## SE 380 - HW 2

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#### 1 1

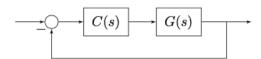


Figure 1: Control system in 1 and 2

Consider the feedback control system where

$$G(s) = \frac{5}{(1+s)\left(1+\frac{2\zeta}{\omega_n}s+\frac{s^2}{\omega_n^2}\right)}$$

With  $\omega_n = 10$  and  $\zeta = 0.1$ .

Design a controller C(s) such that the closed-loop system has the following specifications: The steady state error in response to a unit step function is  $e_{\infty} \leq 0.05$ , the gain margin  $k_m \geq 10 \text{dB}$ , and the phase margin  $\phi_m \geq 60^{\circ}$ .

We will design a controller with two parts:  $C_1(s) = \mu/s^p$ , to satisfy the steady state error requirement and we choose p = 0, and  $C_2(s)$ , to be a realizable controller that does not change the steady state behavior of the closed loop system to satisfy the gain and phase margin requirements.

$$y_{\infty} = \frac{C_1(0)C_2(0)G(0)}{1 + C_1(0)C_2(0)C_3(0)}$$
$$= \frac{\mu * 1 * 5}{1 + \mu * 1 * 5}$$
$$= \frac{5\mu}{1 + 5\mu}$$

For our steady state error requirement, we need  $y_{\infty} \leq 0.05$ , so manipulating this, we can see that we need  $\mu \geq 3.8$ . For simplicity, we choose  $\mu = 4$ .

For  $C_2(s)$  to not change the steady state behavior of the closed loop system, we need  $C_2(0) = 1$ . We also need  $C_2(s)$  to be realizable, so we choose to define it in the form  $C_2(s) = \frac{L^*(s)}{C_1(s)G(s)}$ . The steady state gain of G(s) is 5, so we need  $L^*(0) = 5$ . For the controller to be realizable, it must have the same degree as G(s), 3. For a phase margin of at least  $60^\circ$  and a gain margin of atleast 10 dB, we will choose an arbitrary crossover point  $\omega_c$  for the magnitude path of the bode plot of the controller to hit zero such that these two requirements are satisfied. We will choose  $\omega_c = 10^1$  for simplicity (Any choice of  $\omega_c$  will work). For the margins to be appropriately large, it is safe to place one pole at least one decade before  $\omega_c$  and the other two poles at least one decade after  $\omega_c$ .

$$C_2(s) = \frac{L^*(s)}{C_1(s)G(s)}$$

$$L^*(s) = \frac{5}{(1 + \frac{s}{100})(1 + \frac{s}{10^2})^2}$$

$$C(s) = C_1(s)C_2(s)$$

$$= C_1(s)L^*(s)\frac{1}{G(s)}$$

$$= 4.0 \frac{5}{(1 + \frac{s}{100})(1 + \frac{s}{10^2})^2} \frac{(1+s)\left(1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2}\right)}{5}$$

$$= 4.0 \cdot \frac{(1+s)\left(1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2}\right)}{(1 + \frac{s}{10^0})(1 + \frac{s}{10^2})^2}$$

In code, we can verify that the controller satisfies the requirements:

```
import math
import control as ct
import matplotlib.pyplot as plt

omega_n = 10
zeta = 0.1

s = ct.tf('s')
G = 5 / (1 + s) / (1 + 2 * zeta / omega_n * s + s**2 / omega_n**2)

# G(s) Bode plot
plt.figure()
ct.bode_plot(G, margins=True)
plt.show()

# G(s) step response
plt.figure()
t, y = ct.step_response(G / (1 + G))
```

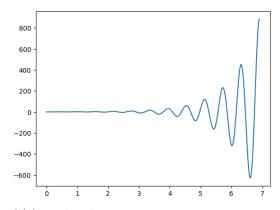
```
plt.plot(t, y)
plt.show()
mu = 4
C_1 = mu
pole_1 = 10**0
pole_2 = 10**2
L_star = 5 / ((1 + (s / pole_1)) * (1 + (s / pole_2))**2)
C_2 = L_{star} * (1 / G)
C = C_1 * C_2
# C(s) Bode plot
plt.figure()
ct.bode_plot(C * G, margins=True)
plt.show()
# C(s) step response
plt.figure()
t, y = ct.step\_response((C * G) / (1 + (C * G)))
plt.plot(t, y)
plt.show()
# Steady State Output at end of step response
print(f"Steady State Output: {y[-1]}")
# Prints out
# Steady State Output: 0.9523809526136096
   G(s) Bode Plot
        Gm = 0.41 (at 10.10 rad/s), Pm = -52.05 deg (at 11.65 rad/s)
    Magnitude
10<sup>-2</sup>
      10^{-3}
                                           102
                     10<sup>0</sup>
                                10<sup>1</sup>
      -45
    -45
-90
-135
-180
```

G(s) Step Response

10<sup>0</sup> 1 Frequency (rad/sec)

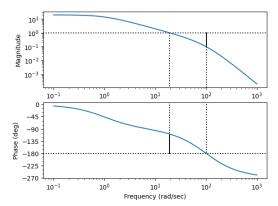
-225 -270

10<sup>2</sup>

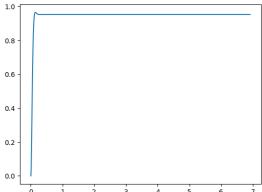


#### C(s) Bode Plot

Gm = 10.20 (at 101.00 rad/s), Pm = 71.17 deg (at 19.26 rad/s)



### C(s) Step Response



As we can see, the steady state error is less than 0.05 (the output is > 0.95 at the end of the step response once the oscillations have settled), the gain margin is greater than 10 dB, and the phase margin is greater than  $60^{\circ}$ .

## 2 2

For the same feedback control system as part 1, design a controller C(s) such at hat the closed-loop system has the following specifications: No overshoot, the settling time at 1% is  $T_s^{1\%} \leq 0.5\%$ , and the steady-state error in response to a unit step function is  $|e_{\infty}| = 0$ .

To do this we will adapt the controller from part 1. The controller from part one consists of  $C_1(s)$  which was used to control the steady-state error, and  $C_2(s)$  which was used to make the

system stable and satisfy the gain and phase margin requirements. We will keep  $C_2(s)$  the same since we still want the controller to stabilize the system (satisfying the gain and phase margin requirements is an extra bonus to keep the system in a "safe" region of stability) and replace  $C_1(s)$  with a controller that will make the system have no overshoot and a settling time of 0.5%. To do this we want to use a proportional-integral controller as it increases the steady state gain to zero error and only marginally reduces the phase margin.

$$mu = 2 \cdot \alpha$$

$$c = \frac{\mu}{\alpha}$$

$$T = \frac{10}{\omega_c}$$

$$C_3(s) = c + \frac{c}{T} \frac{1}{s}$$

We will keep  $\alpha=10$  and  $T=10/\omega_c$  using our crossover  $\omega_c$  value from part 1 to keep the phase margin decline limited to  $\approx 6\%$ . We decide to set our increase of the steady state gain to  $\mu=2\cdot\alpha$  instead of  $\alpha$  since the value reached the settling time requirement too slowly.

We can verify that the controller satisfies the requirements in code:

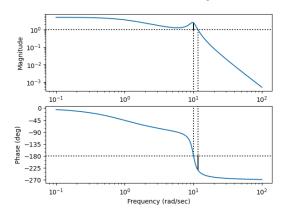
```
import math
import numpy as np
import control as ct
import matplotlib.pyplot as plt
omega_n = 10
zeta = 0.1
s = ct.tf('s')
G = 5 / (1 + s) / (1 + 2 * zeta / omega_n * s + s**2 / omega_n**2)
# G(s) Bode plot
plt.figure()
ct.bode_plot(G, margins=True)
plt.show()
# G(s) step response
plt.figure()
t, y = ct.step_response(G / (1 + G))
plt.plot(t, y)
plt.show()
omega_c = 10**1
# We don't rely on C_1 to control the steady-state error
C_{1} = 1
pole_1 = 10**0
```

```
pole_2 = 10**2
L_star = 5 / ((1 + (s / pole_1)) * (1 + (s / pole_2))**2)
C_2 = L_{star} * (1 / G)
alpha = 10
mu = 2 * alpha # the two here is a tunable parameter to control how much to increase steady-s
T = 10 / omega_c
c = mu / alpha
C_3 = c + (c / T) * (1 / s)
C = C_1 * C_2 * C_3
# C(s) Bode plot
plt.figure()
ct.bode_plot(C * G, margins=True)
plt.show()
# C(s) step response
plt.figure()
t, y = ct.step\_response((C * G) / (1 + (C * G)))
plt.plot(t, y)
plt.show()
# time idx at t = 0.5
idx = np.argmin(np.abs(t - 0.5))
print(f'Overshoot: {1 - max(y)}')
print(f"Max error after settling point (t = 0.5): {max(np.abs(y[idx:] - 1))}")
print(f"Steady-state error: {np.abs(y[-1] - 1)}")
# Prints out:
# Overshoot: -2.8851916411554157e-08
# Max error after settling point (t = 0.5): 0.0019246920997199046
# Steady-state error: 2.1373960601422937e-08
```

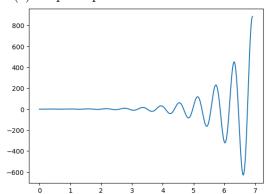
As we can see the overshoot is zero (modulo floating point rounding issues at  $\approx 1e - 8$ ), the error after t = 0.5 stays at less that 0.1% satisfying the settling time requirement, and the steady state error is zero (neglibly small at  $\approx 1e - 8$ ).

G(s) Bode Plot

Gm = 0.41 (at 10.10 rad/s), Pm = -52.05 deg (at 11.65 rad/s)

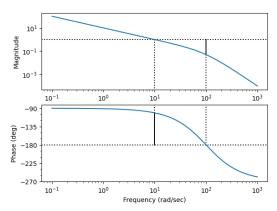


## G(s) Step Response



# C(s) Bode Plot

Gm = 20.00 (at 100.00 rad/s), Pm = 78.69 deg (at 9.90 rad/s)



C(s) Step Response

