## Brady Metherall

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## 1 Model

The laser cavity is treated as the composition of five independent process—gain, nonlinearity, loss, dispersion, and modulation. Expressions for each component will be derived from the generalized nonlinear Schrödinger equation [2, 5, 7, 9],

$$\frac{\partial A}{\partial z} = -i\frac{1}{2}\beta_2 \frac{\partial^2 A}{\partial T^2} + \frac{1}{6}\beta_3 \frac{\partial^3 A}{\partial T^3} + i\gamma |A|^2 A + \frac{1}{2}g(A)A - \alpha A,\tag{1}$$

where A is the complex amplitude of the pulse,  $\beta_2$  and  $\beta_3$  are the second and third order dispersion coefficients respectively,  $\gamma$  is the coefficient of nonlinearity, g(A) is the gain, and  $\alpha$  is the loss of the fiber.

#### 1.1 Gain

Within the Er-doped gain fiber the other four processes are assumed to be negligible, and so (1) reduces to

$$\frac{\partial A}{\partial z} = \frac{1}{2}g(A)A\tag{2}$$

with

$$g(A) = \frac{g_0}{1 + E/E_{sat}},$$

where  $g_0$  is a small signal gain,  $E_{sat}$  is the energy at which the gain begins to saturate, and

$$E = \int_{-\infty}^{\infty} |A|^2 \, dT,$$

is the energy of the pulse [3, 4, 7, 8, 9]. We shall first transform (2) into an equation in terms of the energy. Taking

$$\frac{\partial A}{\partial z} = \frac{1}{2} \cdot \frac{g_0 A}{1 + E/E_{sat}},$$

multiplying by  $\bar{A}$ , the complex conjugate of A, and then adding the complex conjugate gives

$$\frac{d|A|^2}{dz} = \frac{g_0|A|^2}{1 + E/E_{sat}},$$

which after integrating becomes

$$\frac{dE}{dz} = \frac{g_0 E}{1 + E/E_{sat}}.$$

For  $E \ll E_{sat}$  the energy grows exponentially, whereas for  $E \gg E_{sat}$  the gain has saturated and so the energy grows linearly. A closed form of the energy can be found by separating and integrating yielding

$$E(z) = E_{sat}W_0 \left(\frac{E_0}{E_{sat}}e^{E_0/E_{sat}}e^{g_0z}\right),\tag{3}$$

where  $W_0$  is the Lambert W function. However, only the exiting energy is of interest, thus (3) can be written as

$$E' = E_{sat} W_0 \left( \frac{E}{E_{sat}} e^{E/E_{sat}} e^{g_0 L_g} \right),$$

where E is the energy of the incoming pulse, and E' is the energy after traveling through the length of the gain fiber. Since  $E \sim |A|^2$  the gain in terms of the amplitude is given by

$$G(A) = \left[ \frac{E_{sat}}{E} W_0 \left( \frac{E}{E_{sat}} e^{E/E_{sat}} e^{g_0 L_g} \right) \right]^{1/2} A. \tag{4}$$

## 1.2 Nonlinearity of Fiber

The effect of the nonlinearity of the fiber can also be found from (1):

$$\frac{\partial A}{\partial z} - i\gamma |A|^2 A = 0,$$

which similarly to the gain, can be transformed by multiplying by the complex conjugate of A, and adding its complex conjugate gives

$$\frac{\partial |A|^2}{\partial z} = 0. ag{5}$$

This suggests the envelope of the pulse does not change as it travels through the fiber—a solution of the form  $A=A_0e^{i\varphi}$  can be assumed. Substituting this expression into (5) gives  $\varphi=\gamma|A|^2z$  therefore

$$F(A) = Ae^{i\gamma|A|^2L_f},$$

where  $L_f$  is the length of the fiber.

### 1.3 Loss

Two sources of loss exist within the laser circuit: the loss due to the output coupler and the optical loss due to the circuit. The loss is then given as

$$L(A) = Ce^{-\alpha L}A,$$

where C is the loss due to the output coupler.

## 1.4 Dispersion

The dominant dispersion is due to the chirped fiber Bragg grating (CFBG). The dispersion due to the fiber is negligible in comparison—a 10cm chirped grating can provide as much dispersion as 300km of fiber [1]. The dispersive terms of (1) give

$$\frac{\partial A}{\partial z} = -i\frac{1}{2}\beta_2 \frac{\partial^2 A}{\partial T^2} + \frac{1}{6}\beta_3 \frac{\partial^3 A}{\partial T^3},\tag{6}$$

however, the third order effects of dispersion will be neglected [2, 5]. Although, under some circumstances they may need to be considered since the grating is highly dispersive [2, 6]. Taking the Fourier transform of (6) gives

$$\frac{\partial \mathcal{F} \{A\}}{\partial z} = \frac{1}{2} i \beta_2 \omega^2 \mathcal{F} \{A\}.$$

The Fourier transform of A can be found by integrating and thus,

$$D(A) = \mathcal{F}^{-1} \left\{ e^{i\frac{1}{2}\beta_2 \omega^2 L_D} \mathcal{F} \left\{ A \right\} \right\}$$

is the effect of the grating on the pulse.

#### 1.5 Modulation

Pick a function that is bump-like, infinitely differentiable (I don't know how important that is), and has a maximum of 1. We shall pick

$$M(A) = e^{-T^2/2T_M^2}A,$$

where  $T_M$  is a characteristic width of the modulation, since its Fourier transform is itself. \*\*\*I don't know how to write this.

#### 1.6 Non-Dimensionalization

The structure of each process of the laser can be better understood by re-scaling the time, energy, and amplitude. Specifically, the time shall be scaled by the characteristic modulation time, the energy by the saturation energy, and the amplitude will be scaled so that it is consistent:

$$T = T_M \widetilde{T}, \quad E = E_{sat} \widetilde{E}, \quad A = \left(\frac{E_{sat}}{T_M}\right)^{1/2} \widetilde{A}.$$

The new process maps, after dropping the tildes, become

$$G(A) = \left(\frac{W_0 \left(aEe^E\right)}{E}\right)^{1/2} A,$$

$$F(A) = Ae^{ib|A|^2},$$

$$L(A) = hA,$$

$$D(A) = \mathcal{F}^{-1} \left\{e^{is^2\omega^2} \mathcal{F}\left\{A\right\}\right\},$$

$$M(A) = e^{-T^2/2} A,$$

with the dimensionless parameters

$$a = e^{g_0 L_g} \sim 30, \quad s = \sqrt{\frac{\beta_2 L_D}{2T_M^2}} \sim 0.1, \quad b = \gamma L_F \frac{E_{sat}}{T_M} \sim 0.1, \quad h = Ce^{-\alpha L} \sim 0.25,$$

which control the behaviour of the laser.

## 1.7 Combining the Pieces

$$\mathcal{L}(A) = M(D(L(F(G(A)))))$$

A solution such that  $|\mathcal{L}(A)|^2 = |A|^2$  is sought.

## 2 Results

### 2.1 Linear Solution

Suppose an initial pulse with envelope

$$|A_0| = \sqrt{P}e^{-x^2/2\sigma^2},$$

the after passing through the gain and loss pieces, and neglecting the fibre nonlinearity, the envelope will be

$$|A| = \sqrt{P}g(E)he^{-x^2/2\sigma^2},$$

where

$$g(E) = \left(\frac{W_0(aEe^E)}{E}\right)^{1/2}$$

is the gain component. After the pulse travels through the grating, the envelope will maintain its Gaussian shape, however, it will have spread. This can be represented as

$$|A| = \sqrt{P}g(E)h\zeta(s,b)e^{-x^2/2\tilde{\sigma}^2}$$

where  $\zeta(s,b)$  represents the decrease in the amplitude and  $\tilde{\sigma}^2$  is the new variance. Although, note that the dispersive element conserves energy, thus,

$$\int_{-\infty}^{\infty} Pg(E)^2 h^2 e^{-x^2/\sigma^2} dx = \int_{-\infty}^{\infty} Pg(E)^2 h^2 \zeta^2(s,b) e^{-x^2/\tilde{\sigma}^2} dx,$$

or more simply

$$\sigma = \zeta^2(s, b)\widetilde{\sigma}.$$

Therefore, the envelope as the pulse exits the grating is

$$|A| = \sqrt{P}g(E)h\zeta(s,b)\exp\left(-\zeta^4(s,b)\frac{x^2}{2\sigma^2}\right).$$

Lastly, the pulse is modulated and so

$$|A| = \sqrt{P}g(E)h\zeta(s,b)\exp\left(-\zeta^4(s,b)\frac{x^2}{2\sigma^2} - \frac{x^2}{2}\right).$$

In equilibrium the envelope of the pulse is unchanged after passing through each element, in other words,

$$\sqrt{P}e^{-x^2/2\sigma^2} = \sqrt{P}g(E)h\zeta(s,b)\exp\left(-\zeta^4(s,b)\frac{x^2}{2\sigma^2} - \frac{x^2}{2}\right).$$

For this to be the case

$$\left(\frac{W_0(aEe^E)}{E}\right)^{1/2}h\zeta(s,b) = 1,$$
(7)

as well as

$$-x^{2}/2\sigma^{2} = -\zeta^{4}(s,b)\frac{x^{2}}{2\sigma^{2}} - \frac{x^{2}}{2},$$

which reduces to

$$\sigma = \sqrt{1 - \zeta^4(s, b)}.$$

$$P = \frac{E}{\sqrt{\pi}\sigma}$$

From (7) the equilibrium energy is found to be

$$E = \frac{\zeta^{2}(s,b)h^{2}}{1 - \zeta^{2}(s,b)h^{2}} \ln \left( a\zeta^{2}(s,b)h^{2} \right).$$

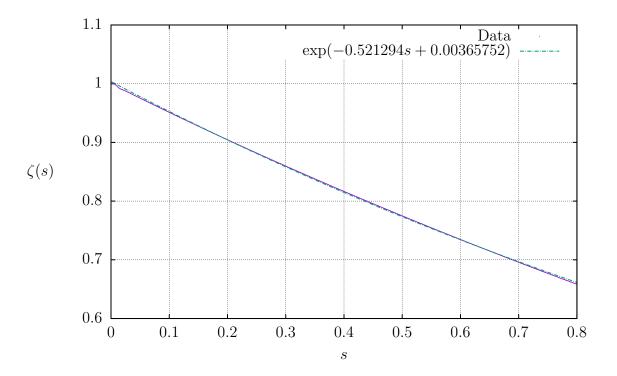


Figure 1:

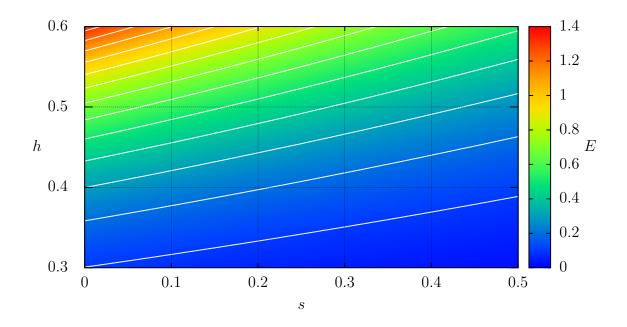


Figure 2: a=30

Parameter	Value
$\beta_2^g L_D$	$10-2000 \text{ps}^2$
$g_0$	$1-10 \mathrm{m}^{-1}$
$\beta_2^f$	$20-50 \mathrm{ps^2/km}$
$  \gamma  $	$0.001 - 0.01 W^{-1} m^{-1}$ [2]
$E_{sat}$	$10^4 \mathrm{pJ}$
$L_G$	2-3m [4, 7, 9]

Table 1: yes

# References

- [1] G. Agrawal. Fiber-Optic Communication Systems. 3rd ed. John Wiley & Sons, Inc., 2002
- [2] G. Agrawal. Nonlinear Fiber Optics. 5th ed. Academic Press, 2013.
- [3] C. S. Bohun et al. Modelling and Specifying Dispersive Laser Cavities. 2015.
- [4] B. Burgoyne, A. Dupuis, and A. Villeneuve. "An Experimentally Validated Discrete Model for Dispersion-Tuned Actively Mode-Locked Lasers". In: *IEEE Journal of Selected Topics in Quantum Electronics* 20.5 (Sept. 2014), pp. 390–398. DOI: 10.1109/JSTQE.2014.2303794.
- [5] M. F. S. Ferreira. Nonlinear Effects in Optical Fibers. John Wiley & Sons, Inc., 2011.
- [6] N. M. Litchinitser, B. J. Eggleton, and D. B. Patterson. "Fiber Bragg Gratings for Dispersion Compensation in Transmission: Theoretical Model and Design Criteria for Nearly Ideal Pulse Recompression". In: *Journal of Lightwave Technology* 15.8 (Aug. 1997), pp. 1303–1313. DOI: 10.1109/50.618327.
- [7] O. V. Shtyrina et al. "Experimental measurement and analytical estimation of the signal gain in an Er-doped fiber". In: *J. Opt. Soc. Am. B* 34.2 (Feb. 2017), pp. 227–231. DOI: 10.1364/JOSAB.34.000227.
- [8] W. T. Silfvast. Laser Fundamentals. 2nd ed. Cambridge University Press, 2004.
- [9] I.A. Yarutkina et al. "Numerical modeling of fiber lasers with long and ultra-long ring cavity". In: Opt. Express 21.10 (May 2013), pp. 12942–12950. DOI: 10.1364/OE.21.012942.