電子類元件 零件承認書文件 CHECK LIST

零件廠商： 威健實業股份有限公司　　品名規格：POWERSTAGE SiC651ACD-T1-GE3 VI/SMD MLP55-31L 50A

技嘉料號：10IFD-500651-01R

項次	文件項目
Data Sheet 檢核項目	
1	DATASHEET (含機構尺寸、端子腳鍍層材質、**MSL Report**)
2	零件 Making 文字面說明
3	零件 Part Number 說明
4	零件 Qualification Test Report
5	料件包裝方式及包裝 Label 之零件 Part number 說明
6	UL Safety Report (If Request)
7	零件耐溫焊接 Profile(包含最高耐焊溫度,時間，焊接/過爐次數與曲線圖)。**註 2**
8	零件樣品 20PCS(Chipset 等高單價，至少 1PCS)
9	**電子零件承認基本調查表。註 3**
10	以上資料電子檔為 PDF 檔，且是同 1 個 File
GSCM 綠色產品管理系統-物料管制文件檢核清單	
物料管制文件 1	GSCM 綠色產品管理系統：零件照片
物料管制文件 2	GSCM 綠色產品管理系統：不使用禁用物質證明書 (保證書)。**註 4**
物料管制文件 3	GSCM 綠色產品管理系統：Data Sheet
GSCM 綠色產品管理系統-MCD 表格	
MCD 表格	物質內容宣告表格 (Material Content Declaration, MCD)
其他文件 (僅適用電阻、電容類之系列元件)	
附件 1	危害物質測試報告 Test Report of Hazardous Substances。**註 5**
附件 2	元件調查表 Component Composition Table

※ 1. 各項說明文件內容應明訂零件交貨時之規格、方式；如捲盤、文字印刷為雷射或油墨等

※ 2. 零件耐溫焊接 Profile 需附相關測試報告 (國際認證之實驗室資格單位所出具之測試報告)

2.1. 基本需符合 JEDEC 規範

2.2. Ambient Temp. (Reflow Temp endurace): >225℃, 70 sec. 零件塑膠材質需 PA9T(含)等級以上

2.3. PASTE IN HOLE 零件塑膠材質需 PA9T(含)等級以上

※ **3. 電子零件適用(技嘉)料號：積體電路(IC) 10H*,10T*,10I*,10D*,10G*,11T***

非 IC 類：10C*,11C*,10L*,11L*,10X*,11X*,10R*,11B*

※ 4. 物料管制文件 2：網通事業群之所屬料件須一併提交 “不使用禁用物質證明書(保證書)+ REACH 調查表”

※ 5. 危害物質測試報告 Test Report of Hazardous Substances：泛指為具有 ISO/IEC 17025 國際認證之實驗室資格單位所出具之測試報告

電子零件承認基本調查表

一、原物料規格/來源

項次	部位名稱/規格	材質	原物料來源產地
1	BOND WIRE	WIRE	SINGAPORE/PAND CRESCENT
2	COPPER CLIP	METAL	Korea/Gyeonggi-do
3	DIE	WAFER	Taiwan /Japan
4	DIE ATTACH	ADHESIVES	USA/IRVANE
5	EXTERNAL PLATING	MATAL MATERIALS PLATING LAYER	SINGPORE/MANDAI
6	LEADFRAME	METAL	Japan/FUJIMINO-SHI
7	LEADFRAME PLATING	MATAL MATERIALS PLATING LAYER	Japan/FUJIMINO-SHI
8	MOLD COMPOUND	EPOXY RESIN	Malaysia/Penang
9	Solder PASTE	ADHESIVES	USA/N.Y

二、晶圓廠(非 IC 類免填)

項次	工廠名稱	生產產地	Wafer (吋)	投產率(%)	自有/外包
1	vanguard	Taiwan	8”	>80%	外包
1	tower	Japan	8”	>80%	外包

三、封裝廠(IC 類)；成品之生產製造工廠(非 IC 類)

項次	工廠名稱	生產產地	投產比率(%)	自有/外包
1	AMKOR	菲律賓	>80	Own
2	Vishay Siliconix TW	TW	>80%	Own

四、產能

總產能(月/PCS)	可供技嘉產能(月/PCS)
200Mpcs/M	5Mpcs/M

※ 1. IC 類之晶圓廠、封裝廠之所有 AVL 請均表列，並提供相關資訊與文件。當異動 (包含 AVL 或相關資訊文件之異動)時，請主動通知技嘉 Sourcer 與 RD 承認單位，並更新文件

※ 2. 非 IC 類零件之成品生產製造工廠之所有 AVL 請均表列，並提供相關資訊與文件。當異動 (包含 AVL 或相關資訊文件之異動)時，請主動通知技嘉 Sourcer 與 RD 承認單位，並更新文件

※ 3. 以上資訊欄位若有不足，可自行增加行數

50 A VRPower® Integrated Power Stage

DESCRIPTION

The SiC651 is a high frequency integrated power stage optimized for synchronous buck applications to offer high current, high efficiency, and high power density performance with very low shutdown current. Packaged in Vishay's proprietary 5 mm x 5 mm MLP package, SiC651 enables voltage regulator designs to deliver up to 50 A continuous current per phase.

The internal power MOSFETs utilize Vishay's latest TrenchFET® technology that delivers industry benchmark performance to significantly reduce switching and conduction losses.

The SiC651 incorporates an advanced MOSFET gate driver IC that features high current driving capability, adaptive dead-time control, an integrated bootstrap switch, and user selectable zero current detection to improve light load efficiency. The driver is also compatible with a wide range of PWM controllers, supports tri-state PWM, and 5 V / 3.3 V PWM logic.

The device also supports PS4 mode to reduce power consumption when the system is in standby state.

The SiC651 offers operating temperature monitoring, protection features, and warning flags that improve system monitoring and reliability.

FEATURES

RoHS COMPLIANT
HALOGEN FREE

- Highly efficient
  - Thermally enhanced PowerPAK® MLP55-31L package
  - Vishay's latest TrenchFET technology and low side MOSFET with integrated Schottky diode
  - Integrated, low impedance, bootstrap switch
  - Power MOSFETs optimized for 19 V input stage
  - Supports PS4 mode light load requirement with low shutdown supply current (5 V, 3 µA)
  - Zero current detection for improved light load efficiency
- Highly versatile
  - 5 V and 3.3 V PWM logic with tri-state and hold-off timer
  - 5 V DSBL#, ZCD_EN# logic with PS4 state support
  - High frequency operation up to 2 MHz
- Robust and reliable
  - Delivers in excess of 50 A continuous current, 70 A, peak (10 ms) and 100 A, peak (10 µs)
  - Over current protection
  - Over temperature flag
  - Over temperature protection
  - Under-voltage lockout protection
  - High side MOSFET short detection
- Effective monitoring and reporting
  - Accurate temperature reporting
  - Warnings and faults reporting flag
- Material categorization: for definitions of compliance please see www.vishay.com/doc?99912

APPLICATIONS

- Multi-phase VRDs for computing, graphics card and memory
- Intel core processor power delivery
  - V_{CORE}, $V_{GRAPHICS}$, $V_{SYSTEM\ AGENT}$
  - V_{CCGI}
- Up to 24 V rail input DC/DC VR modules

TYPICAL APPLICATION DIAGRAM

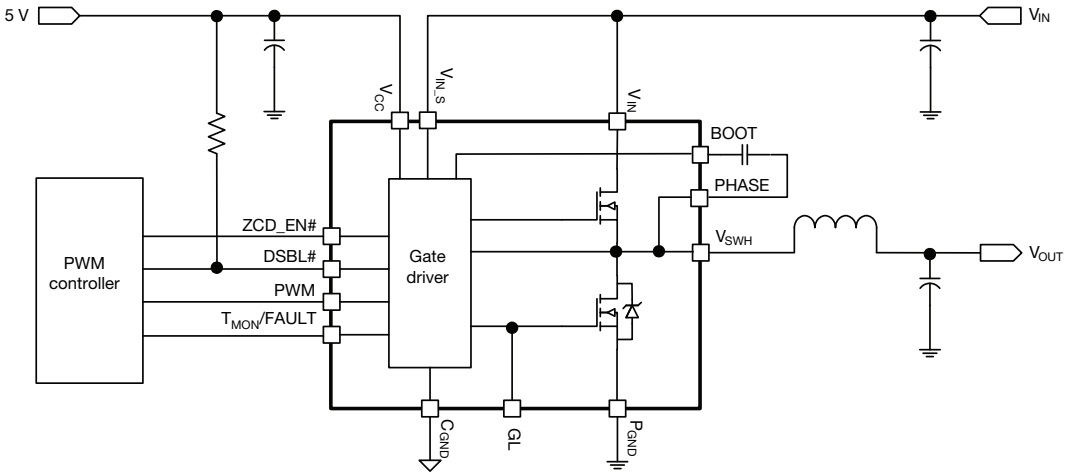
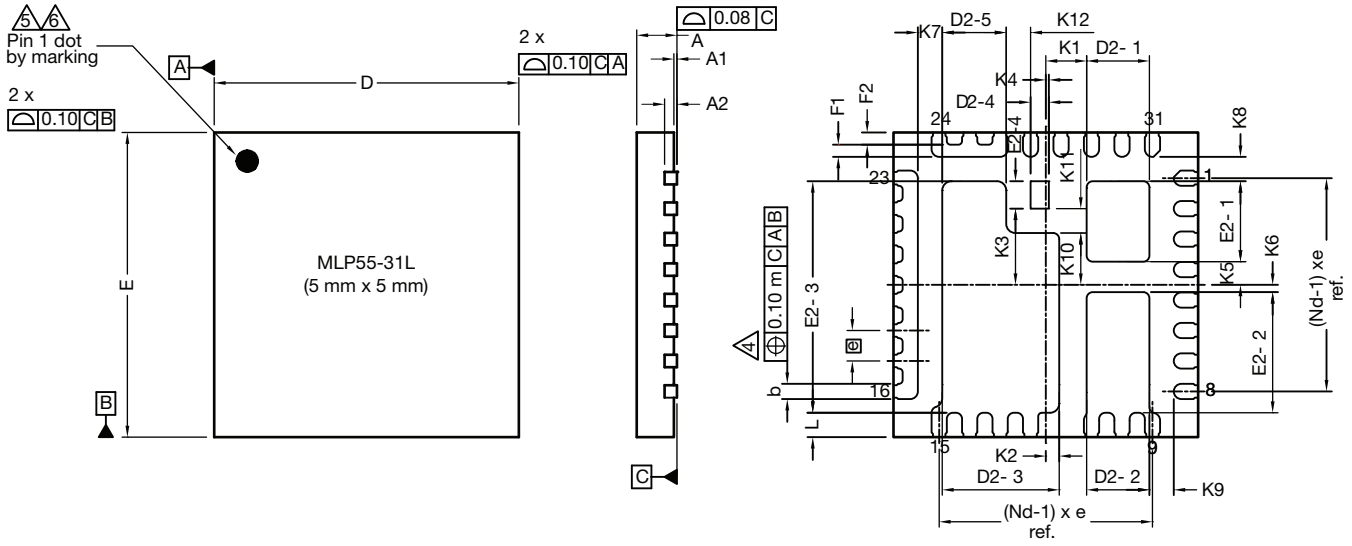


Fig. 1 - Typical Application Diagram

“For more details, please contact VRPower@vishay.com”

PowerPAK® MLP55-31L Case Outline



Top view Side view Bottom view

DIM.	MILLIMETERS			INCHES		
	MIN.	NOM.	MAX.	MIN.	NOM.	MAX.
A (8)	0.70	0.75	0.80	0.027	0.029	0.031
A1	0.00	-	0.05	0.000	-	0.002
A2		0.20 ref.			0.008 ref.	
b (4)	0.20	0.25	0.30	0.008	0.010	0.012
D	4.90	5.00	5.10	0.193	0.196	0.200
e		0.50 BSC			0.019 BSC	
E	4.90	5.00	5.10	0.193	0.196	0.200
L	0.35	0.40	0.45	0.013	0.015	0.017
N (3)		32			32	
Nd (3)		8			8	
Ne (3)		8			8	
D2-1	0.98	1.03	1.08	0.039	0.041	0.043
D2-2	0.98	1.03	1.08	0.039	0.041	0.043
D2-3	1.87	1.92	1.97	0.074	0.076	0.078
D2-4		0.30 BSC			0.012 BSC	
D2-5	1.00	1.05	1.10	0.039	0.041	0.043
E2-1	1.27	1.32	1.37	0.050	0.052	0.054
E2-2	1.93	1.98	2.03	0.076	0.078	0.080
E2-3	3.75	3.80	3.82	0.148	0.150	0.152
E2-4		0.45 BSC			0.018 BSC	
F1		0.20 BSC			0.008 BSC	
F2		0.20 BSC			0.008 BSC	
K1		0.67 BSC			0.026 BSC	
K2		0.22 BSC			0.008 BSC	
K3		1.25 BSC			0.049 BSC	
K4		0.05 BSC			0.002 BSC	
K5		0.38 BSC			0.015 BSC	
K6		0.12 BSC			0.005 BSC	

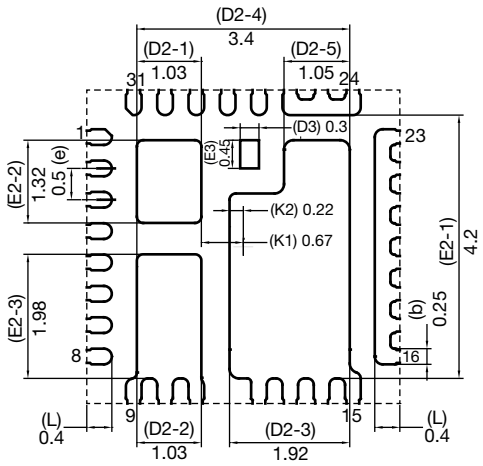
DIM.	MILLIMETERS			INCHES		
	MIN.	NOM.	MAX.	MIN.	NOM.	MAX.
K7		0.40 BSC			0.016 BSC	
K8		0.40 BSC			0.016 BSC	
K9		0.40 BSC			0.016 BSC	
K10		0.85 BSC			0.033 BSC	
K11		0.40 BSC			0.016 BSC	
K12		0.40 BSC			0.016 BSC	
ECN: T16-0644-Rev. E, 24-Oct-16 DWG: 6025						

Notes

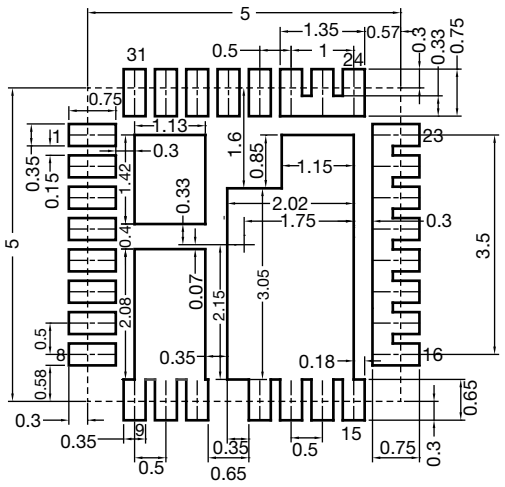
1. Use millimeters as the primary measurement
2. Dimensioning and tolerances conform to ASME Y14.5M. - 1994
3. N is the number of terminals,
   Nd is the number of terminals in X-direction, and
   Ne is the number of terminals in Y-direction
4. Dimension b applies to plated terminal and is measured between 0.20 mm and 0.25 mm from terminal tip
5. The pin #1 identifier must be existed on the top surface of the package by using indentation mark or other feature of package body
6. Exact shape and size of this feature is optional
7. Package warpage max. 0.08 mm
8. Applied only for terminals

Recommended Land Pattern
PowerPAK® MLP55-31L for SiC620, SiC620A

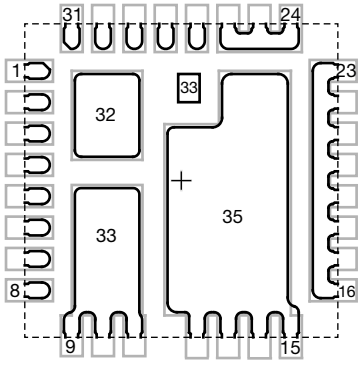
Top side transparent view
(not bottom view)



Land pattern for MLP55-31L



All dimensions in millimeters



Component for MLP55-31L

Land pattern for MLP55-31L

VRPower® Integrated Power Stage Solution

By Ron Vinsant

VRPower® products are integrated power stage solutions optimized for high-performance synchronous buck applications. These devices offer high power conversion efficiency and high power density with low electrical parasitics due to both excellent silicon (MOSFETs and drivers) and packaging design techniques. The devices are available in Vishay's proprietary 4.5 mm by 3.5 mm package for 30 A applications, and the industry-standard 5 mm by 5 mm thermally enhanced MLP package for 60 A applications.

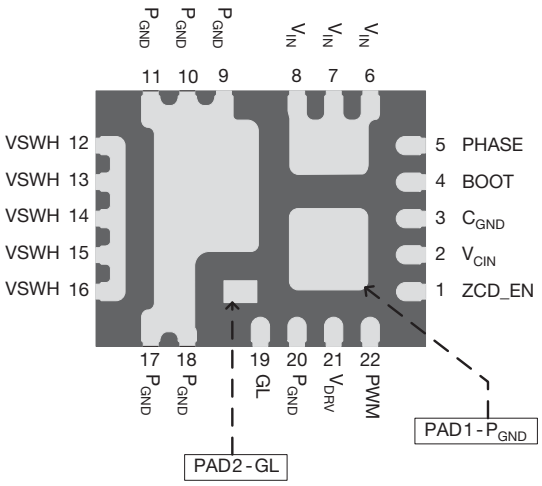


Fig. 1 - 3.5 mm by 4.5 mm package

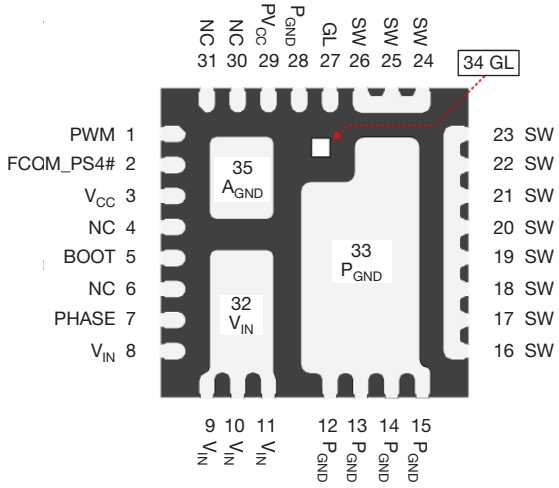


Fig. 2 - 5 mm by 5 mm package

VRPower devices are primarily intended for use in applications with 12 V inputs and < 2 V outputs. The power devices - MOSFETs - are asymmetrical to match the expected duty ratios in the intended operating range. The internal drivers are then matched to the MOSFETs to maximize efficiency.

This application document is meant to be used as a guide to the performance possibilities of some of the most popular Vishay VRPower products. We will cover efficiency and power loss over the operating frequency range of 400 kHz to 1 MHz. The 3.5 mm by 4.5 mm, 30 A device (SiC530) will be covered first, followed by the 5 mm by 5 mm, 60 A device (SiC620). Future application documents will cover EMC, boot resistor, capacitor, and thermal issues, and how they are affected by layout.

The "rated current" of a VRPower device is not an indicator of its performance under steady-state conditions. While it can be misleading, it is intended to be a guide for those applications where there are transient operating conditions requiring high peak currents, such as processors.

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

SiC530: 3.5 mm by 4.5 mm, 30 A

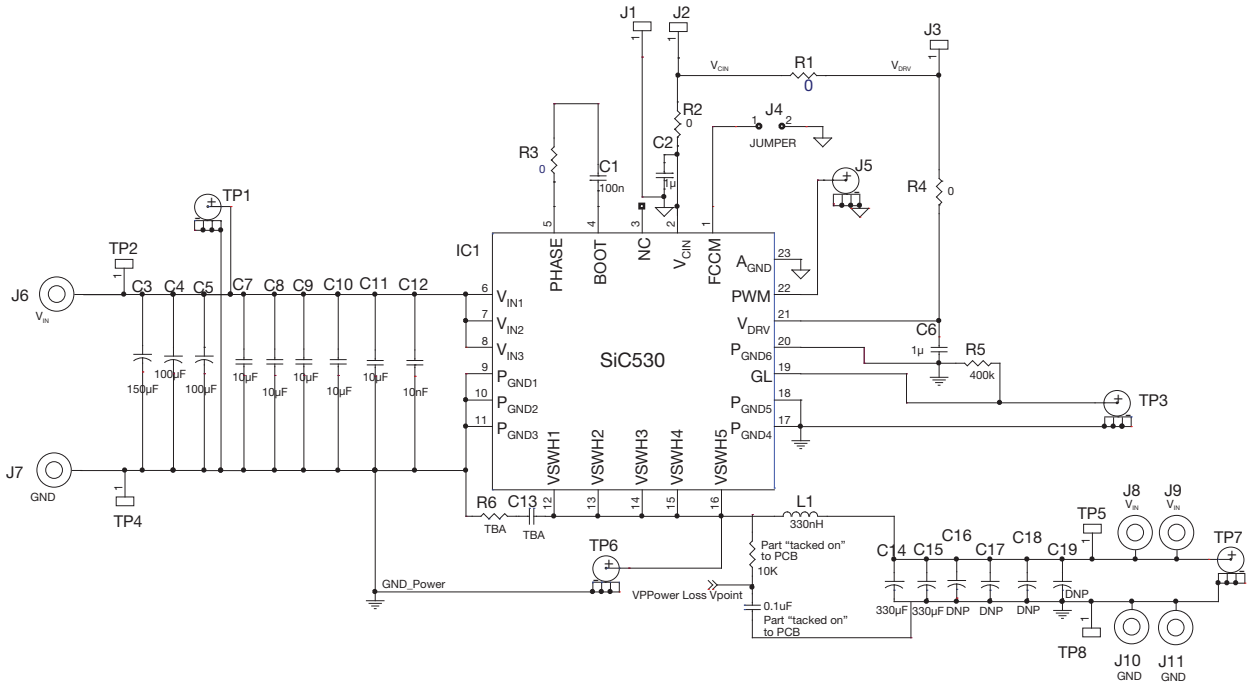


Fig. 3 - SiC530: 3.5 mm by 4.5 mm test board schematic

EFFICIENCY, POWER LOSS, AND OPERATING FREQUENCY

The SiC530 is normally used over a frequency operating range of 500 kHz to 1 MHz. The graph below shows efficiency and bias power requirements over that operating range.

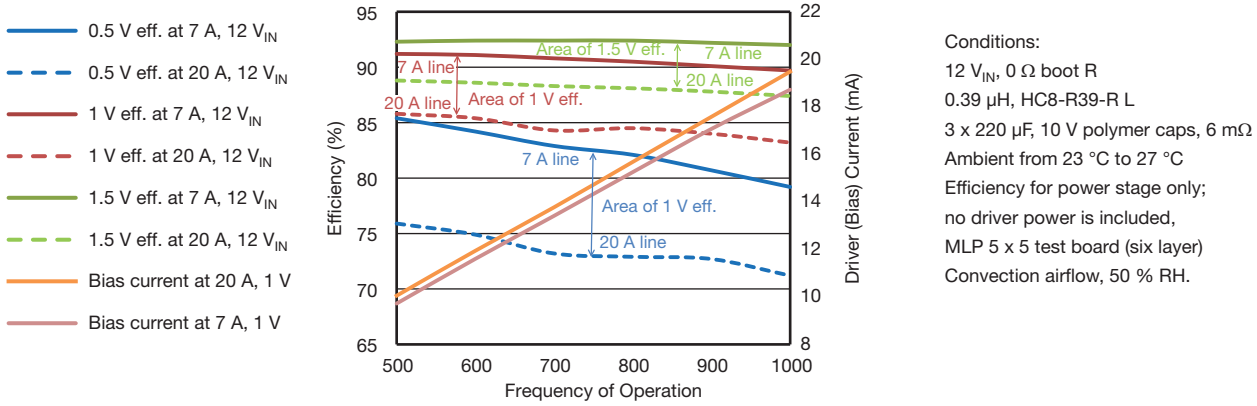


Fig. 4 - Area of efficiency from peak efficiency point (7 A) to max. current (20 A) for three different operating points: 0.5 V, 1 V, and 1.5 V outputs with 5 V MOSFET drive bias currents

Although the SiC530 is rated at 25 A, our testing was limited to 20 A for Fig. 4 due to our PCB construction being only six layers. Since the PCB supplies much of the heatsinking for the SiC530, its thermal properties are critical.

We are often asked about the expected performance of a SiC530. It is a difficult question to answer in general, and even more difficult to answer with any precision. It is instructive, however, to look at some typical examples that are in common use. One such example is shown below in Fig. 5.

VRPower® Integrated Power Stage Solution

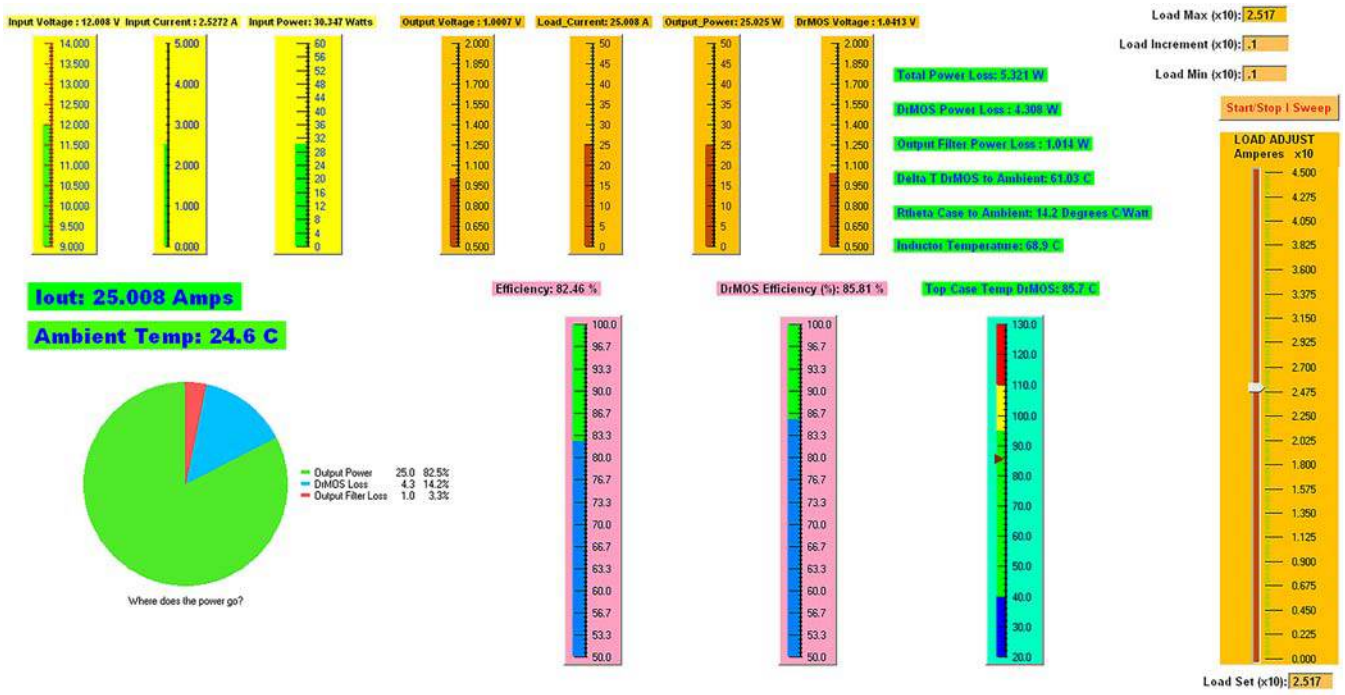
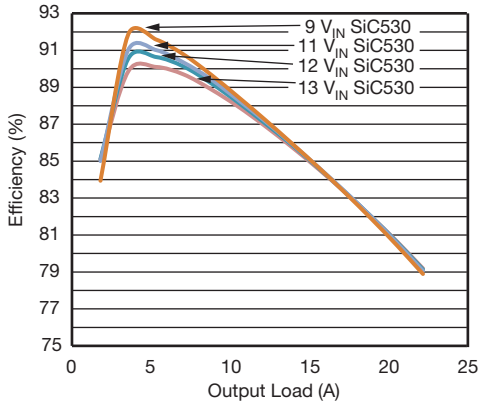


Fig. 5 - "Dashboard" example of the typical performance of a SiC530 with a 1 V output at 500 kHz

In Fig. 5 we can observe some of the expected operating temperatures of key components and their corresponding power losses when using a SiC530 in a 12 V_{IN}, 1 V_{OUT}, 500 kHz application at 25 A.

The term "filter loss" refers to the combination of the filter cap losses and inductor losses. These losses are typically dominated by the inductor.

In Fig. 6 below we can see efficiency at higher frequency operation.



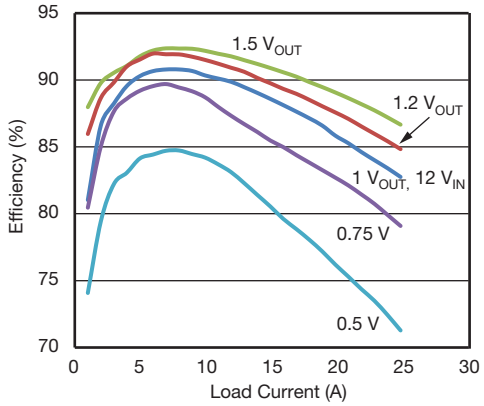
Conditions:
Ambient: 23 °C to 28 °C
0.9 V_{OUT}, 800 kHz
0.22 µH, 3.9 mΩ DCR
(custom)
100 µF x 5R, 1206 caps (13 µA)
220 µF POSCAPS (4)
Single-phase, 0 Ω boot R
SiC530 temp (on top) 65.3 °C at 20 A with 13 V_{IN}
SiC530 efficiency only; does not
include all bias power for board
and controller

Fig. 6 - SiC530 800 kHz, 0.9 V_{OUT} single-phase efficiency vs. load for different V_{IN}

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

In Fig. 7 below we show operation at 500 kHz.



Conditions: 12 V_{IN}, 0 Ω boot R
Inductor: Coiltronics, HC-R39-R, 0.39 µH,
1.55 mΩ DCR
3 x 220 µF, 10 V, polymer cap, 6 mΩ ESR
Ambient: 23 °C to 27 °C
Efficiency for power stage only; no driver power
Convection airflow, 50 % RH
Six-layer PCB

Fig. 7 - Efficiency of SiC530 at 500 kHz for 12 V_{IN} with 0.5 V to 1.5 V output voltage vs. load current

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

SiC620: 5 mm by 5 mm, 60 A

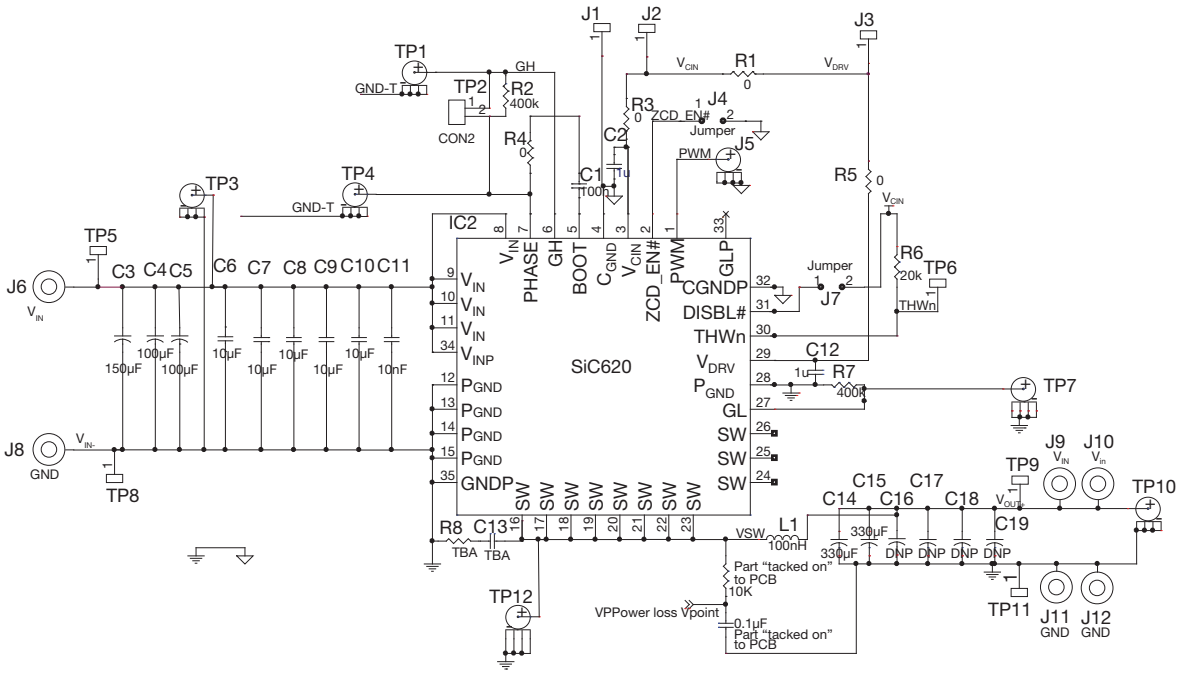
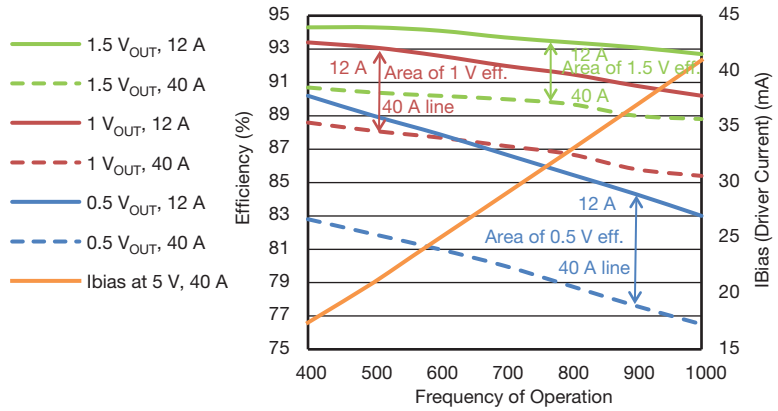


Fig. 8 - SiC620: 5 mm by 5 mm test board schematic

EFFICIENCY, POWER LOSS, AND OPERATING FREQUENCY

The SiC620 is normally used over a frequency operating range of 400 kHz to 1 MHz. The graph below shows efficiency and bias power requirements over that operating range.



Conditions: 12 V_{IN}, 0 Ω boot R
Inductor: Coiltronics, HC8-R39-R, 0.39 µH, 1.55 mΩ DCR
3 x 220 µF, 10 V, polymer cap, 6 mΩ ESR
Ambient: 23 °C to 27 °C
Efficiency for power stage only; no driver power
Convection airflow, 50 % RH
Six-layer PCB

Fig. 9 - Area of efficiency from peak efficiency point (12 A) to max. current (40 A) for three different operating points: 0.5 V, 1 V, and 1.5 V outputs with 5 V MOSFET drive bias currents

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

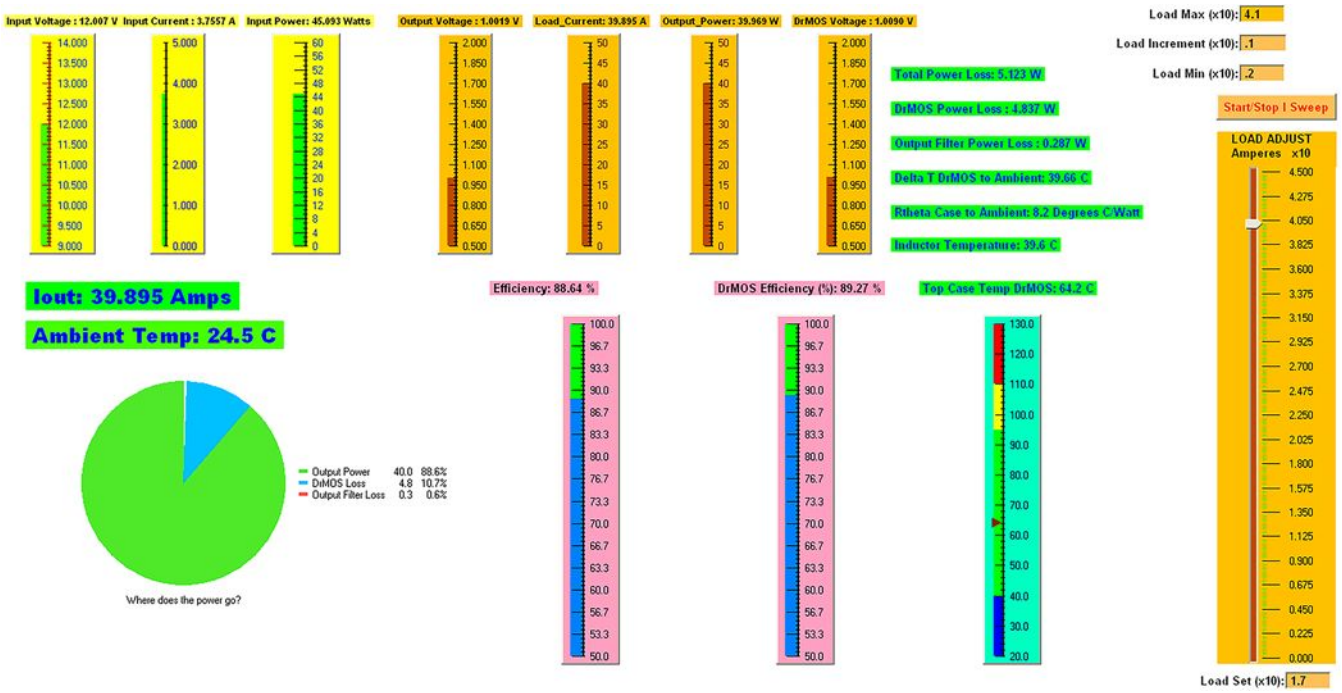
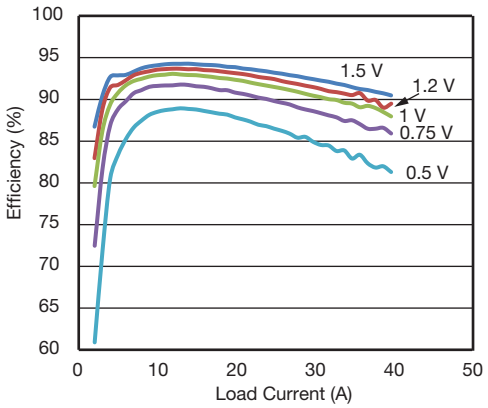


Fig. 10 - "Dashboard" example of the typical performance of the SiC620 with a 40 A, 1 V output at 412 kHz

In Fig. 10 we can observe some of the expected operating temperatures of key components and their corresponding power losses when using an SiC620 in a 12 V_{IN}, 1 V_{OUT}, 412 kHz application at 40 A. Unlike the SiC530 tests, the SiC620 tests were run with some airflow, as this would be the normal environment in higher-power applications.

The term "filter loss" is the combination of the filter cap losses and inductor losses. These losses are typically dominated by the inductor; output filter capacitors are a very small loss term in most applications.

In Fig. 11 below we show operation at 500 kHz.



Conditions:
12 V_{IN}, 0 Ω boot R, 500 kHz
0.25 µH, 744309025 Wurth
3 x 220 µF, 10 V, polymer caps, 6 mΩ
Ambient: 23 °C to 27 °C
Efficiency for power stage only;
no driver power is included
MLP 5 x 5 test board (six-layer)
Convection airflow, 50 % RH

Fig. 11 - Efficiency of SiC620 at 500 kHz for 12 V_{IN} with 0.5 V to 1.5 V output voltage vs. load current

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

ISSUES RELATED TO ALL VRPower PRODUCTS

Inductor Power Loss

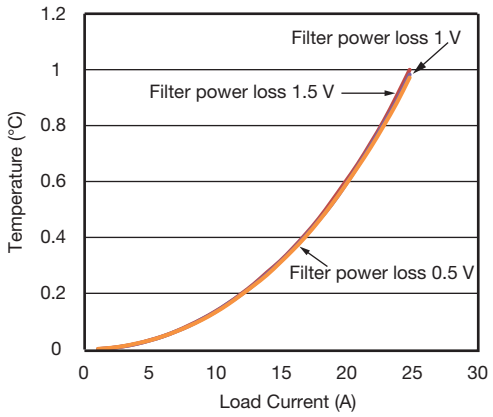


Fig. 12 - Output filter power loss for three different operating points (0.5 V, 1 V, and 1.5 V) for an SiC530

This shows that in general, the power loss in the filter (L1 and C14 through C19, referring to Fig. 3) is dominated by the DC loss term and not AC (magnetic core) losses. This would leave one to believe that the temperature of the inductor would only change due to load and not V_{OUT}.

This is not true, however. The inductor temperature does change with V_{OUT}, as we can see below.

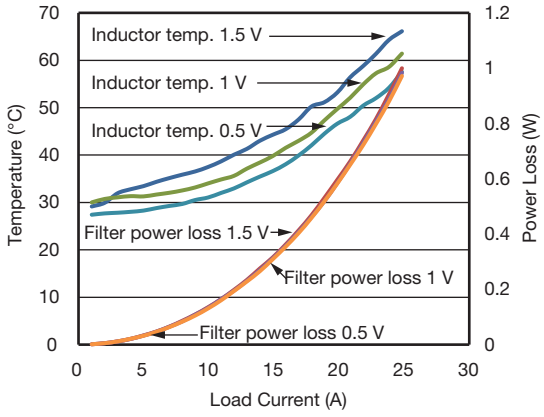


Fig. 13 - Output filter power loss and temperature for three different operating points - 0.5 V, 1 V, and 1.5 V

If a good electrical layout is achieved, the inductor is always placed as close as possible to the V_{SW} pins of the SiC530 to minimize inductance in the path, which causes ringing that places added stress on the device.

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

Here is an example PCB layout showing how close the two components should be.

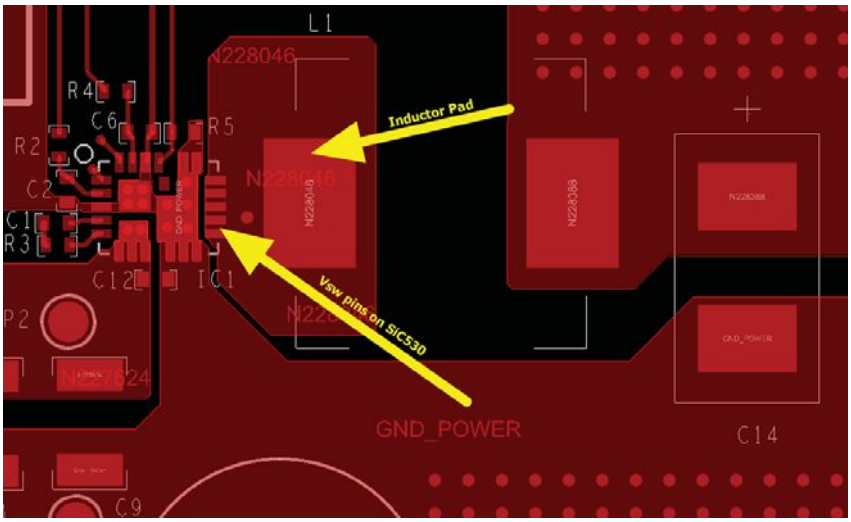


Fig. 14 - SiC530 evaluation board layout showing the close proximity of an inductor to the SiC530

Being close to the switching device allows the inductor to absorb heat from the SiC530; in other words it is a heatsink, and thus is very important to the thermal design of the regulator. If the inductor is placed in airflow it will help keep temperatures down. Keeping other PCB-mounted components out of the airflow path passing the inductor is always helpful.

Below, we can observe that losses, and therefore temperature rise, in the SiC530 are not linearly proportional to V_{OUT} for any specific load point.

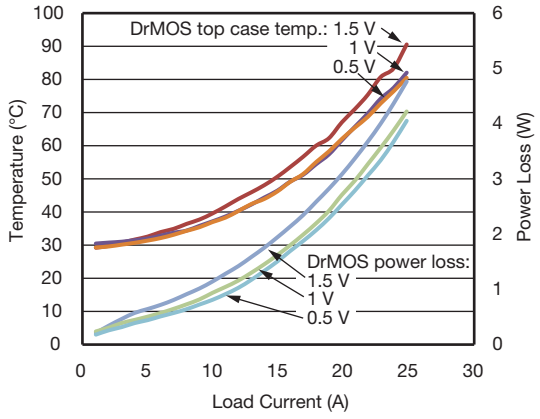


Fig. 15 - SiC530 power loss and top case temperature

This non-linearity shows that while a 1.5 V, 25 A output might not meet required design goals due to temperature rise, at 1 V such a design might be acceptable due to the lower operating temperature of the SiC530.

Please note we are using the same inductor for all outputs for this test. In a typical system design the inductor value would change depending on load specifications such as ripple and transient response. Since the peak value of current in the inductor is one of the parameters that determines switching loss in the high-side MOSFET, results might be different for lower voltages with smaller-value inductors.

VRPower® Integrated Power Stage Solution

Inductor Core Loss

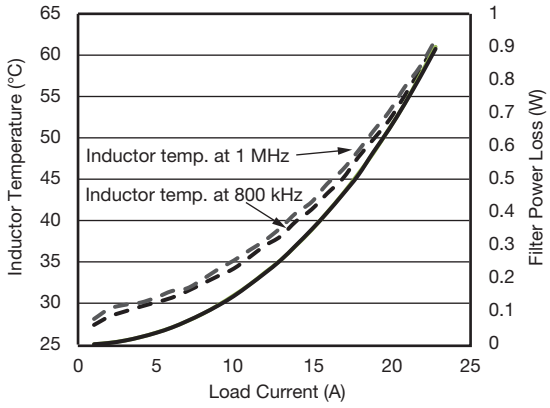
It is often stated that increasing the switching frequency is not prudent as it will increase magnetic losses. If the value of the inductor does not change and the frequency increases, core losses actually go down, not up, as the delta B (flux swing) in the inductor is less.

A typical model for core loss is shown below:

$PL = 492 \times B^{2.22} f^{1.32}$ for Magnetics Inc. high-flux 60 µ core material,

where PL is power loss, B is one half the peak-to-peak flux swing, and f is frequency. Note that the exponent for B is much greater than for f.

Below is an example (note there is little to no change in power loss in the inductor).



Circuit and conditions:
13 V_{IN}, 0.9 V_{OUT}, 0 Ω boot R
800 kHz and 1 MHz
0.22 µH, 8 mm x 8 mm
3 x 220 µF, 10 V, polymer cap,
6 mΩ ESR
Ambient: 23 °C to 27 °C
Power stage only; no driver power
CCM driver power is
SiC530 800K
15.3 mA at 5 V = 76.5 mW
SiC530 1 MHz
18.9 mA at 5 V = 94.5 mW

Fig. 16 - Inductor loss and temperature at two operating frequencies with the same inductor in an SiC530

The additional change in temperature of the inductor is, as we have shown above, due to the increased switching losses in the SiC530, and not inductor loss.

VRPower® Integrated Power Stage Solution

Inductor Saturation

In some VRPower applications, space is critical and the largest component is most often the inductor. Due to its large size, it is the first component to be addressed in solving any space issues.

As the size of the inductor decreases, its ability to store energy decreases. This is dependent on a number of factors, such as magnetic material and operating temperature. If the saturation level of the inductor is exceeded, the currents in the VRPower MOSFETs will increase and cause additional power loss in the VRPower device.

Observing the current in the inductor with a current probe is a useful way of determining if the inductor is heading into saturation.

Below is an example of the normal operation of two inductors of the same type.

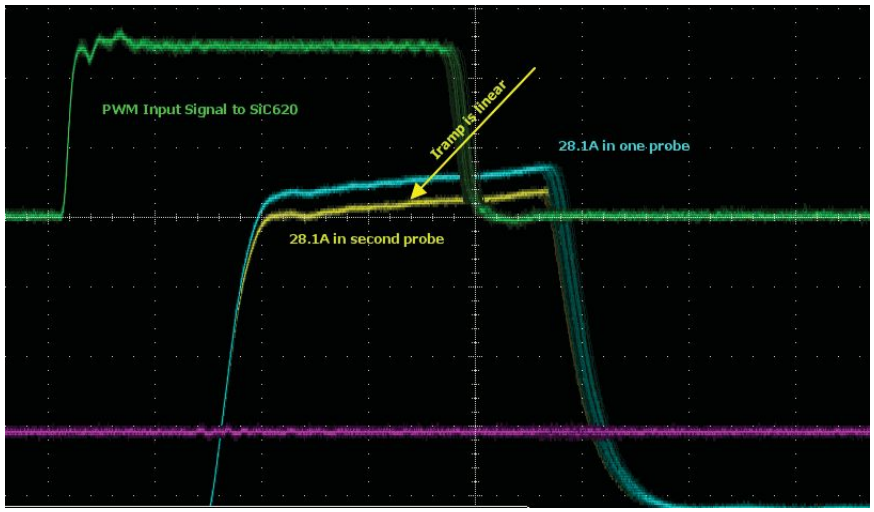


Fig. 17 - Normal inductor operation; linear current ramp

With only a small increment in current from 28.1 A to 30.27 A, we can see the current ramp becoming non-linear.

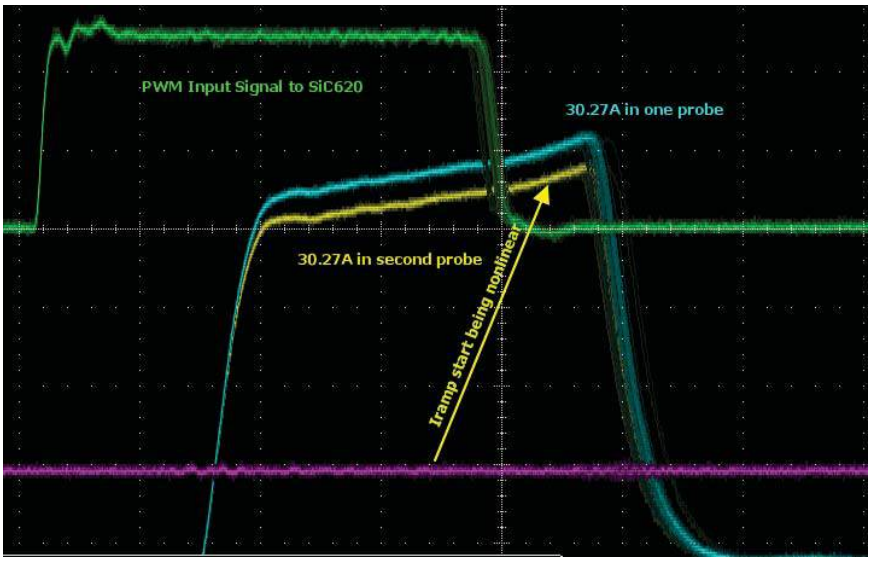


Fig. 18 - Border-line inductor operation; current ramp becoming non-linear

VRPower® Integrated Power Stage Solution

With yet another small increment from 30.27 A to 32.2 A, we see a very large increase in peak current.

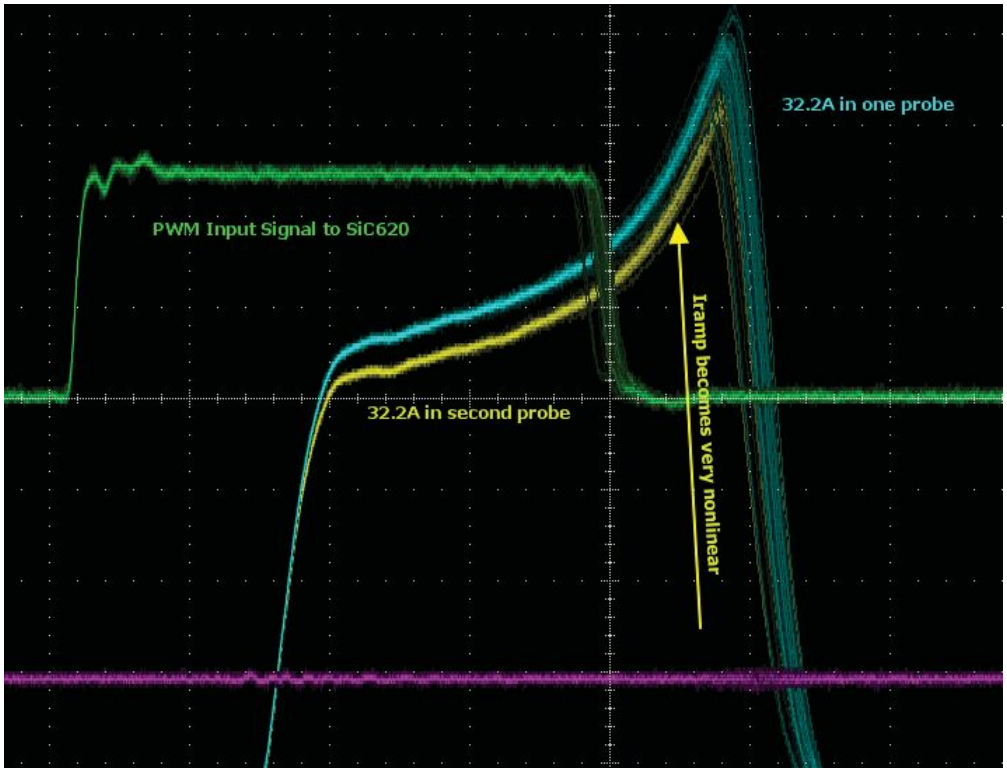


Fig. 19 - Saturated inductor operation; current ramp very non-linear

The peak current increases both conduction losses and switching losses in the high-side MOSFETs of the VRPower device. Operation in this region should be avoided due to increased stresses on the MOSFETs.

If the control system utilizes DCR current sensing, there is also the issue of inaccuracy of the current sense value due to the non-linearity of the value of L.

Another question that frequently arises is the effect of varying L on efficiency and power loss. There are many variables involved, such as PCB layout, physical and electrical size of the inductor, input voltage, boot resistor value, etc.

In Fig. 20 below, we show an example of what might be expected in a typical application for the SiC620. We use three different inductors. One is a 220 nH device with a “standard” height of 6 mm from Vishay; the second is a competitor’s 6 mm inductor, also of 220 nH; and an 8 mm, 300 nH inductor from Vishay. For any specific operating point, a large value of L results in a lower peak current decreasing the switching loss in the upper MOSFET and increasing efficiency. In addition, a larger physical size of L will result in additional heatsinking, further increasing efficiency and lowering operating temperatures. However, this increase in L will lower the ability of the control loop to respond to transient events.

VRPower® Integrated Power Stage Solution

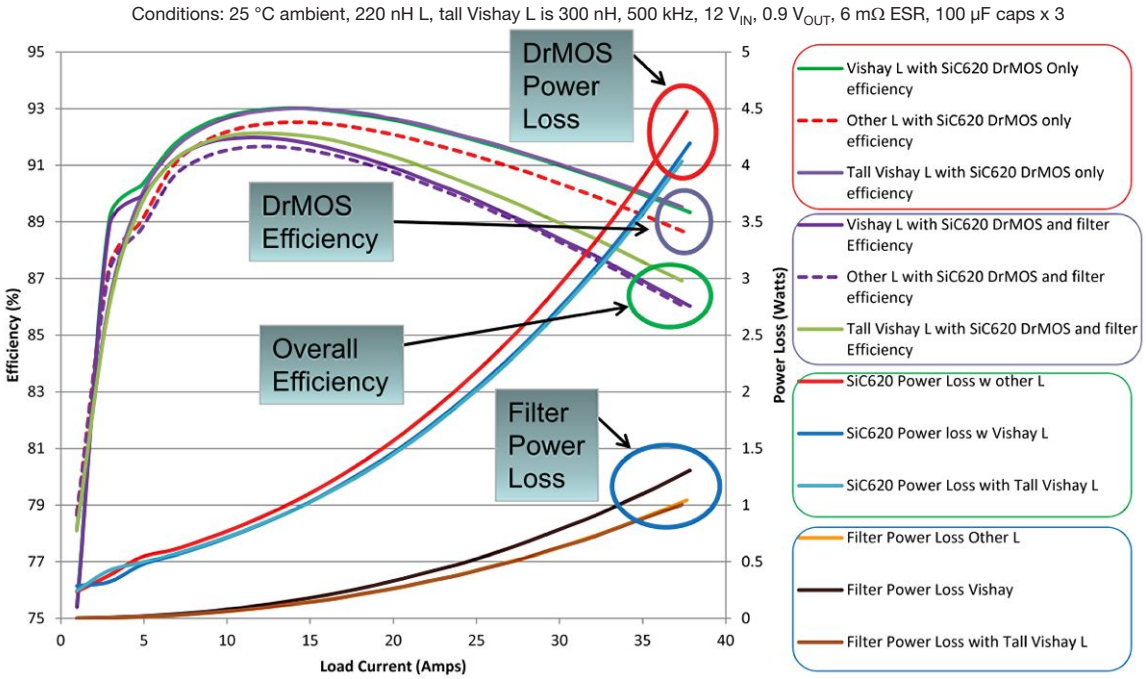
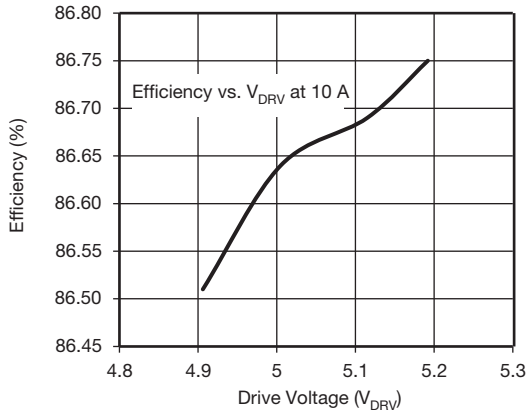


Fig. 20 - Efficiency and power losses vs. load current for the SiC620 with different inductors

A design tool for inductor selection can be found here: www.vishay.com/inductors/calculator/calculator/

V_{DRV} Supply Voltage (MOSFET Gate Voltage)

VRPower devices use a 5 V drive for MOSFET enhancement. Varying this voltage over a small range will not substantially affect the efficiency of the devices. Fig. 21 below shows the effects on efficiency with changes in drive voltage.



Circuit and conditions:
13 V_{IN}, 0.9 V_{OUT}, 1.006 MHz
0.22 µH, 1 mΩ DCR L
3 x 220 µF, 10 V, polymer cap,
6 mΩ ESR
Ambient: 26 °C
Power stage only; no driver power
CCM driver power is
27.6 mA at 5 V = 138 mW
MLP 5 x 5 Test Board

Fig. 21 - Effect on efficiency due to drive voltage on SiC631 (3.5 mm x 4.5 mm)

Although these devices have a UVLO, it is prudent to design the system so that when in operation the VRPower device has a minimum value of 4.5 V for V_{DRV}.

APPLICATION NOTE

VRPower® Integrated Power Stage Solution

V_{CIN} Supply Voltage (Driver V_{CC} Voltage)

It is important that the supply voltage rail for the driver and the controller generating the PWM signal be the same. This requirement is due to the tri-state inputs on the PWM signal to the VRPower device.

Below is a simplified schematic of a VRPower device being driven by a system regulator.

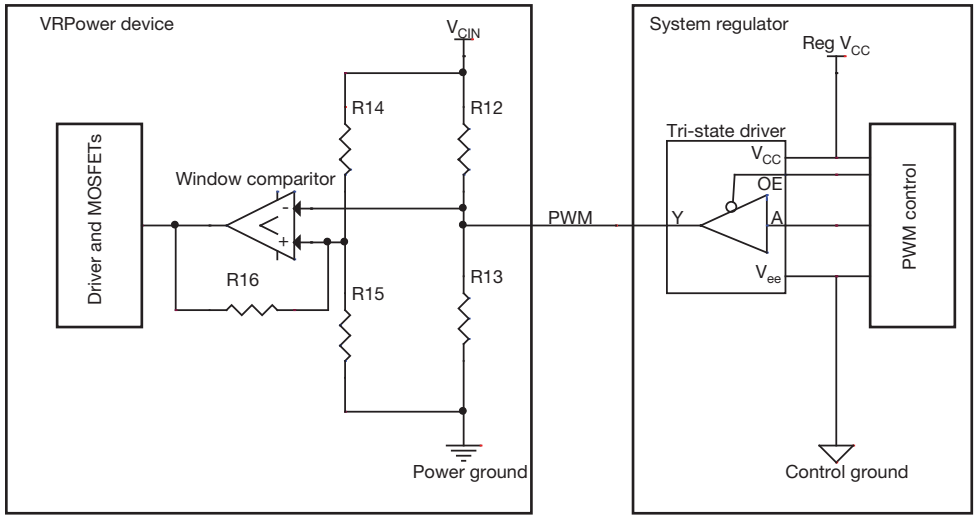


Fig. 22 - Simplified schematic of a VRPower device driven by a system regulator with separate grounds and supply rails

As V_{CIN} changes in magnitude, the threshold of the window comparator sensing the signal from the system regulator tri-state driver will change. If the system regulator's supply rail, Reg V_{CC}, is active before the VRPower device's V_{CIN}, then there can be a region of operation as V_{CIN} rises where the device can have false triggering of the drivers and MOSFETs, leading to erratic behavior and possible device failure.

To a lesser extent this is also true of the ground paths. In order to reduce noise on the PWM signal, it is best not to have the grounds tied as shown in Fig. 22 above, but to tie both power rails and grounds of the system regulator and VRPower device together, as shown below.

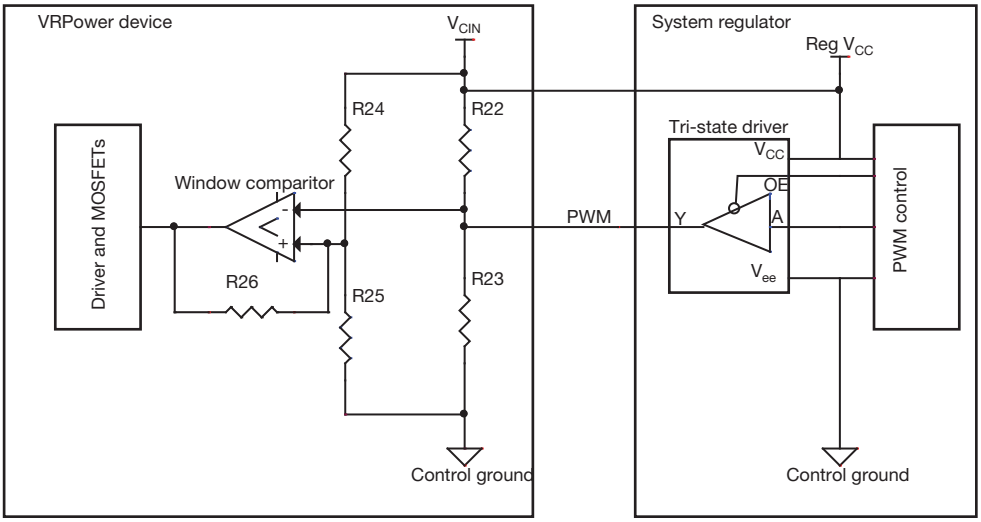


Fig. 23 - Simplified schematic of a VRPower device driven by a system regulator with properly tied grounds and supply rails

VRPower® Integrated Power Stage Solution

Minimum on Time

At higher frequencies like 1 MHz and large input-voltage-to-output-voltage ratios, the parameter of minimum on time, $t_{PWM\_ON\_MIN}$, may be of concern. Since the ratio of V_{IN} to V_{OUT} when in continuous conduction mode is set by the ratio of the high-side MOSFET on time to the off time,

Time on = V_{OUT}/V_{IN} x 1 period; e.g. 0.5 V/12 = 0.0417 or a 4.17 % on time in 1 µs. This equates to 41.7 ns, which is less than the specified minimum PWM input of 50 ns.

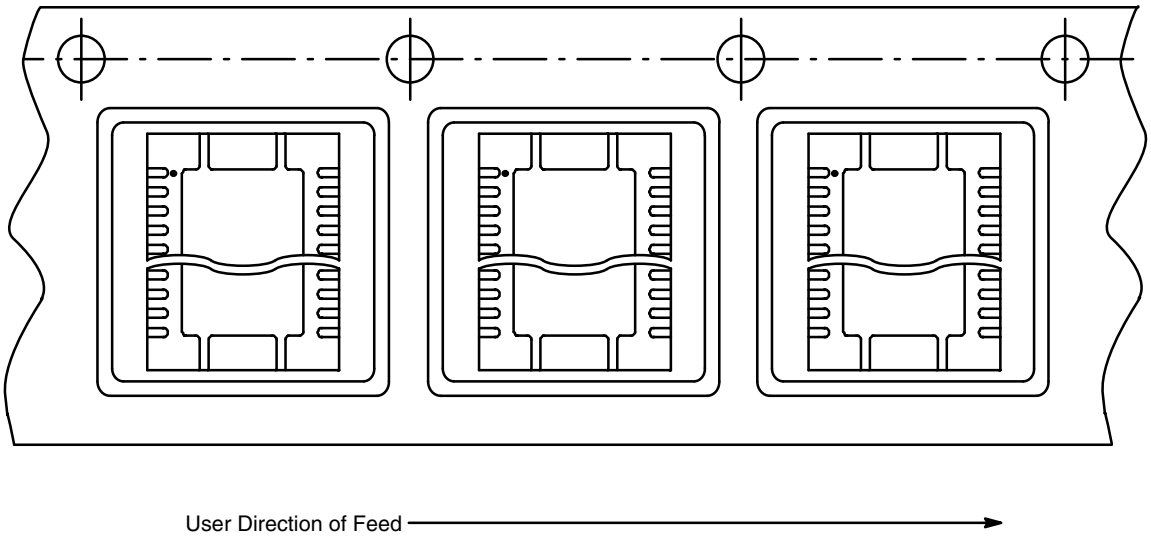
Also consider this parameter on transient response. At load release, the PWM should be at as narrow a width as possible, or perhaps not be generated at all. When simulations are being run, this non-linearity must be considered.

CONCLUSIONS

1. Use the peak current rating as a “pulse” rating; not as a steady-state operating current specification.
2. The inductor is an important contributor to thermal, as well as electrical, design.
3. Do place the inductor close to the VRPower device in the PCB layout.
4. V_{OUT} has a large effect on operating temperature. Higher currents might be possible for applications where the operating temperature is the same, but since output voltage is lower, power loss is less, and therefore output current can be higher.
5. When selecting an inductor, be sure to assess the saturation parameters to minimize thermal and electrical stress on the VRPower device.
6. MOSFET drive voltage has little effect on overall efficiency, but should not drop below 4.5 V.
7. The control system and the VRPower device should be supplied from the same V_{CC} rail.
8. The control system ground should be tied to the analog ground of the VRPower device, not the power ground.
9. Take into account the minimum PWM input pulse when considering operating frequency in your design.

Device Orientation for PowerPAK® MLP65, PowerPAK® MLP55, PowerPAK® MLP55 Double Cooling

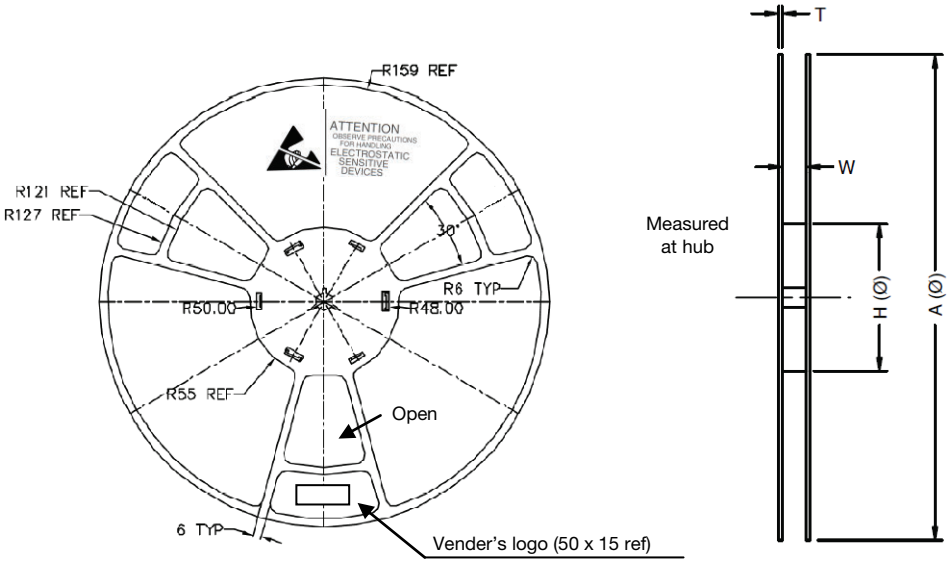
DEVICE ORIENTATION	
PACKAGE	**METHOD**
MLP65-20L	T1
MLP55	T1
MLP55 double cooling	T1



Revision control of this drawing is maintained through Document Control, Pack Specification-PACK-0007-19

Reel

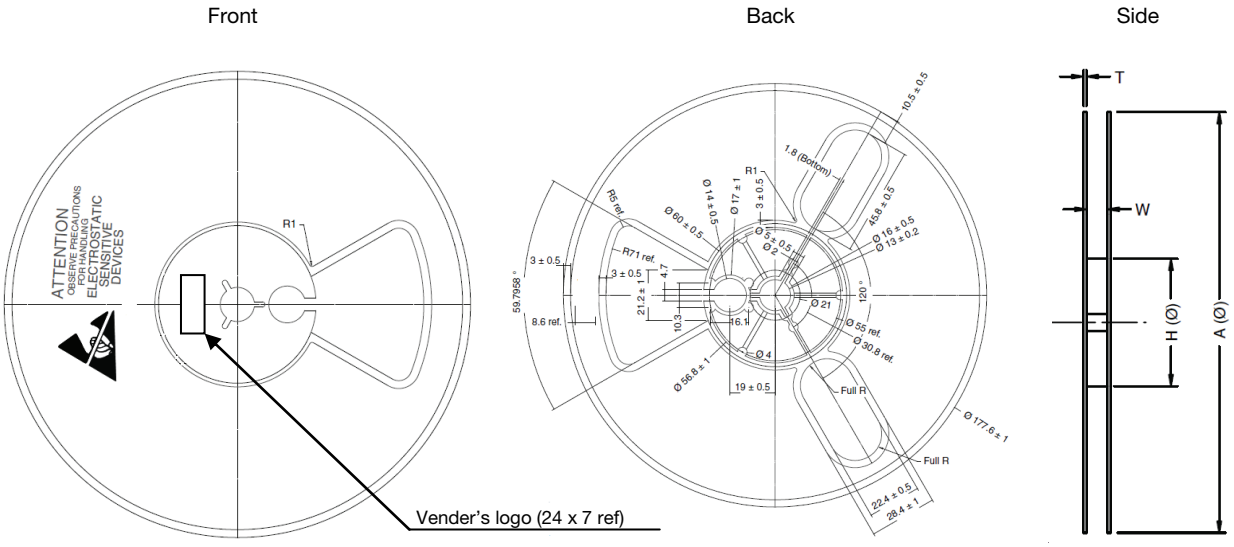
330 mm Reel (Lock Reel)



Notes
1. Material: antistatic or conductor plastic
2. All dimensions in mm
3. ESD-surface resistivity -10^4 Ω to 10^{11} Ω
4. Color: black

VER	APPLICATION		A	W	TAPE WIDTH	H	T
- 1	SOIC-14/16 TO-251 (Short Lead) TO-252/TO-252 (Reverse Lead) PLCC-20 TSSOP-8/14/16/20/28 SSOP-24 SOIC-16 (W)	PowerPAK MLF 9 x 9 PowerPAK MLP 6 x 6 MLF 8 x 8 PowerPAK 8 x 8L PowerPAK 8 x 8 MLP57/MLP66/MLP77 PowerPAK 5 x 9	330 ± 2	16.4 +2 -0	16	100 ± 1	2.5 ± 0.5
- 2	SOIC-8 (N), SOIC-8 (N) epad MSOP-8/10 PowerPAK® SO-8 PowerPAK 1212 PowerPAK 1212-8W MICRO FOOT® MLP33-5, MLP33-8, MLP33-10 QFN (4 x 4)/(3 x 3)/DFN-10 (3 x 3) MLP44/MLP4535/MLP55/MLP65	PolarPAK® PowerPAIR® 6 x 5 PowerPAIR 6 x 3 J PowerPAIR SO-8L PolarPAK1215 PowerPAIR 6 x 3.7 PowerPAK SO-8L PKSO8DCWL	330 ± 2	12.4 +2 -0	12	100 ± 1	2.5 ± 0.5
- 4	SOT-23/143 SC70 MICRO FOOT	TSOP-6, 1206-8 ChipFET PowerPAK SC70 PowerPAK SC75	330 ± 2	8.4 +1.5 -0	8.4	100 ± 1	2.5 ± 0.5
- 5	SOIC-20W/24W D^2PAK SSOP-28 QSOP-36	PowerPAK MLF 10 x 10 MLP60-A6C	330 ± 2	24.4 +2 -0	24	100 ± 1	2.5 ± 0.5
- 8	KGD		330 ± 2	16.4 +2 -0	16	130 ± 1	2.5 ± 0.5

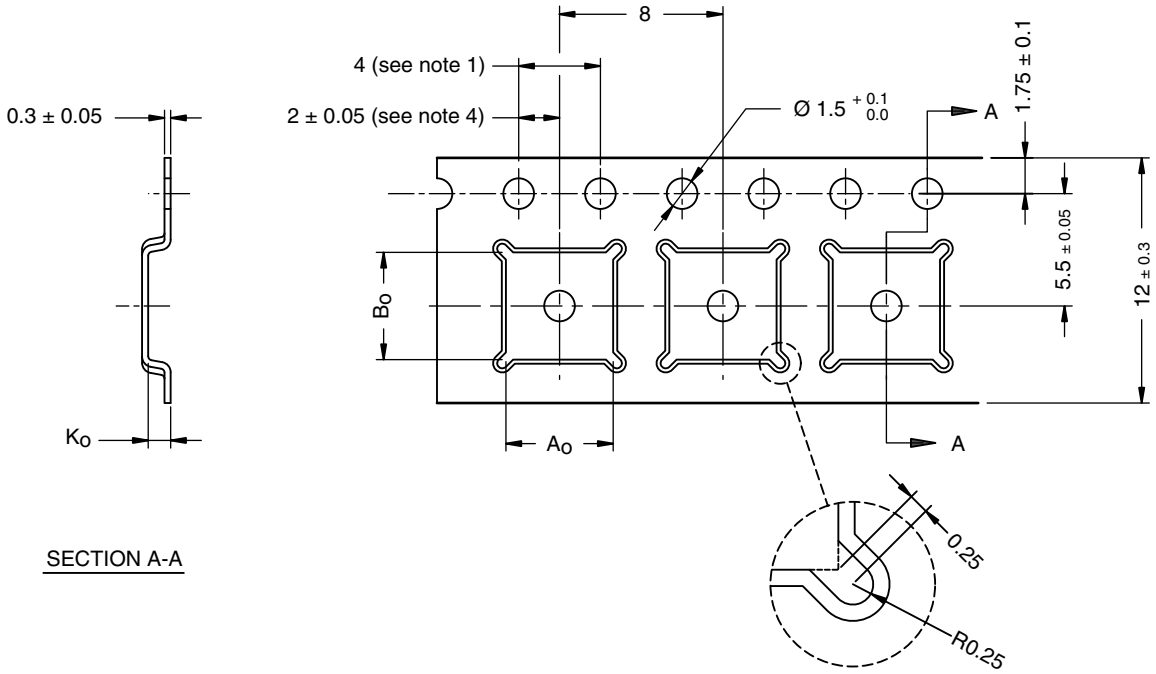
178 mm Reel (Complete Reel)



Notes
1. Material: antistatic or conductor plastic
2. All dimensions in mm
3. ESD-surface resistivity -10^4 Ω to 10^{11} Ω
4. Color: black

VER	APPLICATION		A	W	TAPE WIDTH	H	T
- 3	SOT-23/143 TSOP-5/6/SC70JW-8L 1206-8 ChipFET® SC70/SC75A/SC89 MICRO FOOT SC-89 (SOT-666) SOT23-5, 6 KGD WCSP PowerPAK 0806 PowerPAK SC70	PowerPAK SC75 MiniQFN PowerPAK MLP22-5 PowerPAK ChipFET PowerPAK SC75-6L (PIC) PowerPAK TSC75-6L (PIC) TDFN4 1.2 x 1.6, TDFN8 2 x 2 Thin PowerPAK SC-70 Thin PowerPAK SC-75 µDFN-6L 1 x 1 µDFN-4L 1 x 1	178 ± 2	8.4 +1.5 -0	8.4	62 ± 2	1.5 ± 0.5
- 7	MICRO FOOT PowerPAK 2 x 5	KGD	178 ± 2	12.4 +2 -0	12	55 ± 2	1.6 ± 0.25
ECN: T19-0069-Rev. BX, 18-Mar-2019 DWG: 93-5211-X							

Carrier Tape for MLP55



Version	A_O	B_O	K_O
- 1	5.25 ± 0.1	5.25 ± 0.1	1.10 ± 0.1

Notes

1. 10 sprocket hole pitch cumulative tolerance ± 0.2 mm.
2. Camber not to exceed 1 mm in 100 mm.
3. Material: black conductive polycarbonate.
4. Pocket position relative to sprocket hole measured as true position of pocket, not pocket hole.
5. All sizes in mm unless specified.

T15-0464-Rev. E, 07-Sep-15
DWG: 93-5260-X

ENVIRONMENTAL AND PACKAGE TESTING DATA FOR POWERPAK® MLP55					
STRESS	**SAMPLE SIZE**	**DEVICE HRS./CYC**	**CONDITION**	**TOTAL FAILS**	**FAIL PERCENTAGE**
Bond Integrity	82	41 000	200 °C + N2	0	0.00
HAST	246	24 600	130 °C, 85 % RH	0	0.00
Pressure Pot	246	23 616	121°C, 15 PSIG	0	0.00
Solder Dunk	164	492	260 °C, 10 s	0	0.00
Temp. Cycle	246	246 000	-65 °C to +150 °C	0	0.00

ACCELERATED OPERATING LIFE TEST RESULT	
Sample Size	6803
Equivalent Device Hours	1 530 247 824
Failure Rate in FIT	2.70

Failure Rate in FIT is calculated according to JEDEC® Standard JESD85, *Methods for Calculating Failure Rates in Units of FITs*, based on accelerated high temperature operating life test results by using an apparent activation energy of 0.7 eV. The junction temperature of the device at use is assumed to be 55 °C. A constant failure rate distribution is assumed. The upper confidence bound of the failure rate is 60 %.

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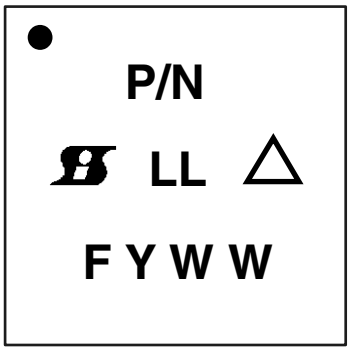
PowerPAK® MLP4535
PowerPAK® MLP55
PowerPAK® MLP66
PowerPAK® MLP77



●	=	Pin 1 Indicator	
P/N	=	Part Number Code	
	=	Siliconix Logo	
△	=	ESD Symbol	
F	=	Assembly Factory Coden	T:TAIWAN assembly
Y	=	Year Code	W:大陸封裝廠
WW	=	Week Code	G:菲律賓封裝廠
LL	=	Lot Code	

The current marking strategy is reflected. Contact your local sales representative for historical marking strategies for these packages.