

JDMD: Extended Dynamic Mode Decomposition with Jacobian Residual Penalization for Learning Bilinear, Control-affine Koopman Models

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TODO: Add abstract

1 Introduction

Controlling complex, underactuated, and highly nonlinear autonomous systems remains an active area of research in robotics, despite decades of previous work exploring effective algorithms and the development of substantial theoretical analysis. Classical approaches typically rely on local linear approximations of the nonlinear system, which are then used in any of a multitude of linear control techniques, such as PID, pole placement, Bode analysis, H-infinity, LQR, or linear MPC. These approaches only work well if the states of the system always remain close to the equilibrium point or reference trajectory about which the system was linearized. The region for which these linearizations remain valid can be extremely small for highly nonlinear systems. Alternatively, model-based methods for nonlinear optimal control have shown great success, as long as the model is well known and an accurate estimate of the global state can be provided. These model-based techniques leverage decades of insight into dynamical systems and have demonstrated incredible performance on complicated autonomous systems [1, 2, 3, 4]. On the other hand, data-driven techniques such as reinforcement learning have received tremendous attention over the last decade and have begun to demonstrate impressive performance and robustness for complicated robotic systems in unstructured environments [5, 6, 7]. While these approaches are attractive since they require little to no previous knowledge about the system, they often require large amounts of data and fail to generalize outside of the domain or task on which they were “trained.”

In this work we propose a novel method that combines the benefits of model-based and data-driven methods, based on recent work applying Koopman Operator Theory to controlled dynamical systems [8, 9, 10, 11, 12]. By leveraging data collected from an unknown dynamical system along with derivative information from an approximate analytical model, we can efficiently learn a bilinear representation of the system dynamics that performs well when used in traditional model-based control techniques such as linear MPC. By leveraging information from an analytical model, we can dramatically reduce the number of samples required to learn a good approximation of the true nonlinear dynamics. We also show the effectiveness of linear MPC on these systems when the learned bilinear system is linearized and projected back into the original state space. The result is a fast, robust, and sample-efficient pipeline for quickly learning a model that beats previous Koopman-based linear MPC approaches as well as purely model-based linear MPC controllers that do not leverage data collected from the actual system. To efficiently learn these bilinear representations,

we also propose a numerical technique that allows for large systems to be trained while limiting the peak memory required to solve the least-squares problem.

In summary, our contributions are:

- A novel extension to extended dynamic mode decomposition (eDMD) that incorporates gradient information from an approximate analytic model;
- a simple linear MPC control technique for learned bilinear control systems that is computationally efficient online, which, when combined with the proposed extension to eDMD, requires extremely little training data to get a good control policy; and
- a recursive, batch QR algorithm solving the least-squares problems that arise when learning bilinear dynamical systems using eDMD.

The paper is organized as follows: in Section 2 we give some background on the application of Koopman operator theory to controlled dynamical systems and review some related works. Section 3 describes the proposed algorithm for combining data-driven and model-based approaches, along with the numerical method for solving the resulting large and sparse linear least-squares problems. Section 4 provides extensive numerical analysis of the proposed algorithm, applied to a simulated cartpole and planar quadrotor model, both subject to significant model mismatch. In Section 5 we discuss the limitations of the method, and finish with some concluding thoughts in Section 6.

2 Background and Related Work

2.1 The Koopman Operator

The theoretical underpinnings of the Koopman operator and its application to dynamical systems has been extensively studied, especially within the last decade [13, 14, 9, 15]. Rather than describe the theory in detail, we highlight the key concepts employed by the current work, and defer the motivated reader to the existing literature on Koopman theory.

We start by assuming we have some discrete approximation of a controlled nonlinear, time-dynamical system whose underlying continuous dynamics are Lipschitz continuous:

$$x^+ = f(x, u) \quad (1)$$

where $x \in \mathcal{X} \subseteq \mathbb{R}^{N_x}$ is the state vector, $u_k \in \mathbb{R}^{N_u}$ is the control vector, and x^+ is the state at the next time step. This discrete approximation can be obtained for any continuous-time, smooth dynamical system in many ways, including implicit and explicit Runge-Kutta methods, or by solving the Discrete Euler-Lagrange equations [16, 17, 18].

The key idea behind the Koopman operator is that the nonlinear finite-dimensional discrete dynamics (1) can be represented by an infinite-dimensional *bilinear* system:

$$y^+ = Ay + Bu + \sum_{i=1}^m u_i C_i y = g(y, u) \quad (2)$$

where $y = \phi(x)$ is a nonlinear mapping from the finite-dimensional state space \mathcal{X} to the (possibly) infinite-dimensional Hilbert space of *observables* $y \in \mathcal{Y}$. We also assume the inverse map is approximately linear: $x = Gy$. In practice, we approximate (1) by choosing ϕ to be some arbitrary finite set of nonlinear functions of the state variables, which in general include the states themselves such that the linear mapping $G \in \mathbb{R}^{N_x \times N_y}$ is exact. Intuitively, ϕ “lifts” our states into a higher dimensional space where the dynamics are approximately (bi)linear, effectively trading dimensionality for (bi)linearity. This idea should be both unsurprising and familiar to most roboticists, since similar techniques have already been employed in other forms, such as maximal-coordinate representations of rigid body dynamics [19, 16, 18], the “kernel trick” for state-vector machines [20], or the observation that solving large, sparse nonlinear optimization problems is often more effective than solving small, tightly-coupled dense problems **TODO: add citations from the trajectory optimization literature.**

The lifted bilinear system (2) can be easily learned from samples of the system dynamics (x_j^+, x_j, u_j) using extended Dynamic Mode Decomposition (eDMD) [15], which is just the application of linear least squares (LLS) to the lifted states. Details of this method will be covered in the next section where we introduce our adaptation of eDMD and present an effective numerical technique for solving the resulting LLS problems.

TODO: mention the most related papers

3 EDMD with Jacobian Residual-Penalization

Existing Koopman-based approaches to learning dynamical systems only rely on samples of the unknown dynamics. Here we present a novel method for incorporating prior knowledge about the dynamics by adding derivative information of an approximate model into the data set to be learned via eDMD.

Given P samples of the dynamics (x_i^+, x_i, u_i) , and an approximate discrete dynamics model

$$x^+ = \tilde{f}(x, u) \quad (3)$$

we can evaluate the Jacobians of our approximate model \tilde{f} at each of the sample points: $\tilde{A}_i = \frac{\partial \tilde{f}}{\partial x}$, $\tilde{B}_i = \frac{\partial \tilde{f}}{\partial u}$. After choosing a nonlinear mapping $\phi : \mathbb{R}^{N_x} \mapsto \mathbb{R}^{N_y}$ our goal is to find a bilinear dynamics model (2) that matches the Jacobians of our approximate model, while also matching our dynamics samples. If we define $\hat{A}_j \in \mathbb{R}^{N_x \times N_x}$ and $\hat{B}_j \in \mathbb{R}^{N_x \times N_u}$ to be the Jacobians of our bilinear dynamics model, projected back into the original state space (a formal definition of these terms will be provided in a few paragraphs), our objective is to find the matrices parameterizing our bilinear dynamics model, $A \in \mathbb{R}^{N_y \times N_y}$, $B \in \mathbb{R}^{N_y \times N_u}$, and $C_{1:m} \in \mathbb{R}^{N_u \times \mathbb{R}^{N_y \times N_y}}$, that minimize the following objective:

$$(1 - \alpha) \sum_{j=1}^P \|\hat{y}_j - y_j^+\|_2^2 + \alpha \sum_{j=1}^P \left(\|\hat{A}_j - \tilde{A}_j\|_2^2 + \|\hat{B}_j - \tilde{B}_j\|_2^2 \right) \quad (4)$$

where $\hat{y}_j^+ = g(\phi(x_j), u_j)$ is the output of our bilinear dynamics model, and $y_j^+ = \phi(x_j^+)$ is the actual lifted state (i.e. observables) at the next time step. Note that \hat{y}_j , \hat{A}_j , and \hat{B}_j are all implicitly functions of the model parameters A , B , and $C_{1:m}$ we're trying to learn.

While not immediately apparent, we can minimize (4) using linear least-squares, using techniques similar to those used previously in the literature [21].

To start, we combine all the data we're trying to learn into a single matrix:

$$E = [A \quad B \quad C_1 \quad \dots \quad C_m] \in \mathbb{R}^{N_y \times N_z}, \quad (5)$$

where $N_z = N_y + N_u + N_y \cdot N_u$. We now rewrite the terms in (4) in terms of E . By defining the vector

$$z = [y^T \quad u^T \quad u_1 y^T \quad \dots \quad u_m y^T] \in \mathbb{R}^{N_z}, \quad (6)$$

we can write down the output of our bilinear dynamics (2) as

$$\hat{y}^+ = Ez. \quad (7)$$

The previously-mentioned projected Jacobians of our bilinear model, \hat{A} and \hat{B} , are simply the Jacobians of the bilinear dynamics in terms of the original state. We obtain these dynamics by ‘lifting’ the state via ϕ and then projecting back onto the original states using G :

$$x^+ = G \left(A\phi(x) + Bu + \sum_{i=1}^m u_i C_i \phi(x) \right) = \tilde{f}(x, u) \quad (8)$$

Differentiating these dynamics gives us our projected Jacobians:

$$\hat{A}_j = \frac{\partial \hat{f}}{\partial x}(x_j, u_j) = G \left(A + \sum_{i=1}^m u_{j,i} C_i \right) \Phi(x_j) = GE\bar{A}(x_j, u_j) = GE\bar{A}_j \quad (9a)$$

$$\hat{B}_j = \frac{\partial \hat{f}}{\partial u}(x_j, u_j) = G \left(B + [C_1 x_j \quad \dots \quad C_m x_j] \right) = GE\bar{B}(x_j, u_j) = GE\bar{B}_j \quad (9b)$$

where $\Phi(x) = \partial \phi / \partial x$ is the Jacobian of the nonlinear map ϕ , and

$$\bar{A}(x, u) = \begin{bmatrix} I \\ 0 \\ u_1 I \\ u_2 I \\ \vdots \\ u_m I \end{bmatrix} \in \mathbb{R}^{N_z \times N_x}, \quad \bar{B}(x, u) = \begin{bmatrix} 0 \\ I \\ [x \ 0 \ \dots \ 0] \\ [0 \ x \ \dots \ 0] \\ \vdots \\ [0 \ 0 \ \dots \ x] \end{bmatrix} \in \mathbb{R}^{N_z \times N_u}. \quad (10)$$

Note we define $\bar{A}_j = \bar{A}(x_j, u_j)$, $\bar{B}_j = \bar{B}(x_j, u_j)$ to lighten the notation, but want to emphasize that these terms are all purely functions of the input data.

Substituting (7) and (9) into (4), we can rewrite our LLS problem as:

$$\underset{E}{\text{minimize}} \sum_{j=0}^P (1 - \alpha) \|Ez_j - y_j^+\|_2^2 + \alpha \|GE\bar{A}_j - \tilde{A}_j\|_2^2 + \alpha \|GE\bar{B}_j - \tilde{B}_j\|_2^2 \quad (11)$$

which is equivalent to

$$\underset{E}{\text{minimize}} (1 - \alpha) \|E\mathbf{Z}_{1:P} - \mathbf{Y}_{1:P}^+\|_2^2 + \alpha \|GE\bar{\mathbf{A}}_{1:P} - \tilde{\mathbf{A}}_{1:P}\|_2^2 + \alpha \|GE\bar{\mathbf{B}}_{1:P} - \tilde{\mathbf{B}}_{1:P}\|_2^2 \quad (12)$$

where $\mathbf{Z}_{1:P} \in \mathbb{R}^{N_z \times P} = [z_1 \ z_2 \ \dots \ z_P]$ horizontally concatenates all of the samples (equivalent definition for $\mathbf{Y}_{1:P}^+ \in \mathbb{R}^{N_y \times P}$, $\bar{\mathbf{A}}_{1:P} \in \mathbb{R}^{N_z \times N_x \cdot P}$, $\tilde{\mathbf{A}}_{1:P} \in \mathbb{R}^{N_z \times N_x \cdot P}$, $\bar{\mathbf{B}}_{1:P} \in \mathbb{R}^{N_z \times N_u \cdot P}$, and $\tilde{\mathbf{B}}_{1:P} \in \mathbb{R}^{N_z \times N_u \cdot P}$).

We can rewrite (12) in standard form using the “vec trick”

$$\text{vec}(AXB) = (B^T \otimes A)\text{vec}(X) \quad (13)$$

where $\text{vec}(A)$ stacks the columns of A into a single vector.

Setting E in (14) equal to X in (13), we get

$$\underset{E}{\text{minimize}} \left\| \begin{bmatrix} (1 - \alpha) \cdot (\mathbf{Z}_{1:P})^T \otimes I_{N_y} \\ \alpha \cdot (\bar{\mathbf{A}}_{1:P})^T \otimes G \\ \alpha \cdot (\bar{\mathbf{G}}_{1:P})^T \otimes G \end{bmatrix} \text{vec}(E) + \begin{bmatrix} (1 - \alpha) \cdot \text{vec}(\mathbf{Y}_{1:P}^+) \\ \alpha \cdot \text{vec}(\tilde{\mathbf{A}}_{1:P}) \\ \alpha \cdot \text{vec}(\tilde{\mathbf{G}}_{1:P}) \end{bmatrix} \right\|_2^2 \quad (14)$$

such that the matrix of coefficients has $(N_y + N_x^2 + N_x \cdot N_u) \cdot P$ rows and $N_y \cdot N_z$ columns. We obtain the data for our bilinear model (2) by solving this large, sparse linear least-squares problem.

3.1 Efficient Recursive Least Squares

In its canonical formulation, a linear least squares problem can be represented as the following unconstrained optimization problem:

$$\min_x \|Fx - d\|_2^2. \quad (15)$$

The solution to this problem is found by solving for the x in which the gradient of the objective function with respect to x is zero, also known as the normal equations:

$$(F^T F)x = F^T d, \quad (16)$$

For small to medium sized problems, this problem is most often solved with either a Cholesky or a QR decomposition. Unfortunately, for very large problems where storage size and numerical conditioning become a concern, forming and factorizing the required matrices can be intractable.

To deal with large problems like the one proposed in (14), a recursive method is used that processes rows of F and d sequentially in batches, avoiding the need for forming or factorizing the whole matrix. To do this, the rows of F and d will be divided up into batches in the following manner:

$$F = \begin{bmatrix} F_1 \\ F_2 \\ \vdots \\ F_N \end{bmatrix}, \quad d = \begin{bmatrix} d_1 \\ d_2 \\ \vdots \\ d_N \end{bmatrix}. \quad (17)$$

The matrix $F^T F$ from (16) can then be represented as the following sum:

$$F^T F = F_1^T F_1 + F_2^T F_2 + \dots + F_N^T F_N, \quad (18)$$

with the right-hand side vector in (16) expressed in a similar fashion:

$$F^T d = F_1^T d_1 + F_2^T d_2 + \dots + F_N^T d_N. \quad (19)$$

The main idea of this recursive method is to maintain an upper-triangular “square root” factor U_i of the first i terms of the sum (18). Given the factorization U_i , we can calculate U_{i+1} using the QR decomposition, as shown in [22]:

$$U_{i+1} = \sqrt{U_i + F_{i+1}} = \text{QR}_R \left(\begin{bmatrix} \sqrt{U_i} \\ \sqrt{F_{i+1}} \end{bmatrix} \right), \quad (20)$$

where QR_R returns the upper triangular matrix R from the QR decomposition.

We handle regularization of the normal equations, equivalent to adding L2 regularization to the original least squares problem, during the base case of our recursion. If we want to add an L2 regularization with weight ρ , we calculate U_1 as:

$$U_1 = \text{QR}_R \left(\begin{bmatrix} \sqrt{F_1} \\ \sqrt{\rho I} \end{bmatrix} \right), \quad (21)$$

The final algorithm for solving a least squares problem in a recursive-batch fashion is described in algorithm 1. This algorithm can be modified to handle L2 regularized least squares problems by simply replacing line 2 of algorithm 1 with $U \leftarrow \text{QR}_R(\text{vcat}(F_1, \sqrt{\rho I}))$, where ρ is the regularizer.

Algorithm 1 Recursive Batch Least Squares with QR

| | | |
|----|---|---|
| 1: | input F, d | ▷ problem data |
| 2: | $U \leftarrow \text{QR}_R(\text{vcat}(F_1, \sqrt{\rho I}))$ | ▷ form initial upper-triangular square-root |
| 3: | $b \leftarrow F_1^T d_1$ | ▷ form initial right hand side vector |
| 4: | for $i = 2 : N$ do | |
| 5: | $U \leftarrow \text{QR}_R(\text{vcat}(U, F_i))$ | ▷ update square-root with new batch |
| 6: | $b \leftarrow b + F_i^T d_i$ | ▷ update right hand side with new batch |
| 7: | end for | |
| 8: | output $x \leftarrow U^{-1} U^{-T} b$ | ▷ forward and backwards substitution to solve for x |

4 Results

The following sections provide various numerical analyses of the proposed algorithm. In lieu of an actual hardware experiment (left for future work), for each simulated system we specify two models: a *nominal* model which is a simplified model approximating the *simulated* model, which contains both parametric and non-parametric model error from the nominal model, and is used exclusively for simulating the system.

All models were trained by simulating the “real” system with an arbitrary controller to collect data in the region of the state space relevant to the task. A set of fixed-length trajectories were collected,

each at a sample rate of 20 Hz. The bilinear eDMD model was trained using the same approach in [21]. For the proposed jDMD method, the Jacobians of the nominal model were calculated at each of the sample points and the bilinear model was learned using the approach outlined in Section 3. All continuous dynamics were discretized with an explicit fourth-order Runge Kutta integrator. The code for the experiments is located at [TODO: include after review](#).

4.1 Models

4.1.1 Cartpole Model

For several of the following analyses we use the canonical cartpole system. The *simulated* cartpole model included a tanh model of Coulumb friction between the cart and the floor, viscous damping at both joints, and a control deadband that was not included in the *nominal* model. Additionally the mass of the cart and pole of the simulated model were altered by 20% and 25% with respect to the nominal model, respectively. The following nonlinear mapping was used when learning the bilinear models: $\phi(x) = [1, x, \sin(x), \cos(x), \sin(2x), \sin(4x), T_2(x), T_3(x), T_4(x)] \in \mathbb{R}^{33}$, where $T_i(x)$ is a Chebyshev polynomial of the first kind of order i .

We analyze the system on two separate control tasks:

1. *MPC Stabilization* about the upward unstable equilibrium, given initial conditions sampled from a uniform distribution of $\pm[1.0, 40^\circ, 0.5, 0.5]$, relative to the upward equilibrium. The control was calculated using a linear MPC policy with a horizon of 1 second.
2. *Swingup* reference trajectory tracking with a linear MPC controller with a time horizon of 1 second. The 5 second swingup trajectories were generated using ALTRO, a high-performance open-source trajectory optimization solver [22, 23].

4.1.2 Planar Quadrotor

As another benchmark example, we use a planar quadrotor model, a simplification of the full quadrotor system with only 3 degrees of freedom. All model parameters were derived off of a real physical system (including experimentally-determined force and torque curves). The *simulated* model included aerodynamic drag terms not included in the *nominal* model, as well as parametric error of about 5% on the system properties (e.g. mass, rotor arm length, etc.).

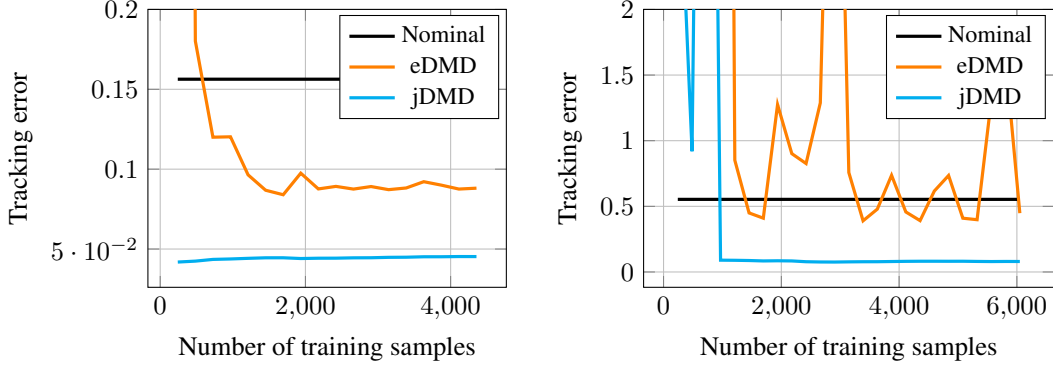
We analyze the system on tasks nearly identical to those of the cartpole system:

1. *LQR Hover stabilization* where the system must stabilize about the origin given initial conditions sampled from the uniform distribution of $\pm[1.0, 1.0, 40^\circ, 0.5, 0.5, 0.25]$, centered about the origin. The system must stabilize using a traditional LQR controller.
2. *Linear MPC trajectory tracking* where the system is given an initial condition take from the same distribution used for the stabilization task, but is asked to track a linear trajectory back to the origin using a linear MPC controller.

4.2 Sample Efficiency

We highlight the sample efficiency of the proposed algorithm in Figures 1a and 1b. For both the cartpole swingup and the quadrotor trajectory tracking tasks, the proposed method achieves better tracking than the nominal MPC controller after just a few training trajectories. In both cases, the classic eDMD approach never achieves the same level of performance as the proposed approach. The lack of continued progress with increasing samples is likely due to a lack of sufficient variety in the training data: after 30-40 training trajectories both methods have effectively learned as much as they can from the distribution from which the training data was sampled.

The training time versus number of training samples is shown in Figure 2 for the cartpole swingup task. While the proposed approach naturally takes longer since it includes much more information



(a) MPC tracking error vs training samples for the cartpole swingup. Tracking error is defined as the average L2 error over all the test trajectories between the reference and simulated trajectories.

(b) MPC tracking error vs training samples for the planar quadrotor. The proposed jDMD method quickly improves upon the linear MPC controller based on the nominal model, whereas eDMD never gets consistently improved performance.

Figure 1: Effect of increased training data on controller performance. With just a few samples the proposed jDMD approach get better performance than the nominal MPC controller, whereas traditional eDMD takes more samples and never achieves the same level of performance. **TODO: combined this into a single plot? Add training time plot to the side?**

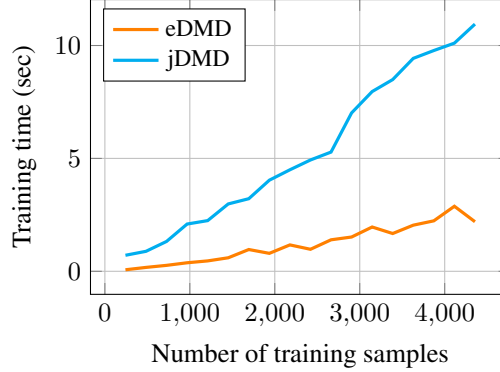


Figure 2: Training time for cartpole models as a function of training samples. The training time complexity is approximately linear.

per sample (adding $N_x + N_u + 1$ rows for every sample), the complexity is approximately linear and the solve times are on the order of seconds for simple systems.

4.3 Lifted versus Projected MPC

Figure 3 also highlights the sample efficiency of the proposed method, while also comparing to the more typical approach of applying the MPC policy in the lifted state space. As shown, the proposed method of applying linear MPC to the projected linearization is much more sample efficient than trying to apply it in the lifted state space. This approach is also advantageous because it reduces the solve time of the linear MPC policy, is more numerically robust (we found the lifted MPC policies tended to suffer from numerical issues when using Riccati recursion to solve for long time horizons), and it is straightforward to apply additional constraints to the original state variables.

4.4 Generalization

We demonstrate the generalizability of the proposed method to tasks outside of its training domain in Figure 4. In both the quadrotor stabilization (Figure 4a) and trajectory tracking (Figure 4b) tasks,

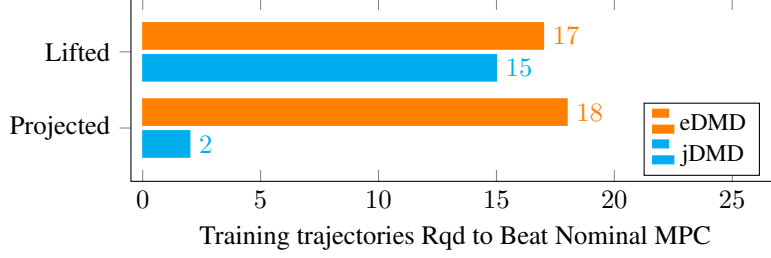
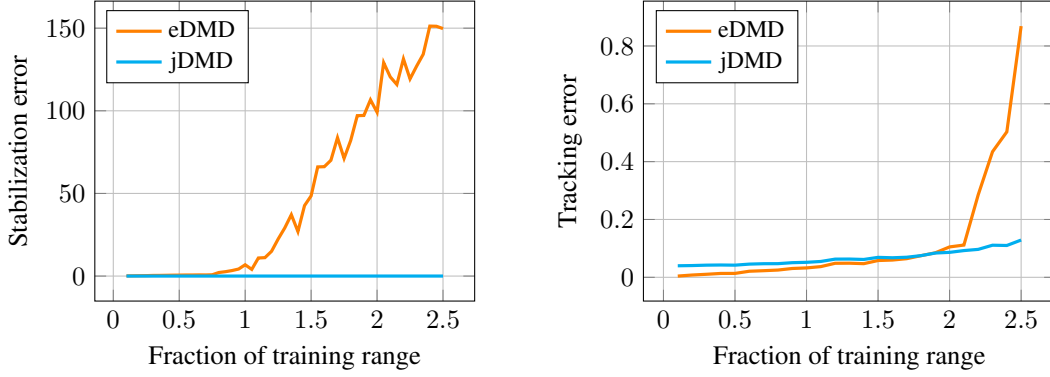


Figure 3: Number of training trajectories requires to beat the nominal MPC controller. The criteria is the L2 norm of the state from the goal state after 4 seconds. The “Lifted” MPC controllers compute the MPC solution in the lifted state space (17 states), whereas the “Projected” MPC controllers project the Jacobians of the bilinear system back into the original state space.



(a) LQR stabilization error over varying ranges of distribution for sampling initial conditions.

(b) MPC tracking error of quadrotor over varying range of distribution for sampling initial conditions. Drastically increasing error for eDMD suggests greater overfitting.

Figure 4: Generalizability with respect to initial conditions sampled outside of the training domain. The initial conditions are sampled from a uniform distribution, whose limits are determined by a scaling of the limits used for the training distribution. A training range fraction greater than 1 indicates the distribution range is beyond that used to generate the training trajectories.

we trained the models by sampling uniformly from a given window of offsets, centered about the origin. To test the generalizability of the methods we increased the relative size of the window from which the test data was sampled, e.g. if the initial lateral position was trained on data in the interval $[-1.5, +1.5]$, we sampled the test initial condition from the window $[-\gamma 1.5, +\gamma 1.5]$. As shown in the results, while the performance of the proposed algorithm remains relatively constant even when $\gamma = 2.5$, whereas the classic eDMD approach loses performance and fails to generalize at all for the stabilization task using and LQR controller (like due to poor derivative information), and up to $\gamma = 2$ for the tracking task using a linear MPC controller.

In Figure 8a we show the effect of changing the equilibrium position for the planar quadrotor, but keeping the delta initial conditions within the training window. As shown, eDMD doesn’t generalize to other equilibrium points, despite the fact that the underlying dynamics are invariant to the equilibrium position. Our proposed approach, however, easily learns this from the derivative information provided by the nominal model.

4.5 Sensitivity to Model Mismatch

While we’ve introduced a significant amount of model mismatch in all of the examples so far, a natural argument against model-based methods is that they’re only as good as your model is at capturing the salient dynamics of the system. We investigated the effect of increasing model mismatch by

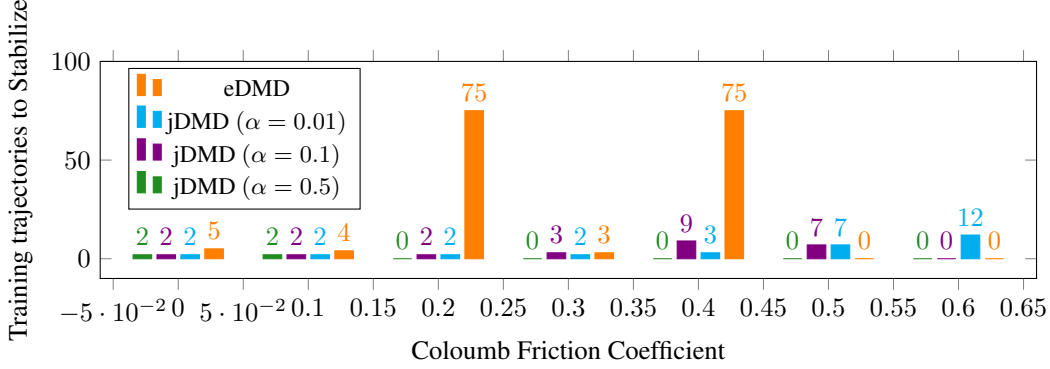


Figure 5: Effect of increasing model mismatch. Displays the number of training trajectories required to consistently stabilize the cartpole system, given an increasing friction coefficient, which the nominal model does not include at all. An entry of 0 signifies that a stabilizing controller wasn’t found with less than 100 training trajectories.

incrementally increasing the Coloumb friction coefficient between the cart and the floor for the cartpole stabilization task. The results are shown in Figure 5. As expected, the number of training trajectories required to find a good stabilizing controller increases for the proposed approach, as long as we set the α value low enough, which intuitively corresponds to a decreased confidence in the nominal model. The samples required by eDMD varied widely, and was unable to find a good enough model above friction values of 0.4. While this could likely be remedied by adjusting the nonlinear mapping ϕ , the proposed approach works well with the given bases.

4.6 Cartpole

As a simple benchmark example, we use the canonical cartpole system. The *simulated* cartpole model included a tanh model of Columb friction between the cart and the floor, viscous damping at both joints, and a control deadband that was not included in the *nominal* model. Additionally the mass of the cart and pole of the simulated model were altered by 20% and 25% with respect to the nominal model, respectively.

We split the analysis of this system into two separate tasks: stabilization about the upward unstable equilibrium from perturbed initial condntions, and the swing-up task where the system must successfully stabilize after starting from the downward equilibrium.

4.6.1 Stabilization

For stabilizing the system about the upward unstable equilibrium, we used an LQR controller to collect trajectories on the simulated system. To learn the bilinear models, we used the following nonlinear mapping: $\phi(x) = [1, x, \sin(x), \cos(x), \sin(2x)] \in \mathbb{R}^{17}$. After learning both models, an MPC controller was designed using the nominal, eDMD, and jDMD models. For the learned bilinear models, MPC controllers were designed using both the “lifted” Jacobians of the bilinear dynamics and the “projected” Jacobians (9). The MPC controllers linearized the dynamics about the equilibrium of $x = [0, \pi, 0, 0]$ and solved the resulting equality-constrained quadratic program using Riccati recursion and a horizon of 41 time steps (2 seconds).

To analyze sample efficiency of the algorithms, we trained the bilinear models with an increasing number of samples. Each controller was tested using 100 different initial conditions sampled from a uniform distribution of initial conditions centered about the upward equilibrium. The average L2 error of the state after 4 seconds and the upward equilibrium was recorded for each controller. The minimum number of training trajectories to get performance consistently better than the nominal MPC controller is reported in Figure 3. As shown, the proposed approach is much more sample efficient even for this relatively simple task than traditional eDMD. It also shows the benefit of

applying the control in the original state space by projecting the linearization back to the original states. To our knowledge, no previous works on applying DMD or Koopman operator theory to controlled systems have used this technique of projecting back into the original state space, although the benefits are immediately apparent: with just a few training trajectories (1 for jDMD and 18 for eDMD) we can learn a model that improves upon our nominal LQR controller policy.

4.6.2 MPC Tracking Performance

To train the bilinear model for the swing-up task, we generated 50 training swing-up trajectories using ALTRO, an open-source nonlinear trajectory optimization solver [22, 23], on the nominal cartpole model. Each trajectory was 5 seconds long and sampled at 20 Hz. A linear MPC controller was then used to track the swing-up trajectories on the simulated system, resulting in significant tracking error due to the model mismatch. After learning both models, a linear MPC policy using the projected dynamics Jacobians was used to track the original swing-up trajectory generated by ALTRO.

The tracking error, defined as the average L2 norm of the error between the reference trajectory and the actual trajectory of the simulated system for 10 test trajectories not included in the training data, was recorded after training both the eDMD and jDMD models with an increasing number of trajectories. The results in Figure 1a clearly show that jDMD produces a high-quality model with extremely few samples, whereas eDMD—even after many training samples—never achieves the same level of performance. The lack of progress with increasing samples is likely a result of poor variety in the training data: after enough samples both methods effectively learn all the information that can be learned from the distribution from which the training data is sampled. This example highlights the value of adding even just a little derivative information to a data-driven approach: it dramatically increases sample efficiency while also improving the quality of the learned model, especially when that model is used in optimization-based controllers such as MPC that rely on derivative information. For reference, the training times are shown in Figure 2. Note that the training algorithms haven’t yet been optimized for max performance but reflect a decent first implementation.

4.7 Planar Quadrotor

As another benchmark example, we use the planar quadrotor model, a simplification of the full quadrotor system with only 3 degrees of freedom. The *simulated* model included aerodynamic drag terms not included in the *nominal*, as well as parametric error of about 5% on the system properties (e.g. mass, rotor arm length, etc.).

Analysis of the planar quadrotor system is also split into 2 separate tasks: stabilization about the hover position with perturbed initial conditions, and a point-to-point translation where the system tracks a linear trajectory between two points with zero initial and terminal velocity.

4.7.1 Stabilization

For stabilizing the system about the upward unstable equilibrium, we used an LQR controller designed using the nominal planar quadrotor model to collect various trajectories. To learn our bilinear eDMD and jDMD, the following nonlinear mapping was used: $\phi(x) = [1, x, \sin(x), \cos(x), 2x^2 - 1] \in \mathbb{R}^{25}$. After learning both models, respective LQR controllers were designed using the bilinear models’ “projected” Jacobians (9). The LQR controllers linearized about hover at the origin ($x = [0, 0, 0, 0, 0]$) and solved the resulting equality-constrained quadratic program using Riccati recursion. Each controller was tested using 30 different initial conditions sampled from a uniform distribution of initial conditions centered about the hover position.

To study how robust eDMD and jDMD are to regularization, we trained multiple bilinear eDMD and jDMD models with increasing L2 (Tikhonov) regularization values. LQR controllers were designed for each model and tested with 100 initial conditions sampled from a uniform distribution centered about the hover position. The average L2 error of the state after 5.0 seconds of simulation, which we’ll refer to in this section as the stabilization error, was recorded for each model. As shown in

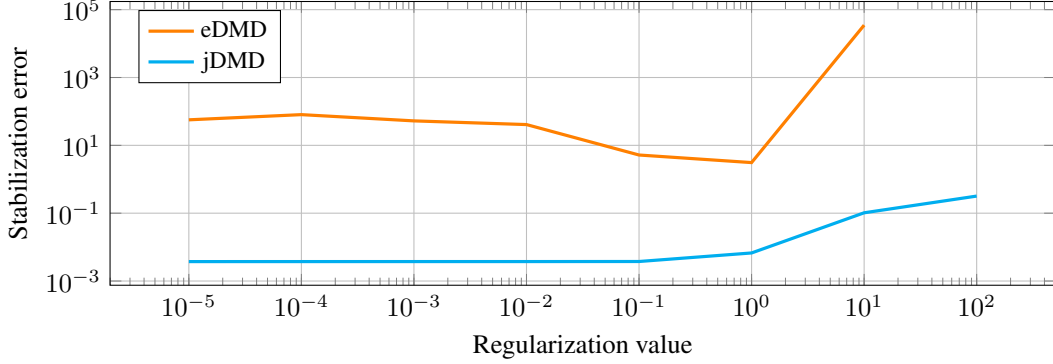


Figure 6: LQR stabilization with equilibrium offset

Figure 7: LQR stabilization error over a range of L2 regularization values. jDMD is much more robust and consistent over small regularization values.

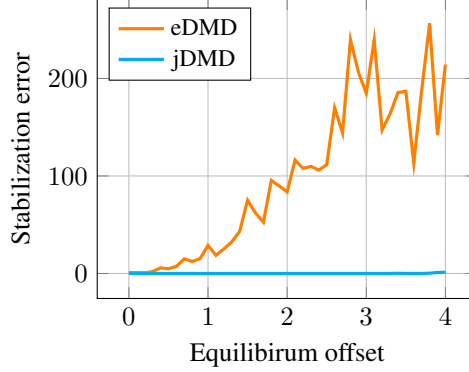
Figure 6, the proposed jDMD method remains robust over a range of small regularization values ($< 10^{-1}$) when compared to nominal eDMD, which clearly has a local optimal around 10^0 . This supports what we found empirically, that jDMD tends to be much “easier” to train and is far more robust to hyperparameters such as the regularization value, when compared to eDMD.

As suggested by Figure 6, eDMD without regularization performs best, but may be prone to overfitting. Therefore, we test eDMD’s and jDMD’s respective LQR controllers on initial conditions sampled from increasingly larger uniform distributions to analyze the generalizability of the lifted, bilinear models. The LQR controllers are tested on 100 samples generated from the uniform distribution, and the average stabilization error is recorded. As seen in Figure 4a, jDMD’s LQR controller is much more robust than eDMD, even when the initial conditions go beyond the scope of the training data. This suggests that adding Jacobian information not only makes eDMD more sample efficient, but can also decrease overfitting and improve generalization.

To further study the robustness of eDMD and jDMD, we tasked the respective LQR controllers for eDMD and jDMD to stabilize under increasingly-varying equilibrium positions. 50 equilibrium positions are sampled from a uniform distribution with increasing bounds, which represent the maximum offset from the origin. The samples are used to test the models’ LQR controllers before recording the average stabilization error. The results in Figure 8a show that jDMD is very robust to the change in equilibrium and is able to successfully stabilize about the equilibrium despite the increasing offset. This is expected because stabilization performance should be invariant with respect to the quadrotor’s equilibrium position, and this information is provided by the Jacobians in jDMD. eDMD’s increasing inability to stabilize for greater equilibrium offsets is likely a result of eDMD being overfitted to the training trajectories, which all stabilize about the origin. Therefore, this example once again highlights the value of adding Jacobian information: it is not only a data augmentation technique for sample efficiency, but also a regularizer that can decrease overfitting, making the learned models (and subsequent controllers) more robust and generalizable.

4.7.2 MPC Tracking Performance

To train the bilinear model for the MPC tracking task, we generated 50 infeasible point-point linear trajectories that all ended at the origin with the planar quadrotor in hover. The starting initial condition of the system was sampled from a uniform distribution about the origin. A linear MPC controller was then used to track the infeasible linear trajectories on the simulated system, resulting in significant tracking error due to the model mismatch. After learning both models, a linear MPC policy (identical to the cartpole example) was used to track the original linear trajectory as best as possible.



(a) LQR stabilization error over increasing equilibrium offset

The tracking error we recorded for 35 test trajectories after training both the eDMD and jDMD models with an increasing number of trajectories. Like the cartpole example, results in Figure 1b clearly show that jDMD produces a high-quality model for MPC tracking with extremely few samples, whereas eDMD—even after many training samples—is never able to develop a model with consistent and similar performance. This is once again highlighted in the results of Figure 4b, which show that eDMD is only able to successfully track trajectories before falling apart when the range of test trajectories exceeds that of the training data. Meanwhile, jDMD is able to consistently track the trajectory to the goal state, despite having greater tracking error in a certain range of trajectories—this further hints at eDMD overfitting on the training data.

5 Limitations

As with most data-driven techniques, it is hard to definitely declare that the proposed method will increase performance in all cases. It is possible that having an extremely poor analytical model may hurt rather than help the training process. However, we found that even when the α parameter is extremely small (placing little weight on the Jacobians during the learning process), it still dramatically improves the sample efficiency. It is also quite possible that the performance gaps between eDMD and jDMD shown here can be reduced through better selection of basis functions and better training data sets; however, given that the proposed approach converges to eDMD as $\alpha \rightarrow 0$, we see no reason to not adopt the proposed methodology as simply tune α based on the confidence of the model and the quantity (and quality) of training data.

6 Conclusion and Future Work

We have presented a simple but powerful extension to eDMD, a model-based method for learning a bilinear representation of arbitrary dynamical systems, that incorporates derivative information from an analytical mode. When combined with a simple linear MPC policy that projects the learned dynamics back into the original state space, we have shown that the resulting pipeline can dramatically increase sample efficiency, often improving over a nominal MPC policy with just a few sample trajectories. Substantial areas for future work remain: most notably testing the proposed pipeline on hardware. Additional directions include lifelong learning or adaptive control applications, residual dynamics learning, as well as the development of specialized numerical methods for solving nonlinear optimal control problems using the learned bilinear dynamics.

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