

EXAMPLE 6-4 A direct current I flows in a straight wire of length $2L$. Find the magnetic flux density \mathbf{B} at a point located at a distance r from the wire in the bisecting plane: (a) by determining the vector magnetic potential \mathbf{A} first, and (b) by applying Biot-Savart law.

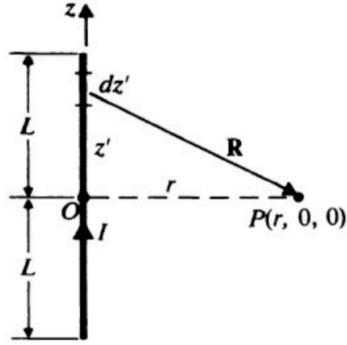


FIGURE 6-5
A current-carrying straight wire (Example 6-4).

Solution Currents exist only in closed circuits. Hence the wire in the present problem must be a part of a current-carrying loop with several straight sides. Since we do not know the rest of the circuit, Ampère's circuital law cannot be used to advantage. Refer to Fig. 6-5. The current-carrying line segment is aligned with the z -axis. A typical element on the wire is

$$d\ell' = \mathbf{a}_z dz'.$$

The cylindrical coordinates of the field point P are $(r, 0, 0)$.

a) By finding \mathbf{B} from $\nabla \times \mathbf{A}$. Substituting $R = \sqrt{z'^2 + r^2}$ into Eq. (6-27), we have

$$\begin{aligned} \mathbf{A} &= \mathbf{a}_z \frac{\mu_0 I}{4\pi} \int_{-L}^L \frac{dz'}{\sqrt{z'^2 + r^2}} \\ &= \mathbf{a}_z \frac{\mu_0 I}{4\pi} \left[\ln(z' + \sqrt{z'^2 + r^2}) \right]_{-L}^L \\ &= \mathbf{a}_z \frac{\mu_0 I}{4\pi} \ln \frac{\sqrt{L^2 + r^2} + L}{\sqrt{L^2 + r^2} - L}. \end{aligned} \quad (6-34)$$

Therefore,

$$\mathbf{B} = \nabla \times \mathbf{A} = \nabla \times (\mathbf{a}_z A_z) = \mathbf{a}_r \frac{1}{r} \frac{\partial A_z}{\partial \phi} - \mathbf{a}_\phi \frac{\partial A_z}{\partial r}.$$

Cylindrical symmetry around the wire assures that $\partial A_z / \partial \phi = 0$. Thus,

$$\begin{aligned} \mathbf{B} &= -\mathbf{a}_\phi \frac{\partial}{\partial r} \left[\frac{\mu_0 I}{4\pi} \ln \frac{\sqrt{L^2 + r^2} + L}{\sqrt{L^2 + r^2} - L} \right] \\ &= \mathbf{a}_\phi \frac{\mu_0 I L}{2\pi r \sqrt{L^2 + r^2}}. \end{aligned} \quad (6-35)$$

When $r \ll L$, Eq. (6-35) reduces to

$$\mathbf{B}_\phi = \mathbf{a}_\phi \frac{\mu_0 I}{2\pi r}, \quad (6-36)$$

which is the expression for \mathbf{B} at a point located at a distance r from an infinitely long, straight wire carrying current I , as given in Eq. (6-11b).

- b) *By applying Biot-Savart law.* From Fig. 6-5 we see that the distance vector *from* the source element dz' *to* the field point P is

$$\mathbf{R} = \mathbf{a}_r r - \mathbf{a}_z z'$$

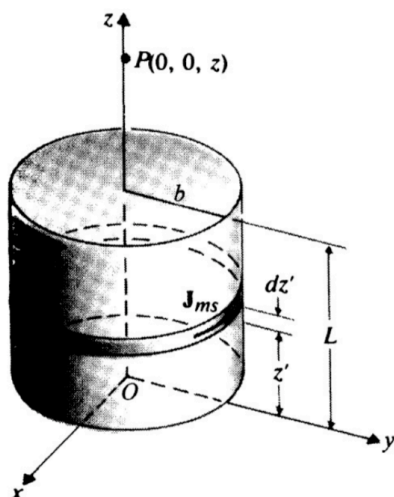
$$d\ell' \times \mathbf{R} = \mathbf{a}_z dz' \times (\mathbf{a}_r r - \mathbf{a}_z z') = \mathbf{a}_\phi r dz'.$$

Substitution in Eq. (6-33c) gives

$$\begin{aligned} \mathbf{B} &= \int d\mathbf{B} = \mathbf{a}_\phi \frac{\mu_0 I}{4\pi} \int_{-L}^L \frac{r dz'}{(z'^2 + r^2)^{3/2}} \\ &= \mathbf{a}_\phi \frac{\mu_0 I L}{2\pi r \sqrt{L^2 + r^2}}, \end{aligned}$$

which is the same as Eq. (6-35). ■

EXAMPLE 6-8 Determine the magnetic flux density on the axis of a uniformly magnetized circular cylinder of a magnetic material. The cylinder has a radius b , length L , and axial magnetization $\mathbf{M} = \mathbf{a}_z M_0$.



Question: \mathbf{B} on z axis?

Methods:

- (1) Calculate \mathbf{J}_m and \mathbf{J}_{ms}
- (2) \mathbf{B} due to \mathbf{J}

FIGURE 6-11

A uniformly magnetized circular cylinder (Example 6-8).

Solution In this problem concerning a cylindrical bar magnet, let the axis of the magnetized cylinder coincide with the z -axis of a cylindrical coordinate system, as shown in Fig. 6-11. Since the magnetization \mathbf{M} is a constant within the magnet, $\mathbf{J}_m = \nabla' \times \mathbf{M} = 0$, and there is no equivalent volume current density. The equivalent magnetization surface current density on the side wall is

$$\begin{aligned} \mathbf{J}_{ms} &= \mathbf{M} \times \mathbf{a}'_n = (\mathbf{a}_z M_0) \times \mathbf{a}_r \\ &= \mathbf{a}_\phi M_0. \end{aligned} \quad (6-64)$$

The magnet is then like a cylindrical sheet with a lineal current density of M_0 (A/m). There is no surface current on the top and bottom faces. To find \mathbf{B} at $P(0, 0, z)$, we consider a differential length dz' with a current $\mathbf{a}_\phi M_0 dz'$ and use Eq. (6-38) to obtain

Example 6-6
 $\mathbf{B} = \mathbf{a}_z \frac{\mu_0 I b^2}{2(z^2 + b^2)^{3/2}} \quad (\text{T}).$

 $\xrightarrow{dI = J_{ms} dz'} d\mathbf{B} = \mathbf{a}_z \frac{\mu_0 M_0 b^2 dz'}{2[(z - z')^2 + b^2]^{3/2}}$

and

$$\begin{aligned} \mathbf{B} &= \int d\mathbf{B} = \mathbf{a}_z \int_0^L \frac{\mu_0 M_0 b^2 dz'}{2[(z - z')^2 + b^2]^{3/2}} \\ &= \mathbf{a}_z \frac{\mu_0 M_0}{2} \left[\frac{z}{\sqrt{z^2 + b^2}} - \frac{z - L}{\sqrt{(z - L)^2 + b^2}} \right]. \end{aligned} \quad (6-65)$$