# 28GHz POWDER Measurements

# Spatial Consistency Modeling

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August 2023

# 1 Spatial Autocorrelation Coefficient

The small-scale spatial autocorrelation coefficient is a metric to characterize the coherence between the voltage amplitudes of received signals across variations in distances, alignment accuracies, and relative velocities.

## 1.1 Separation in Distance

The spatial autocorrelation coefficient  $\rho$  vis-à-vis a separation in distance  $\Delta d$ :

$$\rho(\Delta d) = \rho\Big(\mathbf{x}_{\mathrm{Tx}}, \|\mathbf{x}_{\mathrm{Rx}}(t') - \mathbf{x}_{\mathrm{Rx}}(t)\| = \Delta d, \ \phi(t') = \phi(t), \ v(t') = v(t)\Big), \text{ where}$$

- $\mathbf{x}_{\mathrm{Tx}}(t) = \mathbf{x}_{\mathrm{Tx}}, \forall t \text{ denotes the 3-D position vector of the Tx (fixed)};$
- $\mathbf{x}_{Rx}(t)$  and  $\mathbf{x}_{Rx}(t')$  denote the Rx 3-D position vectors at times t and t', respectively, with  $\Delta d$  being the 3-D Euclidean distance between them;
- $\phi(t)$  and  $\phi(t')$  are the absolute errors in alignment between Tx and Rx antennas (deviation from perfect alignment) at times t and t', respectively;
- v(t) and v(t') denote the relative velocities of the receiver with respect to the transmitter at times t and t', respectively; and
- The conditions  $\phi(t')=\phi(t)$  and v(t')=v(t) ensure that while studying the signal coherence characteristics vis-à-vis a separation in distance  $\Delta d$ , other variables in our measurements (i.e., alignment and velocity) are unchanged.

Mathematically, this spatial autocorrelation coefficient  $\rho(\Delta d)$  is given by

$$\frac{\mathbb{E}\left[\left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right) \cdot \left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right)\right]}{\sqrt{\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right\|^{2}\right]}\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right\|^{2}\right]}}$$

For a route  $\mathcal{R}$ , we define the terms employed in this equation as follows.

Tx configuration:  $\mathcal{P}_{Tx}(t) = \mathcal{P}_{Tx}(t') = \{\mathbf{x}_{Tx}, \ \theta_{Tx}\}, \ \forall t, \ t' \in \mathcal{R};$ 

$$\text{Rx configuration: } \mathcal{P}_{\text{Rx}}(t) = \left\{\mathbf{x}_{\text{Rx}}, \theta_{\text{Rx}}, v_{\text{Rx}}\right\}, \\ \mathcal{P}_{\text{Rx}}(t') = \left\{\mathbf{x}_{\text{Rx}}^{'}, \theta_{\text{Rx}}^{'}, v_{\text{Rx}}^{'}\right\}, \ \forall t, t' \in \mathcal{R}; \\$$

$$\textbf{Evaluation conditions E1:} \ \left\| \mathbf{x}_{\mathrm{Rx}}^{'} - \mathbf{x}_{\mathrm{Rx}} \right\| = \Delta d, \\ \phi(\theta_{\mathrm{Tx}}^{'}, \theta_{\mathrm{Rx}}^{'}) = \phi(\theta_{\mathrm{Tx}}, \theta_{\mathrm{Rx}}), \\ v_{\mathrm{Rx}}^{'} = v_{\mathrm{Rx}}. \\$$

Let N be the number of resolvable Multi-Path Components (MPCs) extracted via the SAGE algorithm at time t at Rx config  $\mathcal{P}_{Rx}(t)$ , with Tx config being  $\mathcal{P}_{Tx}(t)$ ; and let  $A_i$  be the amplitude of the  $i^{\text{th}}$  MPC. Then,

Sample Mean of MPC amplitudes: 
$$\mu(\mathcal{P}_{Tx}(t), \mathcal{P}_{Rx}(t)) = \frac{1}{N} \sum_{i=1}^{N} A_i$$
.

 $\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\right)$  denotes the vector of amplitudes of the MPCs extracted from the measurements collected at the receiver at time t when the Rx config is  $\mathcal{P}_{\mathrm{Rx}}(t)$  and the Tx config is  $\mathcal{P}_{\mathrm{Tx}}(t)$ . Mathematically,

$$\mathbf{A}\Big(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\Big) = [A_1,A_2,\ldots,A_N].$$

The expectation  $\mathbb{E}[\cdot]$  in the above equation for  $\rho(\Delta d)$  is taken over all Tx and Rx configs along the route  $\mathcal{R}$  that satisfy the evaluation conditions **E1**.

The product within the  $\mathbb{E}[\cdot]$  operator in the numerator of  $\rho(\Delta d)$  is a dot-product between the two N-dimensional mean-shifted amplitude vectors.

Note that, to maintain consistency in the vector lengths throughout, we preset the number of MPCs to be considered  $(N^*)$ . So, at the two time-steps along the route t and t', if SAGE returns a different number of MPCs (N for the Tx-Rx config at time t and N' for the Tx-Rx config at time t',  $N \neq N'$ ) and if  $N > N^*$  and/or  $N' > N^*$ , then we pick the  $N^*$ -most amplitude-dominant MPCs.

#### 1.2 Separation in Alignment

The spatial autocorrelation coefficient  $\rho$  vis-à-vis a separation in alignment  $\phi$ :

$$\rho(\Delta\phi) = \rho\Big(\mathbf{x}_{\mathrm{Tx}}, \ \mathbf{x}_{\mathrm{Rx}}(t') = \mathbf{x}_{\mathrm{Rx}}(t), \ |\phi(t') - \phi(t)| = \Delta\phi, \ v(t') = v(t)\Big), \text{ where}$$

- $\mathbf{x}_{\mathrm{Tx}}(t) = \mathbf{x}_{\mathrm{Tx}}, \forall t \text{ denotes the 3-D position vector of the Tx (fixed)};$
- $\mathbf{x}_{Rx}(t)$  and  $\mathbf{x}_{Rx}(t')$  denote the 3-D position vectors of the Rx, at times t and t', respectively;
- $\phi(t)$  and  $\phi(t')$  are the absolute errors in alignment between Tx and Rx antennas (deviation from perfect alignment) at times t and t', respectively, with  $\Delta \phi$  being the difference in alignment accuracies between them;

- v(t) and v(t') denote the relative velocities of the receiver with respect to the transmitter at times t and t', respectively; and
- The conditions  $\mathbf{x}_{\mathrm{Rx}}(t') = \mathbf{x}_{\mathrm{Rx}}(t)$  and v(t') = v(t) ensure that while studying the signal coherence characteristics vis-à-vis a separation in alignment  $\Delta \phi$ , other variables (i.e., distance and velocity) remain unchanged.

Mathematically, this spatial autocorrelation coefficient  $\rho(\Delta\phi)$  is given by

$$\frac{\mathbb{E}\left[\left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right) \cdot \left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right)\right]}{\sqrt{\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right\|^{2}\right]}\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right\|^{2}\right]}}$$

For a route  $\mathcal{R}$ , we define the terms employed in this equation as follows.

Tx configuration:  $\mathcal{P}_{Tx}(t) = \mathcal{P}_{Tx}(t') = \{\mathbf{x}_{Tx}, \ \theta_{Tx}\}, \ \forall t, \ t' \in \mathcal{R};$ 

Rx configuration: 
$$\mathcal{P}_{Rx}(t) = \{\mathbf{x}_{Rx}, \theta_{Rx}, v_{Rx}\}, \mathcal{P}_{Rx}(t') = \{\mathbf{x}_{Rx}^{'}, \theta_{Rx}^{'}, v_{Rx}^{'}\}, \ \forall t, t' \in \mathcal{R};$$

Evaluation conditions E2: 
$$\mathbf{x}_{\mathrm{Rx}}^{'} = \mathbf{x}_{\mathrm{Rx}}, \left| \phi(\theta_{\mathrm{Tx}}^{'}, \theta_{\mathrm{Rx}}^{'}) - \phi(\theta_{\mathrm{Tx}}, \theta_{\mathrm{Rx}}) \right| = \Delta \phi, v_{\mathrm{Rx}}^{'} = v_{\mathrm{Rx}}$$

Let N be the number of resolvable Multi-Path Components (MPCs) extracted via the SAGE algorithm at time t at Rx config  $\mathcal{P}_{Rx}(t)$ , with Tx config being  $\mathcal{P}_{Tx}(t)$ ; and let  $A_i$  be the amplitude of the  $i^{\text{th}}$  MPC. Then,

Sample Mean of MPC amplitudes: 
$$\mu\left(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\right) = \frac{1}{N} \sum_{i=1}^{N} A_{i}$$
.

 $\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\right)$  denotes the vector of amplitudes of the MPCs extracted from the measurements collected at the receiver at time t when the Rx config is  $\mathcal{P}_{\mathrm{Rx}}(t)$  and the Tx config is  $\mathcal{P}_{\mathrm{Tx}}(t)$ . Mathematically,

$$\mathbf{A}\Big(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\Big) = [A_1, A_2, \dots, A_N].$$

The expectation  $\mathbb{E}[\cdot]$  in the above equation for  $\rho(\Delta\phi)$  is taken over all Tx and Rx configs along the route  $\mathcal{R}$  that satisfy the evaluation conditions **E2**.

The product within the  $\mathbb{E}[\cdot]$  operator in the numerator of  $\rho(\Delta\phi)$  is a dot-product between the two N-dimensional mean-shifted amplitude vectors.

Note that, to maintain consistency in the vector lengths throughout, we preset the number of MPCs to be considered  $(N^*)$ . So, at the two time-steps along the route t and t', if SAGE returns a different number of MPCs (N for the Tx-Rx config at time t and N' for the Tx-Rx config at time t',  $N \neq N'$ ) and if  $N > N^*$  and/or  $N' > N^*$ , then we pick the  $N^*$ -most amplitude-dominant MPCs.

## 1.3 Separation in Velocity

The spatial autocorrelation coefficient  $\rho$  vis-à-vis a separation in velocity v:

$$\rho(\Delta v) = \rho\Big(\mathbf{x}_{\mathrm{Tx}}, \ \mathbf{x}_{\mathrm{Rx}}(t') = \mathbf{x}_{\mathrm{Rx}}(t), \ \phi(t') = \phi(t), \ |v(t') - v(t)| = \Delta v\Big), \text{ where}$$

- $\mathbf{x}_{\mathrm{Tx}}(t) = \mathbf{x}_{\mathrm{Tx}}, \forall t \text{ denotes the 3-D position vector of the Tx (fixed)};$
- $\mathbf{x}_{Rx}(t)$  and  $\mathbf{x}_{Rx}(t')$  denote the 3-D position vectors of the Rx, at times t and t', respectively;
- $\phi(t)$  and  $\phi(t')$  are the absolute errors in alignment between Tx and Rx antennas (deviation from perfect alignment) at times t and t', respectively;
- v(t) and v(t') denote the relative velocities of the receiver with respect to the transmitter at times t and t', respectively, with  $\Delta v$  being the difference in Rx velocities to get to positions  $\mathbf{x}_{\mathrm{Rx}}(t)$  and  $\mathbf{x}_{\mathrm{Rx}}(t')$ ; and
- The conditions  $\mathbf{x}_{\mathrm{Rx}}(t') = \mathbf{x}_{\mathrm{Rx}}(t)$  and  $\phi(t') = \phi(t)$  ensure that while the signal coherence characteristics vis-à-vis a separation in velocity  $\Delta v$  are being studied, other variables (i.e., distance and alignment) remain unchanged.

Mathematically, this spatial autocorrelation coefficient  $\rho(\Delta v)$  is given by

$$\frac{\mathbb{E}\left[\left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right) \cdot \left(\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right)\right]}{\sqrt{\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t),\mathcal{P}_{\mathrm{Rx}}(t)\right)\right\|^{2}\right]}\mathbb{E}\left[\left\|\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right) - \mu\left(\mathcal{P}_{\mathrm{Tx}}(t'),\mathcal{P}_{\mathrm{Rx}}(t')\right)\right\|^{2}\right]}}.$$

For a route  $\mathcal{R}$ , we define the terms employed in this equation as follows.

Tx configuration:  $\mathcal{P}_{Tx}(t) = \mathcal{P}_{Tx}(t') = \{\mathbf{x}_{Tx}, \ \theta_{Tx}\}, \ \forall t, \ t' \in \mathcal{R};$ 

Rx configuration: 
$$\mathcal{P}_{Rx}(t) = \{\mathbf{x}_{Rx}, \theta_{Rx}, v_{Rx}\}, \mathcal{P}_{Rx}(t') = \{\mathbf{x}'_{Rx}, \theta'_{Rx}, v'_{Rx}\}, \ \forall t, t' \in \mathcal{R};$$

Evaluation conditions E3: 
$$\mathbf{x}_{\mathrm{Rx}}^{'} = \mathbf{x}_{\mathrm{Rx}}, \phi(\theta_{\mathrm{Tx}}^{'}, \theta_{\mathrm{Rx}}^{'}) = \phi(\theta_{\mathrm{Tx}}, \theta_{\mathrm{Rx}}), \left| v_{\mathrm{Rx}}^{'} - v_{\mathrm{Rx}} \right| = \Delta v.$$

Let N be the number of resolvable Multi-Path Components (MPCs) extracted via the SAGE algorithm at time t at Rx config  $\mathcal{P}_{Rx}(t)$ , with Tx config being  $\mathcal{P}_{Tx}(t)$ ; and let  $A_i$  be the amplitude of the  $i^{th}$  MPC. Then,

Sample Mean of MPC amplitudes: 
$$\mu\left(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\right) = \frac{1}{N} \sum_{i=1}^{N} A_{i}$$
.

 $\mathbf{A}\left(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\right)$  denotes the vector of amplitudes of the MPCs extracted from the measurements collected at the receiver at time t when the Rx config is  $\mathcal{P}_{\mathrm{Rx}}(t)$  and the Tx config is  $\mathcal{P}_{\mathrm{Tx}}(t)$ . Mathematically,

$$\mathbf{A}\Big(\mathcal{P}_{\mathrm{Tx}}(t), \mathcal{P}_{\mathrm{Rx}}(t)\Big) = [A_1, A_2, \dots, A_N].$$

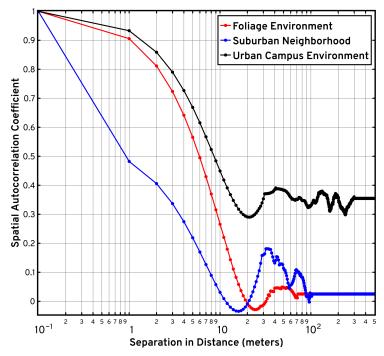


Figure 1:  $\rho(\Delta d)$  vs (log-scale) Separation in Distance  $\Delta d$  (in m).

The expectation  $\mathbb{E}[\cdot]$  in the above equation for  $\rho(\Delta v)$  is taken over all Tx and Rx configs along the route  $\mathcal{R}$  that satisfy the evaluation conditions **E3**.

The product within the  $\mathbb{E}[\cdot]$  operator in the numerator of  $\rho(\Delta v)$  is a dot-product between the two N-dimensional mean-shifted amplitude vectors.

Note that, to maintain consistency in the vector lengths throughout, we preset the number of MPCs to be considered  $(N^*)$ . So, at the two time-steps along the route t and t', if SAGE returns a different number of MPCs (N for the Tx-Rx config at time t and N' for the Tx-Rx config at time t',  $N \neq N'$ ) and if  $N > N^*$  and/or  $N' > N^*$ , then we pick the  $N^*$ -most amplitude-dominant MPCs.

The plots obtained from these evaluations are shown in Figs. 1, 2, and 3.

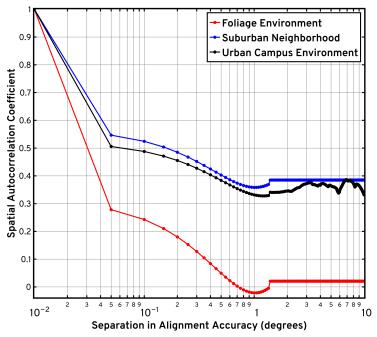


Figure 2:  $\rho(\Delta\phi)$  vs (log-scale) Separation in Alignment Accuracy  $\Delta\phi$  (in deg).

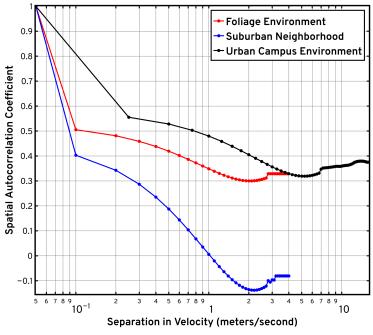


Figure 3:  $\rho(\Delta v)$  vs (log-scale) Separation in Velocity  $\Delta v$  (in m/s).

## 1.4 Physical Interpretation

- The physical interpretation of this spatial autocorrelation coefficient is that  $(-1 \le \rho \le 1)$  is similar to the correlation coefficient metric typically used in probability theory, i.e., are the signals received at two Tx-Rx configs separated in distance/alignment/velocity correlated (if yes, how correlated) or are they independent from each other (i.e., de-correlated).
- So, studying this spatial correlation coefficient in different propagation environments, the idea behind these evaluations is two-fold: analyze the gradient at which 28GHz signals become de-correlated as the separation between two points/configs increases in distance, alignment accuracy, and velocity; and determine the distances or errors in alignment or relative velocity changes at which the 28GHz signals received at two counterpart configurations become completely de-correlated (i.e.,  $\rho$ =0).
- However, since our propagation modeling campaign involved beam-steered measurements, the LoS component remains significant, thereby ensuring that even at large separations, the signals remain relatively correlated with each other.
- Since the MPC delay parameter is a continuous random variable, with no discretization possible because of the variations from one Tx-Rx config along the route to another, only the amplitude parameter of the MPCs is considered.

Similar definitions of  $\rho$  are used in the following works.

#### 2 References

- S. Sun, H. Yan, G. R. MacCartney and T. S. Rappaport, "Millimeter wave small-scale spatial statistics in an urban microcell scenario," 2017 IEEE International Conference on Communications (ICC), Paris, France, 2017.
- M. K. Samimi, G. R. MacCartney, S. Sun and T. S. Rappaport, "28 GHz Millimeter-Wave Ultrawideband Small-Scale Fading Models in Wireless Channels," 2016 IEEE 83rd Vehicular Technology Conference (VTC Spring), Nanjing, China, 2016, pp. 1-6.
- 3. M. K. Samimi, S. Sun and T. S. Rappaport, "MIMO channel modeling and capacity analysis for 5G millimeter-wave wireless systems," 2016 10th European Conference on Antennas and Propagation (EuCAP), Davos, Switzerland, 2016, pp. 1-5, doi: 10.1109/EuCAP.2016.7481507.
- 4. T. S. Rappaport, S. Y. Seidel and K. Takamizawa, "Statistical channel impulse response models for factory and open plan building radio communicate system design," in IEEE Transactions on Communications, vol. 39, no. 5, pp. 794-807, May 1991, doi: 10.1109/26.87142.