ENB440 RF Techniques and Modern Applications



ENB440 - FILTER DESIGN

Design Milestone 1

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Executive Summary

In this report a 70Ω microstrip is characterised through mathematic calculation, then designed and modeled within the CST Design Suite software environment.

Transmission and reflection characteristics are first calculated in section 2.1 in terms of ABCD parameters, from which the geometry of the system is calculated. The microstrip geometries are then independently found by using TX-Line software in section 2.2.

CST modeling methods and S parameters are evaluated in section 3. Passband, return loss and transmission are discussed in terms of the microstrip S parameters.

talk about conclusion

Storm Proposal Contents

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Storm Proposal 1 SCOPE

1 Scope

2 Line Impedance Calculations

2.1 Hand Calculations

First we found the ABCD parameters for the circuit shown in Figure 1. Once found they were converted to scattering parameters.

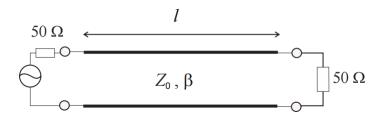


Fig. 1: Theoretical stripline circuit

This circuit consists of two 50Ω loads and two sections of transmission line with an electrical length of λ and an impedence(Z_0) of 70Ω . The wave number (β) is given by:

$$\beta = \frac{2\pi}{\lambda}$$

The unsimplified ABCD representation for this circuit is the following:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 50 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\beta l) & j70sin(\beta l) \\ \frac{jsin(\beta l)}{70} & \cos(\beta l) \end{bmatrix} \begin{bmatrix} 1 & 50 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\beta l) & j70sin(\beta l) \\ \frac{jsin(\beta l)}{70} & \cos(\beta l) \end{bmatrix}$$

As $\beta l = 2\pi$ the sin terms are 0 and the cos terms become 1. The results for the ABCD matrix are as follows:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 100 \\ 0 & 1 \end{bmatrix}$$

The conversion from ABCD to scattering parameters is shown here:

$$S_{11} = \frac{A + B/Z_0 - CZ_0 - D}{A + B/Z_0 + CZ_0 + D} \tag{1}$$

$$S_{11} = \frac{1 + 100/70 - 0 - 1}{1 + 100/70 + 0 + 1} \tag{2}$$

$$S_{11} = \frac{5}{12} \tag{3}$$

$$=20log(S_{11}) = -7.6042dB (4)$$

$$S_{12} = \frac{2(AD - BC)}{A + B/Z_0 + CZ_0 + D} \tag{5}$$

$$S_{12} = \frac{2(1-0)}{1+100/70+0+1} \tag{6}$$

$$S_{12} = \frac{7}{12} \tag{7}$$

$$=20log(S_{12}) = -4.6817dB \tag{8}$$

$$S_{21} = \frac{2}{A + B/Z_0 + CZ_0 + D} \tag{9}$$

$$S_{21} = \frac{2}{A + B/Z_0 + CZ_0 + D}$$

$$S_{21} = \frac{2}{1 + 100/70 + 0 + 1}$$
(9)

$$S_{21} = \frac{7}{12} \tag{11}$$

$$=20log(S_{21}) = -4.6817dB \tag{12}$$

$$S_{22} = \frac{-A + B/Z_0 - CZ_0 + D}{A + B/Z_0 + CZ_0 + D}$$
(13)

$$S_{22} = \frac{-1 + 100/70 - 0 + 1}{1 + 100/70 + 0 + 1} \tag{14}$$

$$S_{22} = \frac{5}{12} \tag{15}$$

$$=20log(S_{22}) = -7.6042dB (16)$$

2.2 **Computer Generated Results**

The National Instruments (NI) program TX-Line was used to generate an approximation of the microstrip geometry. The given laminate, impedance, frequency and electrical length information were input and the program output the microstrip width and length.

These values can be seen in the TX-Line GUI screenshop in figure 2

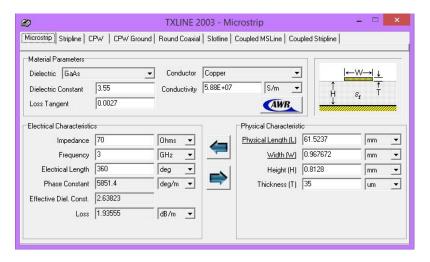


Fig. 2: Screenshot of TX-Line program.

The following data was found from the results:

Characteristic	Result
Phase Constant	0.102126 rad/mm
Physical Length	61.5237 mm
Width	0.967672 mm
Eff. Diel. Const.	2.63823

Storm Proposal 3 MODELING

3 Modeling

The microstrip was modeled in CST, with a frequency range of 2GHz to 4GHz and port information defined at 3GHz. The computer generated results found from TX-Line were initially used and resulted in the model that can be seen below in figure 3.

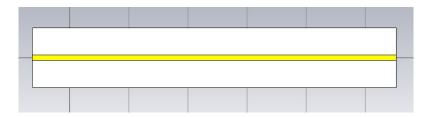


Fig. 3: CST Microstrip model.

The reflection $(S_{11} \text{ and } S_{22})$ and transmission S parameters $(S_{21} \text{ and } S_{12})$ were then found after simulation. These can be seen below in figure 4.

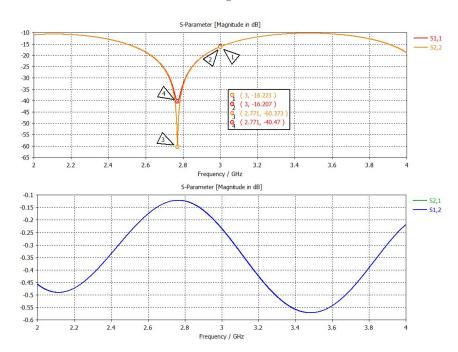


Fig. 4: Top: S_{11} and S_{22} parameters - magnitude. Bottom: S_{21} and S_{12} parameters - magnitude.

It can be seen that the loss of the microstrip along the transmission S parameter S_{21} is 0.239dB. This value is expected - the loss in the copper and dielectric would result in a low loss, especially given the loss tangent of RO4003C being as low as 0.0027.

The passband of the system is seen to peak at 2.771 GHz with very little loss (passband at -60dB S_{11} and -40dB S_{22}). At the specified transmission frequency of 3GHz the reflection of the

Storm Proposal 3 MODELING

microstrip is -16dB, causing return losses. The cause of this is the mismatch between the 50Ω source port and the 70Ω microstrip.

The phase of all S parameters can be seen below in figure 5.

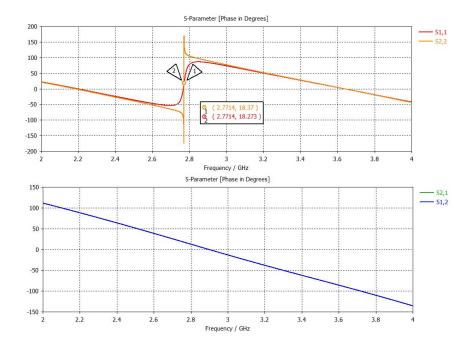


Fig. 5: Top: S_{11} and S_{22} parameters - phase. Bottom: S_{21} and S_{12} parameters - phase.

All S parameter phase plots are linear, as expected.

The S_{11} and S_{22} plots have an abnormality at 2.7714GHz, which is caused by the passband peak.

3.1 CST Optimiser

The CST optimisation software $\,$