

A1

a) Skizze:



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Aus Überlegung:

$$\vec{p}' = -\vec{p}$$

$$\vec{\alpha}' = -\vec{\alpha}$$

$$\Rightarrow \Phi(\vec{r}) = \frac{1}{4\pi\epsilon_0} \left(\frac{\vec{p}(\vec{r}-\vec{\alpha})}{|\vec{r}-\vec{\alpha}|^3} - \frac{\vec{p}(\vec{r}+\vec{\alpha})}{|\vec{r}+\vec{\alpha}|^3} \right) = \frac{1}{4\pi\epsilon_0} \left(\frac{\rho x}{\sqrt{x^2+y^2+(z-a)^2}^3} - \frac{\rho x}{\sqrt{x^2+y^2+(z+a)^2}^3} \right)$$

Überprüfen der

Randbedingung:

$$\phi(\vec{r}) \underset{z=0}{=} \frac{1}{4\pi\epsilon_0} \left(\frac{\rho x}{\sqrt{x^2+y^2+a^2}^3} - \frac{\rho x}{\sqrt{x^2+y^2+a^2}^3} \right) = 0 \quad \checkmark$$

b)

Influenzierte Flächendichten:

$$\sigma(x, y) = \epsilon_0 \vec{n} \cdot \vec{E} \Big|_{z=0} = \epsilon_0 \vec{e}_z \vec{\nabla} \phi \Big|_{z=0} = \epsilon_0 \frac{\partial \phi}{\partial z} \Big|_{z=0}$$

$$\begin{aligned} \frac{\partial \phi}{\partial z} &= \frac{1}{4\pi\epsilon_0} \left(\frac{-\rho x \sqrt{(x^2+y^2+(z-a)^2)} \frac{1}{2\sqrt{x^2+y^2+(z-a)^2}} z(z-a)}{\sqrt{x^2+y^2+(z-a)^2}^6} \right. \\ &\quad \left. + \rho x \sqrt{(x^2+y^2+(z+a)^2)} \frac{1}{2\sqrt{x^2+y^2+(z+a)^2}} z(z+a) \right) \end{aligned}$$

$$= \frac{1}{4\pi\epsilon_0} \left(-\frac{3\rho x (z-a)}{\sqrt{x^2+y^2+(z-a)^2}^5} + \frac{3\rho x (z+a)}{\sqrt{x^2+y^2+(z+a)^2}^5} \right)$$

$$\Rightarrow \sigma(x, y) = \frac{1}{4\pi} \left(\frac{6\rho x a}{\sqrt{x^2+y^2+a^2}^5} \right) = \frac{3\rho x a}{2\pi\sqrt{x^2+y^2+a^2}^5}$$

;) Dipol-Dipol-Wechselwirkung:

$$W_{12} = \frac{1}{4\pi\epsilon_0} \left(\frac{\vec{p}_1 \cdot \vec{p}_2}{|\vec{r}_1 - \vec{r}_2|^3} - 3 \frac{(\vec{r}_1 - \vec{r}_2) \circ \vec{p}_1 \cdot (\vec{r}_1 - \vec{r}_2) \circ \vec{p}_2}{|\vec{r}_1 - \vec{r}_2|^5} \right) =$$

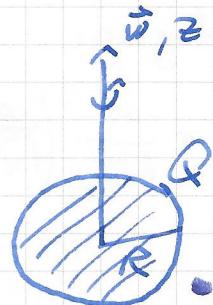
$$= \frac{1}{4\pi\epsilon_0} \left(\frac{-p^2}{8a^3} \right) = W_{12} \quad (a)$$

mit $\vec{p}_1 = \begin{pmatrix} p \\ 0 \\ 0 \end{pmatrix}$
 $\vec{p}_2 = \begin{pmatrix} -p \\ 0 \\ 0 \end{pmatrix}$
 $\vec{r}_1 = \begin{pmatrix} 0 \\ 0 \\ a \end{pmatrix}$
 $\vec{r}_2 = \begin{pmatrix} 0 \\ 0 \\ -a \end{pmatrix}$

$$\vec{F} \sim \vec{e}_z \quad \vec{F} = -\vec{\nabla} W_{12}$$

$$\Rightarrow \vec{F} = -\frac{d}{da} W_{12} \vec{e}_z = \frac{1}{4\pi\epsilon_0} p^2 \frac{-3}{8a^4} \vec{e}_z =$$

$$= -\frac{3p^2}{32\pi\epsilon_0 a^4} \vec{e}_z$$



AZ

$$a) \vec{j}(\vec{r}) = \vec{s}(\vec{r}) \cdot \vec{\nabla}(\vec{r})$$

$$\vec{s}(\vec{r}) = \frac{Q}{\pi R^2} \delta(z) \Theta(R-s)$$

$$\vec{\nabla}(\vec{r}) = \vec{\omega} \times \vec{r}$$

$$\vec{j}(\vec{r}) = \frac{Q}{\pi R^2} \delta(z) \Theta(R-s) \vec{\omega} \times \vec{r}$$

$$\text{Divergenz-Freiheit: } \vec{\nabla} \cdot \vec{j}(\vec{r}) = \frac{Q}{\pi R^2} \delta(z) \Theta(R-s) \vec{\nabla}(\vec{\omega} \times \vec{r}) =$$

$$= \frac{Q}{\pi R^2} \delta(z) \Theta(R-s) \left[\vec{r} \left(\vec{\nabla} \times \vec{\omega} \right) - \vec{\omega} \left(\vec{\nabla} \times \vec{r} \right) \right] = 0 \quad \checkmark$$

$$\Rightarrow \vec{\nabla} \cdot \vec{j}(\vec{r}) = 0$$

$$b) \quad \vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \vec{j}(\vec{r}) \times \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} d\vec{r}' = \vec{r}' = \begin{pmatrix} s' \cos \varphi' \\ s' \sin \varphi' \\ z' \end{pmatrix}$$

$$= \frac{\mu_0}{4\pi} \int_0^R \int_0^{2\pi} \int_0^R \frac{Q}{\pi R^2} S(z) \Theta(R-z) (\vec{w} \times \vec{r}') \times \frac{(-s' \cos \varphi')}{z - z'} \frac{(-s' \sin \varphi')}{\sqrt{s'^2 + z'^2}} s' ds' d\varphi' dz' =$$

$$\vec{r}' = \begin{pmatrix} 0 \\ 0 \\ z' \end{pmatrix}$$

$$= \frac{\mu_0 Q}{4\pi^2 R^2} \int_0^{2\pi} \int_0^R \frac{(\vec{w} \times \vec{r}') \times \frac{(-s' \cos \varphi')}{z} s'}{\sqrt{s'^2 + z'^2}} ds' d\varphi' =$$

NR:

$$\begin{pmatrix} 0 \\ 0 \\ w \end{pmatrix} \times \begin{pmatrix} s' \cos \varphi' \\ s' \sin \varphi' \\ 0 \end{pmatrix}$$

$$= \frac{\mu_0 Q}{4\pi^2 R^2} \int_0^{2\pi} \int_0^R \frac{\begin{pmatrix} -ws' \sin \varphi' \\ ws' \cos \varphi' \\ 0 \end{pmatrix} \times \begin{pmatrix} -s' \cos \varphi' \\ -s' \sin \varphi' \\ z \end{pmatrix} s'}{\sqrt{s'^2 + z'^2}} ds' d\varphi' =$$

$$\begin{pmatrix} -ws' \sin \varphi' \\ ws' \cos \varphi' \\ 0 \end{pmatrix}$$

$$= \frac{\mu_0 Q}{4\pi^2 R^2} \int_0^{2\pi} \int_0^R \frac{\begin{pmatrix} ws' \cos \varphi' \\ ws' \sin \varphi' \\ ws'^2 \end{pmatrix} s'}{\sqrt{s'^2 + z'^2}} ds' d\varphi' =$$

$$ds' d\varphi' =$$

Hinweis:

$$= \frac{\mu_0 Q}{4\pi^2 R^2} \int_0^R 2\pi \vec{e}_z w \frac{s'^3}{\sqrt{s'^2 + z'^2}} z ds' = \vec{e}_z \frac{\mu_0 Q w}{2\pi R^2} \left(\frac{R^2 + z^2}{\sqrt{R^2 + z^2}} - 2|z| \right)$$

$$\vec{r} = \begin{pmatrix} 0 \\ 0 \\ z \end{pmatrix}$$

$$c) \quad \vec{m} = \frac{1}{2} \int d\vec{r}' \vec{r}' \times \vec{j}(\vec{r}') = \frac{1}{2} \int_0^R \int_0^{2\pi} \int_0^R \vec{r}' \times (\vec{w} \times \vec{r}') \frac{Q}{\pi R^2} S(z) \Theta(R-z) s' ds' d\varphi' dz' =$$

$$= \frac{Q}{\pi R^2} \frac{1}{2} \int_0^{2\pi} \int_0^R \int_0^R \begin{pmatrix} s' \cos \varphi' \\ s' \sin \varphi' \\ 0 \end{pmatrix} \times \begin{pmatrix} -ws' \sin \varphi' \\ ws' \cos \varphi' \\ 0 \end{pmatrix} s' ds' d\varphi' dz' =$$

$$= \frac{1}{2} \int_0^R \int_0^{2\pi} \frac{Q}{\pi R^2} \vec{e}_z s'^3 w ds' d\varphi' = \frac{Q}{2\pi R^2} w 2\pi \vec{e}_z \int_0^R s'^3 ds' = \frac{Q w R^2}{R^2} \frac{41}{4} \vec{e}_z =$$

$$\vec{e} = \frac{Q w R^2}{4} \vec{e}_z = \vec{m}$$

Berechne \vec{B}_{dip} :

$$\vec{r} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \quad \text{für} \quad \vec{r} = \begin{pmatrix} 0 \\ 0 \\ z \end{pmatrix}$$

$$\begin{aligned} \vec{B}_{\text{dip}}(\vec{r}) &= \frac{\mu_0}{4\pi|z|^3} \left(3\vec{r}(\vec{m} \cdot \vec{r}) - \vec{m} \right) = \frac{\mu_0}{4\pi|z|^3} \left(3\vec{e}_z \frac{QwR^4}{4} - \frac{QwR^4}{4} \vec{e}_z \right) \\ &= \underline{\underline{\frac{\mu_0 Qw R^4}{8\pi |z|^3} \vec{e}_z}} = \vec{B}_{\text{dip}}(\vec{r}) \end{aligned}$$

Taylorentwicklung des \vec{B} -Feldes aus b)

$$\vec{B}(z) = \vec{e}_z \frac{\mu_0 Qw}{2\pi R^2} \left(\frac{R^2 + 2z^2}{\sqrt{R^2 + z^2}} - 2|z| \right) = \vec{e}_z \frac{\mu_0 Qw}{2\pi R^2} \left(\frac{R^2 + 2z^2}{|z|\sqrt{1 + \frac{R^2}{z^2}}} - 2|z| \right) =$$

Taylorentw. bei $\frac{R^2}{z^2} \approx 0$ für $z \gg R$

$$\begin{aligned} &\approx \vec{e}_z \frac{\mu_0 Qw}{2\pi R^2} \left[\frac{R^2 + 2z^2}{|z|} \left(1 - \frac{R^2}{2z^2} + \frac{3R^4}{8z^4} \right) - 2|z| \right] = \\ &= \vec{e}_z \frac{\mu_0 Qw}{2\pi R^2} \left[\frac{R^2}{|z|} - \frac{R^4}{2|z|^3} + \frac{3R^6}{8|z|^5} + 2|z| - \frac{R^2}{|z|} + \frac{6R^4}{8|z|^3} - 2|z| \right] \\ &= \vec{e}_z \frac{\mu_0 Qw}{2\pi R^2} \left(\frac{1}{4} \frac{R^4}{|z|^2} + \frac{3R^6}{8|z|^5} \right) \approx \underline{\underline{\vec{e}_z \frac{\mu_0 Qw R^2}{8\pi |z|^2} = \vec{B}_{\text{dip}}}} \end{aligned}$$

A3

verschiebungssstrom : $\mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$

a)

$$\Rightarrow \vec{\nabla} \times \vec{B} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \text{mit} \quad \vec{B} = B(s) \vec{e}_y$$

$$\Rightarrow \vec{\nabla} \times \vec{B} = \frac{1}{s} \frac{\partial}{\partial s} (s B(s)) \vec{e}_z = \mu_0 \epsilon_0 K \vec{e}_z$$

$$\Rightarrow \frac{\partial}{\partial s} (s B(s)) = \mu_0 \epsilon_0 K s$$

$$s B(s) = \frac{\mu_0 \epsilon_0 K s^2}{2}$$

$$\Rightarrow B(s) = \frac{\mu_0 \epsilon_0 K s}{2} \Rightarrow \underline{\underline{\vec{B}(s) = \frac{\mu_0 \epsilon_0 K s}{2} \vec{e}_y}}$$

$$b) \vec{s}(\vec{r}, t) = \frac{1}{\mu_0} \vec{E} \times \vec{B} = \frac{\partial \vec{E}}{\partial t} = k \vec{e}_z \Rightarrow \vec{E}(\vec{r}, t) = k t \vec{e}_z$$

$$= \frac{1}{\mu_0} k t \vec{e}_z \times \underbrace{\frac{\mu_0 E_0 K^2}{2} \vec{e}_x}_{\vec{e}_s} = - \underbrace{\frac{E_0 K^2 S t}{2} \vec{e}_s}$$

Energiefluss:

$$J = \int_A \vec{s}(\vec{r}, t) d\vec{F} \leftarrow$$

Fläche mit ~~gerichtetem~~ nach innen gerichtetem Normalsvektor (\vec{e}_s) da einfließende Energie positiv ist.

$$= \int_0^{2\pi} \int_0^R \frac{E_0 K^2 S t}{2} \vec{e}_s \cdot \vec{e}_s R d\varphi dz =$$

$$= \underline{\underline{E_0 K^2 R^2 t / \pi = J}}$$

Energie im Kondensator:

Energiedichte: $w_{em} = \frac{\epsilon_0}{2} \vec{E}^2 + \frac{1}{2\mu_0} \vec{B}^2 = \frac{\epsilon_0}{2} k^2 f^2 + \frac{\mu_0 E_0 K^2 S^2}{8}$

$$\begin{aligned} \epsilon_{em} &= \int_{Kond} w_{em} d^3 r = \int_0^{2\pi} \int_0^R \int_0^S \left(\frac{\epsilon_0}{2} k^2 f^2 + \frac{\mu_0 E_0 K^2 S^2}{8} \right) S d\varphi dz = \\ &= (\pi R^2 \frac{\epsilon_0}{2} k^2 f^2 + 2\pi R \frac{\mu_0 E_0 K^2 S^2}{8}) = \underline{\underline{\epsilon_{em} (t)}}$$

$$\frac{d\epsilon_{em}}{dt} = (\pi R^2 \epsilon_0 k^2 f = J) \quad \square$$

A4

a) $\vec{j}(\vec{r}) = \left[\frac{I}{\pi R_1^2} \theta(R_1 - s) - \frac{I}{2\pi R_2} \delta(s - R_2) \right] \hat{e}_z$

b) $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$

$$\rightarrow \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \mu_0 \vec{j}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \cdot \vec{A}) - \Delta \vec{A} = \mu_0 \vec{j}$$

=0 nach Coulomb-Feldung

Hinweis $\Rightarrow \frac{1}{s} \frac{d}{ds} [s A'(s)] \hat{e}_z = -\mu_0 \vec{j}(\vec{r})$

$s < R_1: \rightarrow \frac{1}{s} \frac{d}{ds} [s A'(s)] = -\frac{\mu_0 I}{\pi R_1^2}$

$$-\frac{\mu_0 I}{\pi R_1^2} s^2 + C = s A'(s)$$

$$-\frac{\mu_0 I}{2\pi R_1^2} s + \frac{C_{1i}}{s} = A'(s)$$

$$\underline{-\frac{\mu_0 I}{4\pi R_1^2} s^2 + C_{1i} \ln(s) + C_{2i} = A(s)}$$

$R_1 < s < R_2:$

$$\frac{1}{s} \frac{d}{ds} [s A'(s)] = 0$$

$$s A'(s) = C_{1m}$$

$$\underline{A(s) = C_{1m} \ln(s) + C_{2m}}$$

$R_2 < s$, kein \vec{B} -Feld $\Rightarrow A(s) = \text{const} = C_{2a}$

$$\rightarrow A(s) = \begin{cases} -\frac{\mu_0 I}{4\pi R_1^2} s^2 + C_{1i} \ln(s) + C_{2i} & s < R_1 \\ C_{1m} \ln(s) + C_{2m} & R_1 < s < R_2 \\ C_{2a} & R_2 < s \end{cases}$$

- Keine singulären Terme,
 $\Rightarrow C_{1i} = 0$
- Setze $C_{2i} = 0$ da 1 Konst. frei wählbar

- Stetigkeit bei $s = R_1$:

$$-\frac{\mu_0 I}{4\pi} = C_{1m} \ln(R_1) + C_{2m}$$

- Differenzierbarkeit bei $s = R_1$:

$$-\frac{\mu_0 I}{2\pi R_1} = \frac{C_{1m}}{R_1} \Rightarrow C_{1m} = -\frac{\mu_0 I}{2\pi}$$

ln Stetigkeitsbedingung:

$$-\frac{\mu_0 I}{4\pi} = -\frac{\mu_0 I}{2\pi} \ln(R_1) + C_{2m}$$

$$\Rightarrow C_{2m} = -\frac{\mu_0 I}{4\pi} + \frac{\mu_0 I}{2\pi} \ln(R_1)$$

$$\Rightarrow A(s) = -\frac{\mu_0 I}{4\pi} - \frac{\mu_0 I}{2\pi} \ln\left(\frac{s}{R_1}\right) = \underline{\underline{-\frac{\mu_0 I}{4\pi} \left(1 + \ln\left(\frac{s^2}{R_1^2}\right)\right)}}$$

Stetigkeit bei R_2 :

$$\Rightarrow A(s) = \underline{\underline{-\frac{\mu_0 I}{4\pi} \left(1 + \ln\left(\frac{R_2^2}{R_1^2}\right)\right)}} \quad s > R_2$$

$$\Rightarrow A(s) = \begin{cases} -\frac{\mu_0 I s^2}{4\pi R_1^2} & s \leq R_1 \\ -\frac{\mu_0 I}{4\pi} \left(1 + 2 \ln\left(\frac{s}{R_1}\right)\right) & R_1 < s < R_2 \\ -\frac{\mu_0 I}{4\pi} \left(1 + 2 \ln\left(\frac{R_2}{R_1}\right)\right) & R_2 < s \end{cases}$$

c) Selbstinduktivität pro Längeneinheit $\frac{L}{l}$:

$$\frac{L}{l} = \frac{1}{I^2} \int_S dF \vec{j}(\vec{r}) \vec{A}(\vec{r}) =$$

$$= \frac{1}{I^2} \left[\int_0^{R_1} \int_0^{2\pi} \int_{-\infty}^{\infty} \frac{I}{\pi R_1^2} \left(-\frac{\mu_0 I s^2}{4\pi R_1^2} \right) s ds dr - \int_{R_1}^{R_2} \int_0^{2\pi} \int_{-\infty}^{\infty} \frac{I}{2\pi R_2} \delta(s-R_2) \left[\frac{-\mu_0 I}{4\pi} \left(1 + 2 \ln\left(\frac{R_2}{R_1}\right) \right) \right] s ds dr \right]$$

$$= \frac{1}{I^2} \left[\int_0^{R_1} \int_0^{2\pi} \int_{-\infty}^{\infty} \frac{I^2 N_0 s^3}{4\pi^2 R_1^4} + \int_0^{2\pi} \frac{I^2 \mu_0}{8\pi^2 R_2} \left(1 + 2 \ln\left(\frac{R_2}{R_1}\right) \right) R_2 dr \right] =$$

$$= -\frac{\mu_0}{8\pi} + \int_0^{2\pi} \frac{\mu_0}{8\pi^2} \left(1 + 2 \ln\left(\frac{R_2}{R_1}\right) \right) dr =$$

$$= -\frac{\mu_0}{8\pi} + \frac{\mu_0}{4\pi} \left(1 + 2 \ln\left(\frac{R_2}{R_1}\right) \right) =$$

$$= \frac{\mu_0}{2\pi} \left[\ln\left(\frac{R_2}{R_1}\right) + \frac{1}{4} \right] = \underline{\underline{\frac{L}{l}}}$$

⑤

⑥

$$\vec{E}_S(z,t) = \{ E_S^+ e^{i(k_S z - \omega t)} + E_S^- e^{i(-k_S z - \omega t)} \}_{\text{ex}}$$

Stetigkeitsbed:

$$\underline{z > 0}: E_1^+ e^{i(k_1 z - \omega t)} + E_1^- e^{i(-k_1 z - \omega t)} \\ u_1 (\hat{u} \times \vec{E}_S^+) e^{i(k_1 z - \omega t)} - n_1 (\hat{n} \times \vec{E}_S^-) e^{i(-k_1 z - \omega t)}$$

$$\underline{z < 0}: E_2^+ e^{i(k_2 z - \omega t)} + E_2^- e^{i(-k_2 z - \omega t)} \\ - u_2 (\hat{u} \times \vec{E}_S^-) e^{i(-k_2 z - \omega t)} + u_2 (\hat{u} \times \vec{E}_S^+) e^{i(k_2 z - \omega t)}$$

$$\underline{z=0} \quad E_1^+ + E_1^- = E_2^+ + E_2^-$$

$$u_1 (E_1^+ - E_1^-) = u_2 (E_2^+ - E_2^-)$$

$$E_1^+ = E_2^+ + E_2^- - E_1^-$$

$$u_1 (E_2^+ + E_2^- - 2E_1^-) = u_2 (E_2^+ - E_2^-)$$

$$-2n_1 E_1^- = E_2^+ (u_2 - u_1) - E_2^- (u_1 + u_2)$$

$$E_1^- = E_2^+ \left(\frac{1}{2} - \frac{u_2}{2u_1} \right) + E_2^- \left(\frac{1}{2} + \frac{u_2}{2u_1} \right)$$

$$E_1^+ = E_2^+ + E_2^- - E_2^+ \left(\frac{1}{2} - \frac{u_2}{2u_1} \right) - E_2^- \left(\frac{1}{2} + \frac{u_2}{2u_1} \right)$$

$$E_1^+ = E_2^+ \cdot \left[1 - \frac{1}{2} + \frac{u_2}{2u_1} \right] + E_2^- \cdot \left[1 - \frac{1}{2} - \frac{u_2}{2u_1} \right]$$

$$E_1^+ = E_2^+ \cdot \left[\frac{1}{2} + \frac{u_2}{2u_1} \right] + E_2^- \cdot \left[\frac{1}{2} - \frac{u_2}{2u_1} \right]$$

(12)

$$\begin{pmatrix} E_1^+ \\ E_1^- \end{pmatrix} = \begin{pmatrix} \frac{1}{2} + \frac{u_2}{2u_1} & \frac{1}{2} + \frac{u_2}{2u_1} \\ \frac{1}{2} - \frac{u_2}{2u_1} & \frac{1}{2} - \frac{u_2}{2u_1} \end{pmatrix} \begin{pmatrix} E_2^+ \\ E_2^- \end{pmatrix} \quad \square$$

③) $E_2^- = 0$

$$\Rightarrow E_1^+ = E_2^+ \left[\frac{u_1 + u_2}{2u_1} \right]$$

$$\Rightarrow E_1^- = E_2^+ \left[\frac{u_1 - u_2}{2u_1} \right]$$

$$\langle S_1^+ \rangle = \frac{1}{2} \epsilon_0 u_1^2 E_2^{+2} \left[\frac{u_1 + u_2}{2u_1} \right]^2 \cdot C \vec{e}_z$$

$$= \frac{1}{2} \epsilon_0 u_1 E_2^{+2} \left[\frac{u_1 + u_2}{2u_1} \right]^2 \cdot C \vec{e}_z$$

$$\langle S_1^- \rangle = -\frac{1}{2} \cos u_1 E_2^{+2} \left[\frac{u_1 - u_2}{2u_1} \right]^2 \cdot C \vec{e}_z$$

$$\langle S_2^+ \rangle = \frac{1}{2} \epsilon_0 u_2 E_2^{+2} e \vec{e}_z$$

$$R = \frac{\langle S_1^- \rangle}{\langle S_1^+ \rangle} = \frac{\left(\frac{u_1 - u_2}{2u_1} \cdot \frac{2u_1}{u_1 + u_2} \right)^2}{\left(\frac{u_1 + u_2}{2u_1} \right)^2} = \left(\frac{u_1 - u_2}{u_1 + u_2} \right)^2$$

$$T = \frac{\langle S_2^+ \rangle}{\langle S_1^+ \rangle} = \frac{u_2}{u_1} \left[\frac{2u_1}{u_1 + u_2} \right]^2$$

$$R + T = \frac{(u_1 - u_2)^2 u_1 + u_2 [2u_1]^2}{(u_1 + u_2)^2 \cdot u_1} = 1$$

$$(u_1 - u_2)^2 u_1 + u_2 [2u_1]^2 = (u_1 + u_2)^2 \cdot u_1$$

$$\frac{u_1^2 - 2u_1u_2 + u_2^2 + u_2^4u_1}{u_1^2 + 2u_1u_2 + u_2^2} = 1 \quad \checkmark$$

(13)