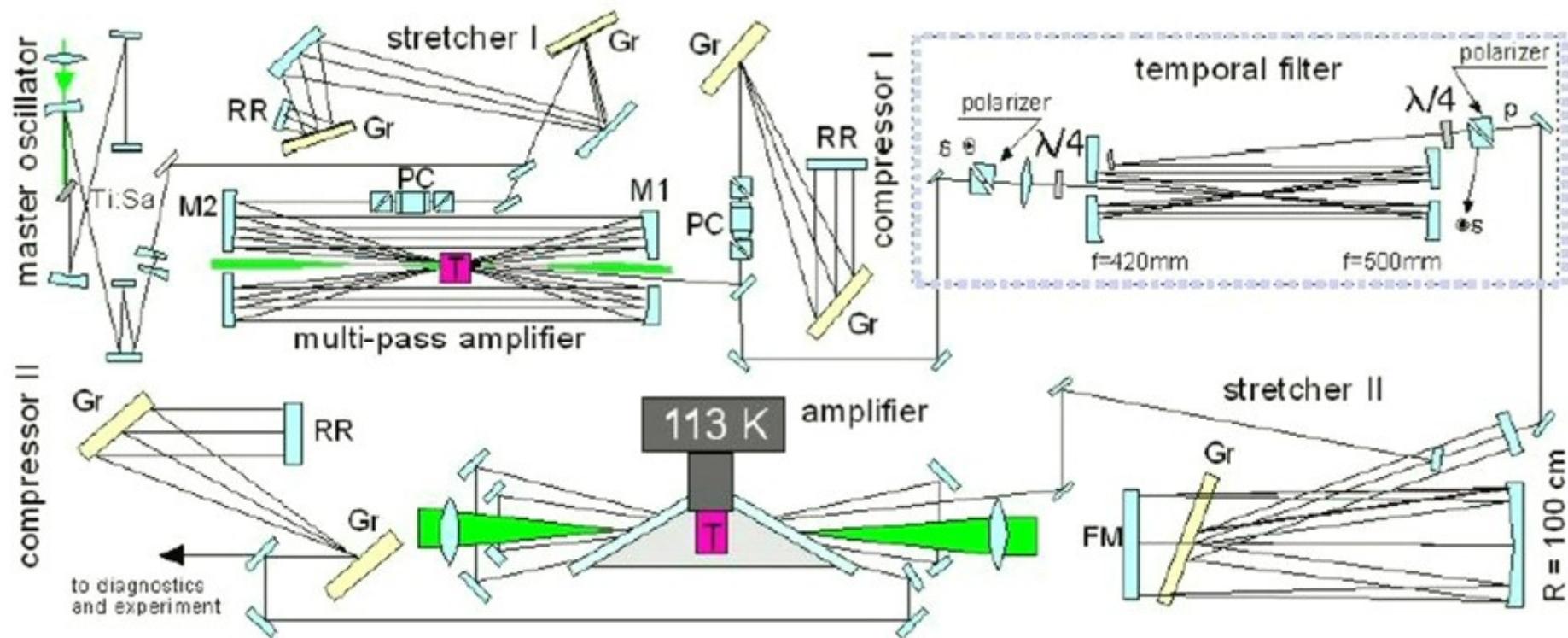


Concept of the Double-CPA laser

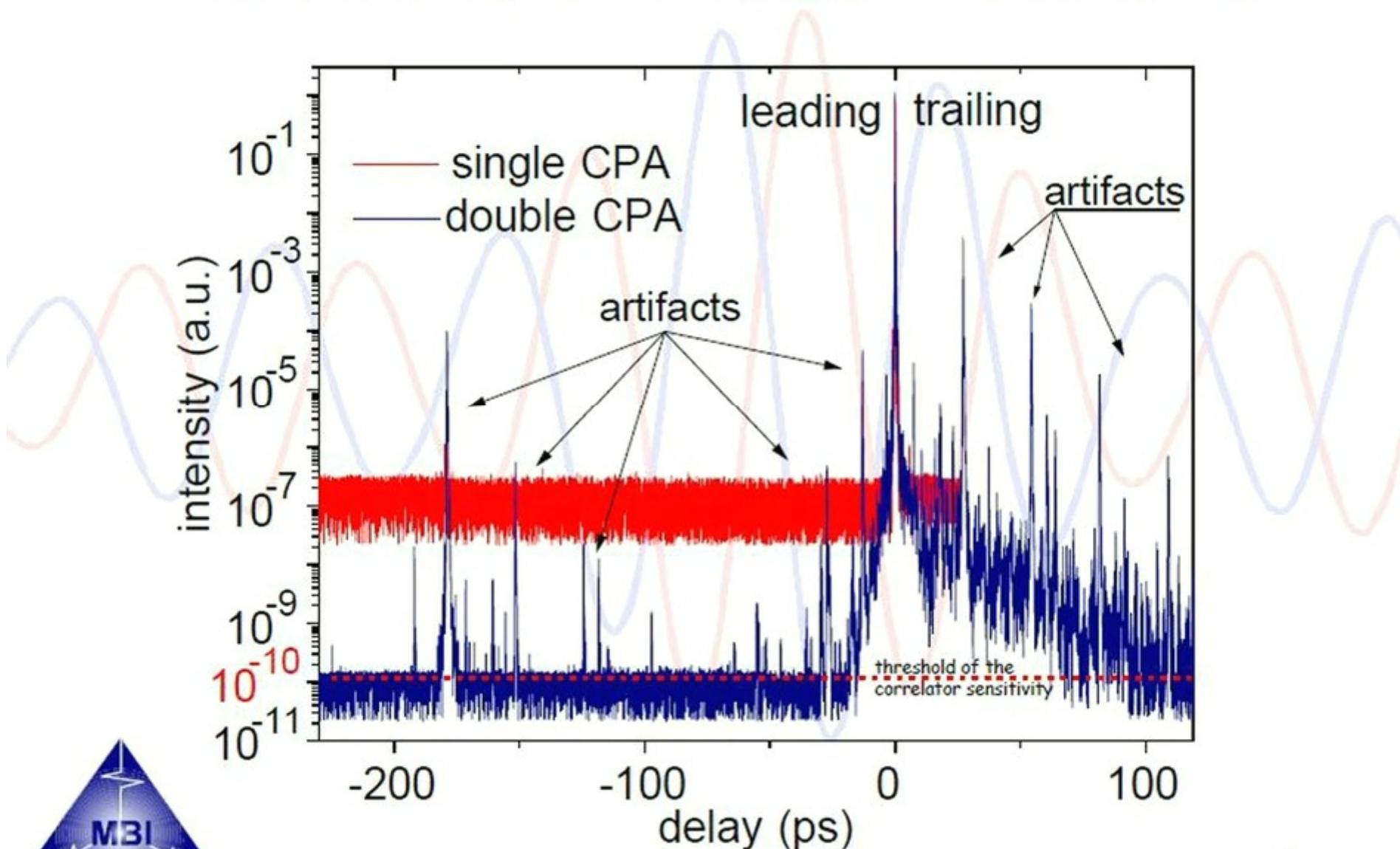


- transmits the short pulse for further amplification
- stops the ASE background and satellite pulses

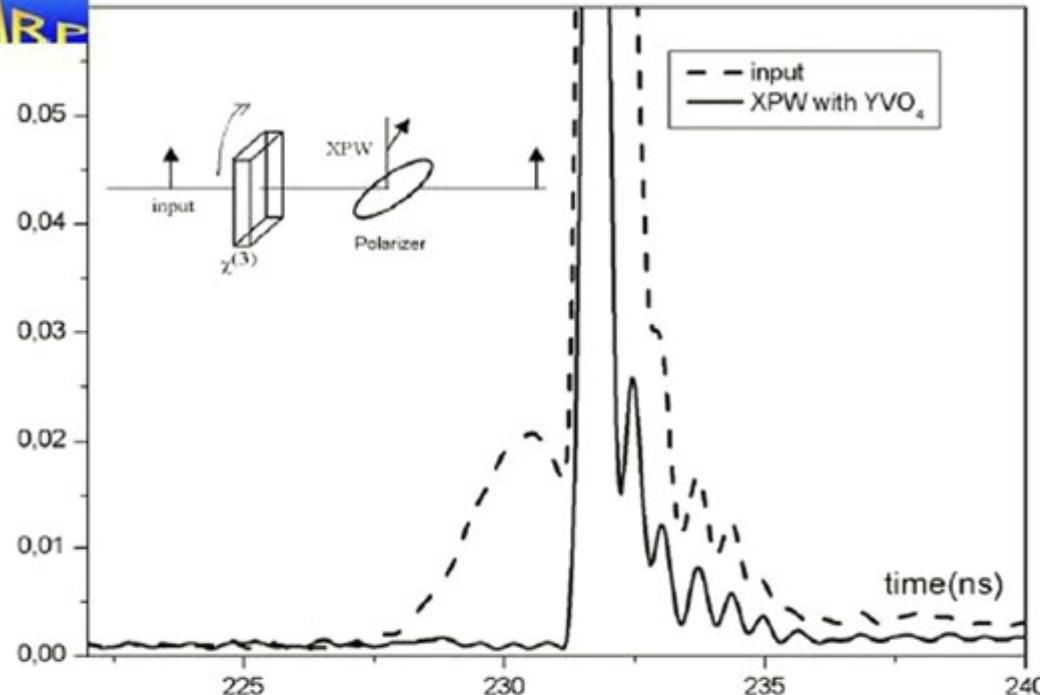
Scheme of the DCPA laser



Contrast of the Double-CPA laser



XPW : generation of an orthogonal polarized



BaF_2 crystal :

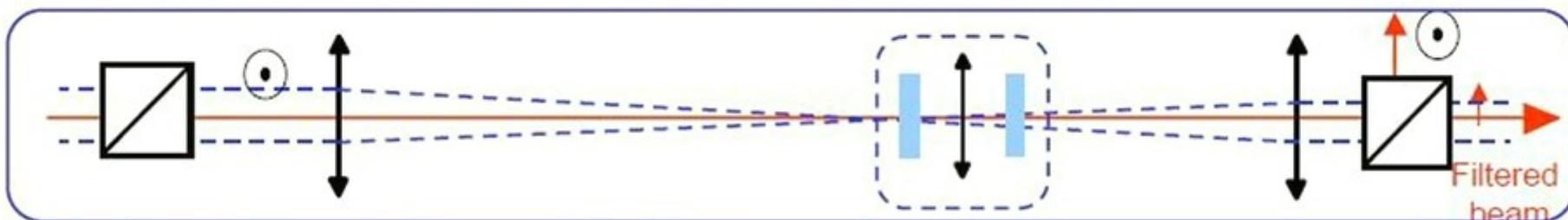
- Low SPM
- High χ^3 anisotropy \Rightarrow correct efficiency
- Adaptable on various laser wavelengths

\Rightarrow Demonstrated at $\lambda=620\text{nm}$, $\lambda=800\text{nm}$, $\lambda=1.06\mu\text{m}$

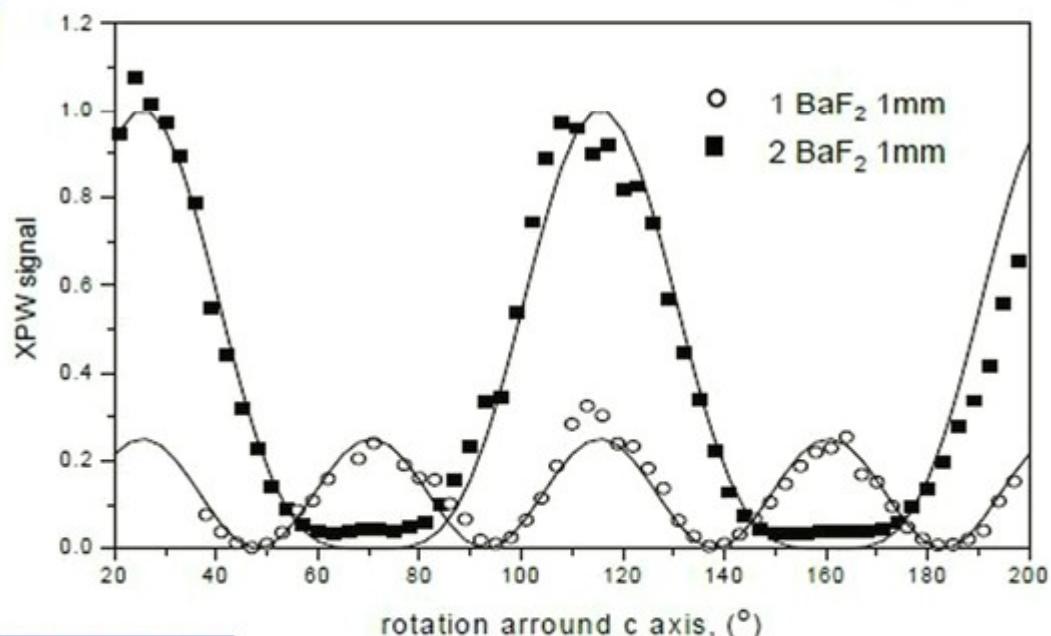
Opt. Lett. 26 (2001) 335, JOSA B 21 (2004) 1659, Opt. Lett., 30

An experimental technique to ensure stability and reliability of the setup with high transmission

- Experiments with two crystals in the far-field :



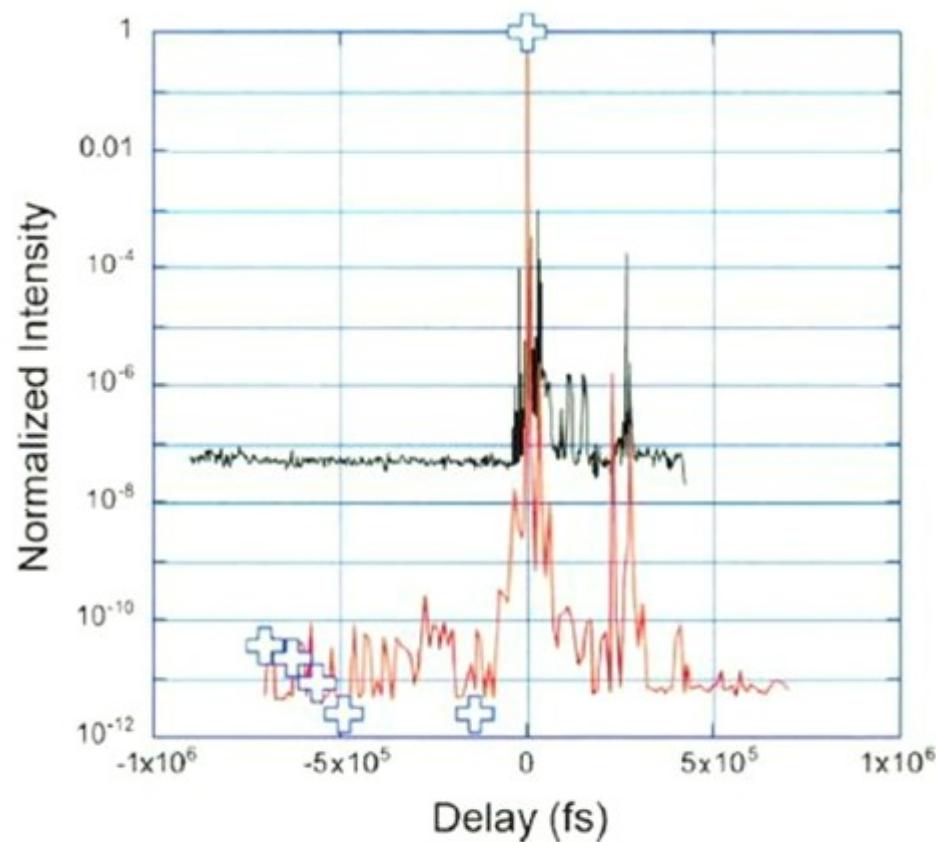
- several crystals successively "imaged"
- 1st crystal $\Rightarrow E_{XPW1}$
- 2nd crystal $\Rightarrow E_{XPW2}$ with the same spatial and temporal properties
- E_{XPW1} and E_{XPW2} can constructively or destructively interfere



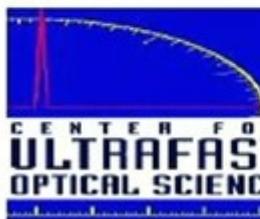
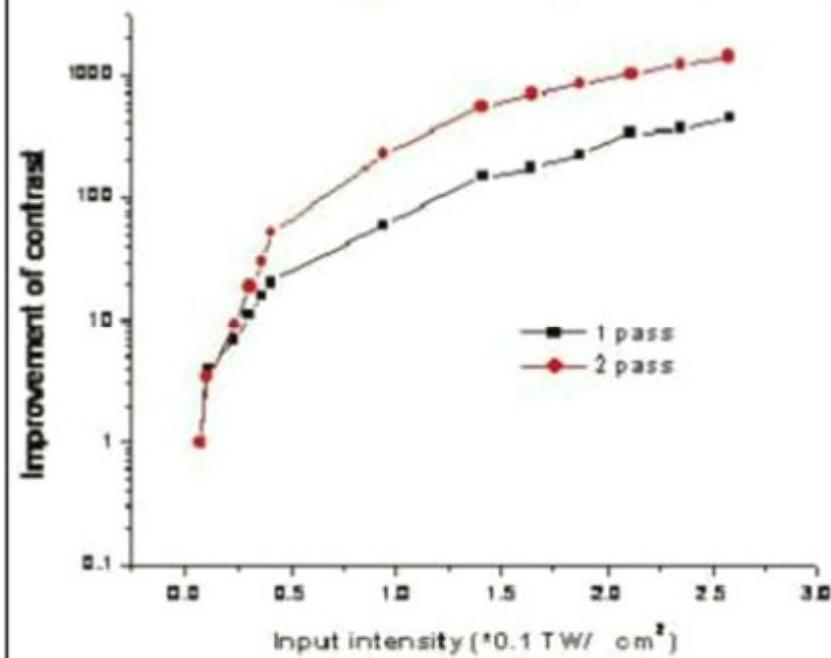
\Rightarrow LOA - THALES LASER Patent FR 04-12964

Fig. 1

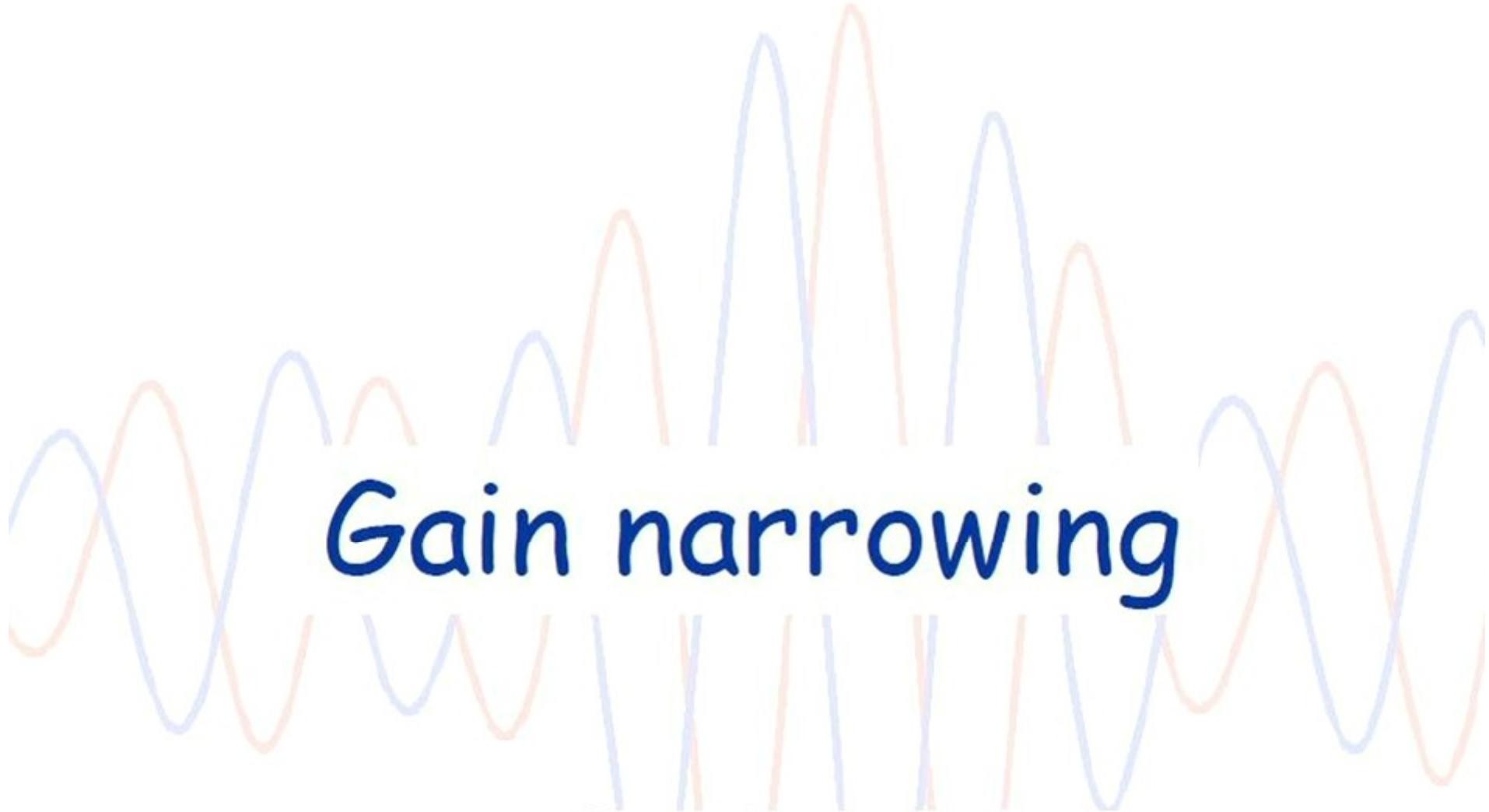
Record contrast of 10^{11} demonstrated at 50 TW



- XPW BaF₂ crystal
- Filtering at a μJ level



V. Chvykov, P. Rousseau, S. Reed, G. Kalinchenko, V. Yanovsky, Generation of 10^{11} contrast 50 TW laser pulses, Opt. Lett, 31, 1456-1458 (2006).

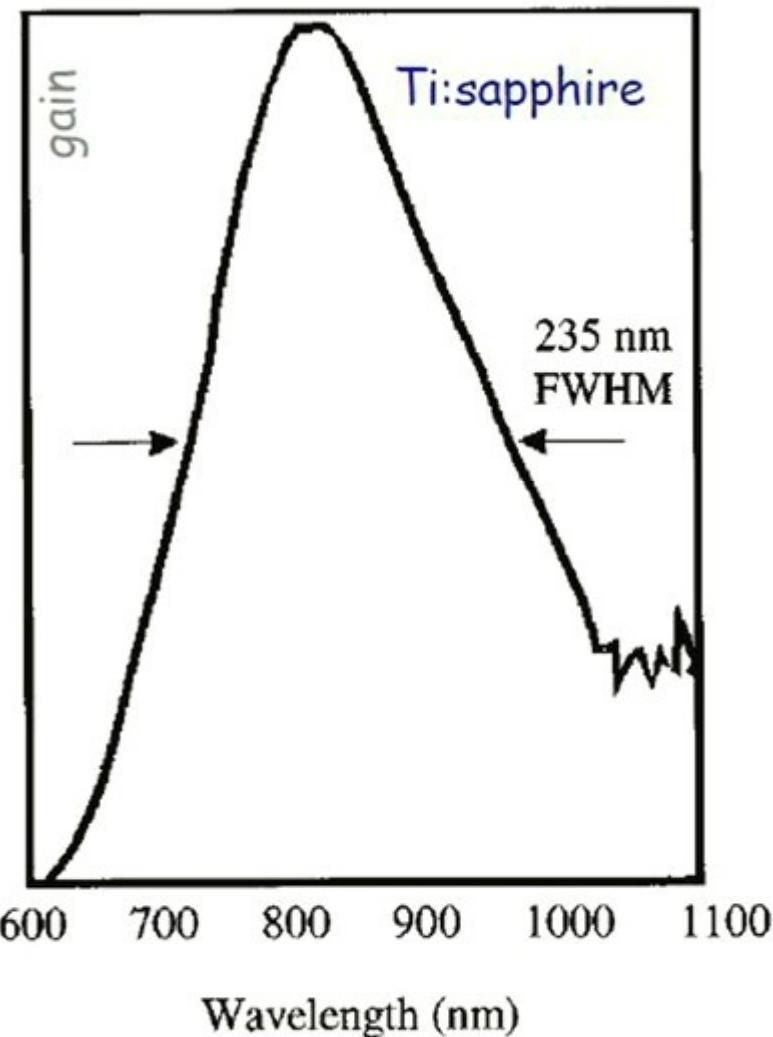


M.P. KALASHNIKOV
K. OSVAY *
I.M. LACHKO
H. SCHÖNNAGEL
W. SANDNER

**Suppression of gain narrowing
in multi-TW lasers with negatively
and positively chirped pulse amplification**

Max-Born-Institut für Nichtlineare Optik und Kurzzeitspektroskopie,
Max-Born-Straße 2a, 12489 Berlin, Germany

Factors limiting pulse duration



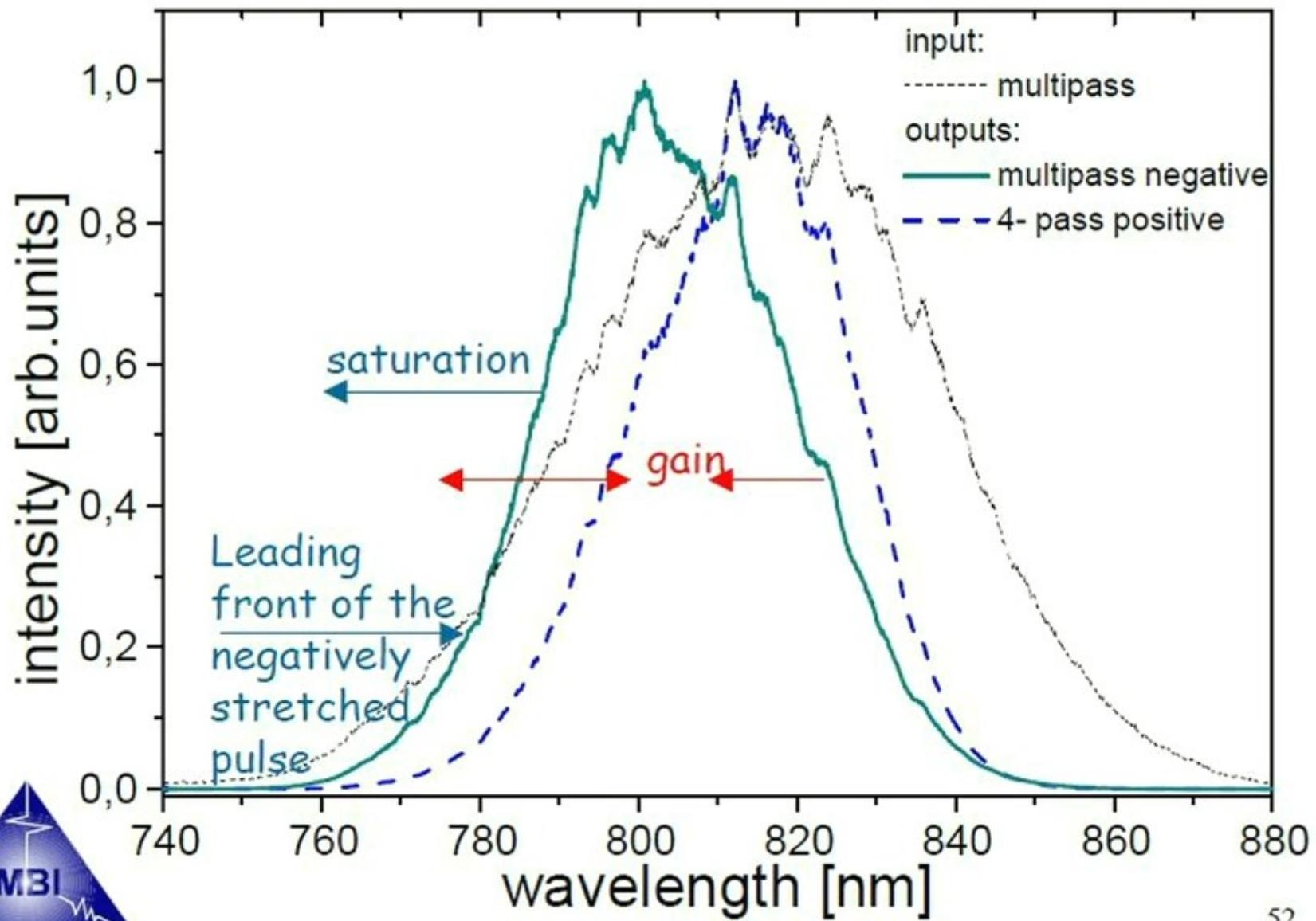
- Gain narrowing - frequency dependence of the gain.

Bandwidth of a nanojoule seed pulse (60-80 nm) amplified to a petawatt is reduced to < 30 nm.

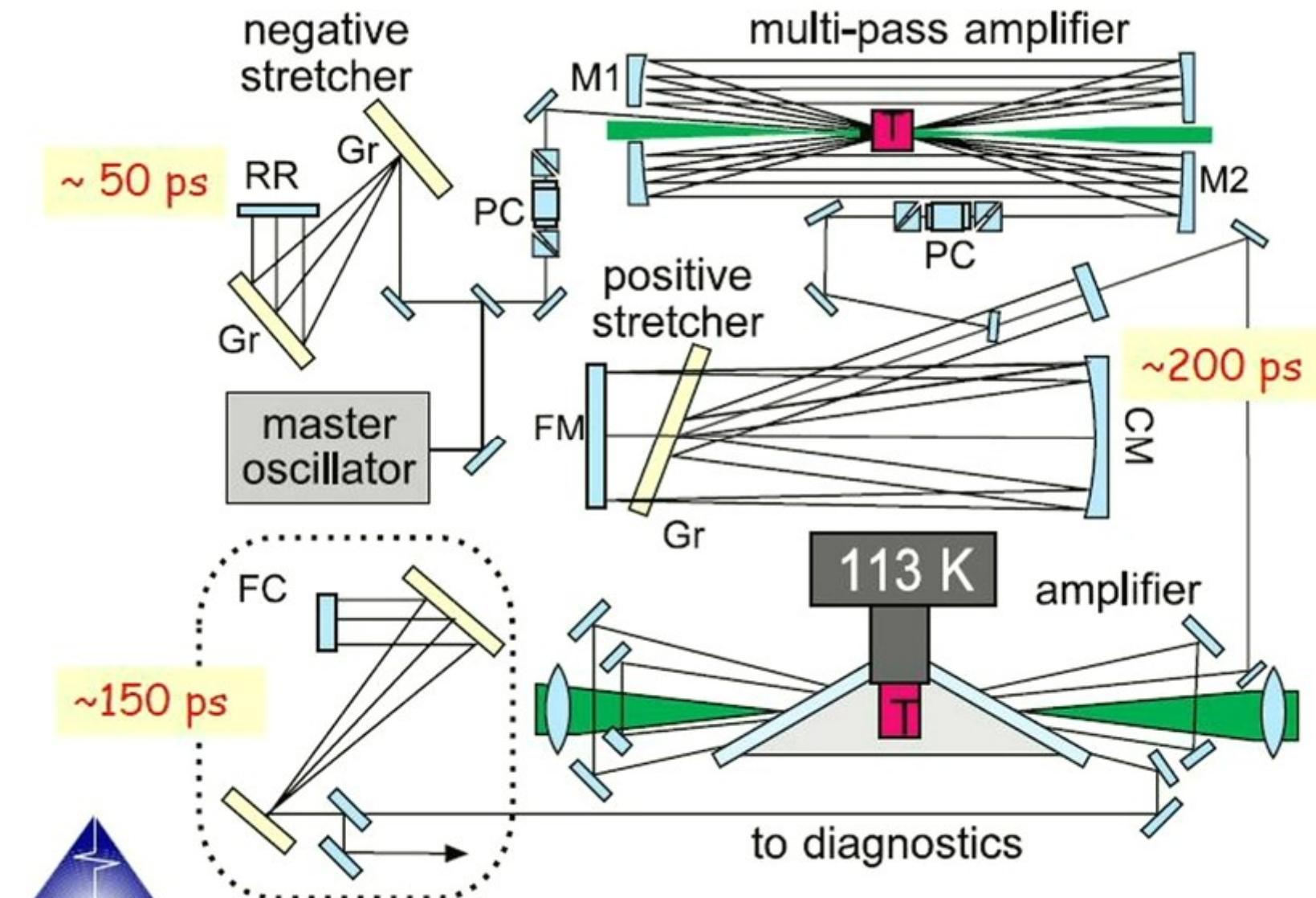
- Saturation of amplification

Similar to the temporal contrast, the spectrum is almost fully determined by the laser front end:
half bandwidth of a good oscillator

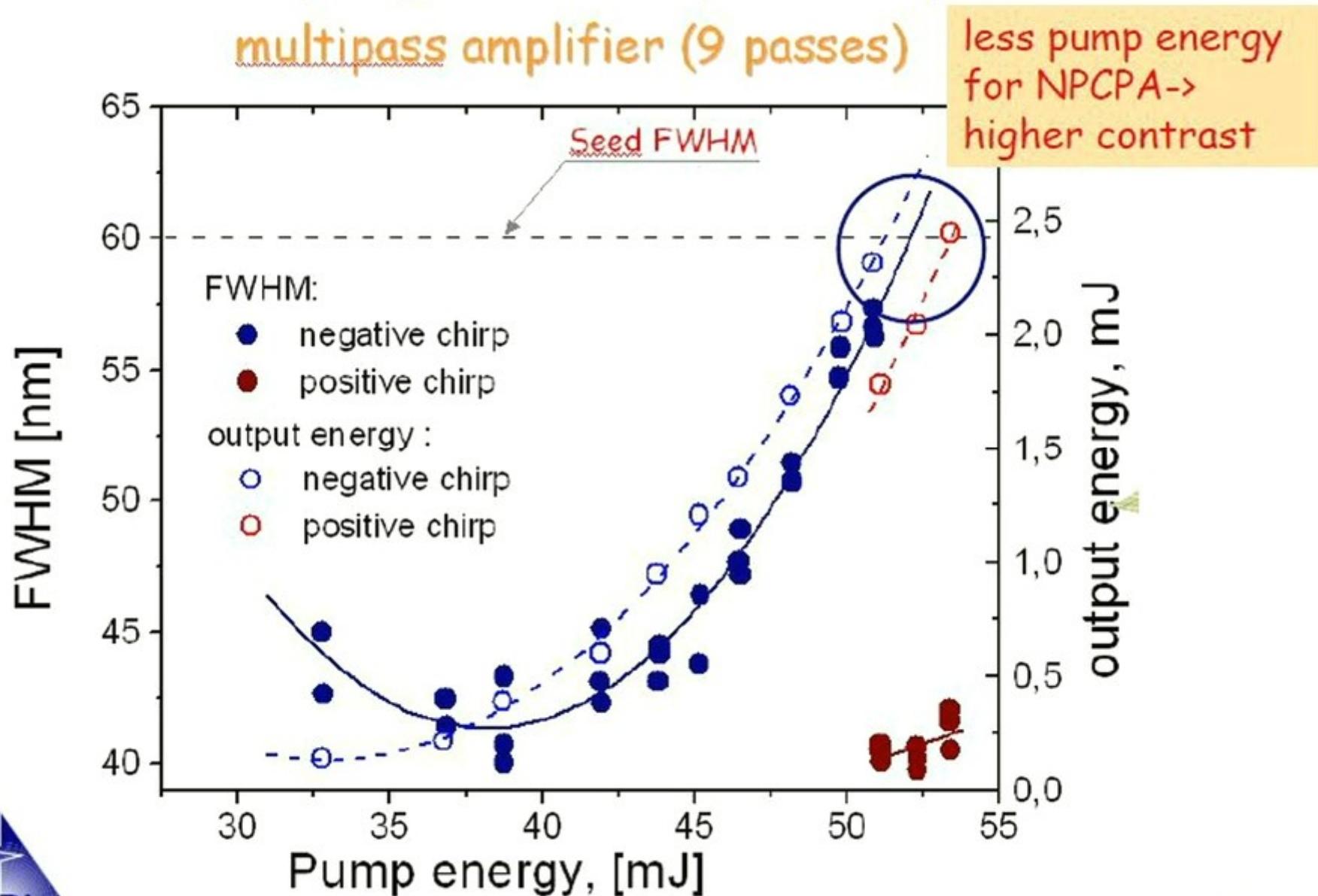
Negatively-positively chirped



Negative- Positive CPA laser (NPCPA)

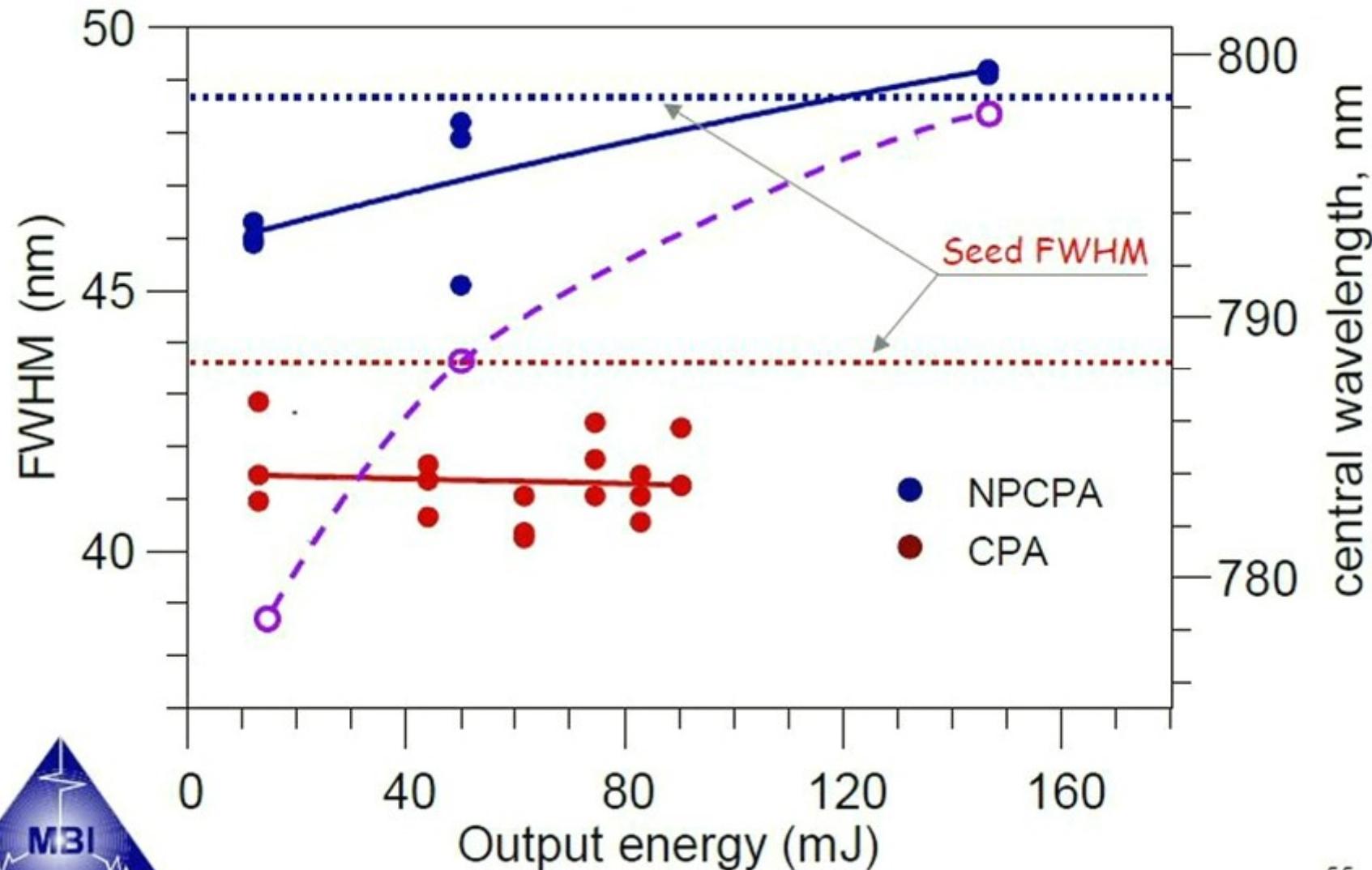


Reshaping of the pulse spectrum

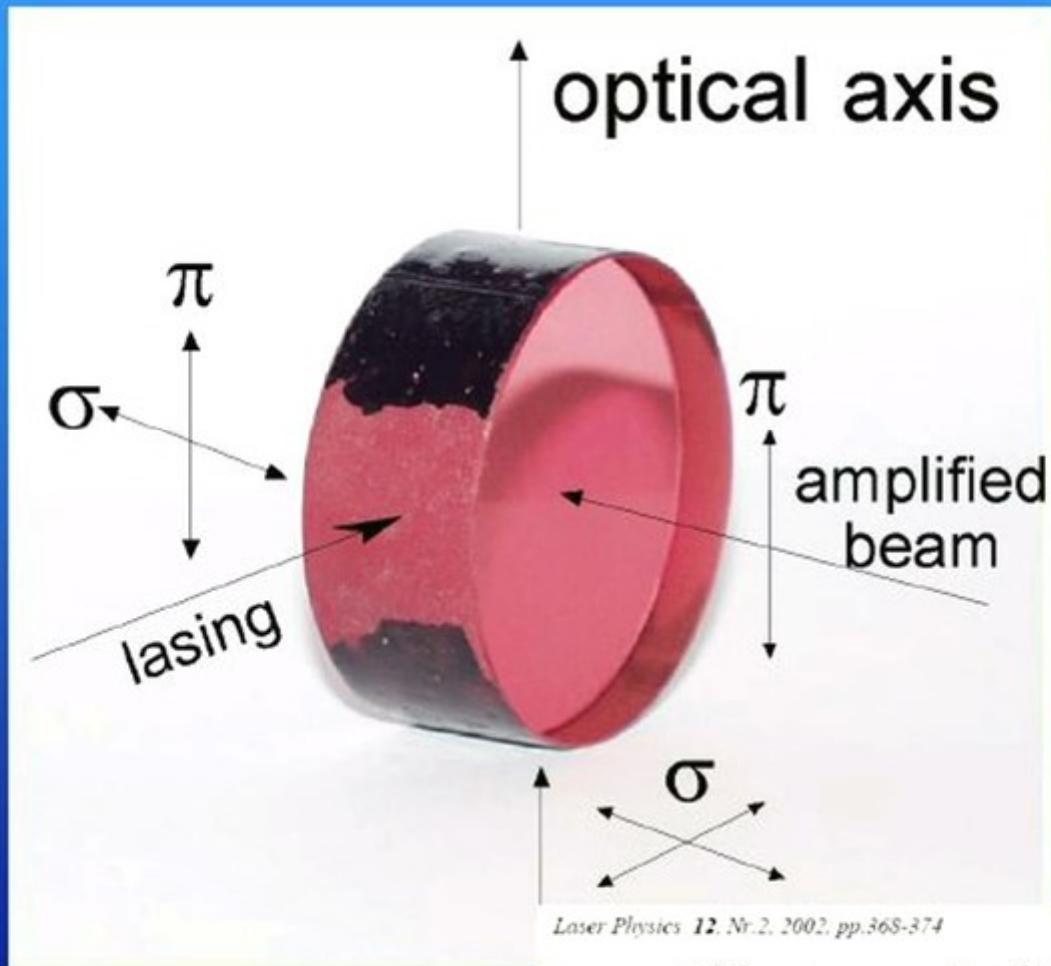


Reshaping the pulse spectrum

power amplifier (4 passes)



Parasitic lasing in a high aperture Ti:sapphire crystal

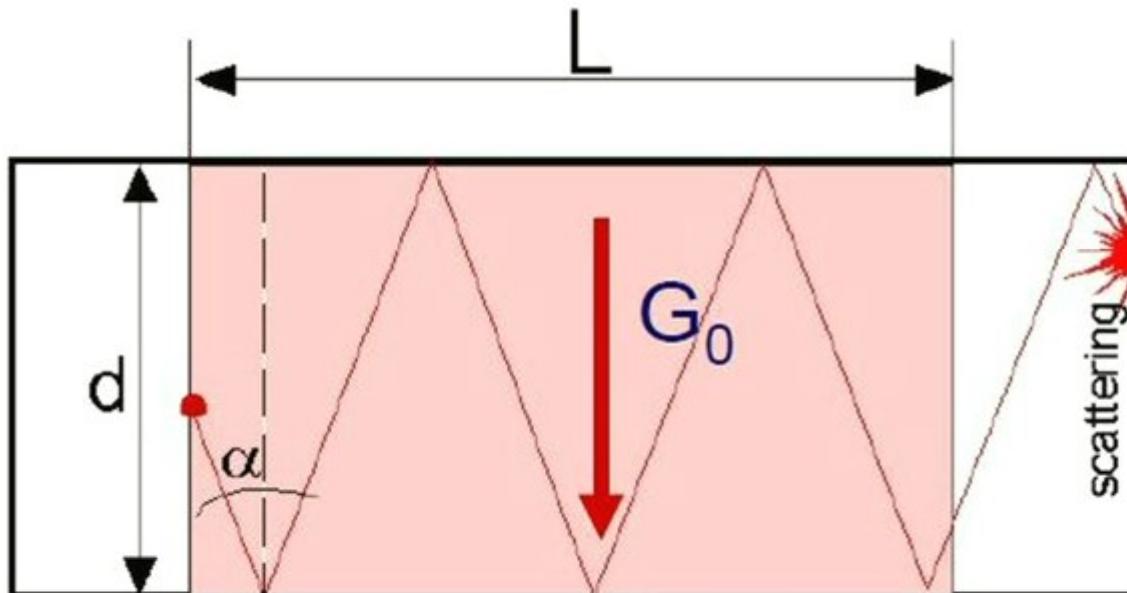


Diameter 35 mm

Thickness 15 mm

Coated by a usual
black paint, $n \sim 1.5$

Parasitic lasing in a high aperture Ti:sapphire crystal



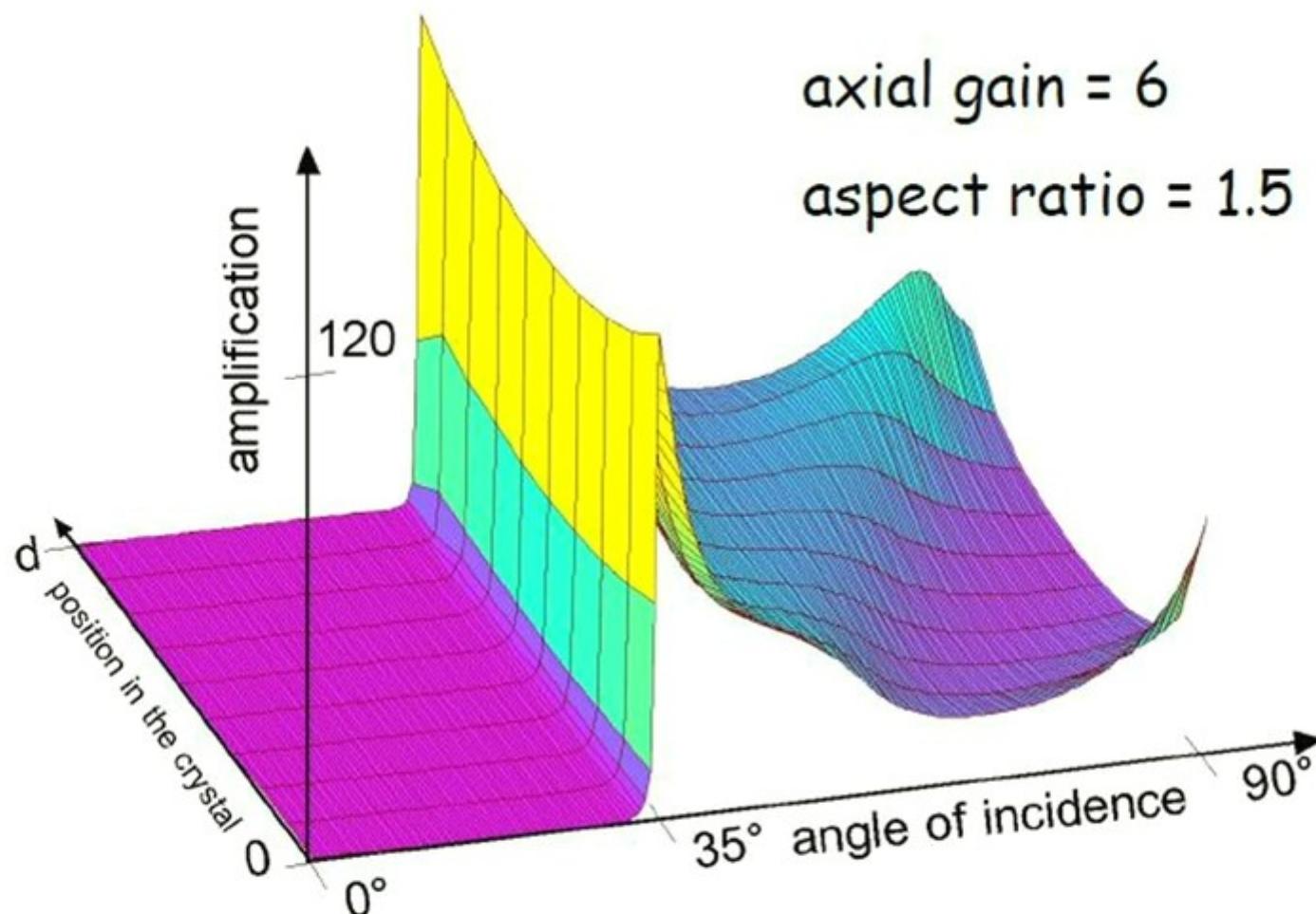
$$G_\pi = R_s^N \exp(A_s \ln G_0 / \sin \alpha)$$

$$G_\sigma = R_p^N \exp(A_s \ln \sqrt{G_0} / \sin \alpha)$$

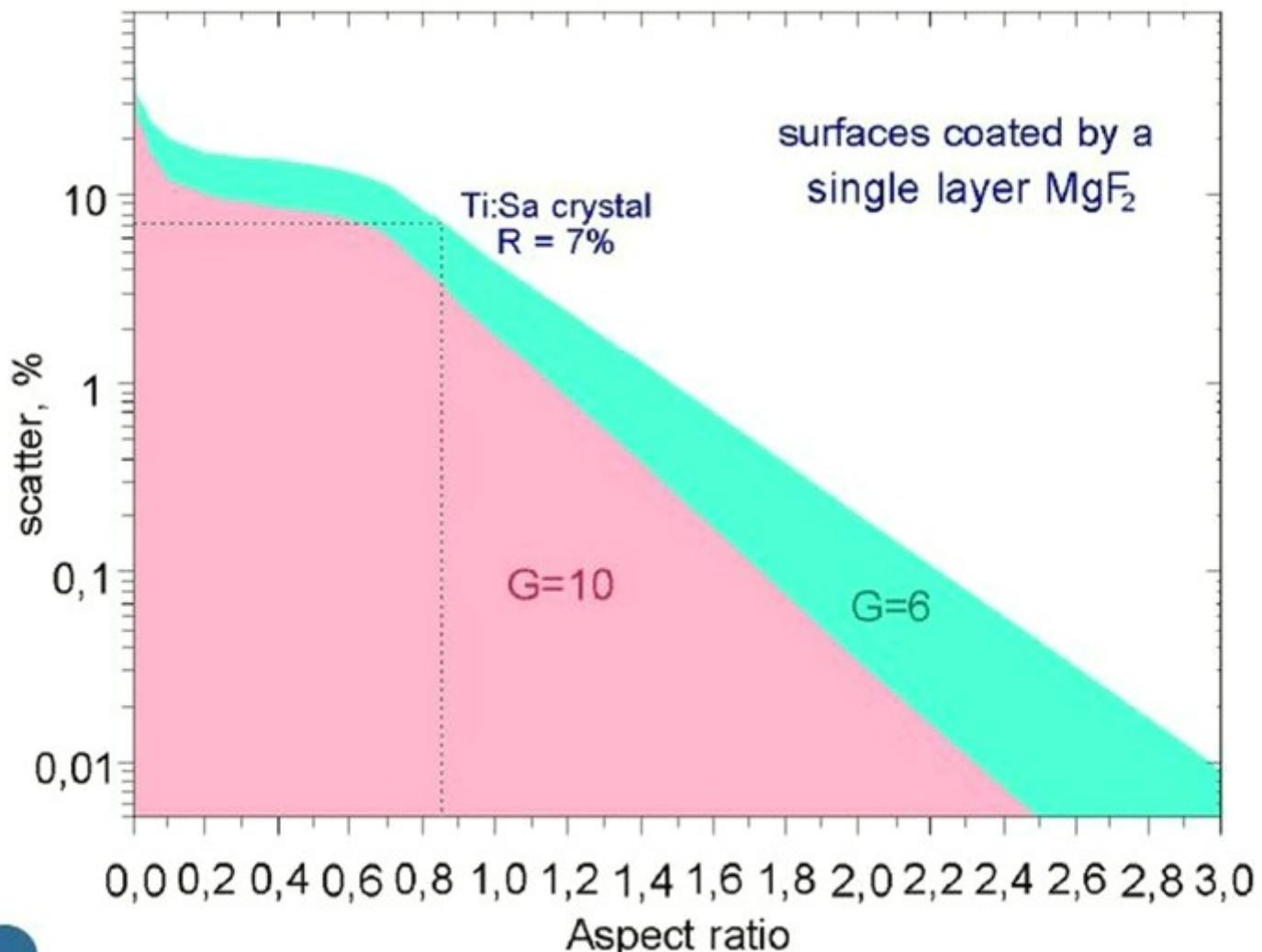
$A_s = L/d$ - aspect ratio
 N - number of reflections
 α - angle of incidence
 G - axial amplification

Free lasing in a Ti:Sa rod

(non-uniform pump).



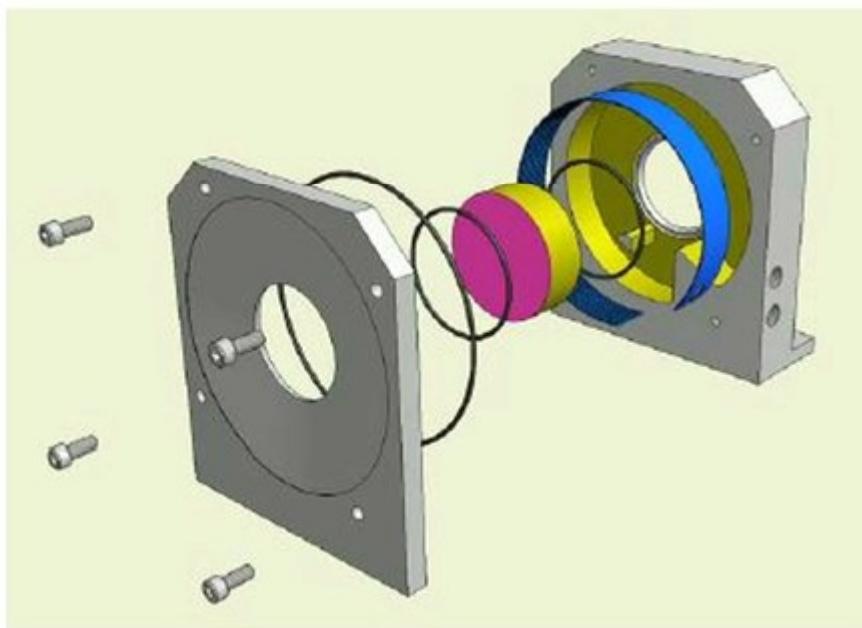
Threshold for parasitic lasing in a Ti:Sa rod



Suppression of Parasitics

1. Transverse parasitics:

Caused by feedback from cylinder surface into gain region
Use an index-matching material at the cylinder surface



Schematic of Ti:sapphire mount

- Index-match liquid has $n_{800}=1.7547$
- Fresnel reflection is only 2×10^{-6}
- Absorber dissolved in liquid **OR** absorbing insert in cell
- Can circulate liquid for cooling if necessary

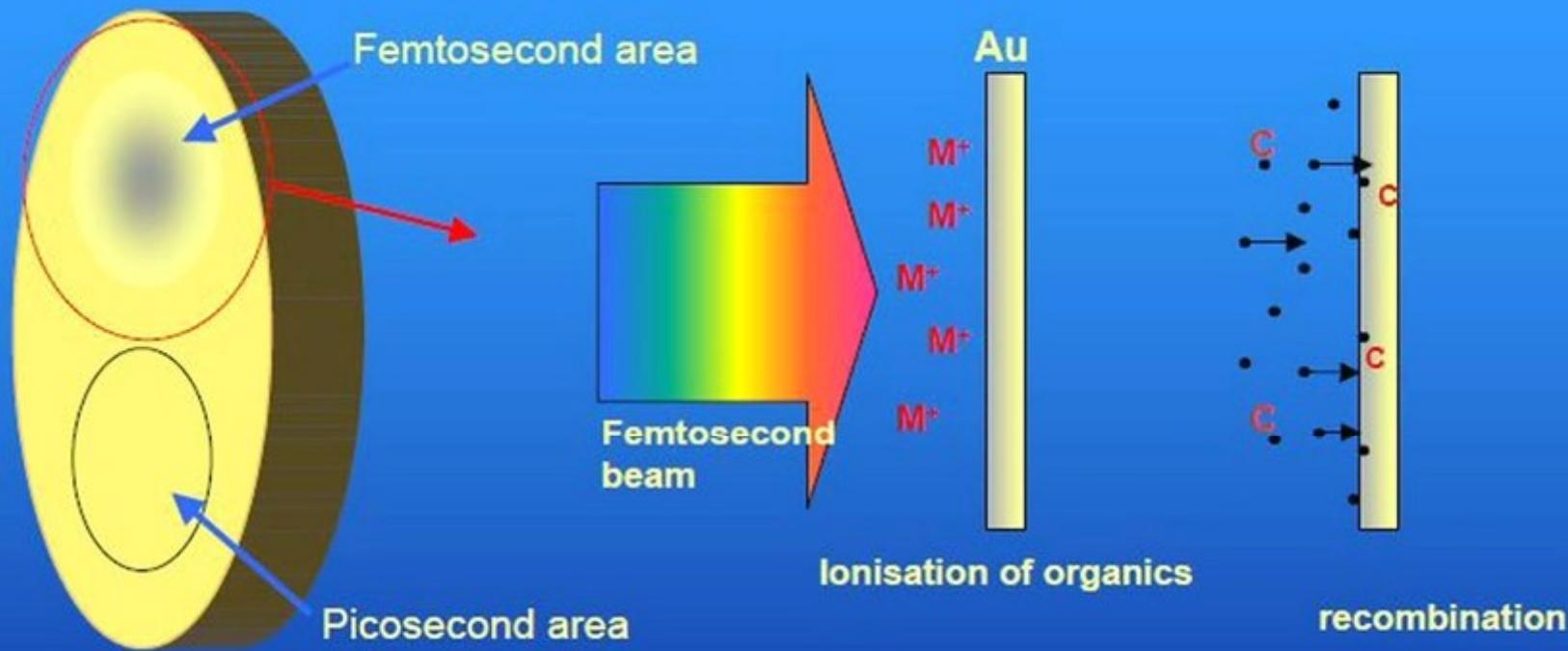
Consequences of high intensity laser and high repetability on gratings



When running at 10 Hz
Total diffraction efficiency decreases from 70 % to 50 % in few days

Diffraction gratings are very expensive:
A set for a 100 TW laser system costs ~ 90 k€

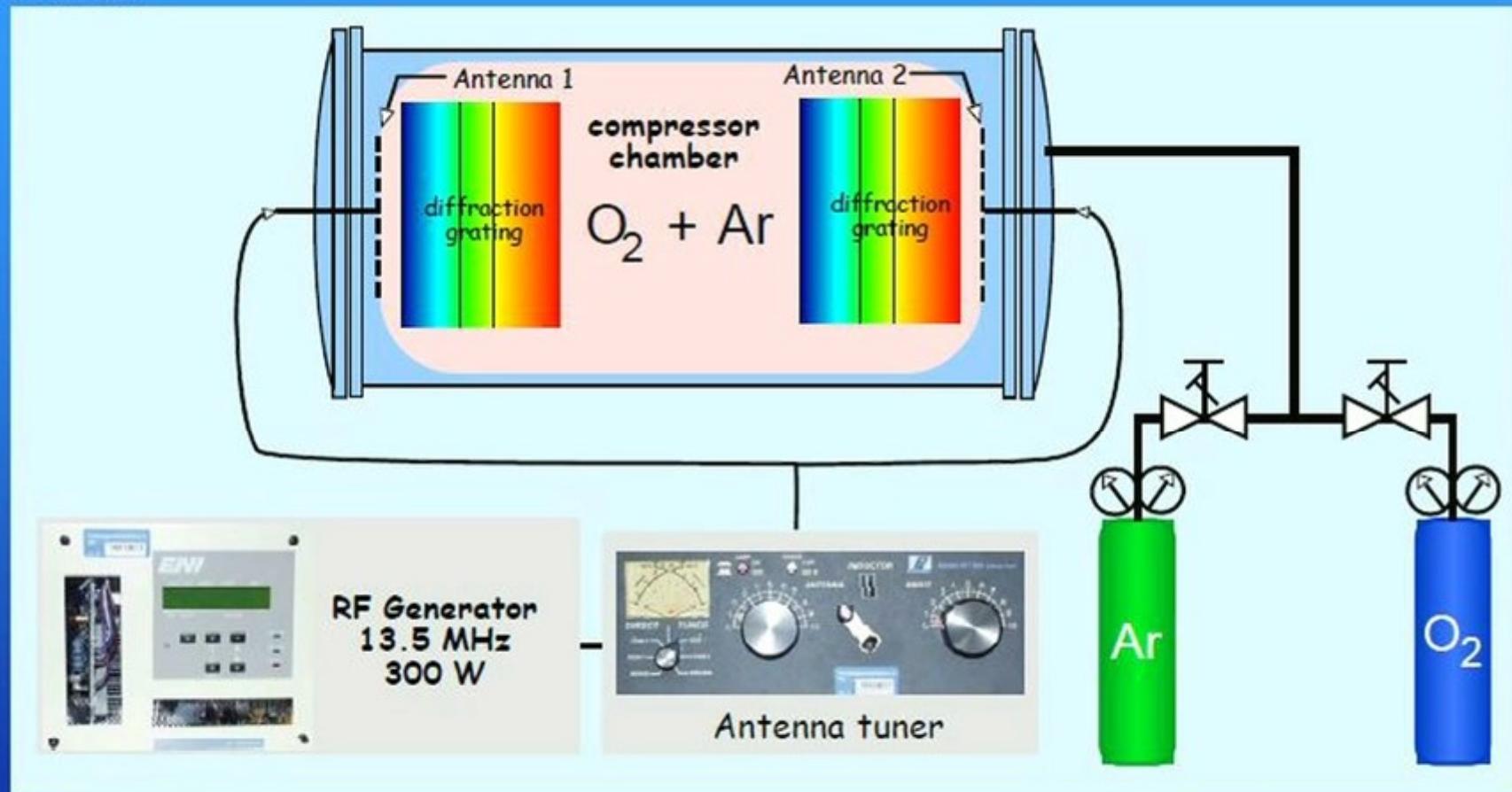
Decontamination of optical elements



Intensity of a recompressed pulse exceeds the value of 10^{12} W/cm^2 . High laser intensity leads to dissociation or/and ionization of organic molecules followed by contamination of the gratings and other optical elements (dielectric mirrors) with carbon.

Cleaning of contaminated optics

experimental setup



typical conditions

pressure: $O_2 : 5 \cdot 10^{-3}$ mbar, $Ar : 3 \cdot 10^{-3}$ mbar

power : 60 W

Pulse characterization

- High dynamic range (temporal contrast)
- Autocorrelation
- FROG
- SPIDER

High dynamic range contrast characterization

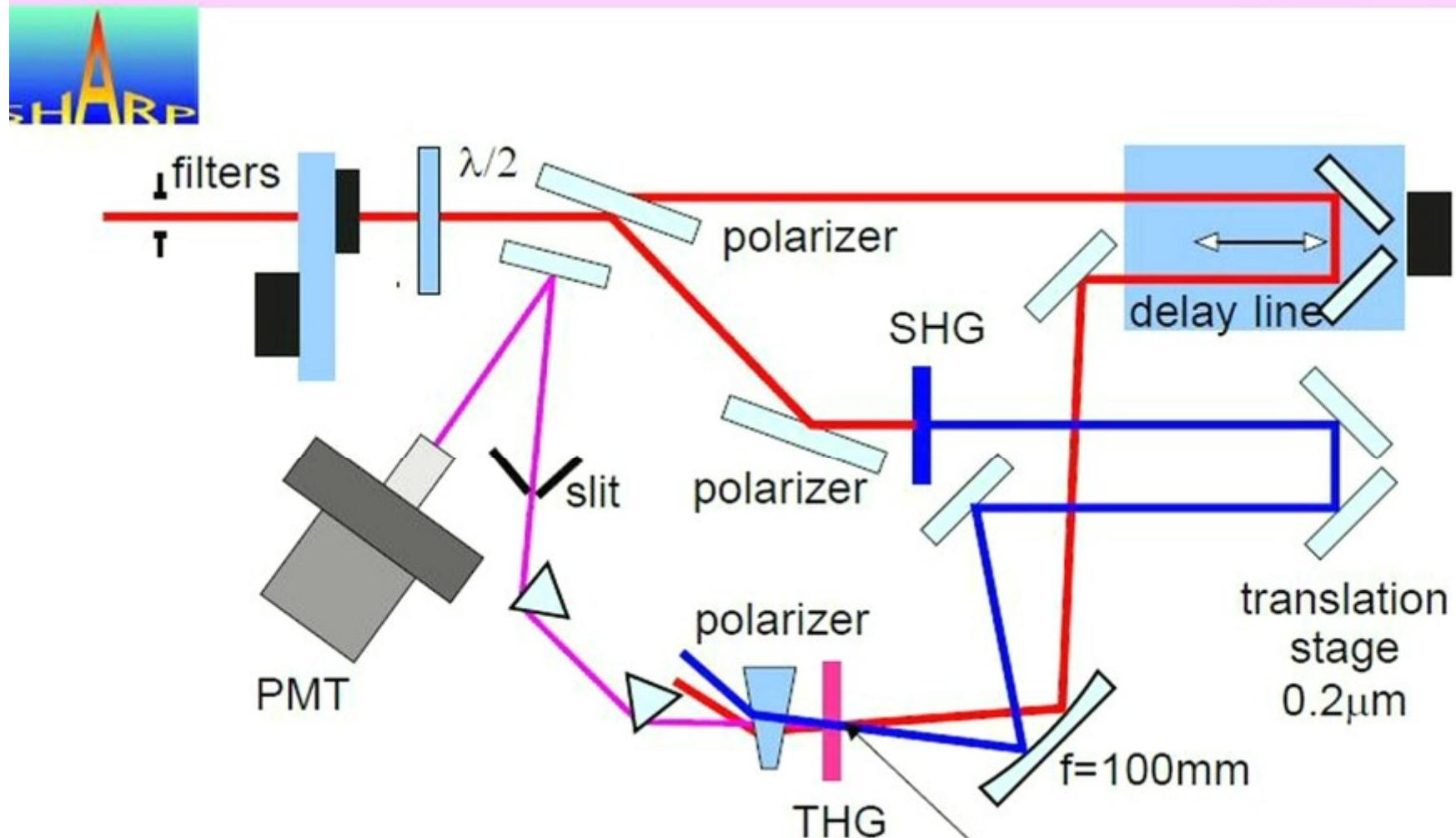
How to measure the contrast within intensity range of 10^{10} - 10^{12} ?



Scanning cross-correlators:

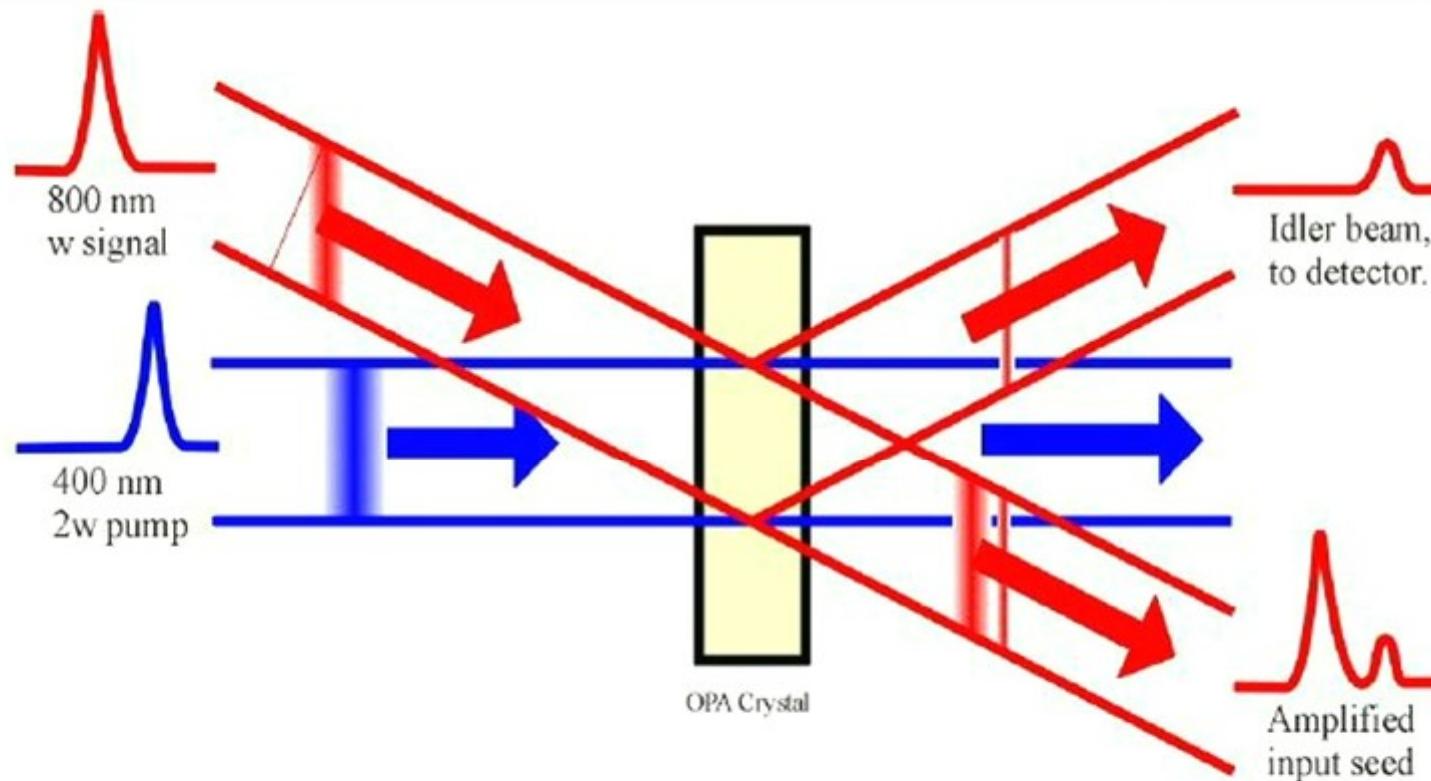
- third order (generation of $3\omega = \omega + 2\omega$)
- optical parametrical (active, amplification)

High dynamic range 3-rd order cross-correlator



- selection of 3ω spectrally,
polarization
- non-collinear

Concept of the OPA correlator



Pedestal is amplified, no longer limited by detector noise.
Idler measurement off axis - direct scatter reduced.

So how do you measure the pulse itself?

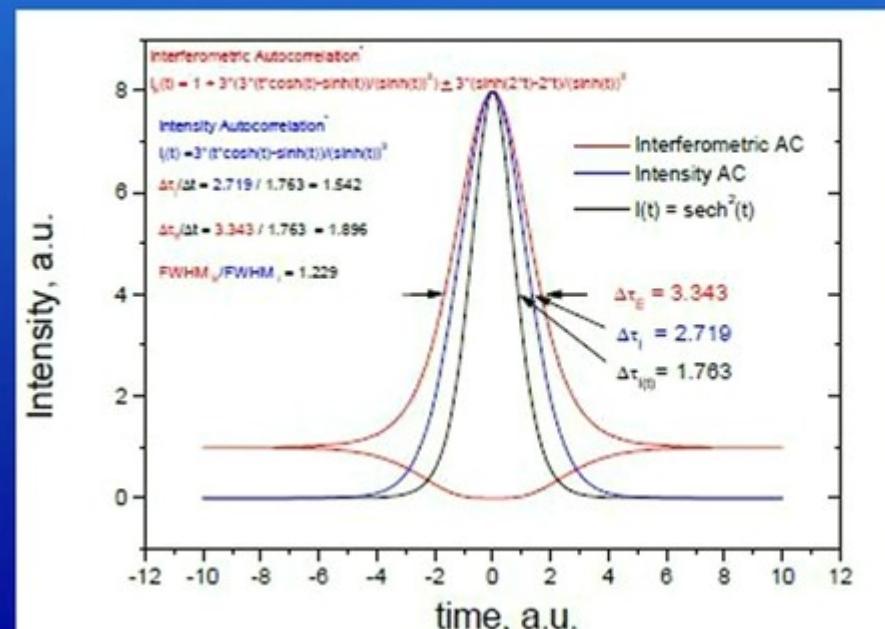
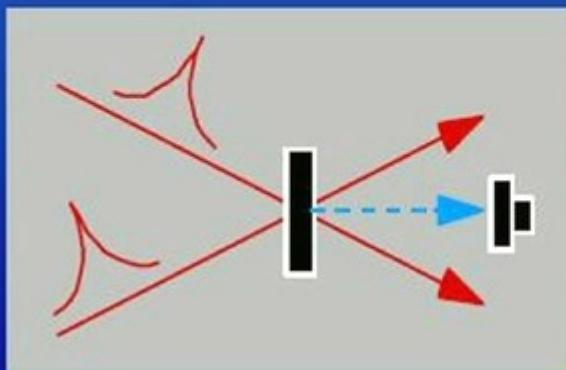
You must use the pulse to measure **itself**.

But that isn't good enough. It's only as short as the pulse.
It's not shorter.

Example: **Intensity Autocorrelation**

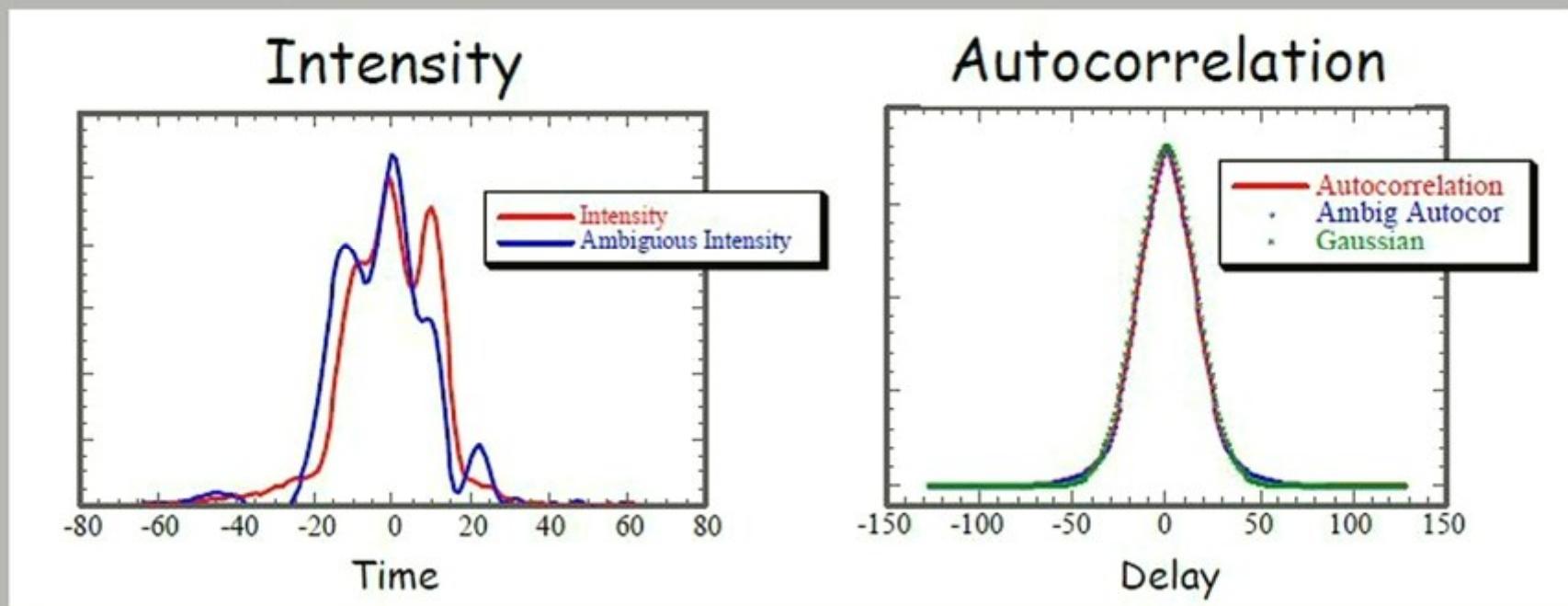
$$\int_{-\infty}^{\infty} I(t)I(t - \tau) dt$$

where $I(t)$ = pulse intensity



Autocorrelations have ambiguities.

These intensities have the same, nearly Gaussian, autocorrelations.



Retrieving the intensity from the autocorrelation is equivalent to the 1D Phase-Retrieval Problem, a well-known unsolvable problem.

We must measure an ultrashort laser pulse's **intensity** and **phase** vs. time or frequency.

A laser pulse has the time-domain electric field:

$$E(t) = \text{Re} \left\{ \sqrt{I(t)} \exp \left[i(\omega_0 t - \phi(t)) \right] \right\}$$

↑ Intensity ↑ Phase

Equivalently, vs. frequency:

(neglecting the negative-frequency component)

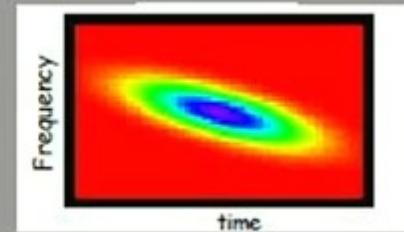
$$\tilde{E}(\omega) = \sqrt{S(\omega)} \exp[-i\varphi(\omega)]$$

↑ Spectrum ↑ Spectral Phase

Knowledge of the **intensity** and **phase** or the **spectrum** and **spectral phase** is sufficient to determine the pulse.

A mathematically rigorous form of the musical score is the “spectrogram.”

If $E(t)$ is the waveform of interest, its spectrogram is:



$$\Sigma_E(\omega, \tau) \equiv \left| \int_{-\infty}^{\infty} E(t) g(t - \tau) \exp(-i\omega t) dt \right|^2$$

where $g(t - \tau)$ is a variable-delay gate function and τ is the delay.
Without $g(t - \tau)$, $\Sigma_E(\omega, \tau)$ would simply be the spectrum.

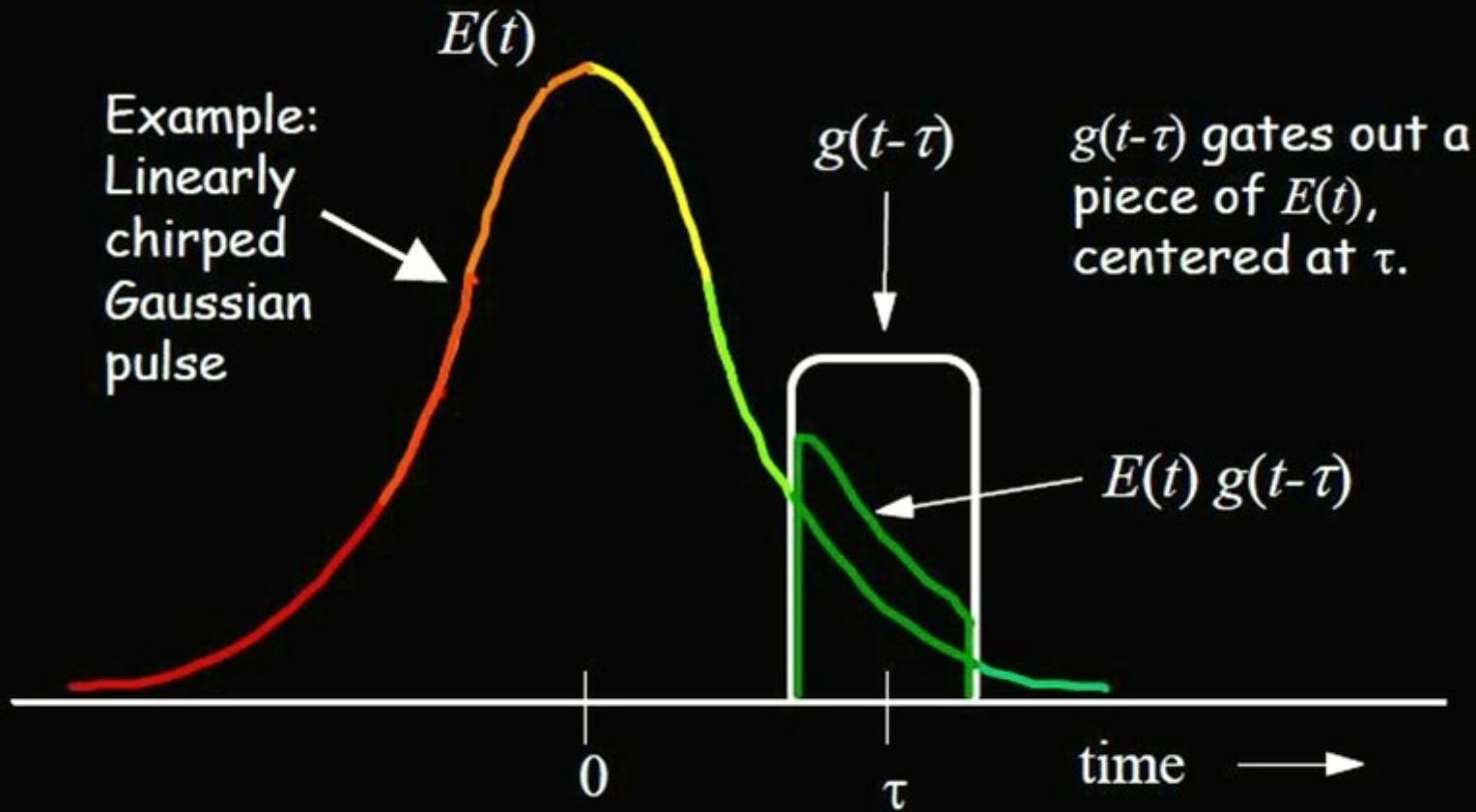
The spectrogram is a function of ω and τ .

It is the set of spectra of all temporal slices of $E(t)$.

The spectrogram is one of many time-frequency quantities, such as the Wigner Distribution and others.

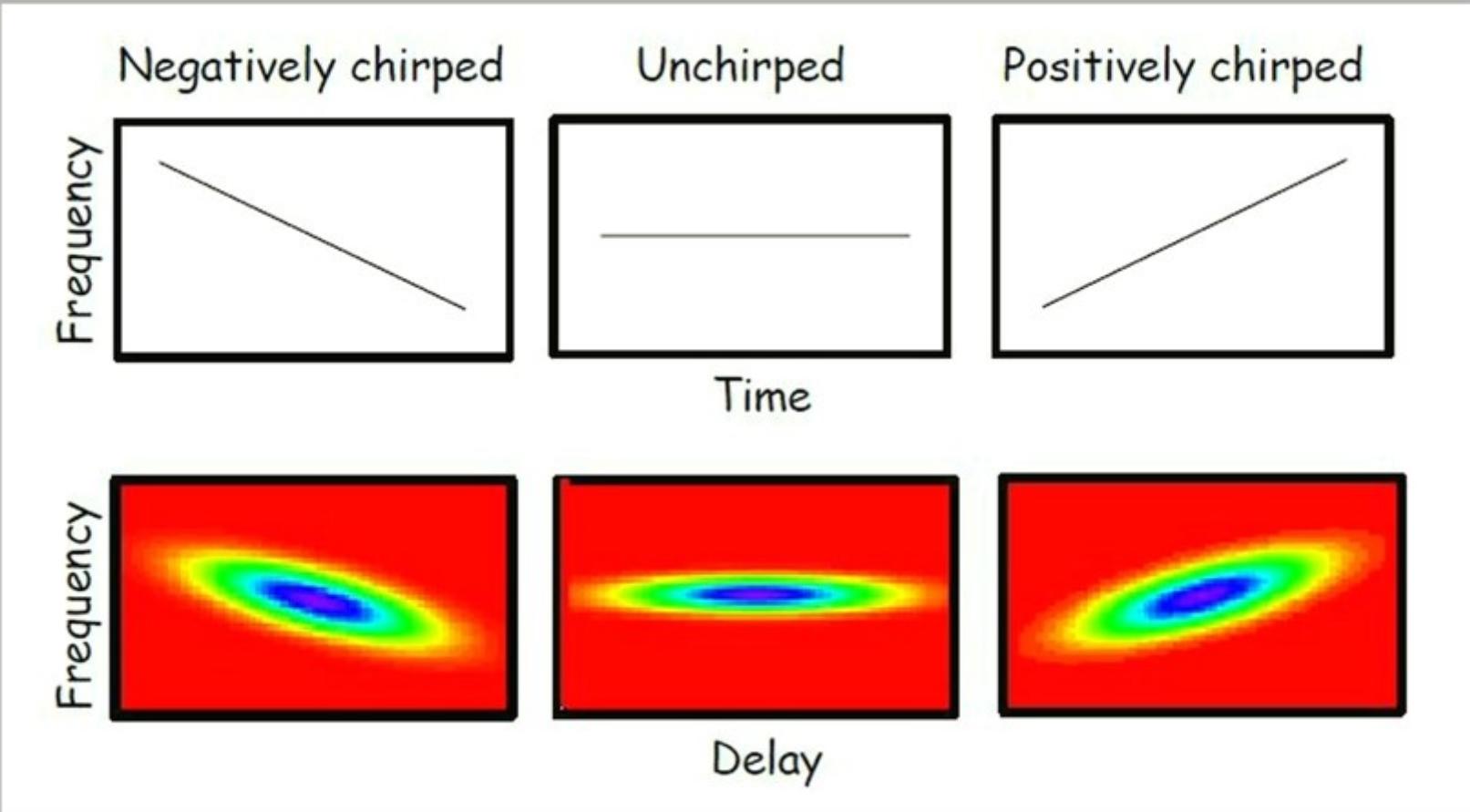
The Spectrogram of a waveform $E(t)$

We must compute the spectrum of the product: $E(t) g(t-\tau)$



The spectrogram tells the color and intensity of $E(t)$ at the time, τ .

Spectrograms for Linearly Chirped Pulses



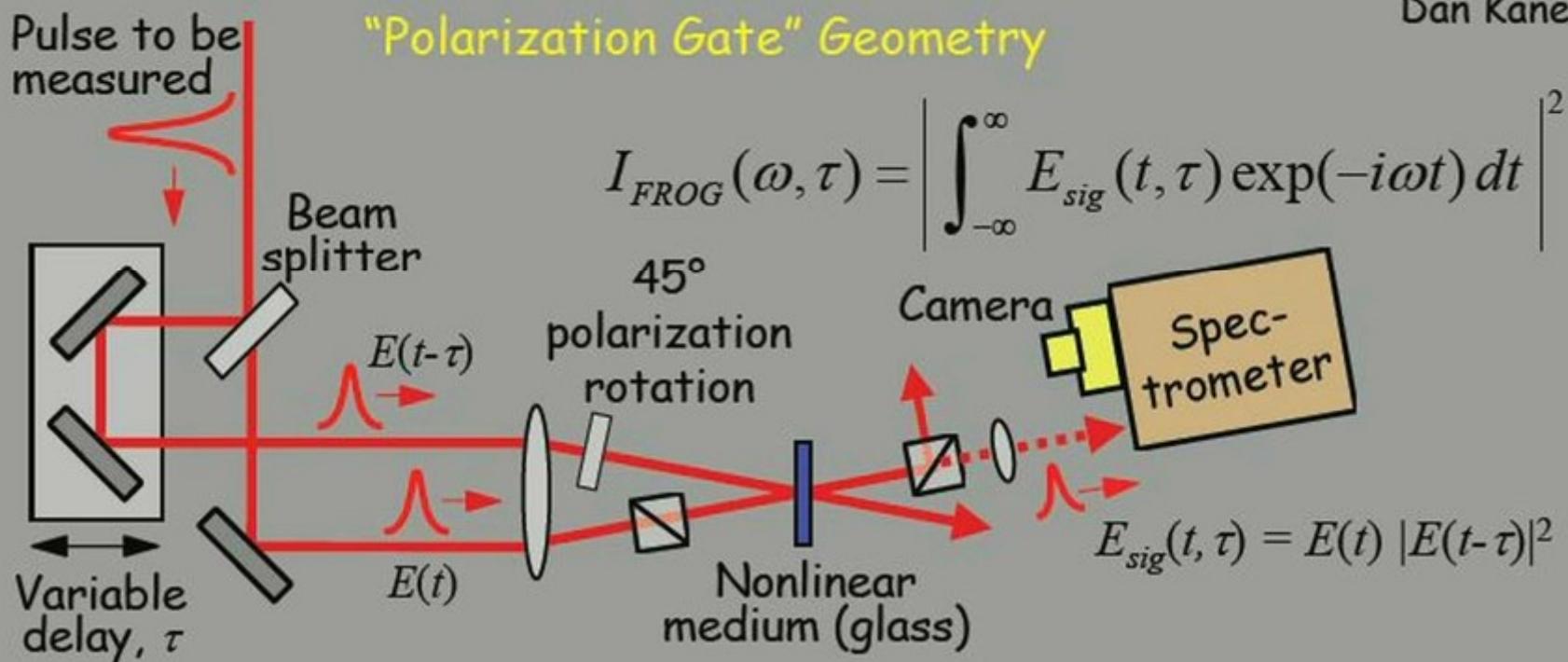
Like a musical score, the spectrogram visually displays the frequency vs. time (and the intensity, too).

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Frequency-Resolved Optical Gating (FROG)

FROG involves gating the pulse with a variably delayed replica of itself in an instantaneous nonlinear-optical medium and then spectrally resolving the gated pulse vs. delay.

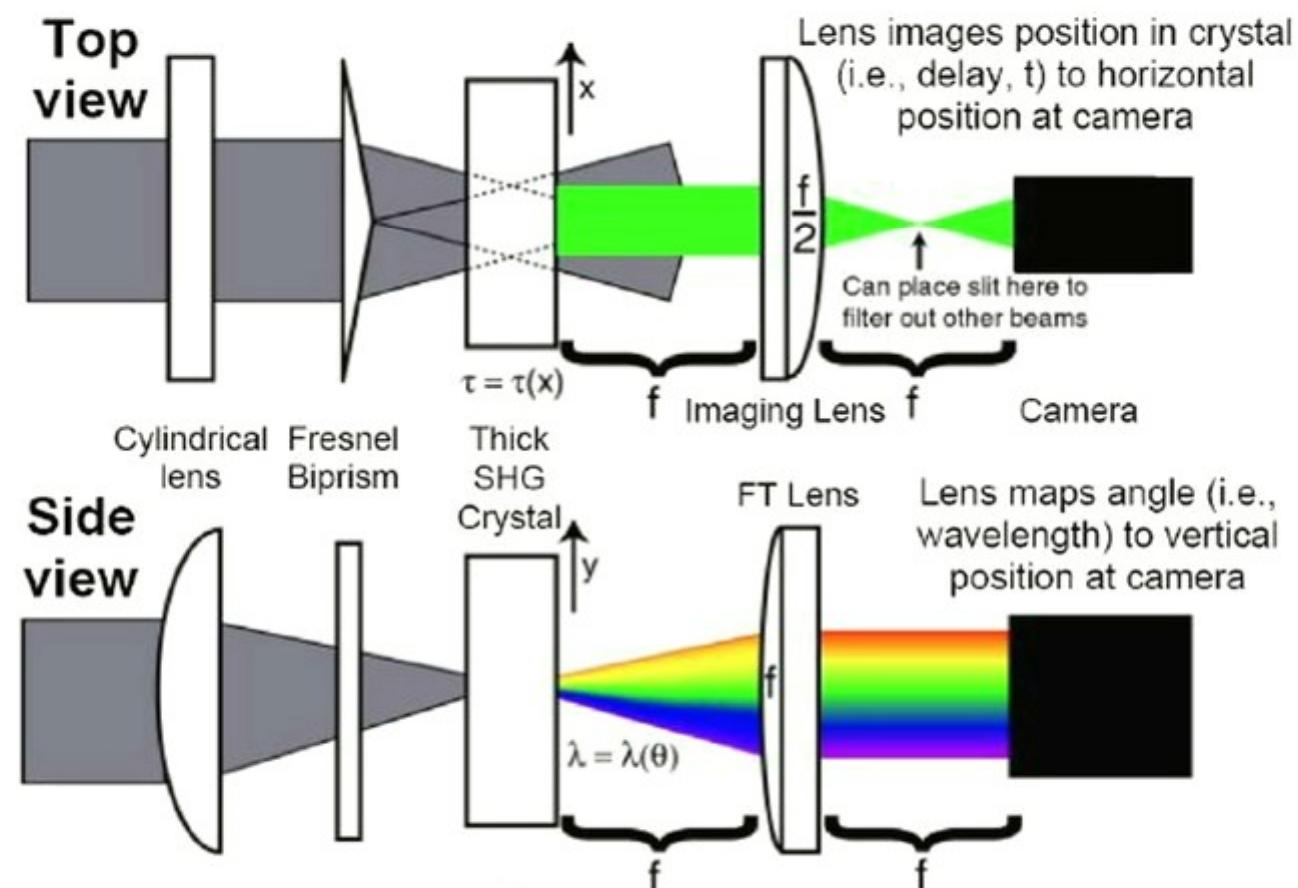
Collaborator:
Dan Kane



Use any ultrafast nonlinearity: Second-harmonic generation, etc.

GRENOUILLE

Grating-Eliminated No-nonsense Observation of
Ultrafast Incident Laser Light E-fields
(GRENOUILLE, which is the French word for "frog").

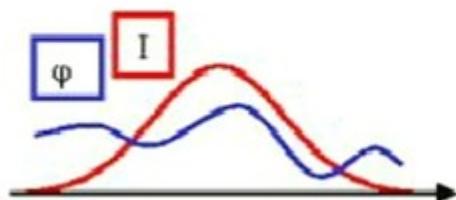


SPIDER

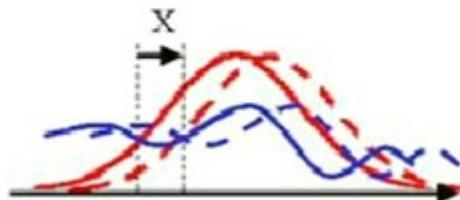
Spectral Phase Interferometry for Direct Electric-Field Reconstruction

based on shearing interferometry in the optical frequency domain

Initial wavefront



Generation of a sheared
wavefront



electric field:

$$E(x) = \sqrt{I(x)} e^{i\phi(x)}$$

shifted:

$$E(x+dx) = \sqrt{I(x+dx)} e^{i\phi(x+dx)}$$

interference pattern as recorded by a
square-law detector:

$$S(x) = I(x) + I(x+dx) + 2\sqrt{I(x)}\sqrt{I(x+dx)} \cos(\phi(x) - \phi(x+dx))$$

phase difference $\Delta\phi(x) = \phi(x) - \phi(x+dx)$ can be easily and algebraically extracted from the interference pattern using standard Fourier processing techniques

spatial phase of the field $\phi(x)$, can then be reconstructed by concatenation

Spectral share interferometry

electric field of the pulse in the frequency domain:

$$\tilde{E}(\omega) = \sqrt{\tilde{I}(\omega)} e^{i\phi(\omega)}$$

shared electric field :

$$\tilde{E}(\omega + d\omega) = \sqrt{\tilde{I}(\omega + d\omega)} e^{i\phi(\omega + d\omega)}$$

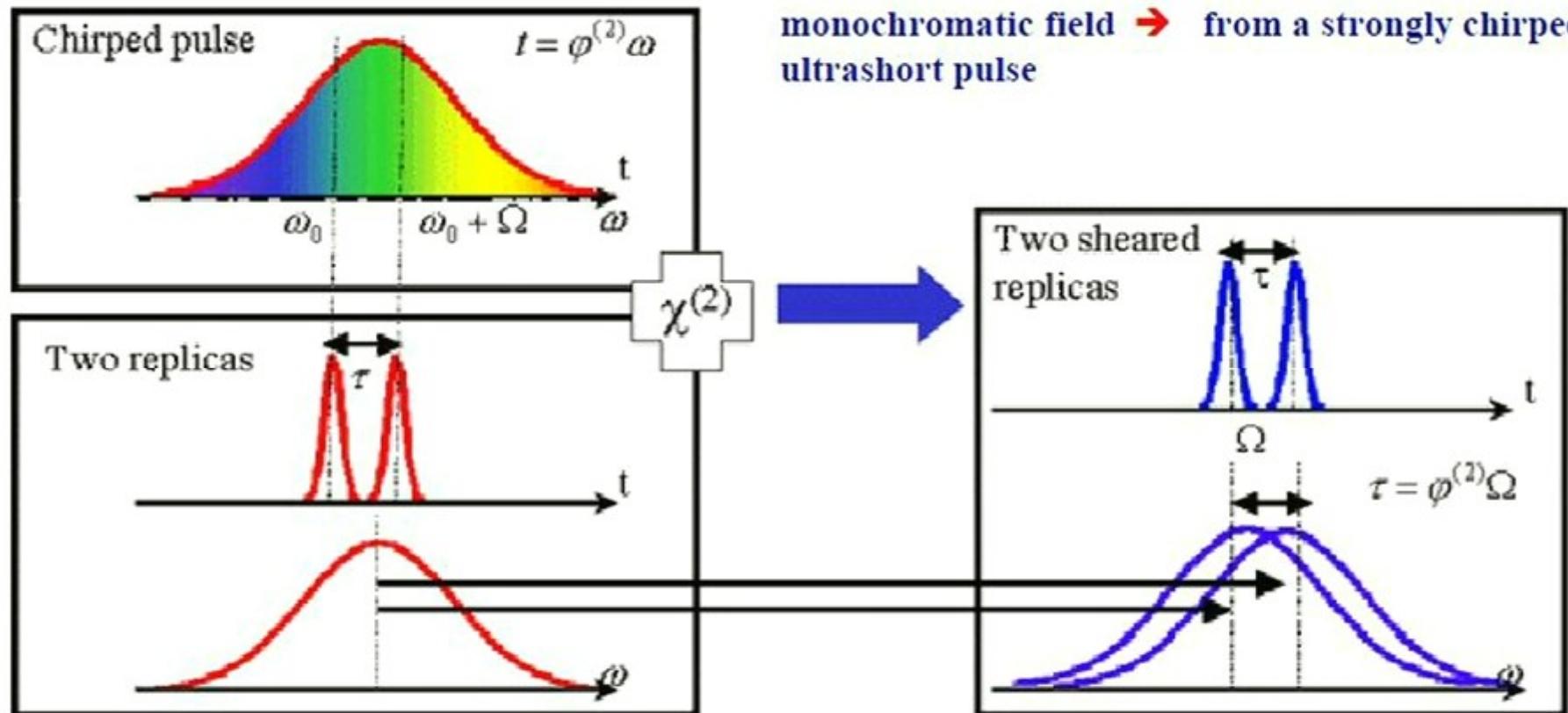
interference pattern: $\tilde{S}(\omega) = \tilde{I}(\omega) + \tilde{I}(\omega + d\omega) + 2\sqrt{\tilde{I}(\omega)}\sqrt{\tilde{I}(\omega + d\omega)} \cos(\phi(\omega) - \phi(\omega + d\omega))$

The spectral phase $\phi(\omega)$ can be extracted in the same way as in the case of spatial shearing

Shearing a complex spectral amplitude can be done by sum frequency generation between a monochromatic field of frequency ω_0 , and the field you want to shear $\tilde{E}(\omega)$, resulting in a sheared field $\tilde{E}(\omega + \omega_0)$

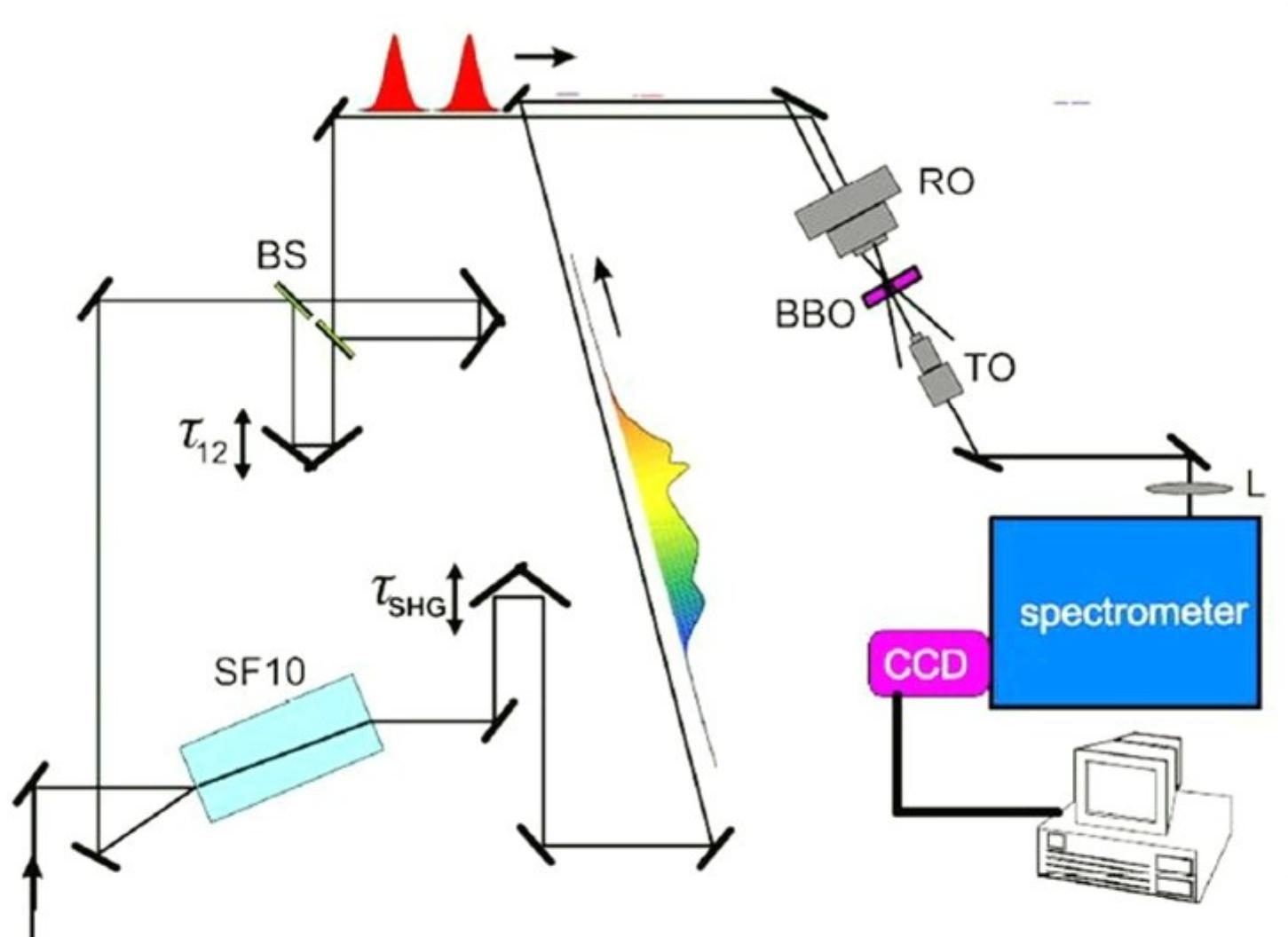
monochromatic frequency → from a strongly chirped ultrashort pulse

SPIDER - principal scheme

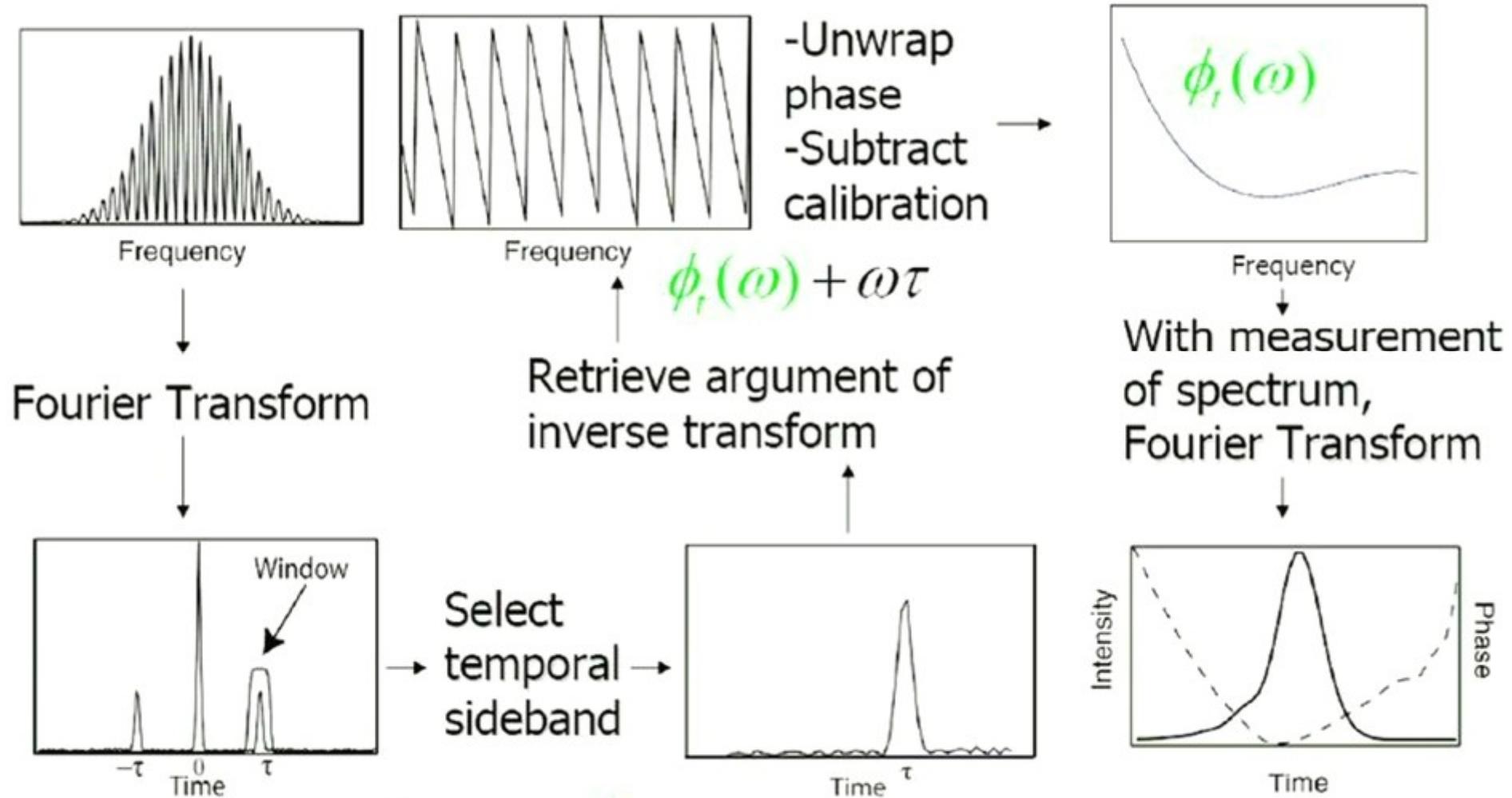


$$\tilde{S}(\omega) = \tilde{I}(\omega + \omega_0) + \tilde{I}(\omega + \omega_0 + \Omega) + 2\sqrt{\tilde{I}(\omega + \omega_0)} 2\sqrt{\tilde{I}(\omega + \omega_0 + \Omega)} \cos(\phi(\omega + \omega_0) - \phi(\omega + \omega_0 + \Omega) + \omega\tau)$$

SPIDER optical setup



Fourier Transform Spectral Interferometry (FTSI)



$$\tilde{S}'(t) = \tilde{A}_{AC}(t - \tau)$$

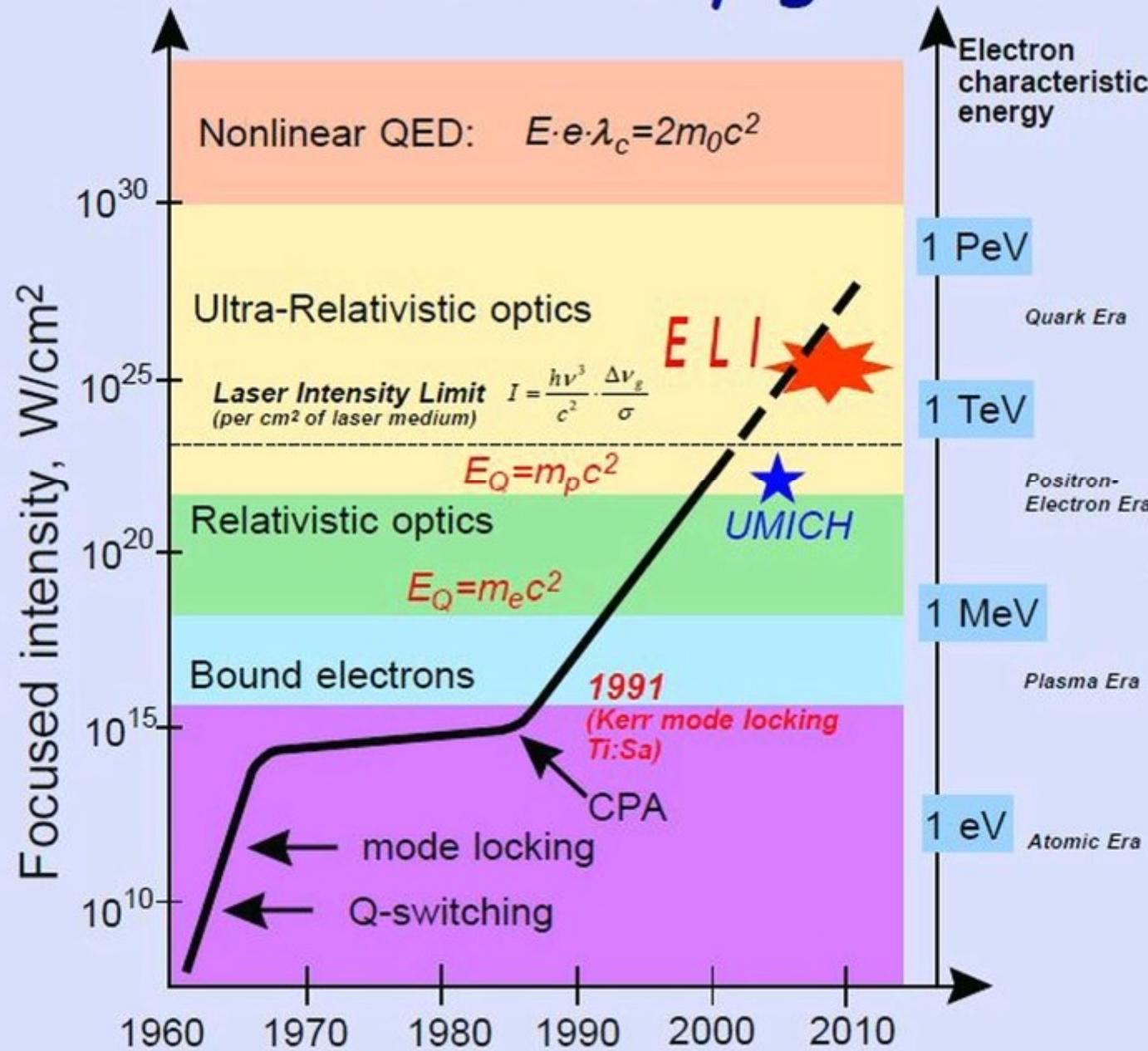
EXTREME LIGHT INFRASTRUCTURE (ELI)

Joint EU-project

Exawatt (10^{18} W) laser facility

Ultra-relativistic Laser-matter Interaction

Laser Intensity growth



Schematic picture of the exawatt system starting with a front-end producing 5-fs pulses at the joule level (PW).

