# 1 Project Expenditure Profile

## 1.1 Fundamental Expenditure Behavior

The underlying distribution of expenditures (independent of cost escalation and schedule delay),  $I_0(t)$ , is assumed to be a sinusoid:

$$I_0(t,d) = K \frac{\pi}{2d} \sin\left(\frac{\pi t}{d}\right),\tag{1}$$

where d is the total duration of the project (in years) and K is the initial estimate of the total final project cost.

For d held constant, the cumulative expenditures on the project at time t,  $E_0(t)$ , is the integral of the incremental spend function:

$$E_0(t) = \int_0^t I_0(t') dt'$$

$$= -\frac{K}{2} \left[ \cos \left( \frac{\pi t}{d} \right) - 1 \right]$$
(2)

These functions have the feature that evaluating  $E_0$  at the end of the project (time t equal to d, the project duration) reproduces the total project cost:

$$E_0(d) = K. (3)$$

### 1.2 Schedule Slip

For eq. (2) to be valid, d must be computed ahead of time and not changed during the course of the project. (On-the-fly schedule slip will be implemented in future versions.)

Historically, schedule slip typically occurred continuously throughout all stages of projects, with the effects being most severe towards the end of each project. DOE/EIA-0485 provides data for cost and schedule escalation for nuclear project in the US up to 1986. For each project, expected completion dates are provided at each of six milestones: Project start, 25% completion, 50% completion, 75% completion, 90% completion, and 100% completion.

Using this data, probability distributions were developed for the schedule slip factors during each phase (0-25% completion, 25-50% completion, and so on). Various probability distributions were examined against the data; the gamma distribution produced the closest match. Data for each completion stage were fitted to gamma distributions  $S_i$  with the following parameters:

$$S_i \sim \Gamma(\alpha_i, \beta_i)$$

Project Stage	$\alpha_i$	$\beta_i$
0-25%	2.422	0.419
25-50%	4.219	0.166
50-75%	7.923	0.018
75-90%	3.555	0.227
90-100%	8.758	0.026

Each project has a statically-defined initial schedule estimate,  $d_0$ , pulled from the reactor project profile. This duration is divided among five project stages of equal length. Each stage's duration  $d_i$  is then escalated by a factor generated from the appropriate probability distribution.

$$d_i = \frac{\Gamma\left(\alpha_i, \beta_i\right) d_0}{5} \tag{4}$$

The total project duration d is the total of the durations of all stages:

$$d = \sum_{i=1}^{5} d_i \tag{5}$$

#### 1.3 Cost Escalation

#### 1.3.1 Basic Escalation Model Form

For most historical projects, cost escalation occurred in all stages of the project and became more severe over time. The new incremental and cumulative expenditure functions are named  $I_e(t)$  and  $E_e(t)$ , respectively. The behavior of these functions is predicated on an escalated total final project cost at time d:

$$E_e(d) = (1 + \epsilon) E_0(d) \tag{6}$$

The final total escalation factor,  $\epsilon$ , is calculated by:

$$\epsilon = \Gamma(\alpha, \beta),$$

where  $\Gamma$  is the gamma distribution,  $\alpha$  is the shape parameter, and  $\beta$  is the rate parameter. At present, values of  $\alpha = 1.2$  and  $\beta = 0.6$  are being used.

This model escalates the fundamental expenditure profile  $I_0(t)$  with an exponential escalator term,  $e^{\alpha t}$ . An appropriate exponential growth rate  $\alpha$  must be determined, in order to reproduce the desired value of  $E_e(d)$ :

$$\int_0^d I_0(t) e^{\alpha t} dt = E_0(d) (1 + \epsilon)$$
 (7)

#### 1.3.2 Determining the Appropriate Escalation Rate Factor, $\alpha$

Evaluating the integral and some algebraic manipulation produce the analytically unsolvable expression:

$$e^{\alpha d} - \frac{2(1+\epsilon)\alpha^2 d^2}{\pi^2} = 2(1+\epsilon) - 1 \tag{8}$$

The bisection method is an efficient way to evaluate this expression for alpha, using probabilistically-generated values of  $\epsilon$  and d. To guarantee that such a search will be able to locate the appropriate value, it must be demonstrated that the following function  $f(\alpha, d, \epsilon)$  is monotonic over all possible values of  $\alpha$ , d, and  $\epsilon$ .

$$f(\alpha, d, \epsilon) = e^{\alpha d} - \frac{2(1+\epsilon)\alpha^2 d^2}{\pi^2} - 2(1+\epsilon) + 1 \tag{9}$$

If f is not monotonic in the region of interest, there will be multiple solutions for  $\alpha$ , and the search will merely locate one of them without regard to their validity. Monotonicity is proven if the partial derivative of f with respect to  $\alpha$  is positive everywhere in its valid domain:

$$\frac{\partial f}{\partial \alpha} = de^{\alpha d} - \frac{4(1+\epsilon)d^2}{\pi^2} \alpha \ge 0, \quad \alpha \in [0,2], \ d \in [5,15], \ \epsilon \in [0,2]$$
 (10)

The bisection method will evaluate the fitness of varying values of  $\alpha$  for fixed values of d and  $\epsilon$ , so it is sufficient to explore the monotonicity of the partial derivative with respect to  $\alpha$ , rather than the gradient of f.

The value ranges for d and  $\epsilon$  are set in accordance with the model's limits for acceptable escalation parameters. The value range for  $\alpha$  was set after experimentation with the resultant alpha values for a set of test d and  $\epsilon$  values that spanned their respective permitted value ranges. Actual realistic values of  $\alpha$  are expected to be substantially less than 1; however, for the sake of robustness,  $\alpha$  is evaluated up to 2.

 $\frac{\partial f}{\partial \alpha}$  was evaluated iteratively for 1000 values each of  $\alpha$ , d, and  $\epsilon$ , evenly spanning their value ranges. See figures X and Y for plots.

### [plots forthcoming]

In all tested cases the value of the partial derivative was greater than zero. Therefore,  $f(\alpha, d, \epsilon)$  is monotonic and the binary-search approach for calculating appropriate  $\alpha$  values is valid.