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(54) **Particulate filter ash loading prediction method and vehicle using the same**

Verfahren zur Prognose der Ladung von Partikelfilterasche und Fahrzeug damit

Procédé de prédiction du chargement en cendres d'un filtre à particules et véhicule l'utilisant

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Description

[0001] The present invention relates to the field of internal combustion engines, and, more particularly, to internal combustion engines having exhaust aftertreatment devices.

[0002] Internal combustion engines come in a number of forms, the most common of which are spark-ignited gasoline fueled engines and compression-ignition, diesel-fueled engines. The compression-ignition, or diesel-type engine is used in many commercial and industrial power applications because its durability and fuel economy are superior to the spark-ignited gasoline-fueled engines. A diesel engine utilizes the heat of the compression of the intake air, into which a timed and metered quantity of fuel is injected, to produce combustion. The nature of the diesel engine cycle is that it has a variable air-fuel ratio that can, under partial power conditions, rise to levels significantly above stoichiometric. This results in enhanced fuel economy since only the quantity of fuel needed for a particular power level is supplied to the engine.

[0003] One of the issues with a diesel-type engine is the impact on emissions. In addition to the generation of carbon monoxide and nitrous oxide, there is a generation of particulates in the form of soot. A number of approaches are employed to reduce particulates while, at the same time, reducing oxides of nitrogen to ever more stringent levels as mandated by government regulations. Stoichiometric engines have been proposed to achieve this balance since they enable the use of an automotive type catalyst to reduce oxides of nitrogen. By operating the engine at or near stoichiometric conditions, a three-way catalyst may be utilized. However, operation in this manner causes a substantial increase in diesel particulates. Accordingly, a particulate filter (PF) in the form of a diesel particulate filter (DPF) must be employed to filter out the particulates, but the generation of particulates in a significant amount require that frequent regeneration of the filters, through temporary heating or other means, is necessary to remove the collected particulate matter. A wall-flow DPF will often remove 85% or more of the soot during operation. Cleaning the DPF includes utilizing a method to burn off the accumulated particulate either through the use of a catalyst or through an active technology, such as a fuel-burner, which heats the DPF to a level in which the soot will combust. This may be accomplished by an engine modification which causes the exhaust gasses to rise to the appropriate temperature. This, or other methods, known as filter regeneration, is utilized repeatedly over the life of the filter. One item that limits the life of the DPF is an accumulation of ash therein that will cause the filter to require replacement or some other servicing, such as a cleaning method, to remove the accumulated ash. The accumulated ash causes a reduction in the efficiency of the DPF and causes increased back pressure in the exhaust system of the diesel engine system.

U.S. Patent Application Pub. No. US 2007/0251214 discloses an apparatus for detecting a state of a DPF with a differential pressure sensor. An electronic control unit estimates an amount of ash remaining in the DPF based on the output of the differential pressure sensor immediately after the regeneration process. Alternatively, the residue ash amount may be calculated based on the difference between a ratio of the variation rate of the input manifold pressure with the variation rate of the differential pressure immediately after the regeneration process and an equivalent ratio regarding a thoroughly new or almost new diesel particulate filter. The residue ash amount is calculated every time a regeneration process is carried out and stored in memory. This method is problematic since the backpressure assessment after regeneration can be misleading if the soot has not been entirely removed and since the backpressure due to the ash accumulation measured after each regeneration can vary leading to misleading assumptions about the ash content.

U.S. Patent No. 6,622,480 discloses a DPF unit and regeneration control method that adjusts the start timing of a regeneration operation. The method includes an estimate of the ash accumulated quantity that is in the exhaust gas and accumulated in the filter and the correction of the exhaust pressure judgment value for judging the regeneration operation start based on the ash accumulated estimation value. The ash quantity is determined from the quantity of lubricant oil consumed according to the engine operation state. The effective accumulation in the filter with ash is reflected in the judgment of regeneration start timing because the exhaust pressure judgment value to be used for judging the regeneration operation start is corrected with the ash accumulation estimation value. The use of oil consumption is problematic since the lubricant oil may be consumed in ways other than being combusted. Further, even if the oil is not combusted, it is not necessarily passed through the DPF.

EP 1 437 493 A1 discloses an exhaust gas purification system and method. The method uses a filter differential pressure to determine and estimate an ash accumulation amount inside the filter. When the estimated accumulation amount is higher than a set reference value a warning lamp is lit in order to signal for the exchange of the filter.

[0004] It is also possible that direct-injected gasoline engines may require the use of a PF in the future, as a result of ever increasing governmental emissions standards.

[0005] What is needed in the art is a system that maximizes the life of a PF, such as a DPF, while ensuring that the regeneration process is done in an efficient, eco-

nomical manner.

[0006] It is therefore the object of the present invention to comply with one or all of these needs.

[0007] This object is met according to the invention by the teaching of claim 1 and 11 respectively, while features developing the solution in an advantageous manner are set forth in the further claims.

[0008] In one form, the invention includes a particulate filter ash loading prediction method including the steps of determining a service age for the particulate filter; calculating an ash accumulation rate in the particulate filter; determining a maximum service age for the particulate filter dependent upon the ash accumulation rate; and comparing the service age to the maximum service age. If the service age exceeds the maximum service age then indicating that a service and/or replacement of the particulate filter is needed due to ash loading.

[0009] According to an embodiment a particulate filter ash loading prediction method, may comprise the steps of: determining a service age for the particulate filter; calculating an ash accumulation rate in the particulate filter; determining a maximum service age for the particulate filter dependent upon the ash accumulation rate; and comparing the service age to the maximum service age, if the service age exceeds the maximum service age then indicating that at least one of service and replacement of the particulate filter is needed due to ash loading.

[0010] The ash loading prediction method may further comprise a step of regenerating the particulate filter dependent upon a delta pressure measurement across the particulate filter and the ash accumulation rate.

[0011] The determining a maximum service age step may further include using a predetermined maximum ash loading limit to determine the maximum service age.

[0012] The ash loading prediction method may further comprise a step of determining a normalized delta pressure adjustment factor using a normalized delta pressure value derived from a calculation that uses a filter delta pressure measurement as an input.

[0013] If the normalized delta pressure adjustment factor does not exceed a predetermined maximum delta pressure adjustment value then an adjusted normalized delta pressure may be calculated using the normalized delta pressure adjustment factor and a normalized delta pressure.

[0014] The normalized delta pressure may be calculated using equations from SAE 2002-01-1015 and a delta pressure reading across the particulate filter.

[0015] The step of determining a normalized delta pressure adjustment factor may additionally use an ash loading value as an input.

[0016] The ash loading value may determined from one of the ash accumulation rate and the service age, and an end of service life ratio and an ash loading table.

[0017] Once the ash accumulation rate is greater than zero then the end of service life ratio and the ash loading table to determine the ash loading value may not be used.

[0018] The ash loading prediction method of claim 1,

may further comprise a step of delaying a determination of a maximum average lifetime of the particulate filter until after the particulate filter has experienced a predetermined minimum time of use.

[0019] According to another embodiment a vehicle, may comprising: an internal combustion engine; a particulate filter connected to said internal combustion engine; a controller operatively connected to the internal combustion engine and to the particulate filter, the controller being configured to execute the steps of an ash loading prediction method, the method may include the steps of the aforementioned embodiment.

[0020] The above-mentioned and other features and advantages of this invention, and the manner of attaining them, will become more apparent and the invention will be better understood by reference to the following description of an embodiment of the invention taken in conjunction with the accompanying drawings, wherein:

Fig. 1 is a schematic drawing of a vehicle with an internal combustion engine employing an embodiment of an ash loading prediction method of the present invention;

Figs. 2A and 2B depict a schematical representation of the method utilized in the vehicle of Fig. 1; and

Figs. 3A and 3B depict a schematical representation of another embodiment of a method utilized in the vehicle of Fig. 1.

[0021] Corresponding reference characters indicate corresponding parts throughout the several views. The exemplification set out herein illustrates one embodiment of the invention and such exemplification is not to be construed as limiting the scope of the invention in any manner.

[0022] Referring now to the drawings, and more particularly to Fig. 1, there is shown a vehicle 10, which may be an agricultural work vehicle, a forestry work vehicle or a construction type vehicle utilizing an engine system that includes an air intake 12, an engine 14, a fuel supply system 16 (labeled FUEL in Fig. 1), and an exhaust system 18 (labeled EXHAUST in Fig. 1). Engine 14 has at least one piston reciprocating within an engine block that is connected to a crankshaft for producing a rotary output (not shown). Each piston is movable within a variable volume combustion chamber that receives air for combustion from air intake 12 and fuel from fuel supply system 16. The products of combustion pass through exhaust system 18.

[0023] The engine system additionally includes a diesel particulate filter (DPF) 20 (labeled DPF in Fig. 1) and a catalyst 22 (labeled CAT in Fig. 1). Although the embodiment of the invention illustrated in the drawings and described herein is with reference to a diesel engine having a DPF, it is understood that the present invention can likewise apply to other types of engines using a PF, such

as a direct-injected gasoline engine, etc. An air intake flow 24 passes into engine 14 for the purposes of combustion, having an exhaust flow 26 that passes through DPF 20 and a gas flow 28 that continues through catalyst 22 and is exhausted in the form of gas flow 30 to the environment. DPF 20 and catalyst 22 may be combined into one unit or catalyst 22 may be positioned at a different location or omitted from the engine system. A controller 32 interacts with sensors 34 and 36 as well as fuel supply system 16 to control the flow of fuel and to sense the pressure drop across DPF 20. DPF 20 may be regenerated as directed by controller 32 with input of the sensors 34 and 36, each of which provide pressure readings so that the pressure drop across DPF 20 can be calculated by controller 32 based on the difference in pressure measurements between sensors 34 and 36. Controller 32 provides input to fuel supply system 16, which may cause engine 14 to change the exhaust temperature flowing through exhaust system 18 to DPF 20, causing a regeneration of DPF 20.

[0024] Now, additionally referring to Figs. 2A and 2B, there is shown an ash loading prediction method 100 utilized within controller 32, which may be interconnected to other sensors and control systems. Controller 32 may have other functions unrelated or indirectly related to the functions of method 100 of the present invention. Method 100 includes a step 102 in which the DPF service age ρ , as well as the time between regenerations ψ are separately integrated by a process of integration or summing. This summing of the DPF service age ρ and this step also keeps track of the time between regenerations ψ . At step 104, a decision is made as to whether DPF 20 requires a regeneration. This may be decided upon the delta pressure across DPF 20 as sensed by sensors 34 and 36 under the control of controller 32 and upon other portions of method 100, such as the compensation for the ash loading that is occurring in DPF 20. With the ash loading prediction being made by the present invention, then the contribution of backpressure in DPF 20 that is attributed to the particulate matter that is to be cleaned from DPF 20 can be accurately assessed to determine if it is time for a regeneration of DPF 20 to take place. If no regeneration is needed, step 104 proceeds back to step 102 but the time continues to be tracked for the DPF service age ρ and the time between regenerations ψ . If a DPF regeneration needs to take place as decided at step 104, method 100 proceeds to step 106 in which a DPF regeneration cycle is initiated and takes place.

[0025] A predetermined minimum DPF age τ , schematically shown as step 108 is used in step 110 to compare to the DPF service age ρ to see if ρ is greater than or equal to τ . If the integrated DPF service age ρ is not greater than or equal to the minimum DPF age τ , then method 100 resets the time between regenerations ψ to be equal to zero, at step 112, so that it will then start re-accumulating time at step 102. This portion of method of 100 ensures that at least a minimum age for DPF 20 is realized before establishing a service life for DPF 20. In

the event that the DPF service age ρ exceeds or is equal to the minimum DPF age τ , method 100 proceeds to step 114 to determine if a maximum average time α has been set. If the answer is no, then the maximum average time is set to the most recent time between regenerations ψ and ψ_{AVG} is also set equal to ψ , at step 116. If the maximum average time α has been previously set, then method 100 proceeds from step 114 to step 118 in which the running average of the time between regeneration is calculated by the equation of ψ_{AVG} being set equal to $(\psi_{AVG} + \psi) / 2$. Then at step 120, an end-of-service Life ratio Λ is set equal to the running average of time between regenerations ψ_{AVG} divided by the maximum average time α and the time between regenerations ψ is set to zero. Method 100 then proceeds to step 122, in which it is determined whether the end-of-service life ratio Λ is less than or equal to the end-of-service life ratio maximum Λ_L . If the answer is no, then method 100 proceeds to step 102. If the end-of-service life ratio Λ is less than or equal to end-of-service life ratio maximum Λ_L , then method 100 proceeds to step 126 in which the ash loading μ is set using the end-of-service life Λ as an input to a two-dimensional lookup table as illustrated in step 124 where the end-of-service life ratio Λ is used to determine the ash loading μ . Method 100 then proceeds to step 134.

[0026] Steps 128, 130, and 132 are carried out as an input to step 134. A DPF delta pressure reading is taken at step 128 by way of sensors 34 and 36 measuring the delta pressure across DPF 20. The DPF delta pressure reading at step 128 is converted to a normalized delta pressure (Norm-DP) at step 130 using equations from Konstandopoulos, et al., which is contained in SAE 2002-01-1015. The output of step 130 is Norm-DP as illustrated in step 132, which serves as an input to step 134. At step 134, the normalized delta pressure adjustment factor δ is established using Norm-DP and the ash loading μ as inputs. Normalized DP adjustment factor table 136 is utilized with Norm-DP and ash loading μ as inputs to a three dimensional lookup table. At step 140, it is determined whether the normalized delta pressure adjustment factor δ is greater than or equal to the maximum normalized delta pressure adjustment factor δ_L (which may be a predetermined value) established at step 138. If the normalized delta pressure adjustment factor δ is less than the maximum normalized delta pressure adjustment factor δ_L , then method 100 proceeds to step 142 in which an adjusted normalized DPF delta pressure is calculated using the normalized delta pressure adjustment factor δ and Norm-DP and then method 100 proceeds back to step 102. If the normalized delta pressure adjustment factor δ is greater than or equal to the maximum normalized delta pressure adjustment factor δ_L , then method 100 proceeds from step 140 to step 144 in which an indication is made that service or the replacement of the DPF 20 is necessary. The indication may be in the form of an illuminated warning light on a console supervised by an operator or some other form of communication of the information to the operator of vehicle

10 or to maintenance personnel. Additionally, at step 144, when the service or replacement of DPF 20 takes place, variables are set to zero such as ψ_{AVG} , ρ , α , Λ , μ , δ .

[0027] At step 146, if DPF service age ρ is greater than or equal to the maximum DPF service age ρ_L then method 100 proceeds to step 144. If the DPF service age ρ is not greater than or equal to the maximum DPF service age ρ_L then method 100 proceeds to step 102. The maximum DPF service age ρ_L is calculated at step 148 using the maximum ash loading μ_L and the ash accumulation rate U using the formula depicted in step 148. The ash accumulation rate U is calculated at step 152 by setting it equal to the ash loading μ divided by the DPF service age ρ .

[0028] Now, additionally referring to Figs. 3A and 3B, there is illustrated a method 200, which is another embodiment of the present invention. Method 200 is substantially similar to method 100 in many respects, with the similar steps retaining the same number as in method 100. For the sake of clarity each of the elements discussed above remain unchanged except where a step is inserted or diverted differently in method 200. At step 202 the ash accumulation rate U is tested to see if a value has been assigned to it. If no positive value is assigned to ash accumulation rate U , then method 200 proceeds from step 104 to step 106. If a non-zero positive value has been assigned to ash accumulation rate U , then method 200 proceeds to calculate the ash loading μ using the formula shown in step 204. Method 200 also tests to see if the DPF service age ρ is greater than or equal to the maximum DPF service age ρ_L at step 146, then method 200 proceeds to step 144. At step 144 an indication is made that service or the replacement of the DPF 20 is necessary. The indication may be in the form of an illuminated warning light on a console supervised by an operator or some other form of communication of the information to the operator of vehicle 10 or to maintenance personnel. Additionally, at step 144, when the service or replacement of DPF 20 takes place, variables are set to zero such as ψ_{AVG} , ρ , α , Λ , μ , δ , U .

[0029] If the DPF service age ρ , at step 146, is not greater than or equal to the maximum DPF service age ρ_L then method 200 proceeds to step 102. This variation is incorporated to allow method 200 to skip the calculation of the end-of-service-life ratio Λ and to skip other steps that are not needed since the ash accumulation rate U has been established. Following step 142, decision block 206 determines if DPF 20 needs to be regenerated, using the same or similar criteria as used in step 104. If DPF 20 needs to be regenerated then method 200 proceeds to step 106. If DPF 20 does not need to be regenerated, then decision block 206 directs method 200 to step 102.

[0030] Once DPF 20 is regenerated at step 106 method 200 proceeds to decision block 208, wherein if the ash accumulation rate U is greater than 0, and if the ash accumulation rate U has been assumed to be constant, then method 200 proceeds to step 112. If the ash accumulation rate U is not greater than 0, or if the ash accu-

mulation rate U has been assumed to not be constant, then method 200 proceeds to step 110. The assumption that the ash accumulation rate U is constant is a predetermined selection which may be made by either the operator, maintenance personnel, and/or a factory selection.

[0031] DPF 20 may be in the form of a wall-flow filter that traps soot with a very high efficiency, even above 90%. When the soot cake layer has been established within DPF 20, filling the inlet channel walls, the pressure increases across DPF 20 and a soot trapping efficiency of higher than 99% may be achieved. It is common to measure a pressure drop across DPF 20 through the use of a delta pressure sensor, which may include two sensors, such as those illustrated in Fig. 1 as sensors 34 and 36. The readings from sensors 34 and 36 are used to predict DPF 20 soot loading. These predictions can be made with models, such as those developed by Konstandopoulos, et al., (SAE 2002-01-1015). A high filtration efficiency DPF 20 also traps ash, which can come from high ash lube oil, excessive oil consumption, and high ash fuels, such as biodiesel. As ash gradually accumulates in DPF 20, the DPF 20 delta pressure signal received by controller 32 at a given soot level will be higher. This behavior is due to ash occupying space in the inlet channels of DPF 20, leaving less surface/volume for soot distribution.

[0032] Overall, ash accumulation is generally a slow process. Total exhaust system back pressure due to ash starts to become noticeable above 2,500 hours of engine operation for greater than 130 kilowatt applications, and above 1,500 hours of operation for less than 130 kilowatt applications. However, in addition to the effect on engine performance due to higher back pressure, the delta pressure sensor readings increase as a result of the ash loading. Without any compensation for ash loading, the time interval between regenerations starts to decrease since the aftertreatment control system will determine that a DPF 20 regeneration needs to occur based on delta pressure readings.

[0033] It is known that ash loading of DPF 20 will cause higher delta pressure readings across DPF 20 to become progressively higher with soot loading and that such effects cannot be remedied by merely averaging. Also, ash accumulation can take a significant amount of engine operation time to show substantial effects on DPF delta pressure signals and exhaust back pressures.

[0034] Methods 100 and 200 deal with ash that is accumulated in DPF 20 with time, and recognizes that the normalized delta pressure readings will tend to increase, leading to more frequent regenerations. The increase in the number of regenerations can be tied in direct proportion to the overall average time between regenerations. The maximum average time α is calculated early on in engine and aftertreatment service life. Although it can be calculated from the first several samples of time between regenerations, waiting for DPF service age ρ to pass a minimum DPF age τ allows there to be ample time for

the maximum average time α to be established and thereby avoid a possible over calculation of the maximum average time between regenerations.

[0035] After the maximum average time α is calculated, it will be continuously referenced to calculate the end-of-service life ratio Λ using the ongoing calculation of the running average of time between regenerations ψ_{AVG} . As DPF 20 loads with ash and the regeneration frequency increases, Λ decreases from 1.0. However, as ash accumulates in DPF 20, the normalized and non-normalized delta pressure will trend at higher levels for the same soot loading than if there was no ash present in DPF 20.

[0036] From experimental testing, it has been found that the end-of-service life ratio Λ can be used as an input to a DPF ash loading μ lookup table. The ash loading μ is then used as an input to a three-dimensional table to calculate the normalized DPF 20 delta pressure adjustment factor δ to compensate for the ash loading effect on the normalized DPF delta pressure calculation. The other input to the three-dimensional table is the normalized DPF delta pressure Norm-DP, which is derived using a measured DPF delta pressure and the equations from Konstandopoulos, et al. As ash continues to accumulate, the necessary compensation for the normalized DPF delta pressure will increase in order to accurately measure DPF 20 soot loading. Once the normalized delta pressure adjustment factor δ exceeds a maximum normalized delta pressure adjustment factor δ_L , DPF 20 will reach the end-of-service life.

[0037] DPF ash loading μ is also used to calculate the ash accumulation rate U . The ash accumulation rate U is calculated based on DPF ash loading μ and the number of hours of DPF service age ρ . After the ash accumulation rate U is established, the maximum DPF service age ρ_L is calculated using the ash accumulation rate U and the maximum DPF ash loading μ_L which is defined by the user. With subsequent hours, the DPF service age ρ is compared to the maximum DPF service age ρ_L . Once DPF 20 reaches the maximum DPF service age ρ_L then DPF 20 needs to be serviced and/or replaced.

[0038] After the ash accumulation rate U and the DPF service age ρ are calculated, there is no need to continue calculating the running average of time between regenerations ψ_{AVG} , and the end-of-service-life ratio Λ . The ash loading μ is calculated using the DPF service age ρ in order to calculate the normalized DPF delta pressure adjustment factor δ .

[0039] Advantageously, the present invention provides a statistically based ash model to monitor and verify the ash prediction that is not based on fuel consumption history, as utilized in prior art systems. Further, the method is also capable of flagging excessive oil consumption or poor fuel quality that results in excessive loading of DPF 20. Additionally, the present invention reduces the number of DPF regenerations when the DPF 20 is approaching the end-of-service life. The method can also generate an input for a monitor after determining that an ash service warning or engine degradation is occurring

or may occur. Yet further, the present invention can compensate for the use of biodiesel, which has a tendency to create additional ash over petroleum based diesel.

[0040] While this invention has been described with respect to at least one embodiment, the present invention can be further modified within the spirit and scope of this disclosure. This application is therefore intended to cover any variations, uses, or adaptations of the invention using its general principles. Further, this application is intended to cover such departures from the present disclosure as come within known or customary practice in the art to which this invention pertains and which fall within the limits of the appended claims.

Claims

1. A particulate filter ash loading prediction method, comprising the steps of:

determining a service age (ρ) for the particulate filter (20);

calculating an ash accumulation rate (u) in the particulate filter (20);

determining a maximum service age (ρ_L) for the particulate filter (20) dependent upon the ash accumulation rate (u); and

comparing the service age (ρ) to the maximum service age (ρ_L), if the service age (ρ) exceeds the maximum service age (ρ_L) then indicating that at least one of service and replacement of the particulate filter (20) is needed due to ash loading, **characterised by** a further step of determining a normalized delta pressure adjustment factor (δ) using a normalized delta pressure value derived from a calculation that uses a filter delta pressure measurement as an input; and

determining a maximum normalized delta pressure adjustment factor (δ_L); and

comparing the normalized delta pressure adjustment factor (δ) to the maximum normalized delta pressure adjustment factor (δ_L), if the normalized delta pressure adjustment factor (δ) exceeds the maximum normalized delta pressure adjustment factor (δ_L) then indicating that at least one of service and replacement of the particulate filter is needed due to ash loading.

2. The ash loading prediction method according to claim 1, **characterised by** a further step of regenerating the particulate filter (20) dependent upon a delta pressure measurement across the particulate filter (20) and the ash accumulation rate (u).

3. The ash loading prediction method according to claim 1 or 2, **characterised in that** the determining a maximum service age step further includes using

a predetermined maximum ash loading limit to determine the maximum service age (ρ_L).

4. The ash loading prediction method according to claim 1, **characterized in that** if the normalized delta pressure adjustment factor (δ) does not exceed a predetermined maximum normalized delta pressure adjustment value (δ_L) then calculating an adjusted normalized delta pressure using the normalized delta pressure adjustment factor (δ) and a normalized delta pressure. 5
5. The ash loading prediction method according one of the claims 1 to 4, **characterized in that** the step of determining a normalized delta pressure adjustment factor (δ) additionally uses an ash loading value as an input. 10
6. The ash loading prediction method according to claim 5, **characterized in that** the ash loading value is determined from one of the ash accumulation rate (u) and the service age (ρ), and an end of service life ratio and an ash loading table. 20
7. The ash loading prediction method according to one of the claims 1 to 6, **characterized in that** once the ash accumulation rate (u) is greater than zero then not using the end of service life ratio and the ash loading table to determine the ash loading value. 25
8. The ash loading prediction method according to one of the claims 1 to 6, **characterized by** a further step of delaying a determination of a maximum average lifetime of the particulate filter (20) until after the particulate filter (20) has experienced a predetermined minimum time of use. 30
9. A vehicle, comprising: 35
 - an internal combustion engine (14); 40
 - a particulate filter (20) connected to the internal combustion engine (14);
 - a controller (32) operatively connected to the internal combustion engine (14) and to the particulate filter (20), the controller (32) being configured to execute the steps of an ash loading prediction method according to one of the previous claims. 45

Patentansprüche

1. Verfahren zur Prognose der Ladung von Partikelfilterasche, umfassend die Schritte: 50
 - Bestimmen einer Gebrauchsdauer (ρ) für den Partikelfilter (20);
 - Berechnen einer Ascheakkumulationsrate (U) 55

in dem Partikelfilter (20);

Bestimmen einer maximalen Gebrauchsdauer (ρ_L) für den Partikelfilter (20) in Abhängigkeit von der Ascheakkumulationsrate (U); und

Vergleichen der Gebrauchsdauer (ρ) mit der maximalen Gebrauchsdauer (ρ_L), wobei, wenn die Gebrauchsdauer (ρ) die maximale Gebrauchsdauer (ρ_L) überschreitet, dann angezeigt wird, dass entweder Wartung und Ersatz des Partikelfilters (20) infolge der Aschebelastung erforderlich ist,

gekennzeichnet durch einen weiteren Schritt des Bestimmens eines normalisierten Druckdifferenzanpassungsfaktors (δ) unter Verwendung eines normalisierten Druckdifferenzwerts, der aus einer Berechnung abgeleitet ist, die eine Filterdifferenzdruckmessung als Eingabe verwendet; und

Bestimmen eines maximalen normalisierten Druckdifferenzanpassungsfaktors (δ_L); und Vergleichen des normalisierten Druckdifferenzanpassungsfaktors (δ) mit dem maximalen normalisierten Druckdifferenzanpassungsfaktor (δ_L), wobei, wenn der normalisierte Druckdifferenzanpassungsfaktor (δ) den maximalen normalisierten Druckdifferenzanpassungsfaktor (δ_L) überschreitet, dann angezeigt wird, dass mindestens eines von Wartung und Ersatz des Partikelfilters infolge der Aschebelastung erforderlich ist.

2. Verfahren zur Prognose der Aschebelastung nach Anspruch 1, **gekennzeichnet durch** einen weiteren Schritt des Regenerierens des Partikelfilters (20) in Abhängigkeit von einer Druckdifferenzmessung über dem Partikelfilter (20) und der Ascheakkumulationsrate (U).
3. Verfahren zur Prognose der Aschebelastung nach Anspruch 1 oder 2, **dadurch gekennzeichnet, dass** der Schritt zum Bestimmen einer maximalen Gebrauchsdauer ferner das Verwenden eines vorbestimmten maximalen Aschebelastungsgrenzwerts einschließt, um die maximale Gebrauchsdauer (ρ_L) zu bestimmen.
4. Verfahren zur Prognose der Aschebelastung nach Anspruch 1, **dadurch gekennzeichnet, dass**, wenn der normalisierte Druckdifferenzanpassungsfaktor (δ) einen vorbestimmten maximalen normalisierten Druckdifferenzanpassungswert (δ_L) nicht überschreitet, dann eine angepasste normalisierte Druckdifferenz unter Verwendung des normalisierten Druckdifferenzanpassungsfaktors (δ) und einer normalisierten Druckdifferenz berechnet wird.
5. Verfahren zur Prognose der Aschebelastung nach einem der Ansprüche 1 bis 4, **dadurch gekenn-**

zeichnet, dass der Schritt des Bestimmens eines normalisierten Druckdifferenzanpassungsfaktors (δ) zusätzlich einen Aschebelastungswert als Eingabe verwendet.

6. Verfahren zur Prognose der Aschebelastung nach Anspruch 5, **dadurch gekennzeichnet, dass** der Aschebelastungswert aus einer von der Ascheakkumulationsrate (U) und der Gebrauchsdauer (ρ) sowie einem "Ende der Nutzungsdauer" (EOSL)-Verhältnis und einer Aschebelastungstabelle bestimmt wird.

7. Verfahren zur Prognose der Aschebelastung nach einem der Ansprüche 1 bis 6, **dadurch gekennzeichnet, dass**, sobald die Ascheakkumulationsrate (U) größer als Null ist, dann nicht das "Ende der Nutzungsdauer" (EOSL)-Verhältnis und die Aschebelastungstabelle zur Bestimmung des Aschebelastungswerts verwendet werden.

8. Verfahren zur Prognose der Aschebelastung nach einem der Ansprüche 1 bis 6, **gekennzeichnet durch** einen weiteren Schritt des Verzögerns einer Bestimmung einer maximalen durchschnittlichen Nutzungsdauer des Partikelfilters (20) bis zu der Zeit, nach der der Partikelfilter (20) eine vorbestimmte Mindestverwendungszeit durchlaufen hat.

9. Fahrzeug, umfassend:

einen Verbrennungsmotor (14);
einen Partikelfilter (20), der mit dem Verbrennungsmotor (14) verbunden ist;
eine Steuerung (32), die in Wirkbeziehung mit dem Verbrennungsmotor (14) und dem Partikelfilter (20) verbunden ist, wobei die Steuerung (32) konfiguriert ist, um die Schritte des Verfahrens zur Prognose der Aschebelastung gemäß einem der vorhergehenden Ansprüche auszuführen.

Revendications

1. Procédé de prédiction du chargement en cendres d'un filtre à particules, comprenant les étapes consistant à :

déterminer une durée d'utilisation (ρ) pour le filtre à particules (20) ;
calculer un taux d'accumulation de cendres (u) dans le filtre à particules (20) ;
déterminer une durée d'utilisation maximale (ρ_L) pour le filtre à particules (20) en fonction du taux d'accumulation de cendres (u) ; et
comparer la durée d'utilisation (ρ) à la durée d'utilisation maximale (ρ_L), si la durée d'utilisa-

tion (ρ) dépasse la durée d'utilisation maximale (ρ_L), alors indiquer que l'entretien ou le remplacement du filtre à particules (20) sont nécessaires en raison du chargement en cendres, **caractérisé par** une étape supplémentaire consistant à

déterminer un facteur d'ajustement de différentiel de pression normalisé (δ) en utilisant une valeur de différentiel de pression normalisée dérivée d'un calcul qui utilise une mesure de différentiel de pression du filtre comme entrée ; et
déterminer un facteur d'ajustement de différentiel de pression normalisé maximal (δ_L) ; et
comparer le facteur d'ajustement de différentiel de pression normalisé (δ) au facteur d'ajustement de différentiel de pression normalisé maximal (δ_L), si le facteur d'ajustement de différentiel de pression normalisé (δ) dépasse le facteur d'ajustement de différentiel de pression normalisé maximal (δ_L), alors indiquer que l'entretien et/ou le remplacement du filtre à particules sont nécessaires en raison du chargement en cendres.

2. Procédé de prédiction du chargement en cendres selon la revendication 1, **caractérisé par** une étape supplémentaire consistant à régénérer le filtre à particules (20) en fonction d'une mesure de différentiel de pression à travers le filtre à particules (20) et du taux d'accumulation de cendres (u).

3. Procédé de prédiction du chargement en cendres selon la revendication 1 ou 2, **caractérisé en ce que** l'étape de détermination d'une durée d'utilisation maximale comporte en outre l'utilisation d'une limite maximale de chargement en cendres prédéterminée pour déterminer la durée d'utilisation maximale (ρ_L).

4. Procédé de prédiction du chargement en cendres selon la revendication 1 **caractérisé en ce que**, si le facteur d'ajustement de différentiel de pression normalisé (δ) ne dépasse pas un facteur d'ajustement de différentiel de pression normalisé maximal (δ_L), alors un différentiel de pression normalisé ajusté est calculé en utilisant le facteur d'ajustement de différentiel de pression normalisé (δ) et un différentiel de pression normalisé.

5. Procédé de prédiction du chargement en cendres selon une des revendications 1 à 4, **caractérisé en ce que** l'étape de détermination d'un facteur d'ajustement de différentiel de pression normalisé (δ) utilise également une valeur de chargement en cendres comme entrée.

6. Procédé de prédiction du chargement en cendres selon la revendication 5, **caractérisé en ce que** la valeur de chargement de cendres est déterminée à

partir du taux d'accumulation de cendres (u) ou de la durée d'utilisation (ρ), et d'un taux de fin de durée de vie et d'une table de chargement en cendres.

7. Procédé de prédiction du chargement en cendres selon une des revendications 1 à 6, **caractérisé en ce qu'**une fois que le taux d'accumulation de cendres (u) est supérieur à zéro, alors le taux de fin de durée de vie et la table de chargement en cendres ne sont plus utilisés pour déterminer la valeur de chargement en cendres.

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8. Procédé de prédiction du chargement en cendres selon une des revendications 1 à 6, **caractérisé par** une étape supplémentaire consistant à retarder une détermination d'une durée de vie moyenne maximale du filtre à particules (20) jusqu'à ce que le filtre à particules (20) ait connu un temps minimal d'utilisation prédéterminé.

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9. Véhicule, comprenant :

un moteur à combustion interne (14) ;

un filtre à particules (20) relié au moteur à combustion interne (14) ;

un contrôleur (32) fonctionnellement relié au moteur à combustion interne (14) et au filtre à particules (20), le contrôleur (32) étant configuré pour exécuter les étapes d'un procédé de prédiction du chargement en cendres selon une des revendications précédentes.

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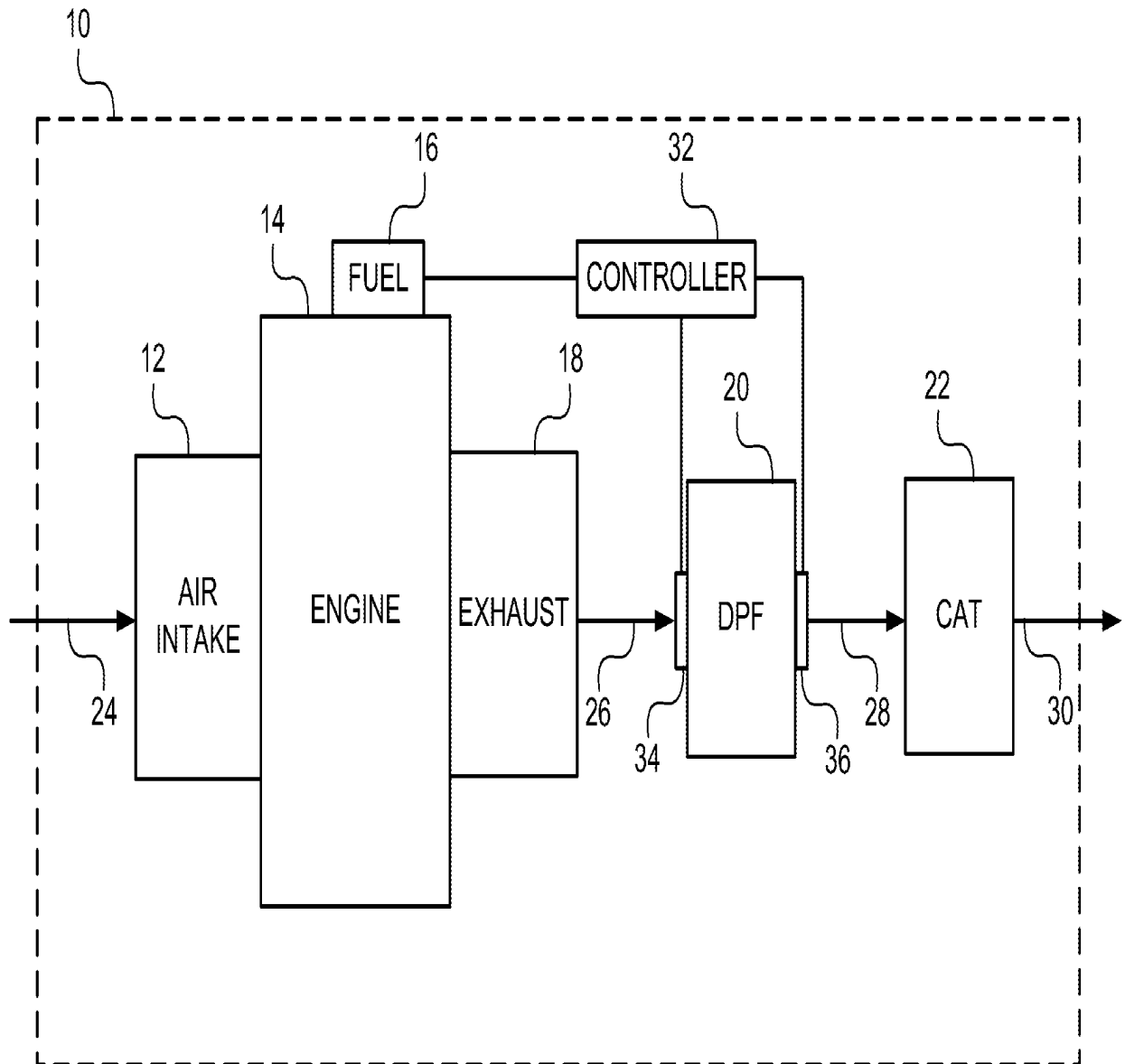


FIG. 1

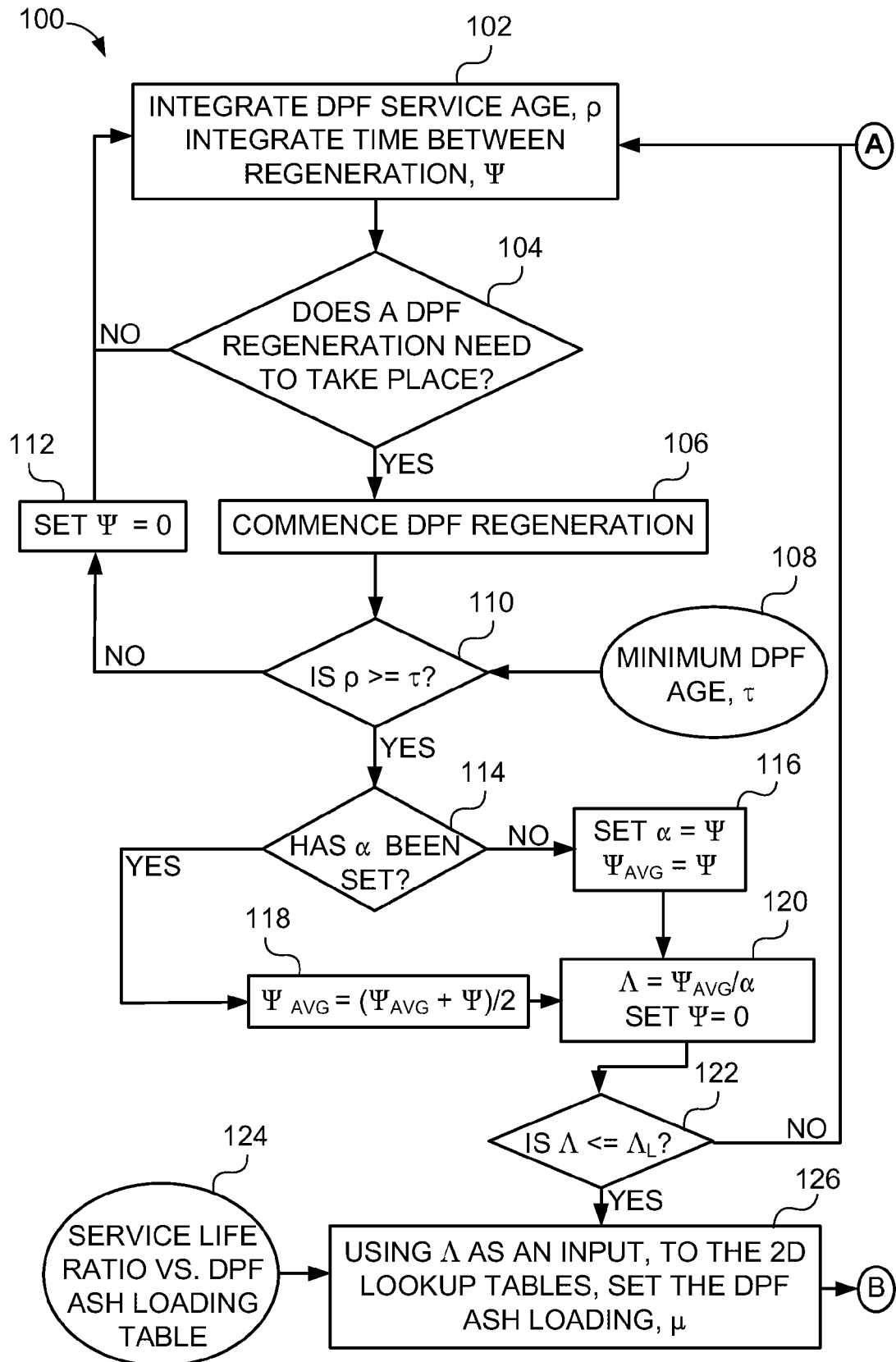
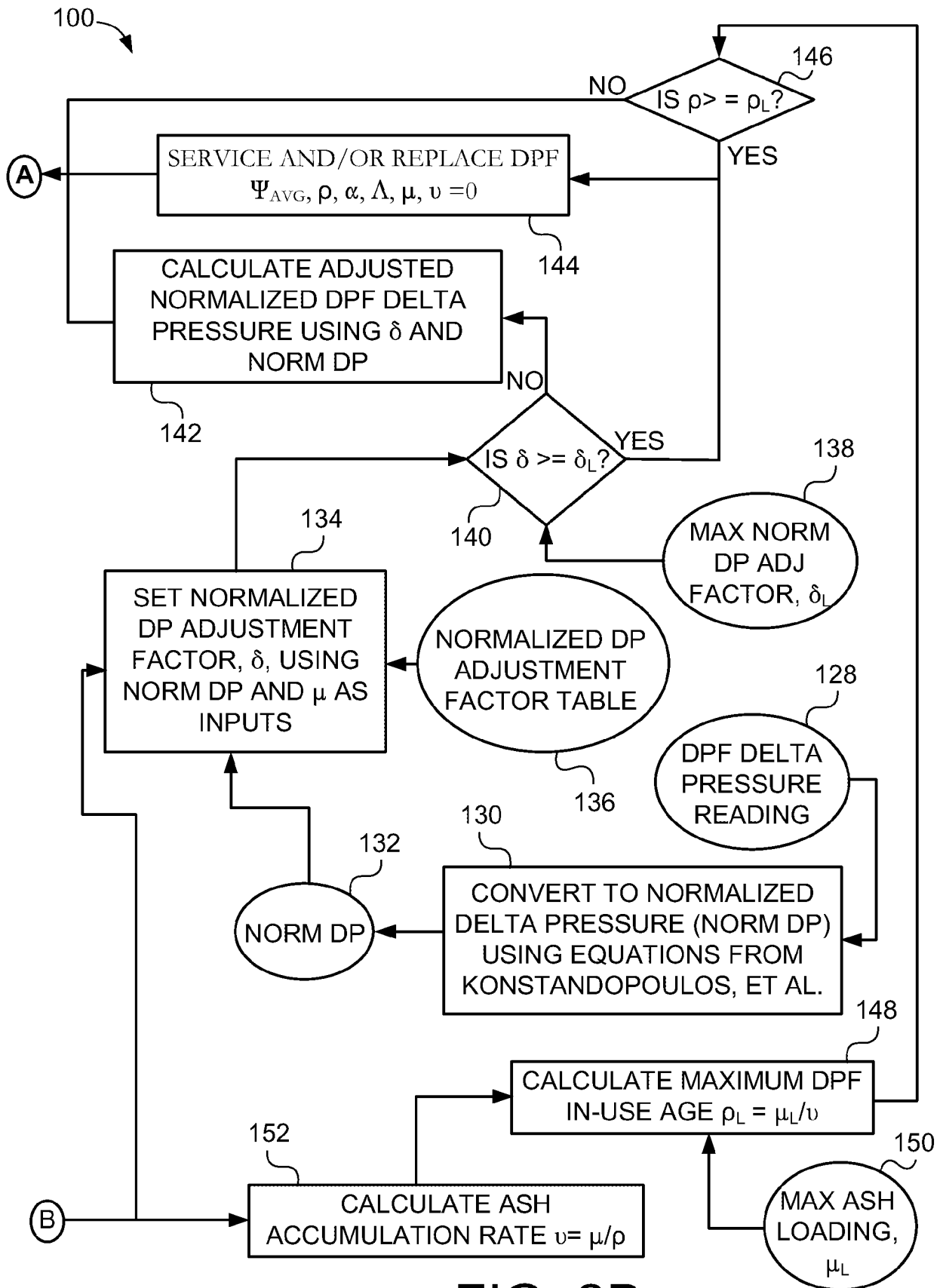


FIG. 2A



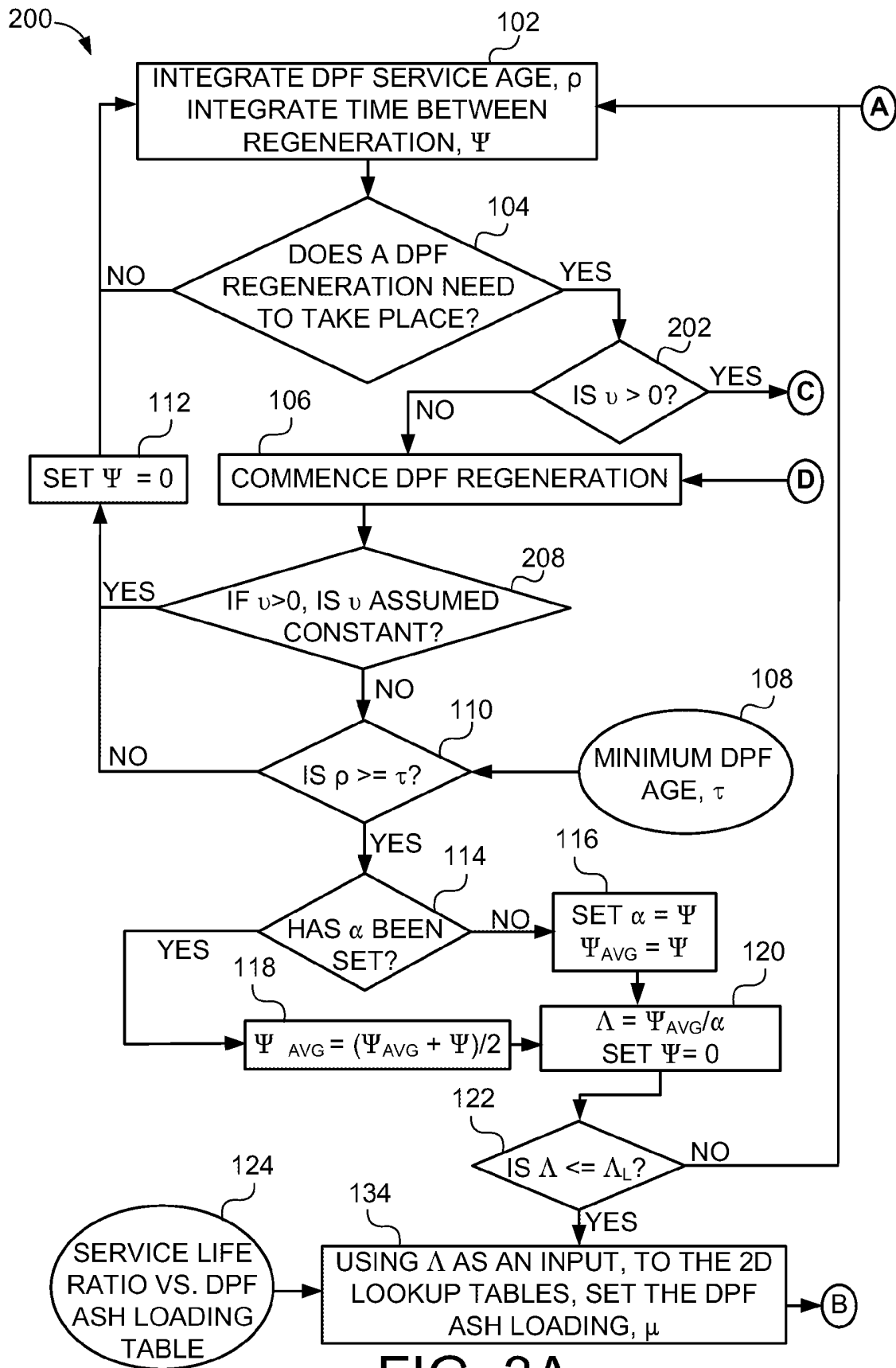
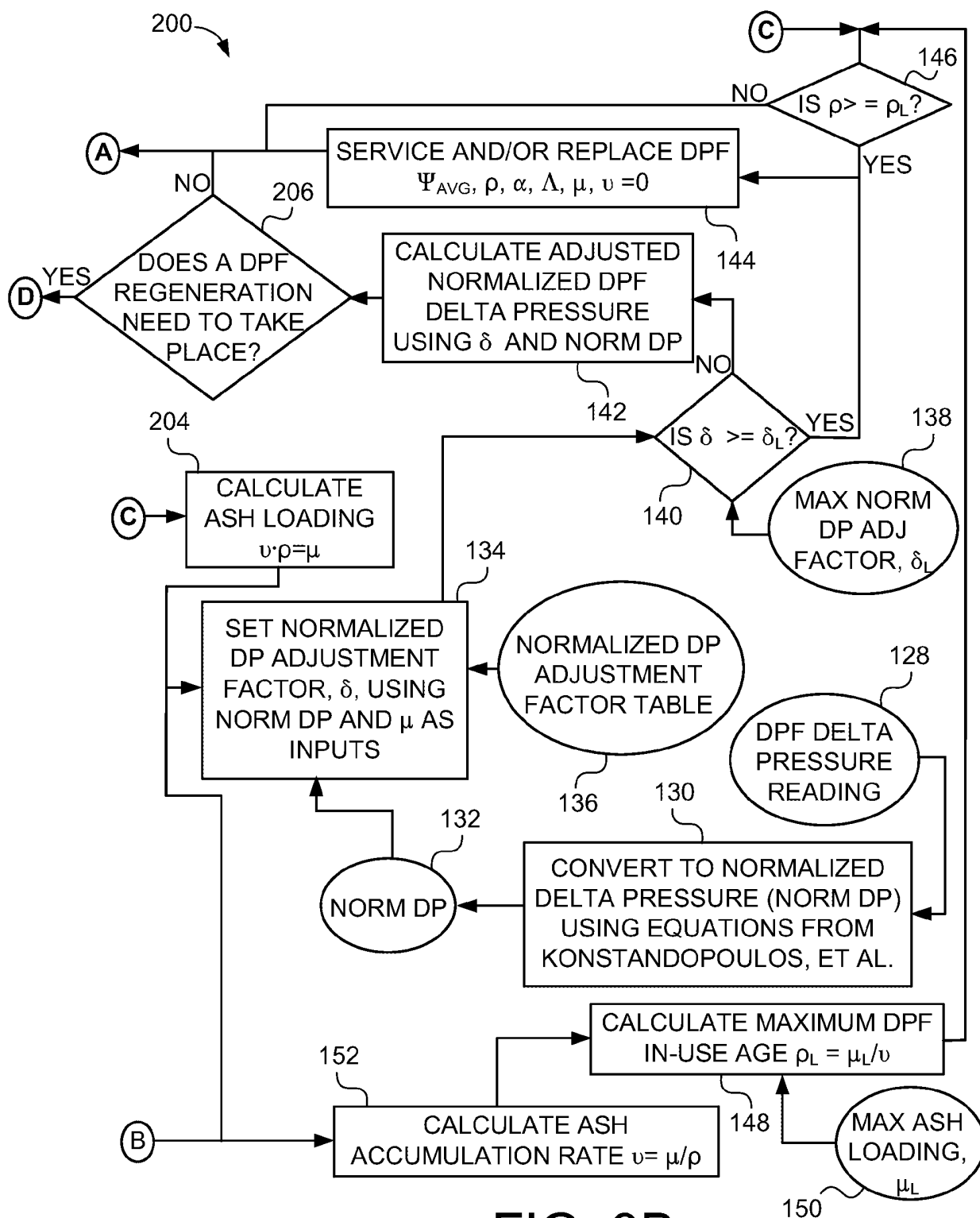


FIG. 3A



REFERENCES CITED IN THE DESCRIPTION

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