#physics

Q1

Q₁a

We begin with

$$\left(rac{dQ}{dt}
ight)_{IN} = \dot{Q}_x e_x + Q_x \omega imes e_x + \dot{Q}_y e_y + Q_y \omega imes e_y + \dot{Q}_z e_z + Q_z \omega imes e_z$$

Grouping,

$$egin{aligned} &=\left[\dot{Q}_xe_x+\dot{Q}_ye_y+\dot{Q}_ze_z
ight]+\left[Q_x\omega imes e_x+Q_y\omega imes e_y+Q_z\omega imes e_z
ight] \ &\left[\left(rac{dQ}{dt}
ight)_{IN}=\left(rac{dQ}{dt}
ight)_{ROT}+ec{\omega} imesec{Q} \end{aligned}$$

Q₁b

We begin,

$$\left(rac{dr}{dt}
ight)_{IN} = \left(rac{dR}{dt}
ight)_{IN} + v_r + \omega imes r'$$

Taking time derivatives,

$$\left(rac{d^2r}{dt^2}
ight)_{IN} = \left(rac{d^2R}{dt^2}
ight)_{IN} + rac{d}{dt} \left(rac{dr'}{dt}
ight)_{ROT} + \dot{\omega} imes r' + \omega imes rac{dr'}{dt}$$

Applying Q rule and product rule,

$$\begin{split} \left(\frac{d^2r}{dt^2}\right)_{IN} &= \left(\frac{d^2R}{dt^2}\right)_{IN} + \left(\frac{d^2r'}{dt^2}\right)_{ROT} + \omega \times \left(\frac{dr'}{dt}\right)_{ROT} + \dot{\omega} \times r' + \omega \times \left(\left(\frac{dr'}{dt}\right)_{ROT} + \omega \times r'\right) \\ &\left(\frac{d^2r}{dt^2}\right)_{IN} = \left(\frac{d^2R}{dt^2}\right)_{IN} + \left(\frac{d^2r'}{dt^2}\right)_{ROT} + \omega \times v'_r + \dot{\omega} \times r' + \omega \times (v'_r + \omega \times r') \\ &\left(\frac{d^2\vec{r}}{dt^2}\right)_{IN} = \left(\frac{d^2\vec{R}}{dt^2}\right)_{IN} + \left(\frac{d^2r'}{dt^2}\right)_{ROT} + \dot{\vec{\omega}} \times \vec{r'} + \dot{\vec{\omega}} \times (\vec{\omega} \times \vec{r'}) + 2\vec{\omega} \times \vec{v'}_r \end{split}$$

As desired

Q₁c

By inspection, angular velocity is constant and rotation frame velocity is zero.

$$\left[ec{\dot{\omega}} imesec{r'} o 0
ight]$$

$$\left| 2 ec{\omega} imes ec{v_r'}
ight.
ightarrow 0$$

Q₁d

We make the appropriate substitutions,

$$egin{split} \left(rac{d^2ec{r}}{dt^2}
ight)_{IN} &= \left(rac{d^2ec{R}}{dt^2}
ight)_{IN} + \left(rac{d^2r'}{dt^2}
ight)_{ROT} + ec{\omega} imesec{r'} + ec{\omega} imes(ec{\omega} imesec{r'}) + 2ec{\omega} imesec{v'}_r \ & \\ \left(rac{d^2ec{r}}{dt^2}
ight)_{IN} &= ec{g_0} + \left(rac{d^2r'}{dt^2}
ight)_{ROT} + ec{\omega} imes(ec{\omega} imesec{r'}) \end{split}$$

Moving centrifugal terms to left side, and multiplying by m

$$F_{tot} - ec{\omega} imes (ec{\omega} imes ec{r'}) = m igg(rac{d^2 r'}{dt^2}igg)_{ROT} + m ec{g}_0$$

We now define q

$$\left[ec{g} = ec{g_0} - ec{\omega} imes (ec{\omega} imes ec{r'})
ight]$$

We now define F_{tot} ,

$$egin{align} F_{moon} + mec{g} &= migg(rac{d^2r'}{dt^2}igg)_{ROT} + mec{g}_0 \ \\ migg(rac{d^2r'}{dt^2}igg)_{ROT} &= mec{g} + F_{moon} - mec{g}_0 \ \\ \hline F_{tidal} &= F_{moon} - mec{g}_0 \ \end{bmatrix}$$

If absolute generality is desired, recall that $g_0=\left(rac{d^2R}{dt^2}
ight)_{IN}$. Then, more generally, we can say

$$oxed{F_{tidal} = F_{moon} - migg(rac{d^2ec{R}}{dt^2}igg)_{IN}}$$

Q₁e

This is just gravitational force,

$$migg(rac{d^2ec{R}}{dt^2}igg)_{IN} = -rac{GM_mm}{r^2}\hat{R}_{M-E}$$

$$oxed{\left(rac{d^2ec{R}}{dt^2}
ight)_{IN} = -rac{GM_m}{|ec{R}_{M-E}|^3}ec{R}_{M-E}}$$

We define it negative, since acceleration of the Earth points from Earth to the Moon.

Q1f

We begin,

$$F_{tidal} = F_{moon} - m igg(rac{d^2 ec{R}}{dt^2}igg)_{IN}$$

Use the above $\left(\frac{d^2R}{dt^2}\right)_{IN}$ from e, noting that acceleration now points in the same direction as $-R_{M-E}$,

$$F_{tidal} = igg[rac{GM_m m}{(|ec{R}_{M-E}| + r_E)^2} + rac{GM_m m}{|ec{R}_{M-E}|^3} ec{R}_{M-E}igg] (-\hat{R}_{M-E}) \ F_{tidal} = igg[rac{GM_m m}{|ec{R}_{M-E}|^2 (1 + rac{r_E}{|ec{R}_{M-E}|})^2} + rac{GM_m m}{|ec{R}_{M-E}|^2} igg] (-\hat{R}_{M-E}) pprox rac{GM_m m}{R_{M-E}^2} igg[rac{rac{2r_E}{R_{M-E}}}{1 + rac{2r_E}{R_{M-E}}} igg] (-\hat{R}_{M-E}) \ igg[F_{tidal} pprox rac{GM_m m}{R_{M-E}^2} igg[rac{2r_E}{R_{M-E} + 2r_E} igg] (-\hat{R}_{M-E}) igg]$$

Direction is from Moon to Earth.

$$oxed{\left|F_{tidal}
ight|pproxrac{GM_{m}m}{R_{M-E}^{2}}igg[rac{2r_{E}}{R_{M-E}+2r_{E}}
ight]}$$

Q2

Q2a

$$\left. \left(rac{dQ}{dt}
ight)
ight|_{IN} = \left(rac{dQ}{dt}
ight)_{ROT} + \left[ec{\omega} imes ec{Q}
ight]$$

Applying this,

$$\left. \left(rac{dr_lpha'}{dt}
ight)
ight|_{IN} = \left(rac{dr_lpha'}{dt}
ight)_{ROT} + ec{\omega} imes ec{r_lpha'}$$

Since the masses are glued to the axes directly, the position vectors do not change in the rotating frame. Therefore,

$$\left(rac{dr_{lpha}'}{dt}
ight)_{ROT} = 0 \implies \left[\left(rac{dr_{lpha}'}{dt}
ight)_{FIX} = ec{\omega} imes ec{r_{lpha}'}
ight]$$

as desired

Q₂b

Multiply both sides by $m_{\alpha}\vec{r_{\alpha}'}$,

$$\left(rac{dr'_lpha}{dt}
ight)_{FIX} = ec{\omega} imesec{r'_lpha} \implies m_lphaec{r'_lpha} imes\left(rac{dr'_lpha}{dt}
ight)_{FIX} = m_lphaec{r'_lpha} imes(ec{\omega} imesec{r'_lpha})$$

Applying vector identity,

$$m_lpha ec{r_lpha'} imes \left(rac{dr_lpha'}{dt}
ight)_{FIX} = m_lpha |r_lpha'|^2 ec{\omega} - m_lpha (ec{r_lpha'} \cdot ec{\omega}) ec{r_lpha'}$$

Sum over all α and use tensor notation,

$$ec{r_lpha'} imes m_lpha \dot{r}_lpha' = m_lpha igg[\omega_i |r_lpha'|^2 - x_{lpha i}(x_{lpha j}\omega_j)igg] \$\$Explicitly writing the summations, \$\$igg[\sum_lpha ec{r_lpha'} imes m_lpha \dot{r}_lpha' = \sum_lpha m_lpha igg[\omega_i |r_lpha'|^2 + x_{lpha i}(x_{lpha j}\omega_j)igg] \$$$

As desired

Q₂c

$$egin{aligned} \sum_{lpha}ec{r_lpha'} imes m_lpha\dot{r}_lpha' &= \sum_lpha m_lphaigg[\omega_i|r_lpha'|^2 - x_{lpha i}\sum_j x_{lpha j}\omega_jigg] \ I_{ij} &= \sum_lpha m_lphaigg[\delta_{ij}|ec{r}_lpha'|^2 - x_{lpha i}x_{lpha j}igg] \end{aligned}$$

Rearranging the first, to fit I_{ij} ,

$$oxed{\sum_{j}I_{ij}\omega_{j}=\sum_{lpha}ec{r_{lpha}^{\prime}} imes m_{lpha}\dot{r}_{lpha}^{\prime}}$$

This is just the sum of angular momenta is the moment of inertia multiplied by the angular frequency.

Q3

Q3a

West side is further from center. Since Earth spins West to East, in northern hemisphere, water deflects west.

Q3b

The vertical component of angular velocity is $\omega \sin 30 = \omega/2$, so the horizontal force is then

$$a_{horiz}=2S imes\omega=2S\omega/2=S\omega$$

The vertical component is simply gravity, so the bouyant force angle is then below. This is perpendicular to the surface tilt, so finding surface tilt angle inverts the arguments,

$$an heta = rac{g}{\omega S} \implies an(heta_{tilt}) = rac{\omega S}{g}$$

Height is then

$$\Delta h = W an(heta_{tilt}) = \boxed{\Delta h = rac{S\omega}{g}W}$$

Q₃c

Wind travels west

At the equator, air travels West relative to the ground. It moves from east to west.

This is intuitive from the coriolis effect. Below the equator, air approaches from the South and is therefore deflected to the left by the coriolis effect. This leftward deflection approaching from South corresponds to moving west from East to West. Above the equator in the northern hemisphere, air approaches from the North, and the deflection is toward the right. Air approaches from the north, and again, this corresponds to moving west from East to West.

Q3d

Larger angular velocity.

Barely above ground so ground travels at around same speed stationary. But also traveling eastward (with the Earth) relative to the ground, so it has a faster angular velocity.

Yes They both point radially outward if the object is moving Eastward at the equator like the rocket.

Yes Simple angular velocity to translational velocity conversion.

Q4

Q4a

The angular velocity vector points up from the north pole. Using conventional handedness, the y' direction must be pointing north. From the λ latitude, we can draw a diagram and see

$$oxed{\omega_{x'}=0, \;\;\; \omega_{y'}=\omega\cos(\lambda), \;\;\; \omega_{z'}=\omega\sin(\lambda)}$$

Q4b

$$V_{x'}=V_0\cos(lpha),~~V_{z'}=V_0\sin(lpha)$$

From simple physics,

$$oxed{v_{x'}^{0th} = V_0 \cos(lpha), \;\; v_{z'}^{0th} = V_0 \sin(lpha) - gt, \;\; v_{y'}^{0th} = 0}$$

Q4c

We have

$$\omega_{y'} = \omega \cos(\lambda), ~~ \omega_{z'} = \omega \sin(\lambda)$$

Computing $a=2v_r^{0th} imes \omega$ is then trivial,

$$egin{aligned} a_{x'} &= 2\omega(v_{y'}\sin(\lambda) - v_{z'}\cos(\lambda)) \ \ a_{y'} &= -2\omega v_{x'}\sin(\lambda), \quad a_{z'} &= 2\omega v_{x'}\cos(\lambda) \end{aligned}$$

We add the zeroth order velocities from the previous answer,

$$oxed{a_{x'} = -2\omega(V_0\sin(lpha) - gt)\cos(\lambda)}$$

$$oxed{a_{y'} = -2\omega V_0 \cos(lpha) \sin(\lambda), \quad a_{z'} = 2\omega V_0 \cos(lpha) \cos(\lambda)}$$

Q4d

We have

$$egin{aligned} \ddot{z}(t) &= ec{g}_z - a_{z'} = -g + 2\omega V_0 \cos(lpha) \cos(\lambda) \ \int_0^t dt \ddot{z} &= \dot{z}(t) - \dot{z}(0) = (-g + 2\omega V_0 \cos(lpha) \cos(\lambda))t, \quad z'(0) = V_0 \sin(lpha) \ \implies \dot{z}(t) &= (2\omega V_0 \cos(lpha) \cos(\lambda) - g)t + V_0 \sin(lpha) \end{aligned}$$

Repeating,

$$\int_0^t dt \ \dot{z} = z(t) - z(0) = (2\omega V_0 \cos(lpha) \cos(\lambda) - g)t^2/2 + V_0 \sin(lpha)t, \quad z(0) = 0$$

$$\implies \boxed{z'(t) = rac{2\omega V_0 \cos(lpha) \cos(\lambda) - g}{2}t^2 + V_0 \sin(lpha)t}$$

Q4e

We set z(t) = 0 and assume t > 0,

$$0 = rac{2\omega V_0 \cos(lpha) \cos(\lambda) - g}{2} t^2 + V_0 \sin(lpha) t \ t = rac{2V_0 \sin(lpha)}{g - 2\omega V_0 \cos(lpha) \cos(\lambda)}$$

We apply the "tiny" approximatin,

$$t = rac{2V_0\sin(lpha)}{g}(1-rac{2\omega V_0\cos(lpha)\cos(\lambda)}{g})^{-1}$$

We expect ω to be small, so

$$tpprox rac{2V_0\sin(lpha)}{g}(1+rac{2\omega V_0\cos(lpha)\cos(\lambda)}{g})$$

$$tpprox rac{2V_0\sin(lpha)}{g^2}(g+2\omega V_0\cos(lpha)\cos(\lambda))$$

Q4f

y'(t) points North

We begin as before,

$$\ddot{y}(t) = a_{y'} = -2\omega V_0 \cos(lpha) \sin(\lambda)$$

Integrating twice,

$$y'(t) = -\omega V_0 \cos(\alpha) \sin(\lambda) t^2 + At + B$$

 $\dot{y}(0) = y(0) = 0$, so constants of integration are zero

$$y'(t) = -\omega V_0 \cos(lpha) \sin(\lambda) t^2$$

Q4f

Yes it is already proportional to ω .

Q4h

The conditions are met, and north/south correspond to y and z. From before, we use the velocity to find position and solve for landing time in zeroth order,

$$egin{aligned} v^{0th}_{z'} &= V_0 \sin(lpha) - gt \implies z'^{0th} = V_0 \sin(lpha) t - g t^2/2 \ &\Longrightarrow z'(0) = 0 \implies t_{landing} = rac{2V_0}{g} \sin(lpha) \end{aligned}$$

We now use our coriolis-inclusive y' to get,

$$y'(t) = -\omega V_0 \cos(\alpha) \sin(\lambda) t^2 = -\omega V_0 \cos(\alpha) (\frac{2V_0}{g} \sin(\alpha))^2$$

$$y'(t_{landing}) = -\omega \frac{4V_0^3}{g^2} \sin^2(\alpha) \cos(\alpha)$$

The projectile will land South at a distance of $\omega \frac{4V_0^3}{g^2} \sin^2(\alpha) \cos(\alpha)$.