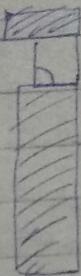
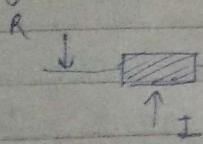


Date - 01 May 2021

Name - Bhupesh Bhatt
Subject - AWP

Roll no - 01911502818
Subject code - ETEC319

Ans 1 (a) Half wave dipole is formed from conducting element which is wire or metal tube which is an electrical half wavelength long.



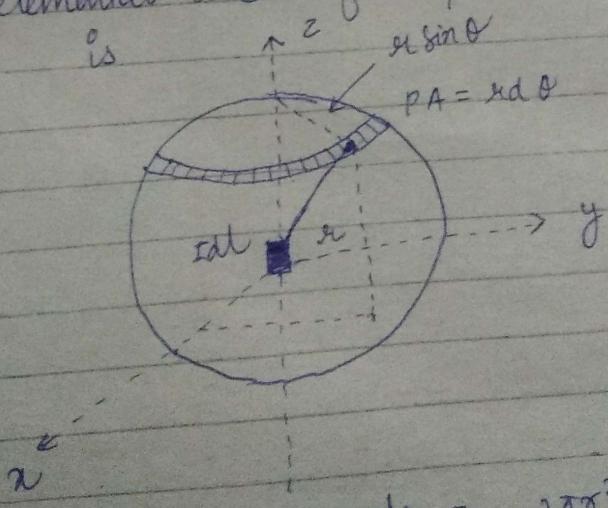
7.5.e coaxial cable

I = Insulator
R = core

The current profile is same at any given time instance on both radiators, each of quarter wavelength. If we send through centre wire and the bnd of coaxial cable is always at ground. For dipole antenna, the inductive and capacitive reactance level cancel each other total

Ans 1 (b) We can calculate the power radiated by a $\lambda/2$ antenna and its radiation resistance as same as has been adopted in case of current element power calculations.

The elemental area of spherical shell from below figure is



$$ds = 2\pi r^2 \sin \theta d\Omega$$

Total power radiated from $\lambda/2$ antenna

is calculated from

radiation half wave dipole

$$P = \oint_S \Phi_{\text{av}} dS$$

$$= \int_0^\pi \frac{30 I_{\text{rms}}^2}{\pi a^2} \left[\frac{\cos^2(\pi/2 \cos \theta)}{\sin^2 \theta} \right] 2\pi a^2 \sin \theta d\theta$$

$$= 60 I_{\text{rms}}^2 \int_0^\pi \left[\frac{\cos^2(\pi/2 \cos \theta)}{\sin \theta} \right] d\theta$$

solving using Simpson's rule $\rightarrow \int_0^\pi \frac{\cos^2(\pi/2 \cos \theta)}{\sin \theta} d\theta$

$$\therefore P = 60 I_{\text{rms}}^2 \times 1.219$$

$$P = 73.140 I_{\text{rms}}^2$$

$$P_R = I_{\text{rms}}^2 R_x$$

Total power radiated
by half wave dipole

$$R_x = 73.14 \quad \times \quad 73 \Omega$$

Ans(1) (c) Reciprocity states that the receive and transmit properties of an antenna are identical. Hence, antennas do not have distinct transmit and receive radiation pattern - if you know the radiation pattern in transmit mode then you also know pattern in receive mode.

The properties of transmitting and receiving antenna that exhibit the reciprocity are -

- Equality of directional pattern
- Equality of Directives
- Equality of effective length
- Equality of Antenna impedances

If any linear & bilateral network consisting the linear and bilateral impedance the ratio of voltage V applied between any two terminals to the current I measured in any branch is same as ratio V to I obtained by interchanging the positions of voltage source and the ammeter used for current measurement.

Ans (4) (a) Beam Efficiency

Beam efficiency states that the ratio of the beam area to the main beam to the total beam area radiated

The energy when radiated from an antenna, is projected according to antenna's directivity. The direction in which an antenna radiates more power has maximum efficiency, while some of the energy is lost in side lobes. The maximum energy radiated by the beam, with minimum losses can be termed as beam efficiency

$$\eta_B = \frac{\Omega_{MB}}{\Omega_A} \quad \begin{matrix} \text{beam area of main beam} \\ \text{total solid beam angle} \end{matrix}$$

(b) Antenna Efficiency.

The efficiency of an antenna is a ratio of power delivered to the antenna relative to power radiated from the antenna. A high efficiency antenna has most of the power present at the antenna's input radiated away

$$\epsilon_R = \frac{\text{radiated}}{P_{\text{input}}}$$

A low antenna has most of the power absorbed as losses within the antenna, or reflected away due to impedance mismatch

Radiating near field

(C) The field surrounding an antenna are divided in 3 categories -

(i) Far field

At the far field region, where $a \gg \lambda/2\pi$, $1/a^2$ and $1/a^3$ terms are neglected to gives the radiated field components with $1/r$ variation only

$$H_\phi = \frac{j K I_{0 d} l}{4\pi a} e^{jka} \sin \theta$$

$$E_\phi = \frac{j n K I_{0 d} l}{4\pi a} e^{-jka} \sin \theta$$

(ii) Near field

In the region where $a < \lambda/2\pi$, the terms with a^2 and a^3 dominate are called near field.

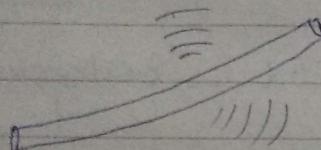
(iii) Reactive field

In the region where $a \ll \lambda/2\pi$, the terms with a^3 are dominating and are called reactive field. The radiated energy is stored & doesn't help in propagation of waves.

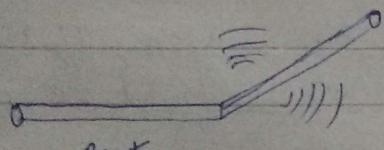
Ans (d) Antenna Array

Antenna array is radiating system, which consist of individual radiator and elements. Each of this radiator while functioning has its own induction field. The elements are placed so closely that each one lies in the neighbouring one's induction field, therefore the radiation pattern produced by them, would be vector sum of individual ones.

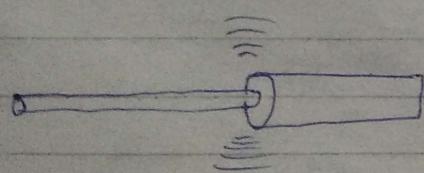
Ans (2) a Radiation mechanism of in antennas



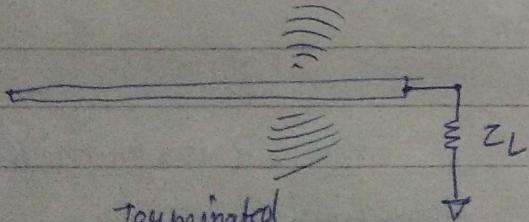
Curved



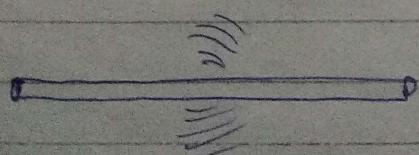
Bent



discontinuous



terminated



Truncated

- charge is not moving
No current, no radiation

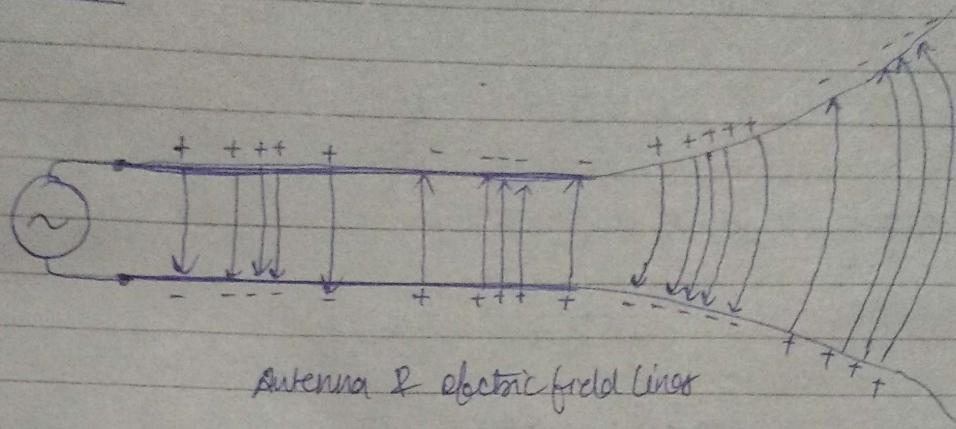
- charge is moving uniform velocity

- Wire is straight and infinite, no radiation
- Wire is curved, bent, discontinuous or terminated or truncated it makes radiation

- charge is oscillating
It radiates even if wire is straight

Single wire

For two wires

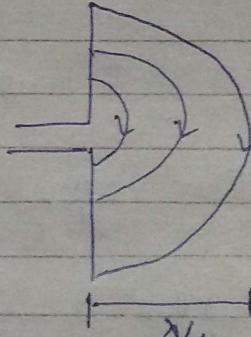


Antenna & electric field lines

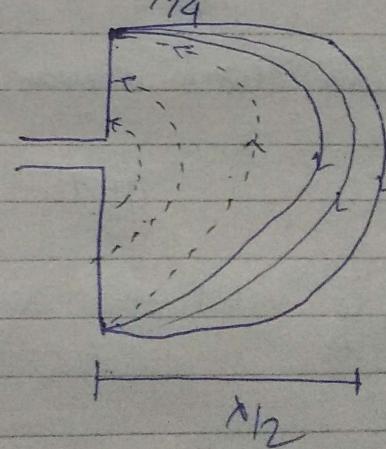
On applying voltage, it creates an electric field between conductors. Electric lines of force \propto electric field intensity. Electric charges are required to excite the field but are not needed to sustain them and may exist in absence

Radiation mechanism

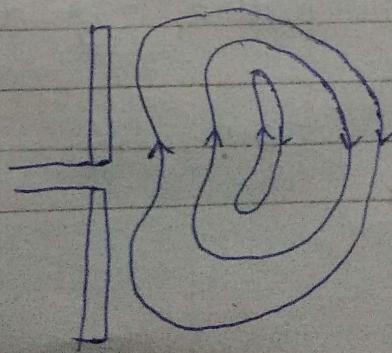
(a) $\Rightarrow t = T/4$ (T = period)



(b) $\Rightarrow t = T/2$ (T = period)



(c) $t = T/2$ (T = period)



Ans(2) (b) We know $B = \nabla \times A \leftarrow$ magnetic vector potential

$$\nabla \times E = -\frac{\partial B}{\partial t} = -\frac{\partial}{\partial t}(\nabla \times A)$$

by changing order of differentiation,

$$\nabla \times E = -\nabla \times \frac{\partial A}{\partial t}$$

$$\nabla \times \left(E + \frac{\partial A}{\partial t} \right) = 0$$

$$E + \frac{\partial A}{\partial t} = -\nabla V$$

For steady DC current, A is considered constant so,

$$E = -\nabla V$$

$$E = -\frac{\partial A}{\partial t}$$

$$\oint E \cdot dl = \frac{\partial \Phi}{\partial t} = -\frac{\partial}{\partial t} \int B \cdot ds = -\frac{\partial}{\partial t} \int_S B \cdot ds$$

Using Stokes theorem

$$\oint_C E \cdot dl = -\oint \frac{\partial A}{\partial t} \cdot dl$$

So, $E = -\frac{\partial A}{\partial t}$ is valid for any arbitrary path at each point as long as E is an induced field intensity.

$$\text{So, } E \cdot dl = -\frac{\partial A}{\partial t} \cdot dl$$

$$E_0 = -\frac{\partial A}{\partial t}$$

where E_A is a component caused by change in vector magnetic potential,

$$E = E_A + E_F \\ = -\nabla V - \frac{\partial A}{\partial t}$$

due to charge \rightarrow due to time varying current

$$V = \frac{1}{4\pi\epsilon} \iiint \frac{\rho dV}{r} \text{ volts}$$

$$A = \oint \frac{\mu}{4\pi} \left(\frac{I}{r} \right) dV \text{ wb/m}$$

$$E = E_A + E_F = -j\omega A - \frac{j}{\omega\mu\epsilon} \nabla(\nabla \cdot A) - \frac{1}{\epsilon} \nabla \times F$$

$$H = H_A + H_F = \frac{1}{\mu} \nabla \times A - \frac{1}{j\omega\mu} \nabla \times F$$