





$$= \frac{(2712.14 - 419.17) \times 5600}{0.704}$$

$$= 18239534.09 \text{ kJ}$$

$$= 18239.53 \text{ MJ}$$

$$\therefore \text{Mass of fuel fired} = \frac{18239534.09}{31380}$$

$$= 581.25 \text{ kg/h}$$

$$\therefore \text{Saving coal per hour} = 700 - 581.25 = 118.75 \text{ kg/h}$$

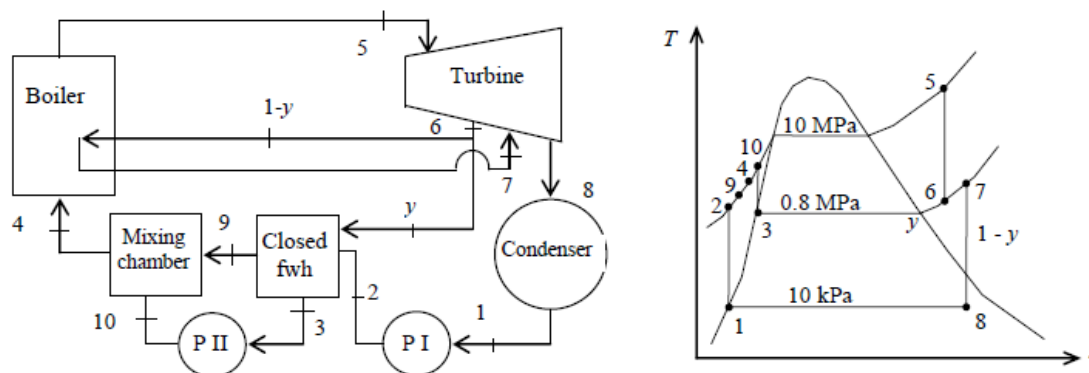
$$\therefore \text{C} \Rightarrow 118.75 \text{ kg/h}$$

###



## Q.2

### Analysis



(a) From the steam tables (Tables A-4, A-5, and A-6),

$$h_1 = h_{f@10\text{kPa}} = 191.81 \text{ kJ/kg}$$

$$v_1 = v_{f@10\text{kPa}} = 0.00101 \text{ m}^3/\text{kg}$$

$$w_{pI,in} = v_1(P_2 - P_1) = (0.00101 \text{ m}^3/\text{kg})(10,000 - 10 \text{ kPa}) \left( \frac{1 \text{ kJ}}{1 \text{ kPa} \cdot \text{m}^3} \right) = 10.09 \text{ kJ/kg}$$

$$h_2 = h_1 + w_{pI,in} = 191.81 + 10.09 = 201.90 \text{ kJ/kg}$$

$$\left. \begin{array}{l} P_3 = 0.8 \text{ MPa} \\ \text{sat. liquid} \end{array} \right\} \begin{array}{l} h_3 = h_{f@0.8\text{MPa}} = 720.87 \text{ kJ/kg} \\ v_3 = v_{f@0.8\text{MPa}} = 0.001115 \text{ m}^3/\text{kg} \end{array}$$

$$w_{pII,in} = v_3(P_4 - P_3) = (0.001115 \text{ m}^3/\text{kg})(10,000 - 800 \text{ kPa}) \left( \frac{1 \text{ kJ}}{1 \text{ kPa} \cdot \text{m}^3} \right) = 10.26 \text{ kJ/kg}$$

$$h_4 = h_3 + w_{pII,in} = 720.87 + 10.26 = 731.13 \text{ kJ/kg}$$

Also,  $h_4 = h_9 = h_{10} = 731.12 \text{ kJ/kg}$  since the two fluid streams that are being mixed have the same enthalpy.

$$\left. \begin{array}{l} P_5 = 10 \text{ MPa} \\ T_5 = 550^\circ\text{C} \end{array} \right\} \begin{array}{l} h_5 = 3502.0 \text{ kJ/kg} \\ s_5 = 6.7585 \text{ kJ/kg} \cdot \text{K} \end{array}$$

$$\left. \begin{array}{l} P_6 = 0.8 \text{ MPa} \\ s_6 = s_5 \end{array} \right\} h_6 = 2812.7 \text{ kJ/kg}$$

$$\left. \begin{array}{l} P_7 = 0.8 \text{ MPa} \\ T_7 = 500^\circ\text{C} \end{array} \right\} \begin{array}{l} h_7 = 3481.3 \text{ kJ/kg} \\ s_7 = 7.8692 \text{ kJ/kg} \cdot \text{K} \end{array}$$

$$\left. \begin{array}{l} P_8 = 10 \text{ kPa} \\ s_8 = s_7 \end{array} \right\} \begin{array}{l} x_8 = \frac{s_8 - s_f}{s_{fg}} = \frac{7.8692 - 0.6492}{7.4996} = 0.9627 \\ h_8 = h_f + x_8 h_{fg} = 191.81 + (0.9627)(2392.1) = 2494.7 \text{ kJ/kg} \end{array}$$

The fraction of steam extracted is determined from the steady-flow energy balance equation applied to the feedwater heaters. Noting that  $\dot{Q} \cong \dot{W} \cong \Delta ke \cong \Delta pe \cong 0$ ,



$$\dot{E}_{in} - \dot{E}_{out} = \Delta \dot{E}_{system} \quad \phi^0(\text{steady}) = 0$$

$$\dot{E}_{in} = \dot{E}_{out}$$

$$\sum \dot{m}_i h_i = \sum \dot{m}_e h_e \longrightarrow \dot{m}_2(h_9 - h_2) = \dot{m}_3(h_6 - h_3) \longrightarrow (1 - y)(h_9 - h_2) = y(h_6 - h_3)$$

where  $y$  is the fraction of steam extracted from the turbine ( $= \dot{m}_3 / \dot{m}_4$ ). Solving for  $y$ ,

$$y = \frac{h_9 - h_2}{(h_6 - h_3) + (h_9 - h_2)} = \frac{731.13 - 201.90}{2812.7 - 720.87 + 731.13 - 201.90} = 0.2019$$

Then,

$$q_{in} = (h_5 - h_4) + (1 - y)(h_7 - h_6) = (3502.0 - 731.13) + (1 - 0.2019)(3481.3 - 2812.7) = 3304.5 \text{ kJ/kg}$$

$$q_{out} = (1 - y)(h_8 - h_1) = (1 - 0.2019)(2494.7 - 191.81) = 1837.9 \text{ kJ/kg}$$

$$w_{net} = q_{in} - q_{out} = 3304.5 - 1837.8 = 1466.6 \text{ kJ/kg}$$

and

$$\dot{m} = \frac{\dot{W}_{net}}{w_{net}} = \frac{80,000 \text{ kJ/s}}{1467.1 \text{ kJ/kg}} = \mathbf{54.5 \text{ kg/s}}$$

$$(b) \quad \eta_{th} = 1 - \frac{q_{out}}{q_{in}} = 1 - \frac{1837.8 \text{ kJ/kg}}{3304.5 \text{ kJ/kg}} = \mathbf{44.4\%}$$