

Robot Dynamics

Introduction to Robotics

EECS 106B/206B

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Dynamics

- **Dynamics**: relation between **accelerations** and **forces**
- Important things to know to solve dynamics...
 - Mass and inertia of all components
 - Relevant forces and torques
 - Actuation, gravity, friction, interaction, etc.
- **Lagrangian Dynamics**
 - An energy approach to finding equations of motion

Newtonian Dynamics

- **Newton's Second Law** for unconstrained point masses:

$$f = \frac{d}{dt}(m\dot{x}) = m\ddot{x}$$

where $\dot{x} \in \mathbb{R}^3$ is the inertial velocity

- We cannot simply write

- Why?
$$\tau = m\ddot{\theta}$$
 - Mechanism is not a point mass
 - Configuration space is not Euclidean or inertial

Basic Formulation

- Instead of a single point mass or a set of independent point masses, we are interested in rigid bodies
- **Rigid bodies** are composed of points that are interconnected!
 - Position (**holonomic**) constraints
- **Generalized coordinates** (q) describe the configuration of a system using fewer variables
 - Manipulator: joint angles (θ)

Dynamics Using Generalized Coordinates

- Dynamics for systems with generalized coordinates (q)
 - Newton's Law does not apply
 - Use the ***Euler-Lagrange equations*** instead

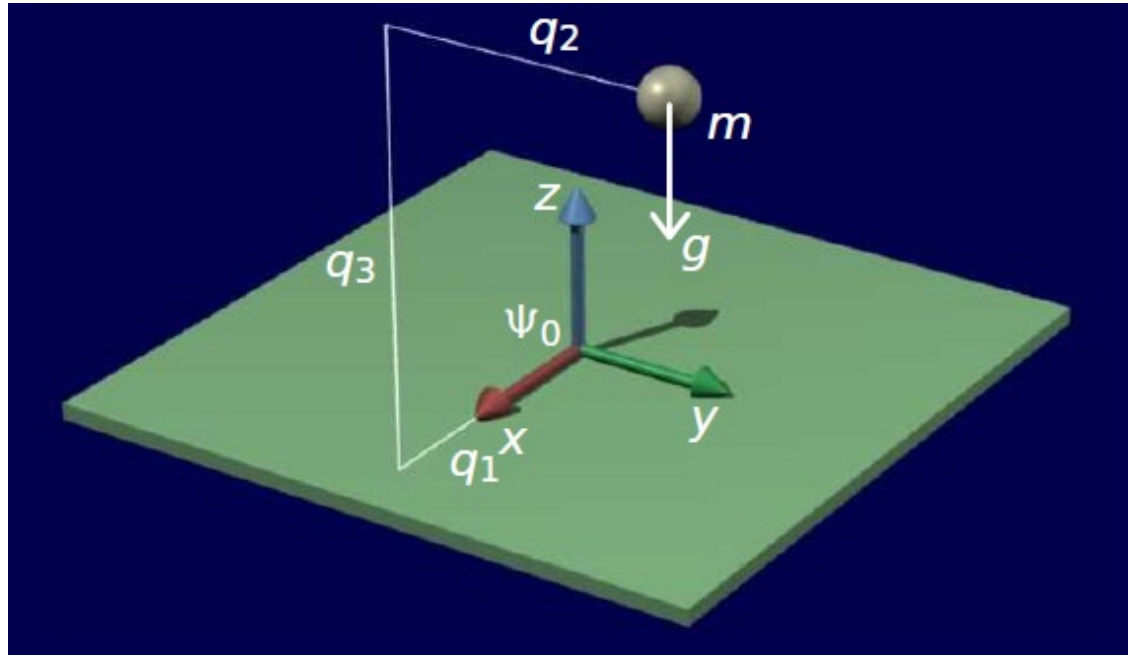
$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = \Upsilon$$

- Where $L(q, \dot{q})$ is the ***Lagrangian*** given by

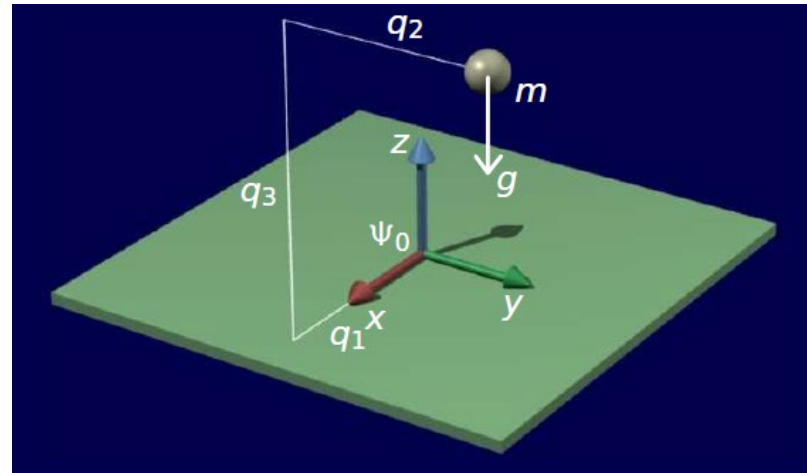
$$L(q, \dot{q}) = T(q, \dot{q}) - V(q)$$

- And Υ is the generalized force associated with \dot{q}

Example: Point Mass



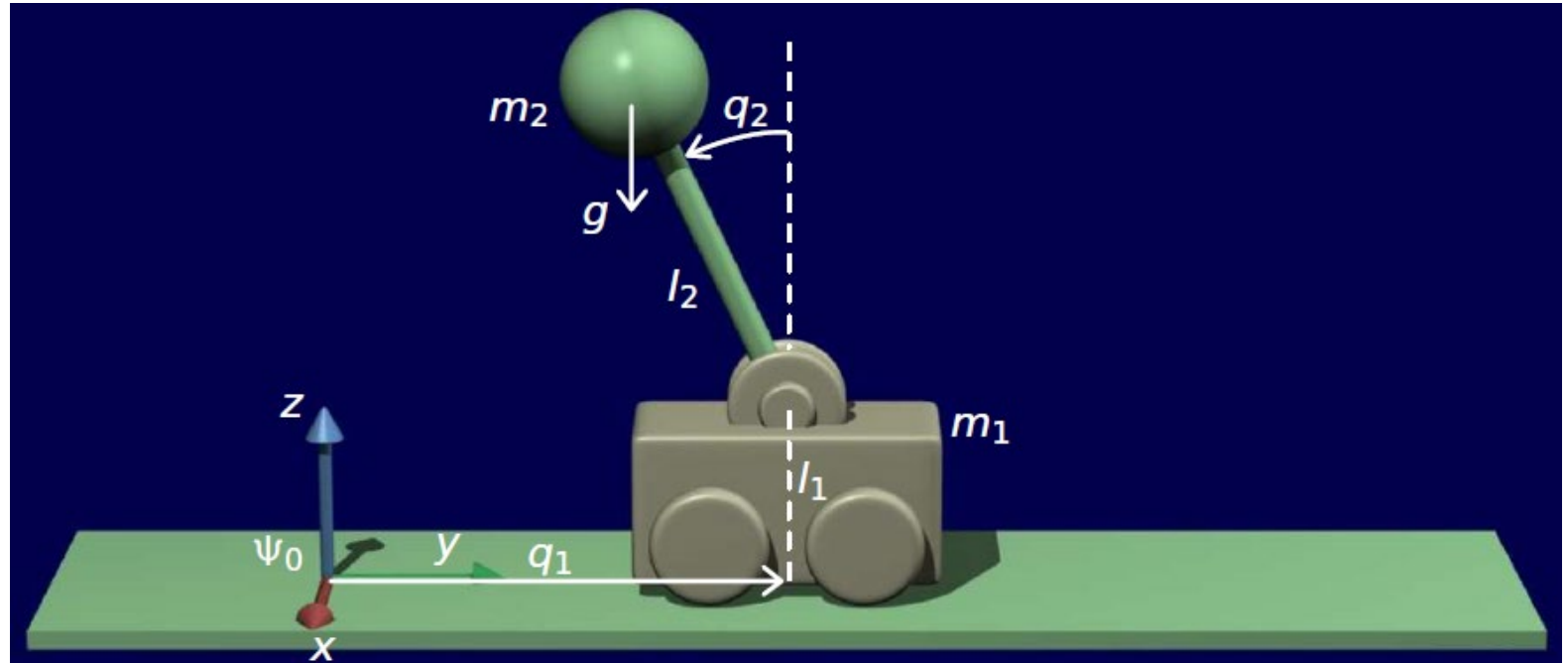
Example: Point Mass



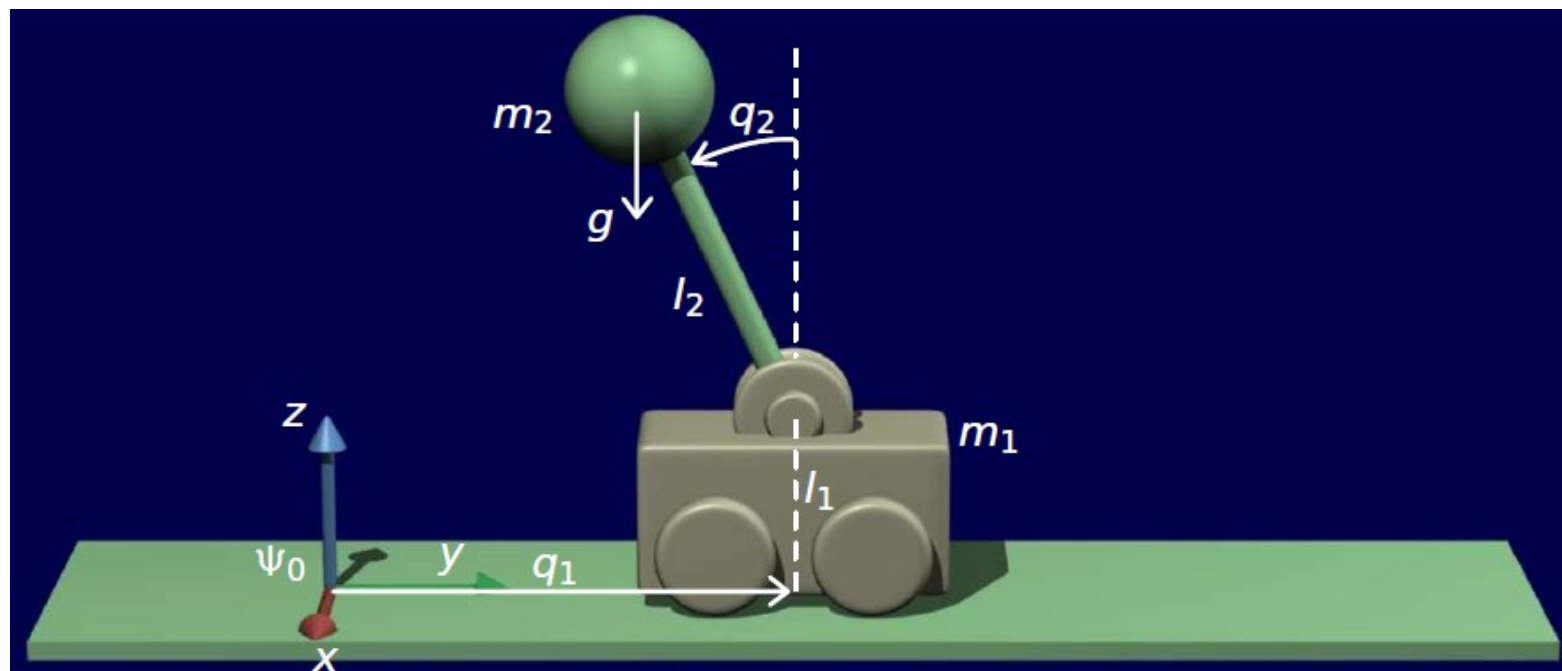
- Kinetic energy: $T(q, \dot{q}) = \frac{1}{2} m \dot{q}^T \dot{q}$
- Potential energy: $V(q) = m g q_3$
- Lagrangian: $L(q, \dot{q}) = T(q, \dot{q}) - V(q)$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = m \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \\ \ddot{q}_3 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ mg \end{bmatrix} = 0$$

Example: Pendulum Cart



Example: Pendulum Cart



- Kinetic energy:

$$T(q, \dot{q}) = \frac{1}{2} m_1 \dot{q}_1^2 + \frac{1}{2} m_2 (\dot{q}_1^2 + l_2^2 \dot{q}_2^2 - 2l_2 \cos(q_2) \dot{q}_1 \dot{q}_2)$$

- Potential energy: $V(q) = m_2 g (l_1 + l_2 \cos(q_2))$

Applying to Mechanisms...

- In order to apply these techniques to robotic mechanisms, we need:
 - **Generalized coordinates** q : choose joint angles θ
 - **Kinetic energy**: energies due to motion of the links
 - **Potential energy**: e.g. gravity on links

Center of Mass (CoM)

- **Center of mass**
 - Balancing point on a rigid body
 - If suspended from that point, body will tend to not rotate
- Compute CoM position as a weighted average

$$\begin{bmatrix} x_{CoM} \\ y_{CoM} \\ z_{CoM} \end{bmatrix} = \int_V \rho(r) \mathbf{r} dV = \frac{1}{m} \iiint_{x,y,z} \rho(x, y, z) \begin{bmatrix} x \\ y \\ z \end{bmatrix} dx dy dz$$

Mass vs. Inertia

- Translation energy vs. rotation energy
 - Point mass m with $\dot{x} = v$: $T = \frac{1}{2}mv^2$
 - Point mass m with $\dot{x} = \omega r$: $T = \frac{1}{2}m(\omega r)^2 = \frac{1}{2}(mr^2)\omega^2$
- Both energies are the same kinetic energy, just expressed in different coordinates!
- Inertia
 - **Inertia** J of a mass m : 'angular weight' s.t. $T = \frac{1}{2}J\omega^2$
 - $\omega \in \mathbb{R}$: angular velocity around a specific axis
 - Inertia depends on axis direction and location

Kinetic Energy of Rigid Body

- Velocity of a point (CoM) in an inertial frame given by

$$\dot{p} + \dot{R}r$$

where $r \in \mathbb{R}^3$ is the point coordinates in body frame

- Then we can express the kinetic energy using a volume integral in the following form

$$T = \frac{1}{2} \int_V \rho(r) \|\dot{p} + \dot{R}r\|^2 dV$$

Kinetic Energy of Rigid Body

- Expanding the product and simplifying (see MLS 4.2)

$$T = \underbrace{\frac{1}{2}m\|\dot{\mathbf{p}}\|^2}_{\text{translational}} + \underbrace{\frac{1}{2}\boldsymbol{\omega}^T \mathbf{I} \boldsymbol{\omega}}_{\text{rotational}}$$

where \mathbf{I} is the **inertia tensor** expressed in the body frame such that

$$\mathbf{I} = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}$$

Kinetic Energy of Rigid Body

- Represented in terms of a body velocity V^b we have the following equation

$$T = \frac{1}{2} (V^b)^T \begin{bmatrix} mI & 0 \\ 0 & I \end{bmatrix} V^b = \frac{1}{2} (V^b)^T \mathcal{M} V^b$$

where \mathcal{M} is the ***generalized inertia matrix*** expressed in the body frame

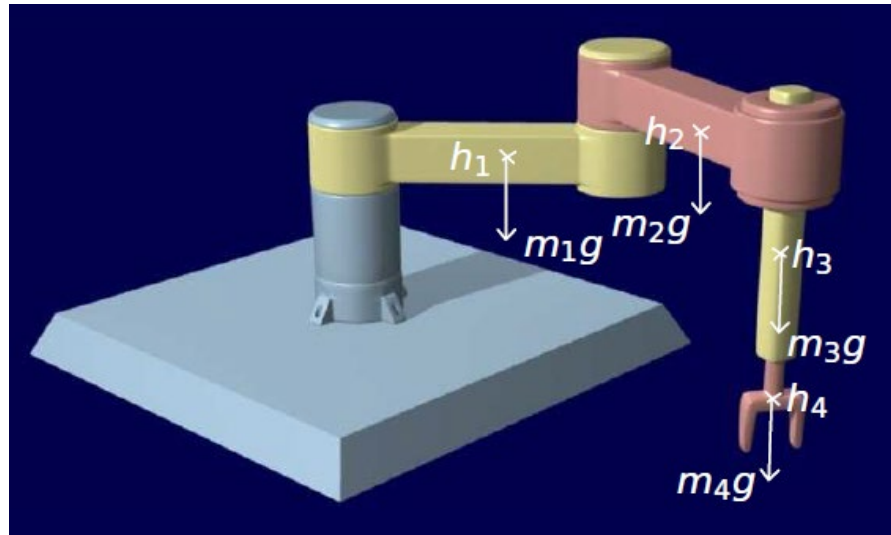
Newton-Euler Equation

- A Lagrangian approach to dynamics can be limited by the **local** parametrization of a given configuration
 - E.g. Euler angles representing orientation
- **Newton-Euler Equations** globally characterize the dynamics of a rigid body subject to external forces and torques (derivation in MLS 4.2)

$$\begin{bmatrix} mI & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \dot{v}_b \\ \dot{\omega}_b \end{bmatrix} + \begin{bmatrix} \omega_b \times m v_b \\ \omega_b \times I \omega_b \end{bmatrix} = F^b$$

Potential Energy of a Manipulator

- Consider the following manipulator



- The potential energy can be summed for each link using the center of mass of each link

$$V(\theta) = \sum_{i=1}^n m_i g h_i(\theta)$$

Kinetic Energy of a Manipulator

- Let's first look at the kinetic energy of a body

$$T = \frac{1}{2} (V^b)^T \mathcal{M} V^b$$

- This can be expressed in terms of joint velocities $\dot{\theta}$ using what we know about Jacobians

$$V^b = J^b(\theta) \dot{\theta}$$

$$T(\theta) = \frac{1}{2} \dot{\theta}^T J^b(\theta)^T \mathcal{M} J^b(\theta) \dot{\theta}$$

Kinetic Energy of a Manipulator

- The kinetic energy of all bodies summed is now

$$T = \frac{1}{2} \dot{\theta}^T M(\theta) \dot{\theta}$$

where is the ***manipulator inertia matrix*** defined as

$$M(\theta) = \sum_{i=1}^n J_i^b(\theta)^T \mathcal{M}_i J_i^b(\theta)$$

- $M(\theta) \in \mathbb{R}^{n \times n}$ is symmetric, positive definite

Equations of Motion for an Open-Chain Manipulator

- We can now put things together into the Lagrangian

$$L(\theta, \dot{\theta}) = \frac{1}{2} \dot{\theta}^T M(\theta) \dot{\theta} - V(\theta)$$

- When substituted into the Euler-Lagrange equation and simplified, we get the following form

$$M(\theta)\ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + N(\theta) = \tau$$

$$N(\theta) = \frac{\partial V}{\partial \theta} \quad C_{ij}(\theta, \dot{\theta}) = \sum_{k=1}^n \Gamma_{ijk} \dot{\theta}_k = \frac{1}{2} \sum_{k=1}^n \left(\frac{\partial M_{ij}}{\partial \theta_k} + \frac{\partial M_{ki}}{\partial \theta_j} - \frac{\partial M_{jk}}{\partial \theta_i} \right) \dot{\theta}_k$$

Equations of Motion for an Open-Chain Manipulator

$$M(\theta)\ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + N(\theta) = \tau$$

- Multiply by M^{-1} to find $\ddot{\theta}$ as a function of τ

$$\frac{d}{dt} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} \dot{\theta} \\ -M^{-1}C\dot{\theta} - M^{-1}N \end{bmatrix} + \begin{bmatrix} 0 \\ M^{-1} \end{bmatrix} \tau$$

- We now have a first order ODE in the form

$$\dot{x} = f(x) + g(x)u$$