# Response Surface Methodology: Central Composite Designs

BIOE 498/598 PJ

Spring 2021

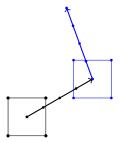
▶ Begin with a FF+CP design.



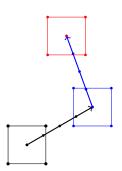
- ▶ Begin with a FF+CP design.
- ► Follow path of steepest ascent until the model breaks.



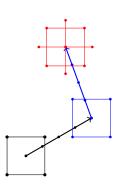
- ▶ Begin with a FF+CP design.
- ► Follow path of steepest ascent until the model breaks.
- ▶ New FF+CP; repeat steepest ascent.



- ▶ Begin with a FF+CP design.
- Follow path of steepest ascent until the model breaks.
- ▶ New FF+CP; repeat steepest ascent.
- ► Stop when model detects lack of fit.



- ▶ Begin with a FF+CP design.
- Follow path of steepest ascent until the model breaks.
- ▶ New FF+CP; repeat steepest ascent.
- ▶ Stop when model detects lack of fit.
- ► **Today**: Fitting a model to a curved response surface.



- ▶ We need two things to model a curved response surfaces:
  - 1. A model that is flexible enough to curve.
  - 2. Data that can detect the curvature.

- ▶ We need two things to model a curved response surfaces:
  - 1. A model that is flexible enough to curve.
  - 2. Data that can detect the curvature.
- The optimal operating conditions correspond to a maximum in the response surface.
- ▶ We need models that can contain maxima.

- ▶ We need two things to model a curved response surfaces:
  - 1. A model that is flexible enough to curve.
  - 2. Data that can detect the curvature.
- The optimal operating conditions correspond to a maximum in the response surface.
- We need models that can contain maxima.
- ► FO + TWI models are curved, but are rarely bounded.

- ▶ We need two things to model a curved response surfaces:
  - 1. A model that is flexible enough to curve.
  - 2. Data that can detect the curvature.
- The optimal operating conditions correspond to a maximum in the response surface.
- ▶ We need models that can contain maxima.
- ► FO + TWI models are curved, but are rarely bounded.

$$y=20+3.6x_1-1.8x_2-0.6x_1x_2$$
  
Set  $x_2=0$ , then  $y\to\infty$  as  $x_1\to\infty$ .

▶ The *true* model for any system is a general nonlinear function

$$y = f(x_1, x_2, \ldots, x_k)$$

▶ The *true* model for any system is a general nonlinear function

$$y = f(x_1, x_2, \ldots, x_k)$$

▶ If you know *f* for your system, congrats! Fit its parameters with regression and use it.

▶ The *true* model for any system is a general nonlinear function

$$y = f(x_1, x_2, \dots, x_k)$$

- ▶ If you know *f* for your system, congrats! Fit its parameters with regression and use it.
- Usually we don't know f, so we approximate it with a simpler function.

▶ The *true* model for any system is a general nonlinear function

$$y = f(x_1, x_2, \dots, x_k)$$

- ▶ If you know *f* for your system, congrats! Fit its parameters with regression and use it.
- Usually we don't know f, so we approximate it with a simpler function.
- We are not claiming that f is a particular shape. Rather, we claim that an approximation is "good enough" over our domain of interest.

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

Let's find the second-order Taylor series of  $f(x_1, x_2)$  centered at zero:

$$f(x_{1},x_{2}) \approx \underbrace{\frac{f|_{0}}{\beta_{0}} + \underbrace{\frac{\partial f}{\partial x_{1}}\Big|_{0}}_{\beta_{1}} x_{1} + \underbrace{\frac{\partial f}{\partial x_{2}}\Big|_{0}}_{\beta_{2}} x_{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1}^{2}}\Big|_{0}}_{\beta_{11}} x_{1}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{2}^{2}}\Big|_{0}}_{\beta_{22}} x_{2}^{2} + \underbrace{\frac{1}{2} \frac{\partial^{2} f}{\partial x_{1} \partial x_{2}}\Big|_{0}}_{\beta_{12}} x_{1} x_{2}$$

$$f(x_{1},x_{2}) \approx \underbrace{\underbrace{\beta_{0} + \beta_{1} x_{1} + \beta_{2} x_{2}}_{FO} + \underbrace{\frac{\beta_{11} x_{1}^{2} + \beta_{22} x_{2}^{2}}_{PQ} + \underbrace{\frac{\beta_{12} x_{1} x_{2}}{TWI}}}_{SO}$$

- ▶ The function f and its derivatives are unknown, so we fit the parameters  $\beta$  with a linear model.
- ▶ In general we will have k factors and the quadratic approximation will be

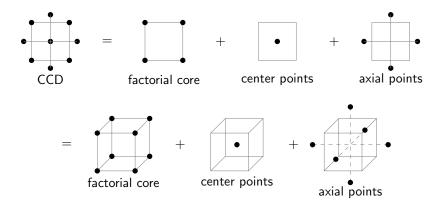
$$y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{i=1}^{j-1} \beta_{ij} x_i x_j.$$

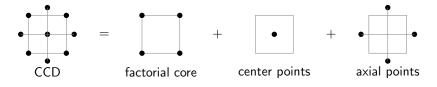
## The Central Composite Design (CCD)

- ▶ A factorial or FF design can estimate FO and TWI terms.
- Estimating curvature requires points beyond the factorial corners.
- One popular option is the Central Composite Design.

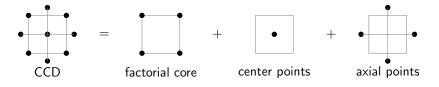
# The Central Composite Design (CCD)

- ▶ A factorial or FF design can estimate FO and TWI terms.
- Estimating curvature requires points beyond the factorial corners.
- One popular option is the Central Composite Design.

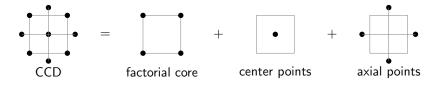




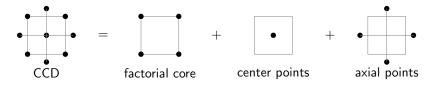
► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.



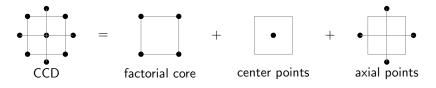
- ► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.



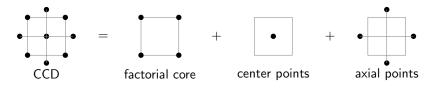
- ► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:



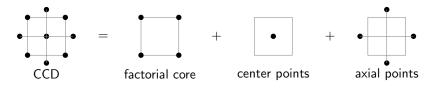
- ► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ▶ One factor is set to  $\pm \alpha$



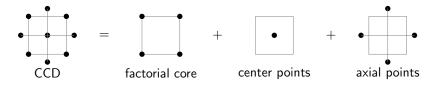
- ► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ▶ One factor is set to  $\pm \alpha$
  - All other factors are set to 0.



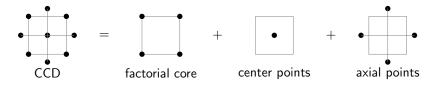
- ► Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - $\triangleright$  One factor is set to  $\pm \alpha$
  - All other factors are set to 0.
- Center points estimate pure error and help (some) with PQ terms.



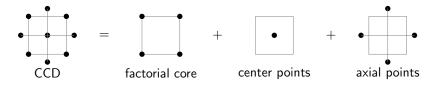
- Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ▶ One factor is set to  $\pm \alpha$
  - All other factors are set to 0.
- Center points estimate pure error and help (some) with PQ terms.
- ► To build a CCD you need to decide:



- Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ▶ One factor is set to  $\pm \alpha$
  - All other factors are set to 0.
- Center points estimate pure error and help (some) with PQ terms.
- ► To build a CCD you need to decide:
  - 1. The size of the FF core



- Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ▶ One factor is set to  $\pm \alpha$
  - All other factors are set to 0.
- Center points estimate pure error and help (some) with PQ terms.
- ► To build a CCD you need to decide:
  - 1. The size of the FF core
  - 2. The number of center runs



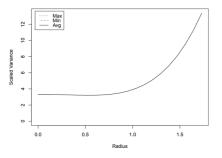
- Factorial points alone estimates the FO and TWI terms. The core must be Resolution V or higher.
- ► Axial points allow estimation of the PQ terms. Without axial points we could only estimate the sum of all PQ terms.
- CCDs have a pair of axial runs for each factor:
  - ightharpoonup One factor is set to  $\pm \alpha$
  - All other factors are set to 0.
- Center points estimate pure error and help (some) with PQ terms.
- ► To build a CCD you need to decide:
  - 1. The size of the FF core
  - 2. The number of center runs
  - 3. The value of  $\alpha$

## Uniform precision

▶ A model has **uniform precision** if the variance at design radius 1 is the same as at the center.

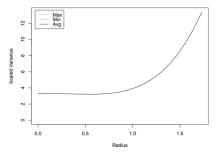
## Uniform precision

▶ A model has **uniform precision** if the variance at design radius 1 is the same as at the center.



### Uniform precision

▶ A model has **uniform precision** if the variance at design radius 1 is the same as at the center.



Choosing the correct number of center points in a CCD ensures uniform precision.

▶ Models are most precise at the center of the design.

- ▶ Models are most precise at the center of the design.
- ▶ Ideally, the change in precision should be independent of the *direction* we move away from the center.

- Models are most precise at the center of the design.
- ▶ Ideally, the change in precision should be independent of the *direction* we move away from the center.

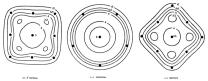


Fig. 2. Variance contours for some 2 dimensional designs

Image from Box and Hunter 1957.

- Models are most precise at the center of the design.
- ▶ Ideally, the change in precision should be independent of the *direction* we move away from the center.

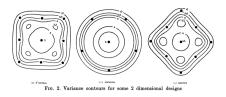


Image from Box and Hunter 1957.

Designs where the variance only depends on the radius are called rotatable designs.

- Models are most precise at the center of the design.
- ▶ Ideally, the change in precision should be independent of the *direction* we move away from the center.

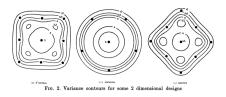


Image from Box and Hunter 1957.

- Designs where the variance only depends on the radius are called rotatable designs.
- ▶ A CCD with *F* factorial points is rotatable when  $\alpha = \sqrt[4]{F}$ .

# Rotatable, uniform precision CCDs

factors $(k)$	2	3	4	5	5 - 1	6
factorial points	4	8	16	32	16	64
axial points	4	6	8	10	10	12
center points	5	6	7	10	6	15
axial distance $(lpha)$	1.414	1.682	2.000	2.378	2.000	2.828
factors (k)	6 – 1	7	7 – 1	8	8 – 1	8 – 2
factorial points	32	128	64	256	128	64
axial points	12	14	14	16	16	16
center points	9	21	14	28	20	13
axial distance $(lpha)$	2.378	3.364	2.828	4.000	3.364	2.828

#### Factor levels in a CCD

Each factor in the CCD will be set at five levels:

$$-\alpha$$
  $-1$  0 1  $\alpha$ 

#### Factor levels in a CCD

Each factor in the CCD will be set at five levels:

$$-\alpha$$
  $-1$  0 1  $\alpha$ 

Unlike a 2-level design, the coded units in a CCD have meaning!

Let's say we're designing a combination screening of three drugs. The absolute widest concentration range we can use for drug A is [-3.2,1.0] on a  $\log_{10}\text{-}\mu\text{M}$  scale. What are the five levels assuming a full-factorial CCD?

Let's say we're designing a combination screening of three drugs. The absolute widest concentration range we can use for drug A is [-3.2, 1.0] on a  $\log_{10}$ - $\mu$ M scale. What are the five levels assuming a full-factorial CCD?

$$F = 2^3 = 8 \Rightarrow \alpha = \sqrt[4]{8} = 1.68$$

Let's say we're designing a combination screening of three drugs. The absolute widest concentration range we can use for drug A is [-3.2, 1.0] on a  $\log_{10}$ - $\mu$ M scale. What are the five levels assuming a full-factorial CCD?

$$F = 2^3 = 8 \Rightarrow \alpha = \sqrt[4]{8} = 1.68$$

$$\begin{aligned} \mathsf{A} &= \mathsf{center}(\mathsf{A}) + \frac{\mathsf{range}(\mathsf{A})}{2\alpha}[\mathsf{code}] \\ &= -1.1 + \frac{1 - (-3.2)}{2(1.68)}[\mathsf{code}] \end{aligned}$$

Let's say we're designing a combination screening of three drugs. The absolute widest concentration range we can use for drug A is [-3.2, 1.0] on a  $\log_{10}$ - $\mu$ M scale. What are the five levels assuming a full-factorial CCD?

$$F = 2^3 = 8 \Rightarrow \alpha = \sqrt[4]{8} = 1.68$$

$$\begin{aligned} \mathsf{A} &= \mathsf{center}(\mathsf{A}) + \frac{\mathsf{range}(\mathsf{A})}{2\alpha}[\mathsf{code}] \\ &= -1.1 + \frac{1 - (-3.2)}{2(1.68)}[\mathsf{code}] \end{aligned}$$