C**AGEQN Continuum Dynamics, Inc. AGDISP Version 8.29 11/16/16 SUBROUTINE AGEON (XOV) AGEQN integrates the equations of motion - Array of locations, velocities, etc. DIMENSION XOV(9,60), XNV(9,60), DV(6,60) DIMENSION YNR(2), ZNR(2), YNL(2), ZNL(2), YNP(4), ZNP(4) Initial XV = XOV sunt in C INCLUDE 'AGCOMMON.INC' from Agdrop. COMMON /DVFV/ IYDV(60,51), IYFV(60,51) !, IYHV(60,51) C this was done in Astris? Sared line 35 Save initial positions ISWC=NVAR SFAC=SDISP+0.5*(1+IBOOM) IBOOM 30=10 1 = yes IF (IBOOM.EQ.1) NSWTM=NSWTH+1 Single Line It Statements DO I=1, NVAR - DO J=1, NSWTM IYDV(I,J)=0IX IYFV(I,J)=0Closed Multiline It Then ENDDO - ENDDO Endit NSTEP=0 TT does not look to do LCPEND=0 00 Enything LSPEND=0 IVTT=NVAR 1-Agszu does not look to change CALL AGSAV (XOV, 0.0) ENDDO or iterate cornent results Initialize integration (211 Subsountine DT=0.0T=0.0DMTN=DTAM ISTT=0 IF (NPRP.NE.O) THEN DO N=1, NPRP CPXI(N)=CPXI(N)+XO-XPRP(N) ENDDO ENDIF IF (LMVEL.EQ.2.AND.XO.GT.0.0) THEN FN=EXP(-AMIN1(CHF*XO, 25.0)) G2PI(1) = CHG*(1.0-FN)ZBAR(1)=HHEL ZBAL(1)=HHEL WHEL=CHW*SQRT(FN) ENDIF Integrate to TMAX 10 NSTEP=NSTEP+1 UTERM=9.58*(1.0-EXP(-(DMIN/1770.0)**1.147)) DT=0.0002*DMIN/UTERM XOV, T From shore go in, DV determined + seturned CALL AGBKG (XOV, DV, T) Solve the equations of motion for the DT time step X Y Z U V W XX XU UU DO I=1, NVAR xov is xv from ogdrop IF (ISW(I).NE.O) THEN IF (DV(1,1).GT.0.0) EXPT=EXP(-AMIN1(DT/DV(1,1),25.0)) STU detault D, set 57 Aginit TEM1=DV(2,I)+9.8*STU*DV(1,I) set to value it TEM2=XOV(4,I)-TEM1 SMOKEY O= MSU/2 bory XNV(1,I) = XOV(1,I) + TEM1 * DT + TEM2 * DV(1,I) * (1.0 - EXPT)XNV(4,I)=TEM1+TEM2*EXPT 1 = forest service TEM1=DV(3, I)-9.8*CTU*STS*DV(1, I) TEM2=XOV(5,I)-TEM1 XNV(2,I) = XOV(2,I) + TEM1 * DT + TEM2 * DV(1,I) * (1.0 - EXPT)XNV(5,I) = TEM1 + TEM2 * EXPTTEM1=DV(4,I)-9.8*CTU*CTS*DV(1,I) TEM2=XOV(6,1)-TEM1 XNV(3,1)=XOV(3,1)+TEM1*DT+TEM2*DV(1,1)*(1.0-EXPT) XNV(6,I)=TEM1+TEM2*EXPT TEM1=DV(5,I)+DV(1,I)*DV(6,I)TEM2=XOV(8,I)-DV(5,I)+DV(1,I)*(XOV(9,I)-2.0*DV(6,I))TEM3=XOV(9,1)-DV(6,1)
XNV(9,1)=DV(6,1)+TEM3*EXPT*EXPT XNV(8,I)=TEM1+TEM2*EXPT-TEM3*DV(1,I)*EXPT*EXPT $\texttt{XNV} \ (\texttt{7,I}) = \texttt{XOV} \ (\texttt{7,I}) + 2.0 \\ \texttt{^*TEM1} \\ \texttt{^*DT+2.0} \\ \texttt{^*TEM2} \\ \texttt{^*DV} \ (\texttt{1,I}) \\ \texttt{^*} \ (\texttt{1.0-EXPT})$ -TEM3*DV(1,I)*DV(1,I)*(1.0-EXPT*EXPT) XNV(7,I) = AMAX1(0.0,XNV(7,I))XNV(9,I) = AMAX1(0.0, XNV(9,I))IF (XNV(3,I).LE.ZREF) THEN $\mathtt{RATE} = (\mathtt{XOV} \, (3,\mathtt{I}) \, - \mathtt{ZREF}) \, / \, (\mathtt{XOV} \, (3,\mathtt{I}) \, - \mathtt{XNV} \, (3,\mathtt{I}) \,)$ DO J=1,9 $\texttt{XNV}\left(\texttt{J},\texttt{I}\right) = \texttt{XOV}\left(\texttt{J},\texttt{I}\right) + \texttt{RATE}^{\star}\left(\texttt{XNV}\left(\texttt{J},\texttt{I}\right) - \texttt{XOV}\left(\texttt{J},\texttt{I}\right)\right)$ 96 97 98 99 ENDDO XNV(3,I) = ZREFISW(I) = -1ENDIF 100 101 102 103 Canopy deposition and total accountancy in height CNEW=CMASS(I) 104 105 IF (LCANF.GT.0) THEN CALL AGCAN (XOV(1,I), XNV(1,I), EDOV(I), EDNV(I), CNEW) 106 107 ETEM=YMASS*CMASS(I)*((EDOV(I)/DIAM)**3-(EDNV(I)/DIAM)**3) 108 CTEM=YMASS*(CMASS(I)-CNEW)*(EDNV(I)/DIAM)**3 109 ATEM=YMASS* (CMASS(I)-CNEW) DH=XNV(3,I)-XOV(3,I)110 IFIX real -> integer 111 112 113 114 115 116 117 118 119 120 NH=MAX0(IFIX(ABS(DH)/0.1)+1,2)DH=DH/(NH-1) IF (CTEM.GT.0.0) THEN NC=0DO N=2,NH HTEM=XOV(3,I)-ZREF+(N-1)*DHIF (HTEM.GT.O.O.AND.HTEM.LT.HCAN-ZREF) NC=NC+1 IF (NC.GT.0) THEN TEMNC=1.0/NC ELSE TEMNC=0.0 123 124 ENDIF ENDIF 125 126 127 128 129 130 -DO N=2,NH DAHH and NAHH set in HTEM=XOV(3,I)-ZREF+(N-1)*DH ${\tt IH=MAXO\,(MINO\,(IFIX\,(HTEM/DAHH)\,+1\,,NAHH)\,,1)}$ Aglims ${\tt TAHFV\,(1,IH)=TAHFV\,(1,IH)+ETEM/\,(NH-1)}$ IF (CTEM.GT.0.0) THEN
IF (HTEM.GT.0.0.AND.HTEM.LT.HCAN-ZREF) THEN 131 132 133 133 134 135 137 138 139 144 144 144 145 147 149 149 151 155 156 161 161 161 161 161 TAHFV(2,IH) = TAHFV(2,IH) + TEMNC*CTEMC ENDIF ENDIF IF (ISW(I).LT.0) TAHFV(3,IH)=TAHFV(3,IH) +YMASS*CNEW*(EDNV(I)/DIAM)**3 LENDDO Total accountancy in distance 20 IF (XNV(2,I).GT.TADDV(ND)) THEN NADD from Aglins, used so part & IF (ND.LT.NADD) THEN initality zonys GOTO 20 ENDIF ENDIF TADFV(1,ND) = TADFV(1,ND) + ETEMTADFV(2,ND)=TADFV(2,ND)+CTEM IF (ISW(I).LT.0) TADFV(3,ND)=TADFV(3,ND) +YMASS*CNEW*(EDNV(I)/DIAM)**3 C Total accountancy in time C try this stream nexdund? IF (T.GT.TATTV(NT)) THEN IF (NT.LT.NATT) THEN NT=NT+1**GOTO 30** ENDIF TATTY, NATT Set in ENDIF IF (XNV(2,1).LT.YGRID2) INMAX=MAX0(INMAX,NT) TATFY AGLAMS 163 DO N=NT, NATT 164 165 TATFV(1,N) = TATFV(1,N) + ETEMTATFV(2,N) = TATFV(2,N) + CTEM166 167 IF (ISW(I).LT.0) TATFV(3,N)=TATFV(3,N) \$ +YMASS*CNEW* (EDNV(I)/DIAM)**3 168 169 ENDDO EFRAC=EFRAC+ETEM 170 171 172 173 CALL AGDSD YMASS* (CMASS(I)-CNEW), EDNV(I), DSCP) !canopy DSD CMASS(I)=CNEW C IF (ISW(I).LT.0) XDTOT=XDTOT+YMASS*CMASS(I) C DO J=1, NSWTM YTEM=0.0 IF (J.EQ.1.AND.IBOOM.EQ.1) THEN IF (IHALF(I).EQ.1) YTEM=1.0 ELSEIF (J.EQ.NSWTM.AND.IBOOM.EQ.1) THEN IF (IHALF(I).EQ.0) YTEM=1.0 ELSE YEDGEZ -> Set by AGLIMS TEM=YEDGE2+(J-1) *SWATH IF (XNV(2, I).GT.TEM.AND.IYDV(I, J).EQ.0) THEN YDRFT=YDRFT+YTEM*YMASS*CMASS(I) IYDV(I,J)=1ENDIF TEM=YFLXV+(J-1) *SWATH IF (XNV(2,I).GT.TEM.AND.IYFV(I,J).EQ.0) THEN FDTOT=FDTOT+YTEM*YMASS*CMASS(I) 192 193 194 IYFV(I,J)=1CALL AGDSD (YTEM*YMASS*CMASS(I), EDNV(I), DSVP) !transport DSD ENDIF 196 197 198 199 IF (ISW(I).LT.O) THEN TEF=(J-SFAC) *SWATH IF (XNV(2, I).LT.TEF) THEN CALL AGDSD (YTEM*YMASS*CMASS(I), EDNV(I), DSSB)
LSE TF (XNV(2, I) LT.TEM) THEN Commented out !spray block DSD 200 201 202 203 204 CALL AGDSD (YTEM*YMASS*CMASS(I), EDNV(I), DSDW)
ENDIF !downwind DSD C YFLXV = Input Flux Plane AGINIT TEM=YFLXV+(J-1)*SWATH205 206 207 208 TEMY=0.5*(XNV(2,I)-TEM)**2/XNV(7,I)TEMM=YTEM*YMASS*CMASS(I)*EXP(-AMIN1(TEMY,25.0))
/SQRT(XNV(7,I)) CALL AGDSD (TEMM, EDNV(I), DSDP) !point DSD ENDIF ENDDO ENDIF ENDDO Determine new positions of vortices IF (LMVEL.NE.O) THEN IF (LMVEL.EQ.2) JHEL=1 DO N=1, NVOR CALL AGVEL (XO, YBAR (N), ZBAR (N), TEM, VBAR, WBAR) YNR(N)=YBAR(N)+DT*VBAR ZNR(N) = ZBAR(N) + DT*WBARCALL AGVEL (XO, YBAL (N), ZBAL (N), TEM, VBAL, WBAL) YNL(N) = YBAL(N) + DT*VBALZNL(N) = ZBAL(N) + DT*WBALIF (NPRP.NE.O) THEN -DO N=1, NPRP CALL AGVEL (XO-XPRP(N), YPRP(N), ZPRP(N), TEM, VBAR, WBAR) YNP(N)=YPRP(N)+DT*VBAR ZNP(N) = ZPRP(N) + DT*WBARLENDDO ENDIF LMVEL O=ground IF (LMVEL.EQ.2) THEN 1 = senzi, Ared NVOR=0 CALL AGVEL(XO, YHEL, ZHEL, TEM, VBAR, WBAR)
YHEL=YHEL+DT*VBAR 2 = heli ZHEL=ZHEL+DT*WBAR 238 239 240 241 242 243 244 245 225 251 255 255 255 255 256 256 256 NVOR=1 JHEL=0 ENDIF -DO N=1, NVOR YBAR(N) = YNR(N)ZBAR(N) = ZNR(N)YBAL(N) = YNL(N)ZBAL(N) = ZNL(N)ENDDO IF (NPRP.NE.O) THEN DO N=1, NPRP YPRP(N) = YNP(N)ZPRP(N) = ZNP(N)ENDDO ENDIF Correct circulation decay IF (XO.GT.0.0) THEN ← DO N=1, NVOR IF (ABS(GDKV(N)).GT.1.0E-10) THEN TEM=AMAX1(1.0,YBAR(N)-YBAL(N))HTEM=2.0*ZBAR(N)/TEM261 262 IF (HTEM.GT.2.0) THEN GDKT=GDKO+(GDK-GDKO)/0.102167/HTEM**3.291 263 264 265 266 ELSE GDKT=GDK ENDIF GDKV(N)=GDKV(N)*EXP(-AMIN1(ABS(GDKT*BSTAB*DT/TEM),25.0)) 267 268 269 270 271 272 273 275 277 278 279 281 282 283 285 288 289 291 292 293 ENDIF IF (GDKV(N).GT.0.001) THEN -DO I=1, NVAR IF (ISW(I).NE.0) YGAUS1=AMAX1(YGAUS1,XNV(2,I)) -ENDDO ENDIF ENDDO ENDIF ENDIF Correct model parameters · C XO=XO+UO*DT IF (NPRP.NE.O) THEN - DO N=1, NPRP CPXI(N)=CPXI(N)+UO*DT RN=CPXI(N)/11.785 VPRP(N)=VPRP(N)*(RPRP(N)/RN)**2 RPRP(N) = RNIF (LMVEL.EQ.2.AND.XO.GT.0.0) THEN IF (XO.LT.40.0*S) THEN FN=EXP(-AMIN1(0.01*CHF*XO,25.0)) G2PI(1) = CHG*(1.0-FN)ZBAR(1)=ZHEL Heli ZBAL(1)=ZHEL WHEL=CHW*SQRT(FN) ELSE WHEL=0.0 ENDIF ENDIF I think this is related to Calputt + Gerpott? 300 Check solution and continue 301 302 T=T+DT303 ISWC=0 304 305 306 307 MSWC=0 IVTT=0 DO I=1, NVAR ISW 1,0,-1 droplet status IF (ISW(I).NE.0) THEN 308 309 DO J=1,9 XOV(J, I) = XNV(J, I) ~ Next position /41 alley set 310 311 312 313 314 315 316 317 318 320 LENDDO IF (LEVAP.NE.O) THEN EDOV(I) = AMAX1 (EDNV(I), DCUT) Euzporzton DMIN=AMIN1 (DMIN, EDOV(I)) IF (IVT(I).EQ.1.AND. (EDOV(I).EQ.DCUT.OR.XOV(2,I).GT.YGRID2)) THEN !turn off save for vapor tracking IVT(I)=0TVTMAX=AMAX1 (TVTMAX,T) ENDIF ENDIF If the y lowshon > grid wax IF (ABS(XNV(2,I)).GT.GRDMX) ISW(I)=-2IF (ISW(I).LT.0) MSWC=1 IF (EDOV(I).LT.2.0) ISW(I)=0 !stop small droplets < 2 um IVTT=IVTT+IVT(I) = 2 Not and supere 325 326 327 328 329 330 331 ENDIF ENDDO IF (T.GE.TMAX) THEN ISWC=0 🛥 MSWC=1 ENDIF Check CALPUFF data collection for later export C 333 334 335 336 337 338 339 IF (LCPFLG.EQ.1.AND.LCPEND.EQ.0) THEN IF (LMVEL.EQ.1.OR.(LMVEL.EQ.2.AND.WHEL/CHW.LT.0.1)) THEN IF ((ABS(G2PI(1)*GDKV(1)).LE.G2PIMN).AND.(T.GE.ETAU)) THEN Bripped for now. MSWC=1 LCPEND=1 340 ENDIF 341 342 ENDIF ENDIF 343 344 Check SCIPUFF end of calculation for this droplet size IF (LSPFLG.EQ.1) THEN IF (LMVEL.EQ.1.OR.(LMVEL.EQ.2.AND.WHEL/CHW.LT.0.1)) THEN IF (ABS(G2PI(1)*GDKV(1)).LE.G2PIMN) THEN ISWC=0 MSWC=1 LSPEND=1 ENDIF ENDIF ENDIF ,modulo MOD I=MAX0(1, IFIX(200.0/DMIN))

IF (MOD(NSTEP, I).EQ.0) MSWC=1

IF (ISWC.NE.0) GOTO 10 CALL AGSAV(XNV,-T)

RETURN END

IF (MSWC.EQ.1) CALL AGSAV(XNV,T)

Back to NOTEP = NSTEP +1

Agegn runs until ISWC=0

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