

# Silicon Photomultiplier Classification of the Pre-Production GCT Camera of CTA

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Silicon Photomultiplier Klassifikation der Pre-Production GCT Kamera von CTA

Master-Thesis von Ben Gebhardt aus Heidelberg

Tag der Einreichung:

1. Gutachten: Dr. Richard White (MPIK)
2. Gutachten: Prof. Jim Hinton (MPIK)
3. Gutachten: Prof. Tetyana Galatyuk (TU DA)



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# Erklärung zur Master-Thesis

Hiermit versichere ich, die vorliegende Master-Thesis ohne Hilfe Dritter nur mit den angegebenen Quellen und Hilfsmitteln angefertigt zu haben. Alle Stellen, die aus Quellen entnommen wurden, sind als solche kenntlich gemacht. Diese Arbeit hat in gleicher oder ähnlicher Form noch keiner Prüfungsbehörde vorgelegen.

Darmstadt, den March 22, 2017

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(B. Gebhardt)

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## 1 SiPM Physics

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### 1.1

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#### 1.2 OCT dependency on cellsize

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LCT5 50, 25 um plots, multiply 25 by 4 tu get 50 um results

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## 2 Experimental Setup

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### 2.1 Oscilloscope

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### 2.2 Power Supply

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### 2.3 Thermal Chamber

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### 2.4 Data Acquisition

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Data acquisition in the Laboratory is realized by a Lab-PC (??etup scheme picture) , that forms the central control station for multiple pieces of equipment. It is connected to the oscilloscope(??etup scheme picture), which records the waveforms of the device in testing, and then sends the data back to the PC via ethernet. The power supplies(??etup scheme picture) control the bias-voltage of the Silicon Photomultipliers, ramping of the bias-voltage is controled by the PC. Lastly the thermal chamber(??etup scheme picture) is connected to the Lab-PC, which controls the temperature, and continuously rechecks it during temperature ramps. All equipment connected via ethernet is plugged into a common hub, to form a local network. The ethernet switch needs to reach at least 10Mbit/s ???, because single waveform files, that include 1000 segments of data taken in sequence mode of the oscilloscope, can be up to 0.5Gb in size. While the temperature of the thermal chamber is ramping from the previous to the next set-point, the data is send to the Lab-PC.

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### 2.5 Shaping Electronics

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### 3 Data Analysis

Analysis of the Silicon Photomultiplier waveforms is done exclusively in python following those steps:

1. data conversion
2. pedestal subtraction
3. peak detection
4. gain extraction
5. calculation

The waveform data, after being transferred to a separate PC, is analysed offline. The goal is to extract event-data from the waveforms in order to produce pulse-area spectra for every bias-voltage at every temperature. To that end, the pedestal of the noise must be found and subtracted from the data. After that, event-pulses are detected and integrated. This generates a list of pulse-areas, which is in turn used to fill a pulse-area histogram. To this pulse-area histogram, a model is fitted from which the gain can be extracted. Due to the linear behavior of the gain with rising bias-voltage, a regression line is fitted, from which the Dark Count Rate and the Optical Cross Talk are calculated using the original pulse-area histogram.

#### 3.1 Tracefile Conversion

The oscilloscope produces the waveform data in its intrinsic data format, called a trace with the data suffix trc in binary. A trace file contains a header and two binary lists, an amplitude based on the oscilloscope's voltage-range and offset, and a list of the same length containing the associated event-time, based on the time-range and horizontal offset. The first step is therefore a conversion of the amplitude and associated event-time of all segments of a waveform trace file into two lists of floats.

#### 3.2 Pedestal Subtraction

A single waveform from the oscilloscope is anticipated to be uncentered, it will be slightly above or below zero, depending on the device setup. The signal is mixed with noise when it is observed and forms a pedestal, shifting the mean of the waveform from its original position to zero. Pedestal subtraction removes this average noise. The first step of the process is reading in the uncentered waveform and calculating an initial mean( $\text{mean}_0$ ). It is expected to be slightly higher than the actual mean of the noise, due to the presence of event-pulses. The waveform is then shifted to about zero, by subtracting the  $\text{mean}_0$ . A second mean of the now nearly centered waveform is taken ( $\text{mean}_1$ ). Now a new, same-sized array is formed and filled with the data from the waveform that is smaller than  $\text{mean}_1$ , the negative noise. The data larger than  $\text{mean}_1$ , the positive noise, is also filled into the array, but is negative-signed. This creates an array of the waveform centered around zero and, above the mean, folded towards the negative. It proved reliably, that calculating the root-mean-square of this helper-array is a solid possibility of stripping the waveform of event-peaks. Taking the root-mean-square with a factor 3 of the helper-array, a cut is now applied to the waveform on both, the positive and negative side. In that fashion, the remnant is the waveform between the positive and the negative root-mean-square and is now called a peakless-signal, representing the noise of the waveform. Pedestal subtraction is done by calculating the mean of this peakless signal and subtracting it from the waveform. After that, the peakless signal is also smoothed by convolving it with a wide-windowed gaussian and subtracted from the waveform to eliminate any slow moving noise.

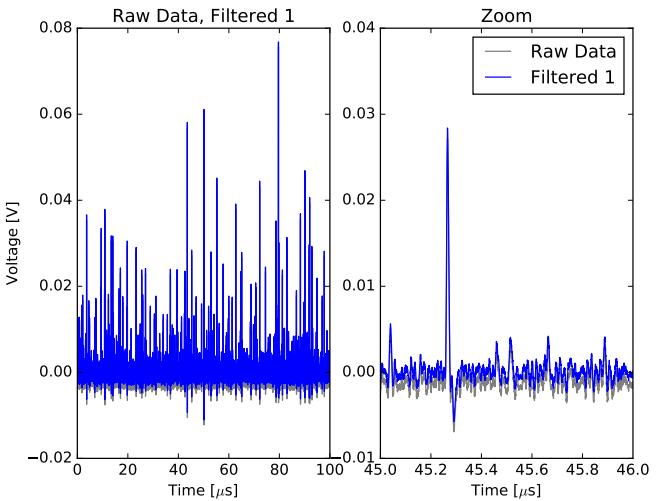


Figure 1: CHEC-S tile

### 3.3 Peak Detection

Peak detection exploits the fact, that the first derivative of an event-peak will cross zero into the negative at the peak maximum. The presence of random noise in the signal however will lead to many false detections. Therefore, before the detection of the event-peaks, the waveform is smoothed with a narrow-window gaussian with a width of about the FWHM of the devices characteristic event-pulse, in order to attenuate non-event peaks. After the first derivative of the signal is calculated, which in python is a fast process if using arrays, a number of parameters decide the validity of the detected peaks. Most important parameters are a certain predetermined minimum amplitude, called the amplitude threshold or: minimum peak height. This is right now determined by eye, but could later be calculated based on the noise level. The second important parameter defining validity is the minimum peak distance, which defines how close two events can occur after another. The value is determined by the FWHM of the device in testing, which I expect to be sensible enough to resolve two events happening close after another. The peak detection algorithm can not distinguish between instantaneous and delayed Optical Cross Talk, but nonetheless, due to the fact, that the signal data is taken over many micro-seconds, all events are detected, independent of their source. On the other hand, this also means, that it is possible for two events to happen at the same time, for example a real photoelectron-event coinciding with delayed Optical Cross Talk. This can not be distinguished and will lead to a slight shift of the amplitude. (because deOCT is partial 1p.e.)

### 3.4 Gain Extraction

The detected peaks are integrated with a window extending symmetrically from the peak maximum, the width is chosen as slightly wider than the peaks FWHM. The generated list of peak areas is generating a peak area histogram, which is fitted with multiple gaussians using iMinuit in python , seen in Figure (??). Two parameters are extracted from the fit to the peak area histogram. The first, the position of the 1p.e. peak is the position of the maximum of the first peak in the histogram, and the position of corresponding multiple p.e. events should be integral factors of the 1p.e. position. This proved to not be the case for some devices, the suspected source of this error is a pedestal generated during the peak integration. I studied the effect of the integration window in more detail in chapter 4.1. A second parameter is extracted from the peak area histogram to deal with this problem, which is the distance between N p.e. peak maxima of the histogram, labeled  $\Delta p.e.$  , which defines the gain. The apparent pedestal of the pulse area histogram makes extraction of the two parameters necessary in order to calculate the Dark Count Rate and the Optical Cross Talk.

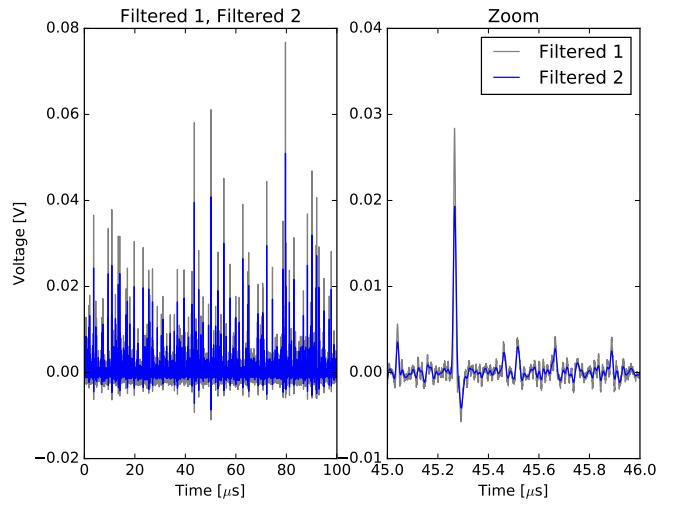


Figure 2: CHEC-S tile

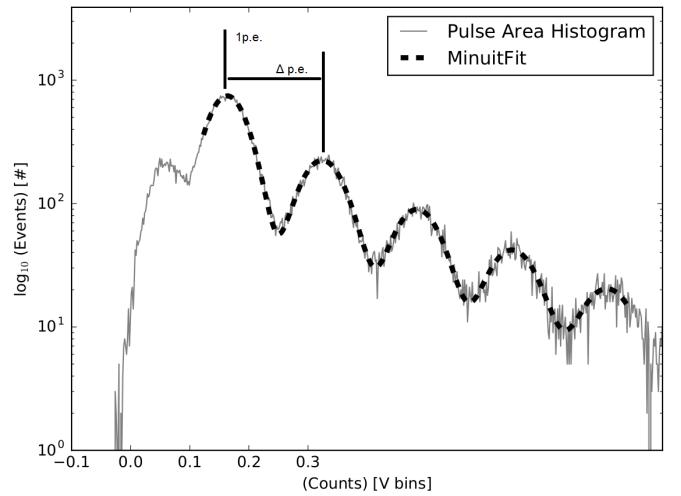


Figure 3: Pulse Area Histogram todo describe more

The gain of a Silicon Photomultiplier has a linear dependence of the supplied bias-voltage. Given that the bias-voltage range is deliberately chosen such that the over-voltage ranges from about 1V growing upwards, the range of linearity only starts at around the point of operation given by the manufacturer of the device. At the higher end of the bias-voltage range the behaviour usually starts to divert from the linearity. In order to get an estimation of the gain over a large range, both previously extracted parameters, the 1p.e. peak and the distance  $\Delta$ p.e. are fitted with a linear regression line. The fit assumes linearity utilizing weighted least squares inherited from pythons statsmodels package. For the fit, only the data, where at least 3 gaussians are fitted to the peak area histogram is taken into account. Plotting both extracted parameters, as well as their respective regression lines versus bias-voltage, as in Figure (4), shows the difference between the two parameters. (SHOW FOR ALL DEVICES IN APPENDIX???) Comparing the manufacturer supplied breakdown-voltage from the datasheet for all devices showed, that the zero-crossing of the 1p.e. regression line is more consistent with datasheet values, in contrast to the zero-crossing of  $\Delta$ p.e., which lies slightly higher. The over-voltage, corresponding to the set bias-voltage at any given temperature is calculated from this breakdown-voltage. Dark Count Rate and Optical Cross Talk are calculated utilizing 1p.e. position and  $\Delta$ p.e. derived from the regression line. Both values are applied, in the calculation, to the peak area histogram with the Dark Count Rate being defined as:

$$DCR = \frac{N_{events(>0.5p.e.)}}{T_{experiment}} \quad (1)$$

Figure 5: The Dark Count Rate of a Silicon Photomultiplier is defined as all events exceeding 0.5 p.e. in amplitude  $N_{events(>0.5p.e.)}$  occurring over the experiment time  $T_{experiment}$

, and the Optical Cross Talk as:

$$OCT = \frac{N_{events(>1.5p.e.)}}{N_{events(>0.5p.e.)}}. \quad (2)$$

Figure 6: The Optical Cross Talk of a Silicon Photomultiplier is defined as all events exceeding 1.5 p.e. in amplitude [ $N_{events(>1.5p.e.)}$ ] divided by all events exceeding 0.5 p.e. in amplitude [ $N_{events(>0.5p.e.)}$ ]

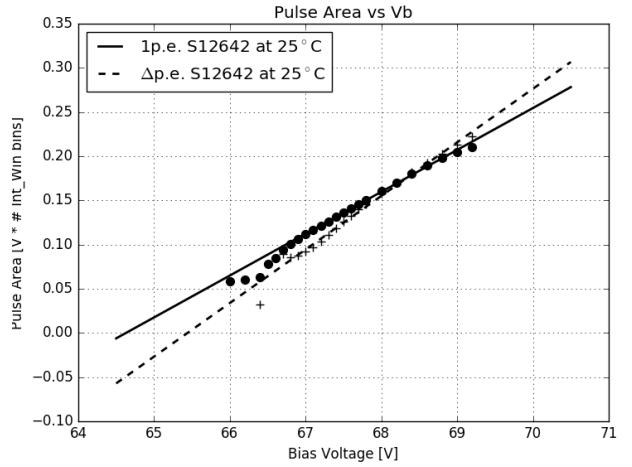


Figure 4: 1p.e. position and  $\Delta$ p.e. plotted versus bias-voltage

## 4 The next three sections might be better in the appendix

### 4.1 The influence of the minimum peak distance

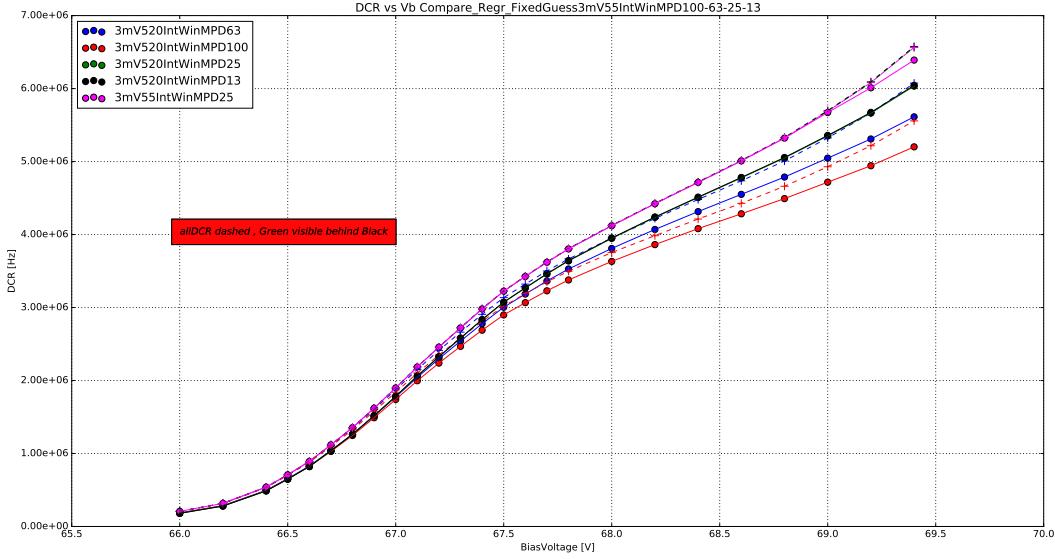


Figure 7: The difference between 4 minimum peak distance windows, in time-bins, during the peak detection. The dashed lines are the Dark Count Rates considering all recorded events, forming an upper limit. In pink, the effect of a different integration window is shown.

The influence of the minimum peak distance is shown in Figure (7). Based on their bin-width, four different windows are tested. With the oscilloscopes sampling rate of  $2.5 \frac{GS}{s}$ , the windows of 100, 63, 25 and 13 time-bins, correspond to 40, 25, 10, 5 ns windows respectively. With a event pulse FWHM of 10ns, setting the minimum peak distance to 100 bins, resulting in a 40ns window is visibly to large, as the algorithm will skip over valid data Figure (7)(red). After an event is detected, skipping over 40ns worth of data will result in errors of the Dark Count Rate, since the calculation uses the complete experiment time. Therefore a more reliable distance window must be chosen. The second window of 25ns was the next approach, originating from the length of the pulse-tail Figure (7)(blue). This would lead to no detected events overlapping with the tail of one previously detected, resulting in a sharper pulse-area spectrum. Compared to a window of approximately the pulse FWHM, the previously discussed window would still lead to lost event-data. Since the sharpness of the pulse-area spectrum is already sufficient, a window around the pulse FWHM was chosen as reference for all measured devices Figure (7)(green). Going lower than the pulse FWHM showed no improvement Figure (7)(black).

### 4.2 The influence of the integration window

Figure (7) also shows the influence of the size and shape of the integration window on the Dark Count Rate. The influence of the chosen integration window is most visible in their respective pulse area spectra. Choosing a narrow, symmetrical integration window of 5ns left and right of the peak maxima, the noise peak, or zero-peak, is much more prominent compared to the pulse area spectrum of a symmetrical 10 ns window. This leads to errors in the multi-gaus fitting step, or the fitting will fail altogether. An asymmetrical integration window of 5ns left, 20ns right, to capture the influence of the pulse-tail proved, at first, to be the best solution as there was no visible zero-peak present. The low amplitude pulses are averaged out by the extended integration window to the right of the pulse-maximum. The downside of the asymmetrical window is the shifting of the pulsle area spectrum and the fact, that the N p.e. peaks get blurred. The next step was widening the window on both sides. This proved the best solution, since there is no zero-peak visible and the N p.e. peaks are gaussian shaped. Please see the Appendix for the respective plots of pulse area spectra of the different windows 9.2 .

### 4.3 The influence of the peak detection threshold??

The peak detection threshold affects the analysis the most.

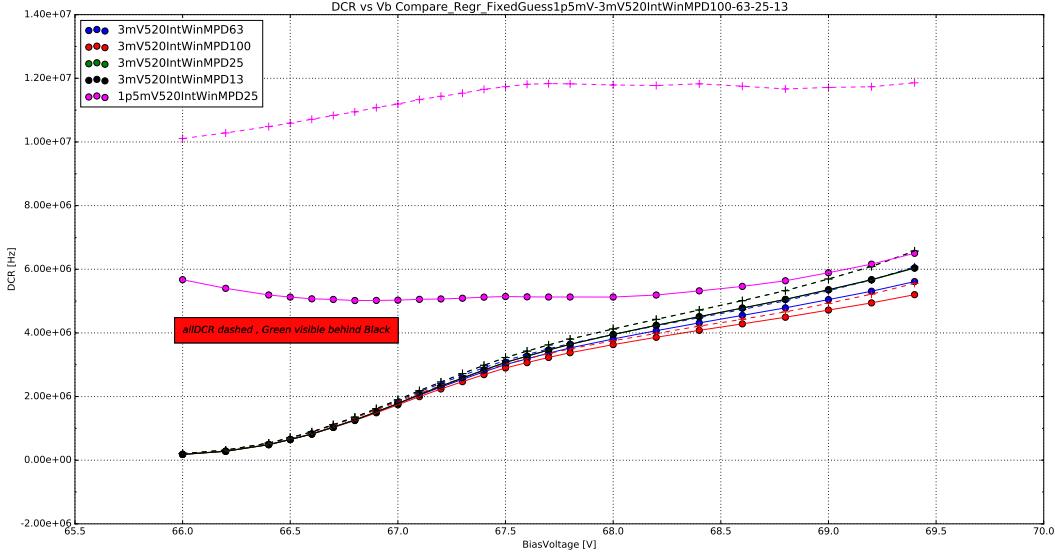


Figure 8: The difference between 4 minimum peak distance windows, in time-bins, during the peak detection. The dashed lines are the Dark Count Rates considering all recorded events, forming an upper limit. In pink, the effect of a different peak detection threshold is shown.

## 5 Results

### Preliminary results chapter

In this chapter, I will list the final results per device in a list of measured criteria. At the end I will conclude with a comparison between devices and to the results from other groups. Overview short table of measured devices LIST?

Manufacturer	pixel size	cell size	coating	connection	shaper	pre-Amp
HPK S12642-1616PA-50	$3\text{mm}^2$	$50\mu\text{m}$	epoxy??	TSV	Iteration 1	CHEC-S buffer
HPK LCT5 S13360-6050CS	$6\text{mm}^2$	$50\mu\text{m}$	silicon resin	wire-bonds	Iteration 2	13V
HPK LCT5 XXXXXXXXXX	$6.915\text{mm}^2$	$75\mu\text{m}$	silicon resin*	wire-bonds(*)	Iteration 3	8V
HPK LCT5 LVR XXXXXX	$6\text{mm}^2$	$50\mu\text{m}$	silicon resin*	TSV(*)	Iteration X	13V
SensL FJ60035	$6\text{mm}^2$	$35\mu\text{m}$	glass	TSV	no	15V

Figure 9: List of SiPM devices which results are presented in this paper. \*unsure

### 5.1 Hamamatsu S12642-1616PA-50 $50\mu\text{m}$ 3mm

The Silicon Photomultiplier by Hamamatsu Photonics designated S12642-1616PA-50 is a 3 mm by 3 mm device. The array uses the through-silicon-via technology, meaning there are no wire-bonds present, the electrical connection is realised through the silicon-body. The pixels are coated with a thin film of epoxy resin(REMOVED according to PRODUCTSHEET). One array consists of 256 pixels, 4 of which are electrically tied together to form a 6mm by 6mm superpixel respectively. This practise is necessary for the pre-production camera CHEC-S, because the focal plane is mechanically designed to house 64 6mm<sup>2</sup> pixels, connected to the TARGET modules. Furthermore I expect this to have an influence on my results due to electrical crosstalk, but this is only of minor concern due to the following. My measurements of the CHEC-S tile concentrate on the array as an as-is device. This means all results, influenced by external factors outside the actual Silicon Photomultipliers physics, are valid on the assumption, that the way I was conducting the measurements is the way the Photomultiplier will later be incorporated into the camera. On that ground, deviations of my results from the results of other groups and the manufacturer itself are expected. To clarify this further, I expect, for example, that the tests done at Hamamatsu Photonics where conducted on a single 3mm by 3mm pixel, not an array of 256 pixels, where 4 are tied together. Also divergence of shaping and amplification electronics between the groups will result

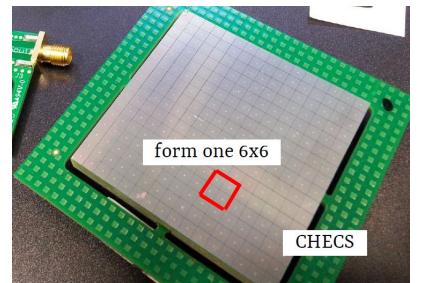


Figure 10: CHEC-S tile

in some differences. For this test, the CHEC-S tile is connected to the CHEC-S buffer, supplied with  $\pm 4$ V, where the signal is amplified. This signal in turn is then shaped via the CHEC-S shaper, iteration (XXXXXXXX in devices chapter) by Luigi Tibaldo. This is done in order to lower the unshaped pulse from a FWHM in the 100s ns to 10ns. This whole amplification and shaping chain is simulating later usage in the TARGET modules. I conducted the measurements multiple times on different pixels of the CHEC-S tile.

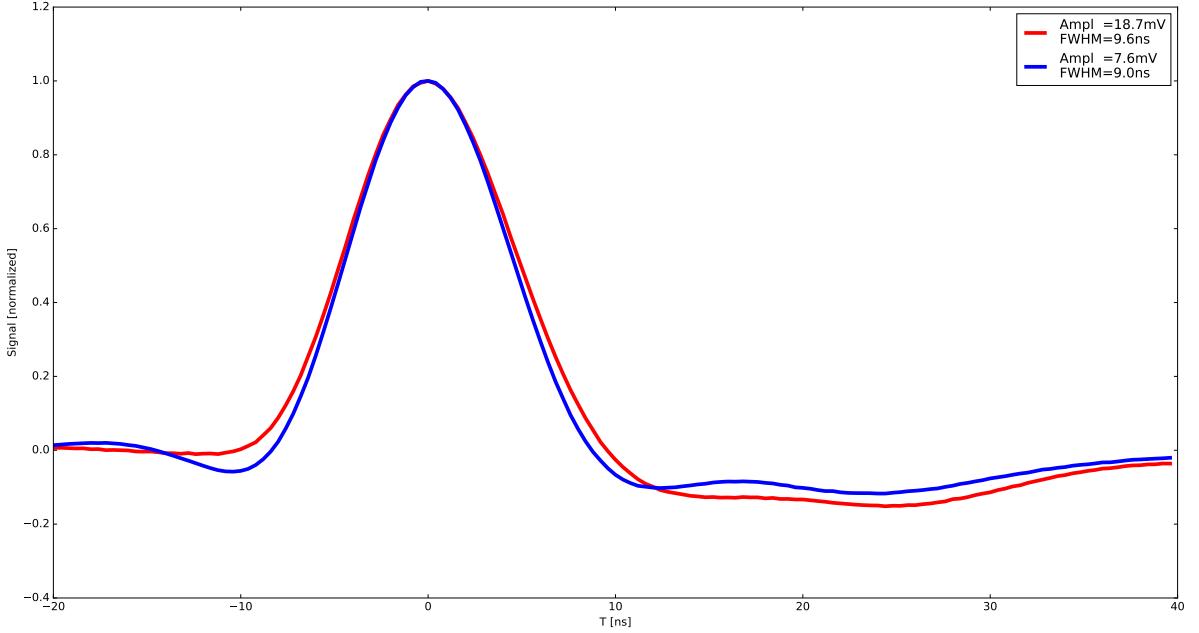


Figure 11: The average pulse shape of the 1photoelectron in blue and the 2photoelectron pulse in red of HPK S12642 at  $25^\circ$  C and 67.8V, which is around the proposed operating point. Both pulses are averaged over  $\gg 1000$  events and normalized to illustrate possible differences in pulsedshape resulting from the utilized shaping electronics. Both pulses have a FWHM of around 10ns and are nearly free of ringing. The resulting average amplitude of the 1p.e. pulse is later used to calculate the Gain in [mV/p.e.] instead of [V\*IntWin] by cross-referencing the 1p.e. amplitude at multiple bias-voltages.

### 5.1.1 Gain

As described above, the average pulse shape fig(11) is used to convert the relative gain from the analysis procedure to an absolute gain in sensible units. This is necessary, because the analysis aims to use pulse-area rather than -height. In Figure (???) (left) the relative gain is shown, the right side shows the gain after conversion. A lower gain with increasing temperature is expected and described in detail in the chapter (physics of SiPMs i guess). In short, increased lattice movement due to higher temperature hinders photoelectron transport. The effects visible at extreme bias-voltages at both ends are analysis related. The gain of a SiPM is expected to be linear over bias-voltage at a constant temperature. In the lower regime at  $V_b = 66.5\text{V}$  my analysis method struggles to pick up pulses, because of the low gain compared to the noise. Depending on the chosen peak-finding threshold, I expect the analysis to interpret noise peaks as 1p.e. peaks at an increasing rate, the lower the overvoltage is. This is visible in the sudden break in linearity at  $30^\circ\text{C}$  and  $35^\circ\text{C}$ , where the gain is almost in a plateau, due to this effect. At the highest bias-voltages the influence of the noise is similar. The point at  $V_{ov} = 5\text{V}$ , which is way over the proposed point of operation at  $V_{ov} = 3\text{V}$ . The same threshold is again counting noise peaks as 1p.e. peaks, but due to the abundance of 1p.e. pulses this just results in an apparent lowering of the gain.

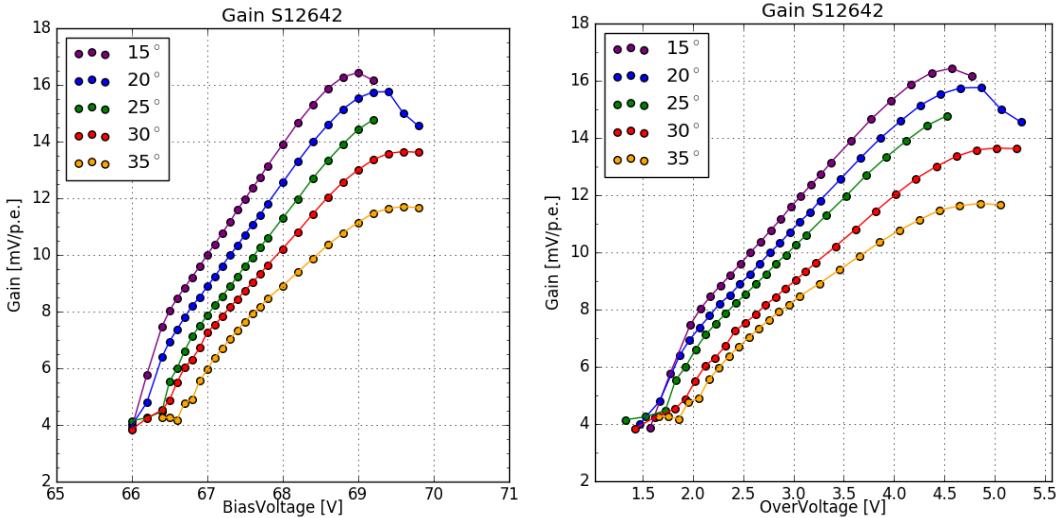


Figure 12: Gain of the HPK S12642 pixel, plotted against over-, bias-voltage and temperature.

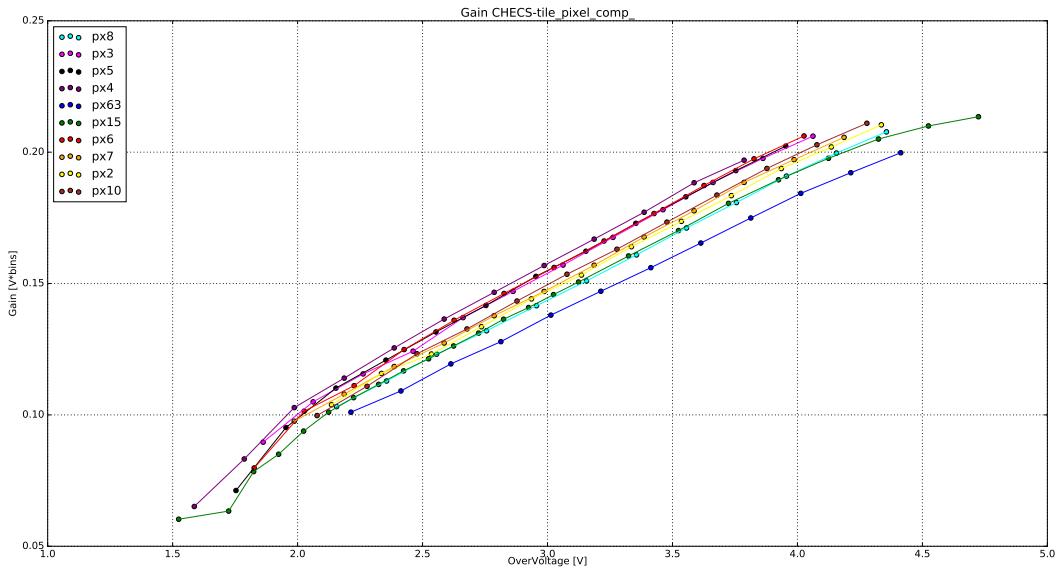


Figure 13:

### 5.1.2 Dark Count Rate

I expect the Dark Count Rate to increase with temperature, which is the case fig(14). I also expect it to follow a nearly linear progression, a sudden turn-up or turn-down of the Dark Count Rate would be analysis related. The turn-up at a certain point is visible in Figure (14), particularly for 15° C (purple) and 20° C (blue) respectively. At 15° C and an Overvoltage of 4V, the Dark Count Rate starts to deviate from the previously linear behaviour. It starts to rise more rapid than before, which I can attribute to the fact, that the Optical Cross Talk at that point is very high; higher than 50% fig(16) (left). I suspect that I do not reach this critical point for the higher temperatures of 25° C (green) and 30° C (red), so the effect is barely, if not at all visible. At 35° C (yellow) I suspect my analysis is not able to count every pulse, due to the high rate of 9-10 MHz. A majority of the pulses overlapping each other and being counted as a 2p.e. event rather than 2 1p.e. events would reduce the Dark Count Rate significantly. At this point, heating of the Silicon Photomultipliers surface due to the high rate could also affect the Dark Count Rate through shifting the temperature slightly upwards, away from 35° C . So that the Dark Count Rate declared at 35° C is in reality the rate at higher temperatures.

At the lower end of the bias-voltage range, I suspect, that a major part of the found 1p.e. pulses are actually noise related. So the Dark Count Rate changing to a plateau is expected. This is also due to the fact, that my measurements are done with a fixed bias-voltage range. Due to the increase of the breakdown-voltage with rising temperature, part of the measured bias-voltage range being a very low over-voltage, attributes to this effect. In order to reliably measure beyond an overvoltage of 2.5V in the lower range, the noise would need to be improved.

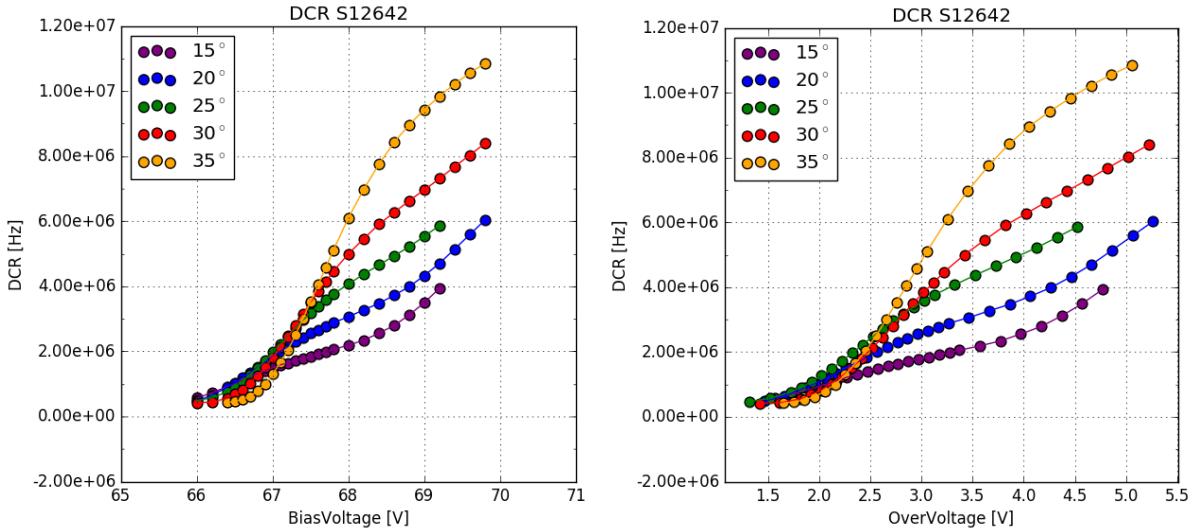


Figure 14: Dark Count Rate of the HPK S12642 pixel, plotted against over-, bias-voltage and temperature.

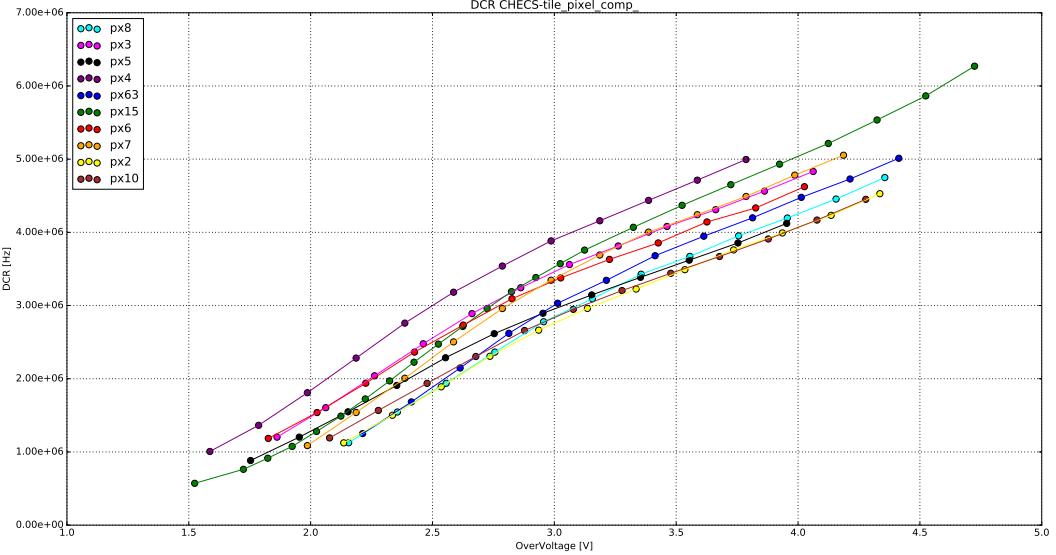


Figure 15:

### 5.1.3 Optical Cross Talk

The Optical Cross Talk should be linear and independent from temperature. This is confirmed for HPK S12642. Minor deviations from that are probably due to slight errors in the breakdown-voltage calculation from the gain regression line. The deviation of 30° C and 35° C below an over-voltage of 2V stems from the way the gain regression line is used to calculate both Dark Count Rate and Optical Cross Talk. At higher temperatures the lower voltage range is dominated by noise, so using the gain regression line to calculate the Optical Cross Talk at those low voltages leads to the visible effect of the first few datapoints of 30° C and 35° C. The deviations between the different groups results at 25° C (green) are caused by 4 major contributions. Firstly the difference in the tested device. While I take measurements on 4 3mm by 3mm pixels electrically tied together, the way the device will later be implemented into CHEC-S, the groups in the US and Hamamatsu Photonics are likely to run tests on 1 3mm by 3mm pixel only. Secondly I suspect a difference in amplification and shaping electronics. The measurements I conducted as well as the measurements of Leicester are done with the same shaper and buffer configuration. The difference here is, thirdly, my measurements are done with dark counts only, while measurements in Leicester are conducted with a pulsed light source and reading out timed windows. This causes the results from Leicester to be difficult to compare against, their surface temperature of the SiPM is likely much higher than 25° C, and thus, a misinterpreted breakdown-voltage at 25° C causes a shift of the Optical Cross Talk to the right. Lastly the difference in actual data taking and analysis procedure must be mentioned, also this is only of minor concern, as we will see with other measured devices.

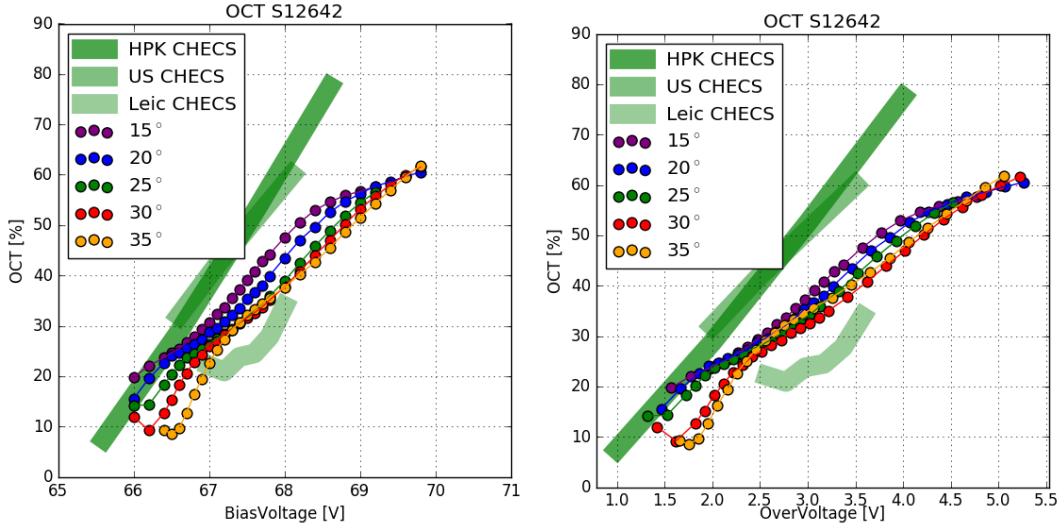


Figure 16: Dark Count Rate of the HPK S12642 pixel, plotted against over-, bias-voltage and temperature.

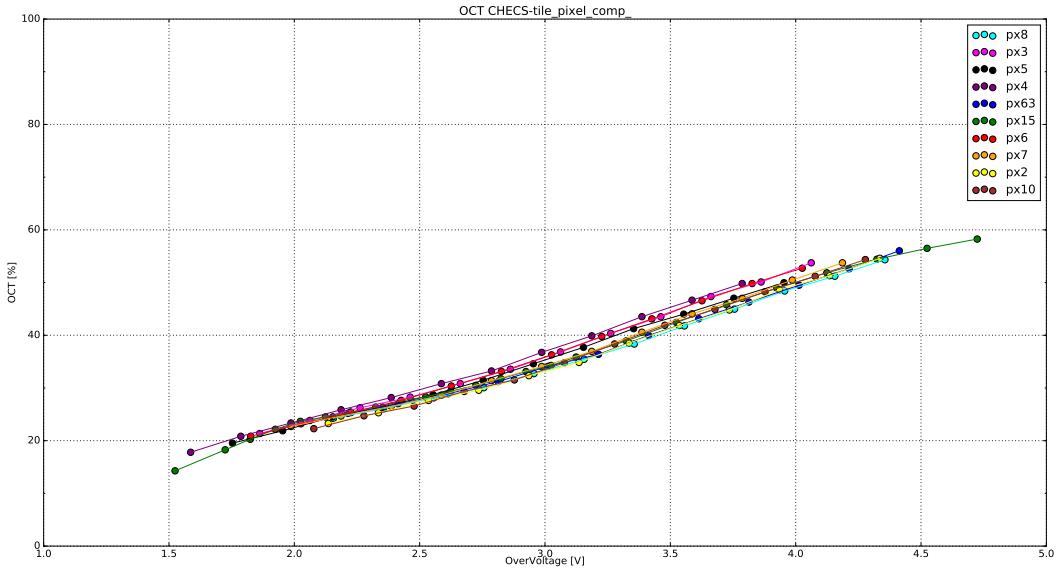


Figure 17:

## 5.2 Hamamatsu LCT5 50 $\mu$ m 6mm

The Silicon Photomultiplier designated HPK S13360 6050CS is an LCT5, meaning Low Cross Talk 5th iteration device from Hamamatsu Photonics. It is one of the most promising candidates for later usage in CHEC-S. It has a pixelsize of  $6\text{mm}^2$  consisting of 14400 cells with a cellsize of  $50\mu\text{m}$ . Tests are done with a single pixel only, in contrast to measurements done on S12642. It is mounted on a ceramic chip and coated with a silicon resin that is UV-transparent. Wire bonds supply the electrical contact. A similar, but not tested, device from the same generation uses through-silicon-via (TSV) technology, realising electrical connection through the silicon, allowing a tighter fit of the cells, with minimal dead-space. The layout of the single pixle test device made external amplification necessary. I used a minicircuits PreAMP Sn XXXXX, which was supplied with 13V during this test. Shaping of the pulse is conducted by a modified CHEC-S shaper, specifications can be found in chapter 2.5. Even though the pulse shape fig(19) makes the pulses appear much harder to analyse, the possibility of events occurring during the ringing window. This assumption proved untrue, due to the devices low Dark Count Rate and Optical Cross Talk.

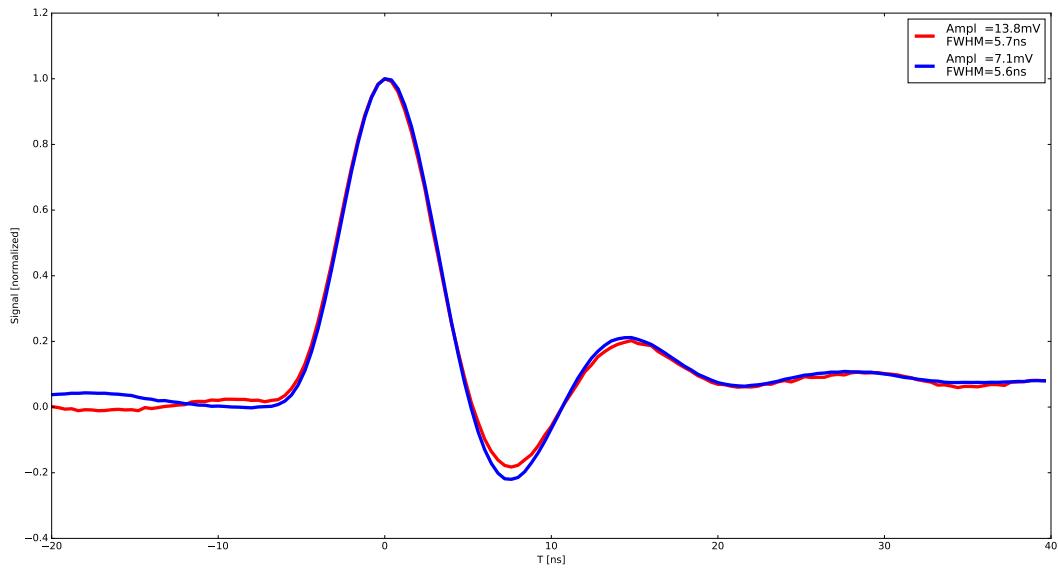


Figure 19: The average pulse shape of the 1photoelectron in blue and the 2photoelectron pulse in red of HPK S13360 6050CS at 25° C and at point of operation. Both pulses have a FWHM of around 5ns and ring for approximately 20ns with an undershoot of 20%.

### 5.2.1 Gain

The gain of the LCT5 50 $\mu\text{m}$  6mm device is clearly linear with some minor outliers at 30°C. The same effect as with S12642 is visible at 35°C, again counting noise peaks as 1p.e. peaks, resulting in an apparent lowering of the gain and the slope changing over into a plateau. In Figure(38)(left) the gain is shown, plotted against over-voltage. It is still dependant on temperature, but due to reliable breakdown-voltage calculation, the spread is much smaller than, if plotted against bias-voltage. The same conversion is done to transform relative gain into an absolute gain with sensible units.

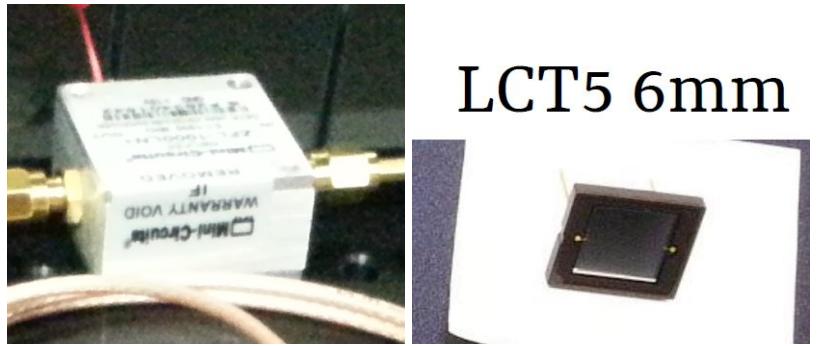


Figure 18: HPK S13360 6050CS pixel / PreAMP pic will be updated

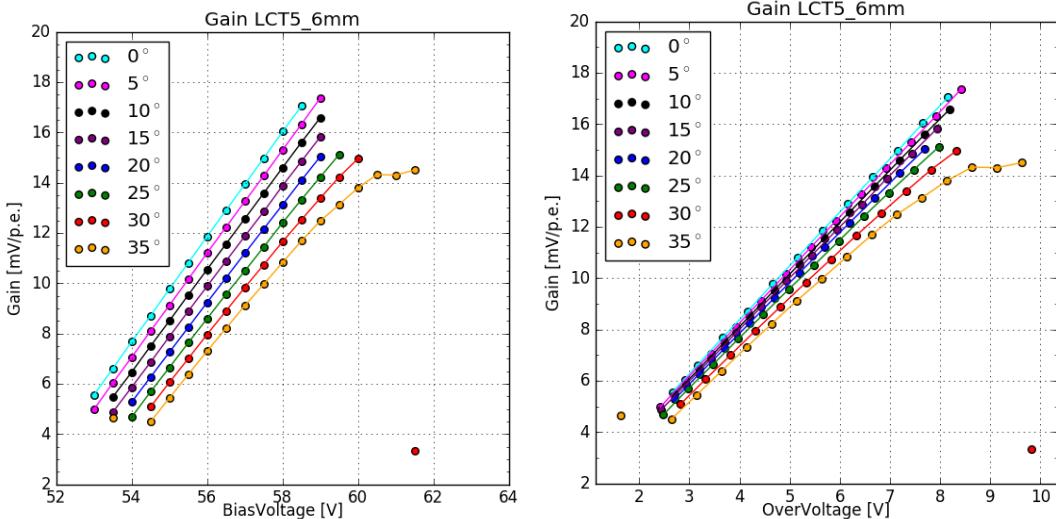


Figure 20: Gain of the HPK S13360 pixel, plotted against over-, bias-voltage and temperature.

### 5.2.2 Dark Count Rate

The Dark Count Rate of two similar HPK S13360 devices is shown in Figure(21). The bars show the difference between the two devices, the results of one device is used as a reference, while the deviation is illustrated with the filled bar. The Dark Count Rate of HPK S13360 follows the expected behaviour, mostly linear in the significant range and rising with increasing temperature. Below an over-voltage of 2.5V my analysis struggles, I suspect the gain to be too low for my analysis to pick up pulses. Thus the regression line calculation is unreliable in this range. The turnup at high over-voltages is most prominent at 0°C(teal) after an over-voltage of 9V. This is also the point where the Optical Cross Talk rises very rapidly.

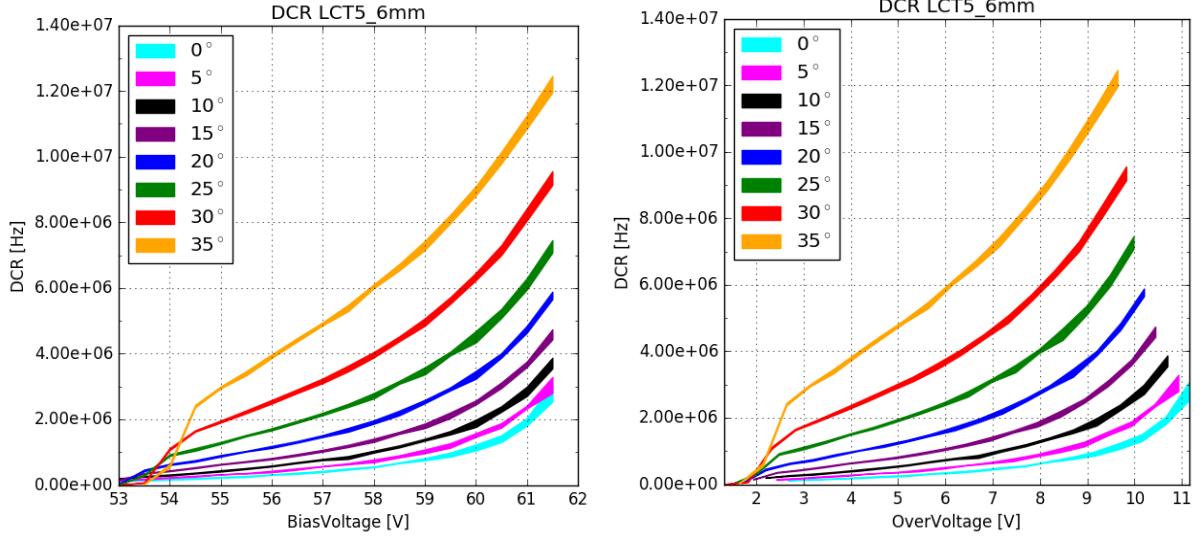


Figure 21: Dark Count Rate of the HPK S13360 pixel, plotted against over-, bias-voltage and temperature.

### 5.2.3 Optical Cross Talk

Compared to measurements on HPK S13360 done at the Nagoya University Japan 21 (faded green bar), I see a very strong correlation of the Optical Cross Talk in the over-voltage range between 2.5V and 9V. The Optical Cross Talk in this range is linear and independent from temperature, with minor deviations attributed to the breakdown-voltage calculation from the regression line, causing the horizontal shift. In contrast to my technique, using only dark counts, the measurements at Nagoya University followed a pulsed light source approach, reading out a time-window after the laser incident. Deviations below an over-voltage of 2.5V are expected, they are very likely caused by the regression line calculation being unreliable in this range due to the analysis method struggling to pick up pulses using dark counts. Above an over-voltage of 9V, which is also the point of the turnup of the Dark Count Rate, the Optical Cross Talk is no longer linear and the deviation from the results of Nagoya University increase very rapidly. I suspect the rapid increase in both Dark Count Rate and Optical Cross Talk to be caused by the over-voltage reaching ranges, where interpretation of noise as a 1p.e. pulse becomes more likely. This, joint together with the usage of the Mini-Circuits amplifier supplied with 13V, makes false interpretation of noise as pulses even more likely. I suspect these two reasons in conjunction are responsible for both, the sudden rise of the Dark Count Rate as well as the deviation of the Optical Cross Talk from linearity and the results of Nagoya University, above over-voltages around 9V. In summary, the correlation between the two measurements, conducted by two different methods of data acquisition and analysis, is evident.

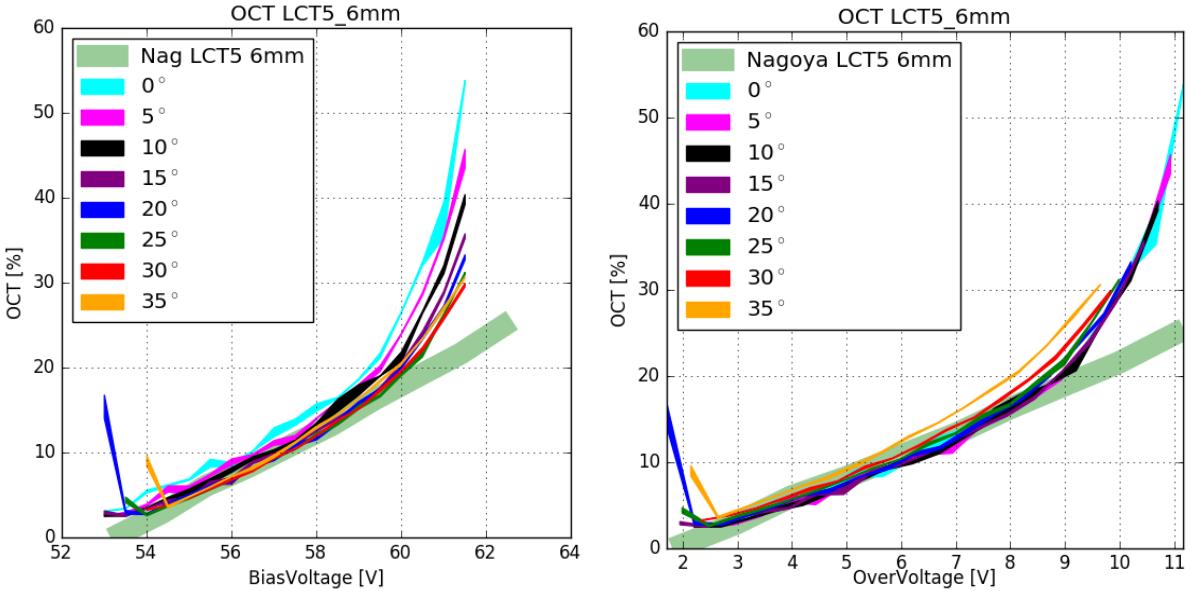


Figure 22: Optical Cross Talk of the HPK S13360 pixel, plotted against over-, bias-voltage and temperature.

### 5.3 Hamamatsu LCT5 75 $\mu$ m 7mm

XXXXXXXXXXXX is a larger LCT5 prototype Silicon Photomultiplier of the same design as S13360-6050CS. With an increase in cellsize to 75 $\mu$ m, the device gains a higher fill-factor than 50 $\mu$ m devices. The pixelarea is also expanded to 6.915mm<sup>2</sup>, which will result in a larger FoV of GCT, see chapter (list of devices etc) !(maybe tom armstrongs simulations)!. Since it is a prototype device, there is limited data from datasheets. The ID number suggests, that it is also a wire-bond device with a UV-transparent silicon-resin coating. It is also a single pixel test device, so external amplification is necessary. I used the same minicircuits PreAMP Sn XXXXX, supplied with 8V during this test. The signal is also shaped by a differently modified CHEC-S shaper, which results in a pulse shape similar to S12642, but with a much lower amplitude.

## LCT5 7mm



Figure 23: HPK LCT5 7mm pixel

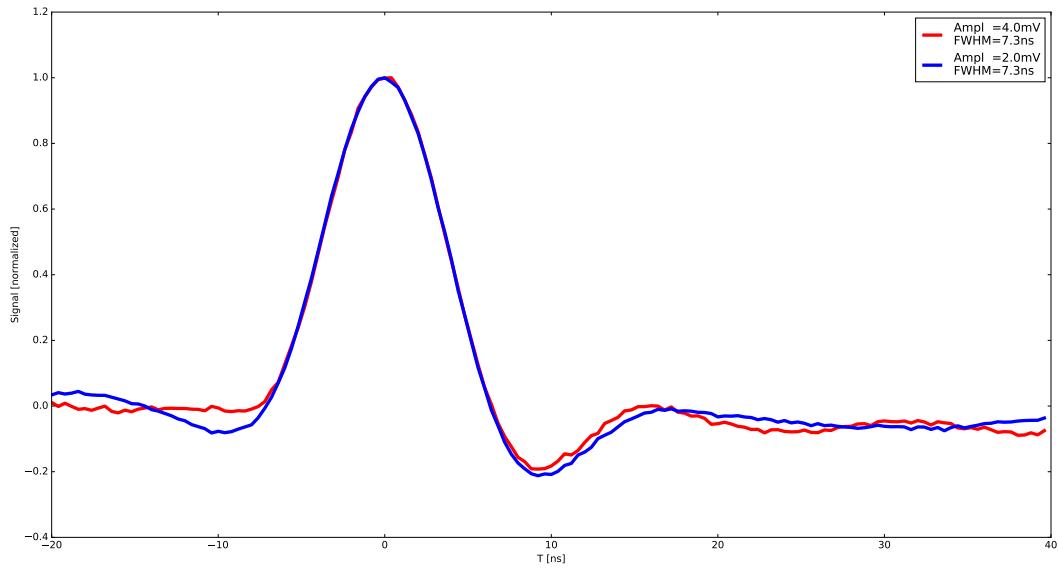


Figure 24: The average pulse shape of the 1photoelectron in blue and the 2photoelectron pulse in red of HPK LCT5 7mm at 25° C and at point of operation. Both pulses have a FWHM of around 7ns and an undershoot of 20%, with no ringing.

### 5.3.1 Gain

Figure(25) shows the gain of the LCT5 7mm device. Two sets of measurements are done for 25°C to extend the measured range. The first set of measurements covers the lower over-voltage range, where the low gain makes external amplification necessary. The same mini-circuits PreAMP (SNXXXXXXX) supplied with 8V was used during this test. I chose the lowest possible amplification of the PreAMP, so that reaching the point of saturation of the oscilloscope is as late as possible as the over-voltage rises. Saturation of the oscilloscope occurs due to the possibility of generating very large p.e. ( $>10$ p.e.) events at the higher over-voltages, which are saturating the input. Joint together, the LCT5 7mm device and the mini-circuits PreAMP at 8V reach this point at an over-voltage of  $\sim 6$ V. In Figure(25) the results from the lower range measurement are displayed as the lower-range green line extending between an over-voltage of 1.6V to 5.4V.

The configuration for the second test removes the PreAMP from the setup, which makes the lower over-voltage range unaccessible, but extends the range to higher over-voltages. This configuration reaches the point of saturation at an over-voltage of  $\sim 8$ V. The higher range measurement results are displayed as the second green line (25°C) extending from 3.4V to 7.2V over-voltage in Figure(25). There is a clearly visible overlap of the two measurements between  $\sim 3.4$ V and  $\sim 5.4$ V. It also seems, that the gain dependency on temperature is reversed. While for all other devices, the gain lowers with rising temperatures, the LCT5 7mm device seems to show inversed behaviour. This inverse behaviour is caused by the calculation of the breakdown-voltage from the gain-regression line, with this and the bias-voltage, the over-voltage is calculated, causing a horizontal shift. Plotting the gain versus bias-voltage shows the expected behaviour.

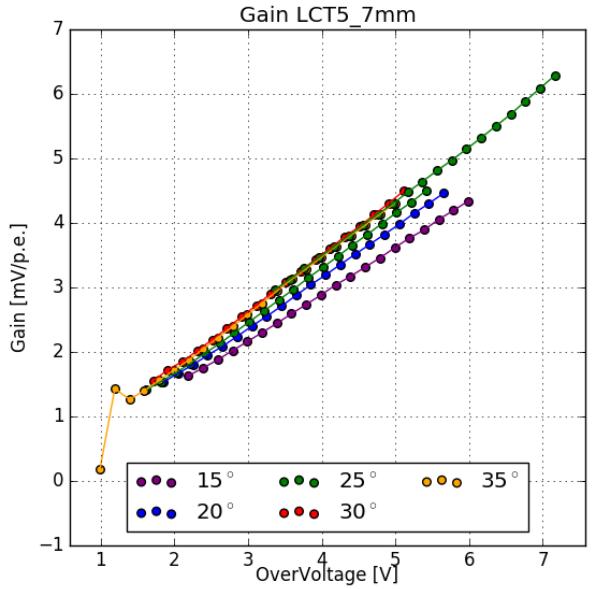


Figure 25: Gain of the HPK LCT5 7mm pixel

The configuration for the second test removes the PreAMP from the setup, which makes the lower over-voltage range unaccessible, but extends the range to higher over-voltages. This configuration reaches the point of saturation at an over-voltage of  $\sim 8$ V. The higher range measurement results are displayed as the second green line (25°C) extending from 3.4V to 7.2V over-voltage in Figure(25). There is a clearly visible overlap of the two measurements between  $\sim 3.4$ V and  $\sim 5.4$ V. It also seems, that the gain dependency on temperature is reversed. While for all other devices, the gain lowers with rising temperatures, the LCT5 7mm device seems to show inversed behaviour. This inverse behaviour is caused by the calculation of the breakdown-voltage from the gain-regression line, with this and the bias-voltage, the over-voltage is calculated, causing a horizontal shift. Plotting the gain versus bias-voltage shows the expected behaviour.

### 5.3.2 Dark Count Rate

The behaviour of the Dark Count Rate of the HPK LCT5 7mm device is shown in Figure(26) and is as expected, in contrast to the behaviour of the gain of LCT5 7mm, as discussed in section 5.3.1. It follows a linear progression in the relevant range and increases with rising temperature. I suspect the over-voltage range above  $\sim 2.5$ V to be relevant. The extended range measurement at  $25^{\circ}\text{C}$  confirms this behaviour. LCT5 7mm shows a linear Dark Count Rate over an over-voltage range of 4V. The faded green bar in Figure(26) shows results from measurements undertaken by the Department of Physics and Astronomy at the University of Catania. Those measurements were conducted on the exact same device, which is an important point, but with a different method of data acquisition and data analysis. LITTLE MORE DETAIL IN PROGRESS. The correlation between the two experiments is evident, although there are differences in the acquisition and analysis process. This is further proof for the relevancy of my analysis.

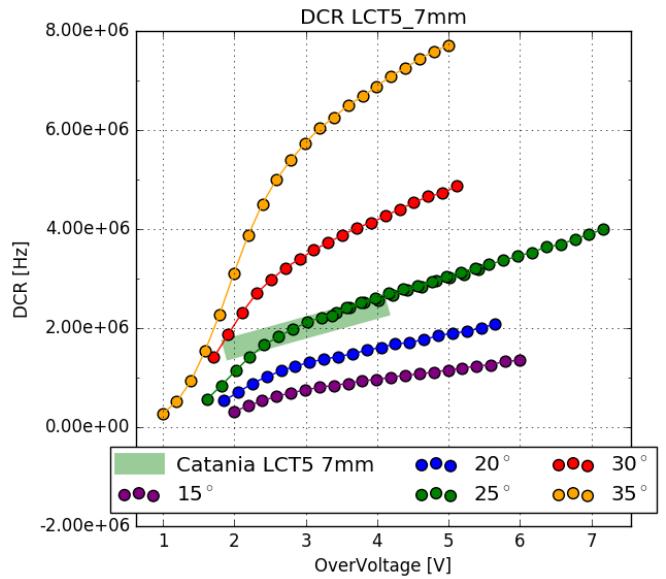


Figure 26: Dark Count Rate of the HPK LCT5 7mm pixel

### 5.3.3 Optical Cross Talk

The Optical Cross Talk is expected to be linear and independent from temperature. This is the case in the, in section 5.3.2 established, relevant over-voltage range of above  $\sim 2.5\text{V}$ . Minor deviations are attributed to the calculation of the breakdown-voltage from the gain-regression line. The over-voltage is calculated from the former and the supplied bias-voltage, which in turn causes a slight horizontal shift. With that, comparing my results to the measurements from the University of Catania shows a strong correlation. Keeping in mind, that the process of data acquisition and analysis is different for both measurements further proofs my analysis valid.

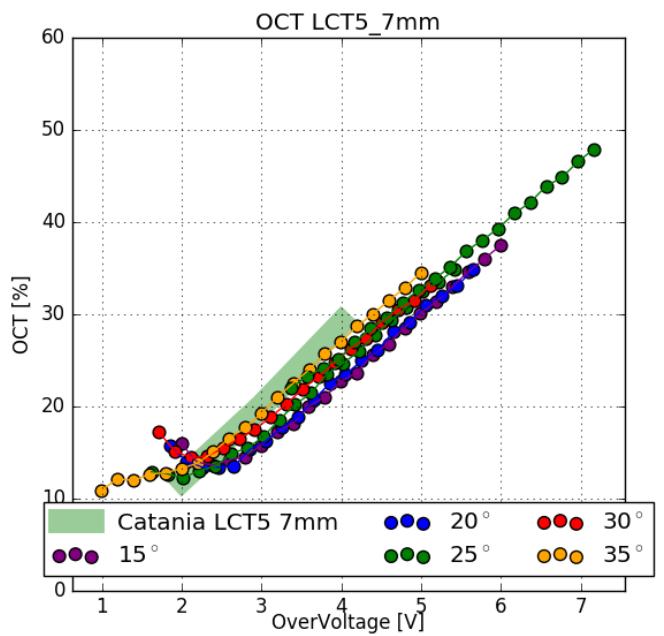


Figure 27: Dark Count Rate of the HPK LCT5 7mm pixel

## 5.4 Hamamatsu LVR $50\mu\text{m}$ 6mm

The Silicon Photomultiplier by Hamamatsu Photonics with the designation 6050HWB-LVR-LCT is a special prototype of the LCT5 design. LVR is an abbreviation of Low Voltage Range, meaning the device is meant to be operated at much lower operation voltages than other LCT5 devices. It has the same physical size as an LCT5  $50\mu\text{m}$  6mm device (S13360 ??), a pixel size of 6mm pixel with a cell-size of  $50\mu\text{m}$ . The recommended point of operation however is  $\sim 15\text{V}$  below that of the S13360 device, specifically at 40.2V(LVR) instead of 54.7V (S13360). The unshaped signal is similar to other LCT5 devices, therefore using the same modified CHEC-S shaper is feasible in this case. After that the signal is amplified with the same mini-circuits PreAMP SNXXXXX supplied with 8.5V.

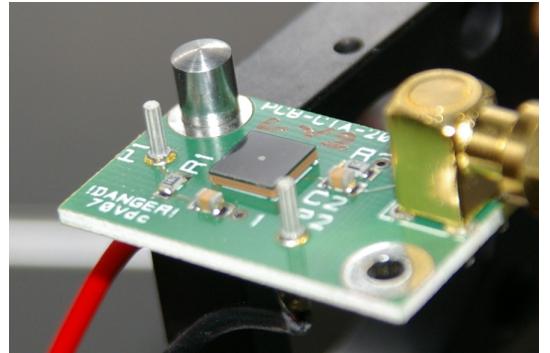


Figure 28: HPK LVR 6mm pixel

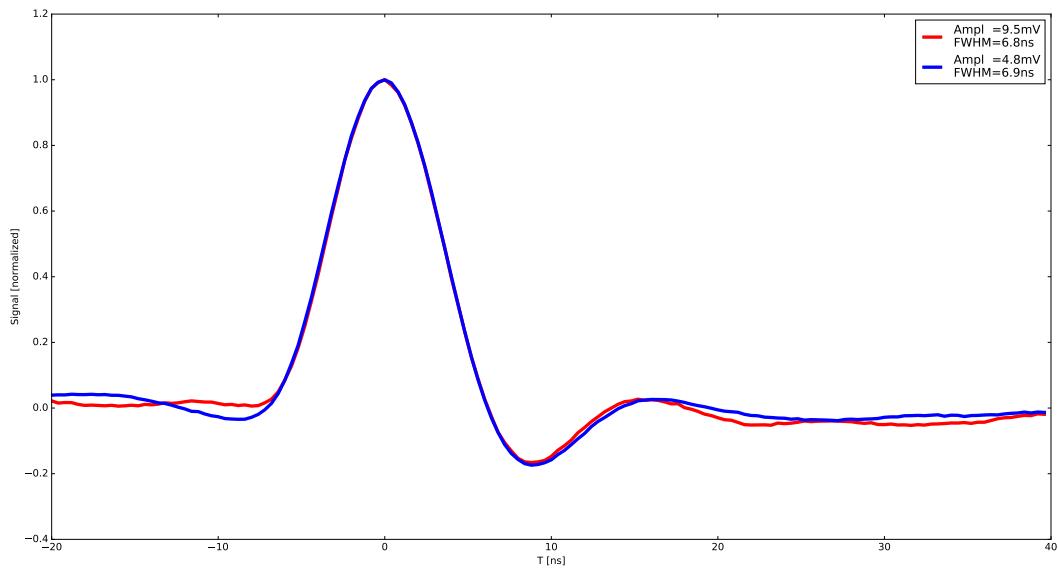


Figure 29: The average pulse shape of the 1photoelectron in blue and the 2photoelectron pulse in red of HPK LVR 6mm at 25° C and at point of operation. Both pulses have a FWHM of around 7ns and an undershoot of 20%, with no ringing.

### 5.4.1 Gain

Figure(30)(left) shows the gain of the LVR 6mm device. It is, as expected, linear over a long range. The flattening of the slope to a plateau shape in the lower over-voltage range, is caused by the analysis being unable to identify peaks lower than the set threshold. Only taking into account the linear region, limits the range, where the results are relevant to an over-voltage range of  $\sim 2.5$ V. Saturation of the oscilloscope in this range is not visible, but a check with a more expanded range revealed, that the point of saturation of the oscilloscope is at an over-voltage of  $\sim 5$ V. The apparent overlap of the gain, when plotted against over-voltage, is based on the calculation of the breakdown-voltage being very reliable due to the large linear range. Plotted versus bias-voltage Figure(30)(right) the expected behaviour of the gain, lowering with increasing temperature, is visible.

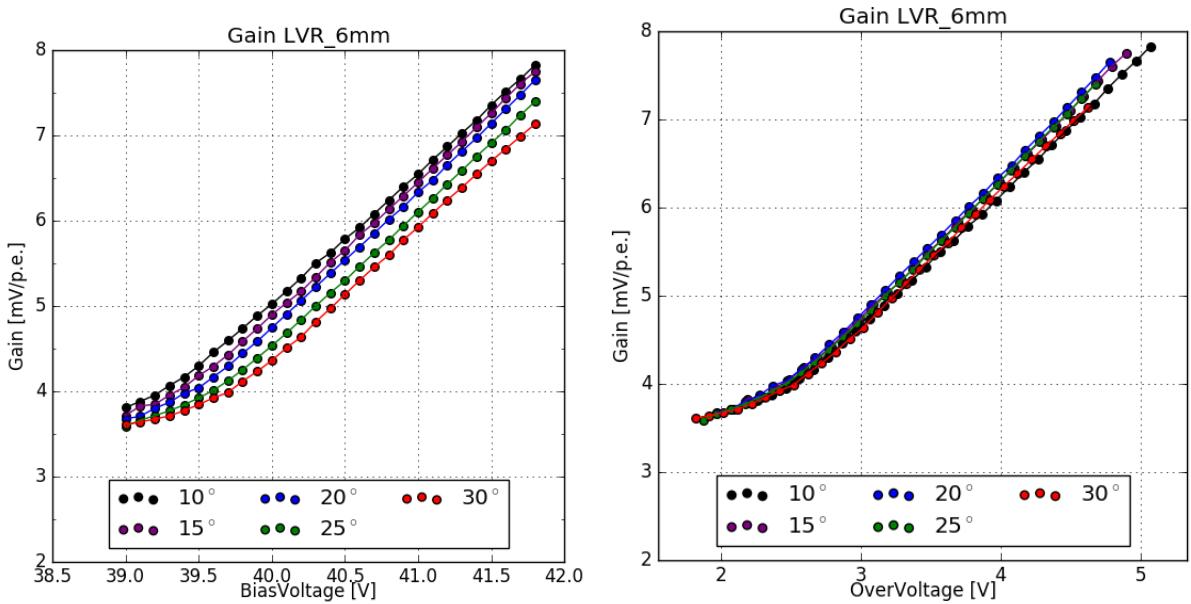


Figure 30: Gain of the HPK LVR 6mm pixel

## 5.4.2 Dark Count Rate and Optical Cross Talk

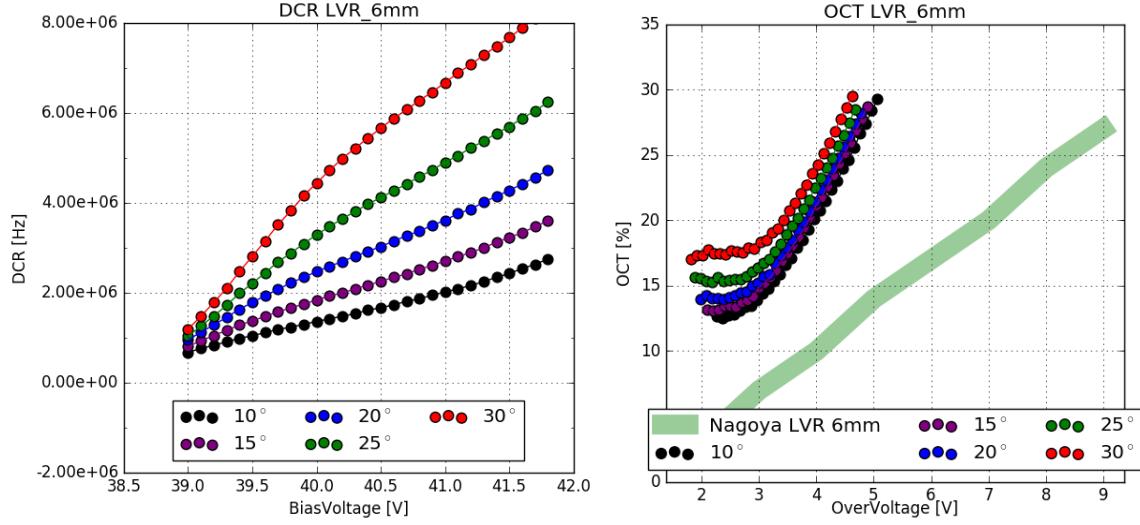


Figure 31: Dark Count Rate and Optical Cross Talk of the HPK LVR 6mm pixel

The Dark Count Rate, taking into account only the relevant over-voltage range of  $>\sim 2.5\text{V}$  seems to correlate with the results form the University of Nagoya. But the resulting Optical Cross Talk is very high compared to results from the University of Nagoya, which also cover a much wider range. Only taking into account the previously established relevant over-voltage range of  $>\sim 2.5\text{V}$ , the resulting Optical Cross Talk is a factor of 2 higher. This uncertainty is a contrast to results from previous devices, where strong correlations between different groups and measurement techniques are evident. I suspect, that the device examined by me and the device present at Nagoya University are slightly different prototypes.

## 5.5 SensL FJ60035 6mm $35\mu\text{m}$

The Silicon Photomultiplier by SensL with the designation FJ-60035 is also a candidate device for use in CHEC-S. It is also a 6mm device, but with a much smaller cellsize of  $35\mu\text{m}$ , using the TSV technology, so there are no wire-bonds present. This results in 22292 cells on a single pixel with a fill-factor of 75%. It is coated with plain glass. The recommended point of operation is around 30V bias-voltage, lower than that of the HPK LVR prototypes. The device is, by the manufacturer, pre-mounted on a printed circuit board, called a test array. This test array contains a fast output, that directly couples to the cells, and a slow output, conventionally read out via the quench resistor. For the conducted tests, I used the fast output, which made amplification with the same mini-circuits PreAMP SNXXXXX supplied with 12V necessary. The SensL device was the first device measured, therefore the analysis procedure used was an older iteration compared to the procedure for the Hamamatsu devices.

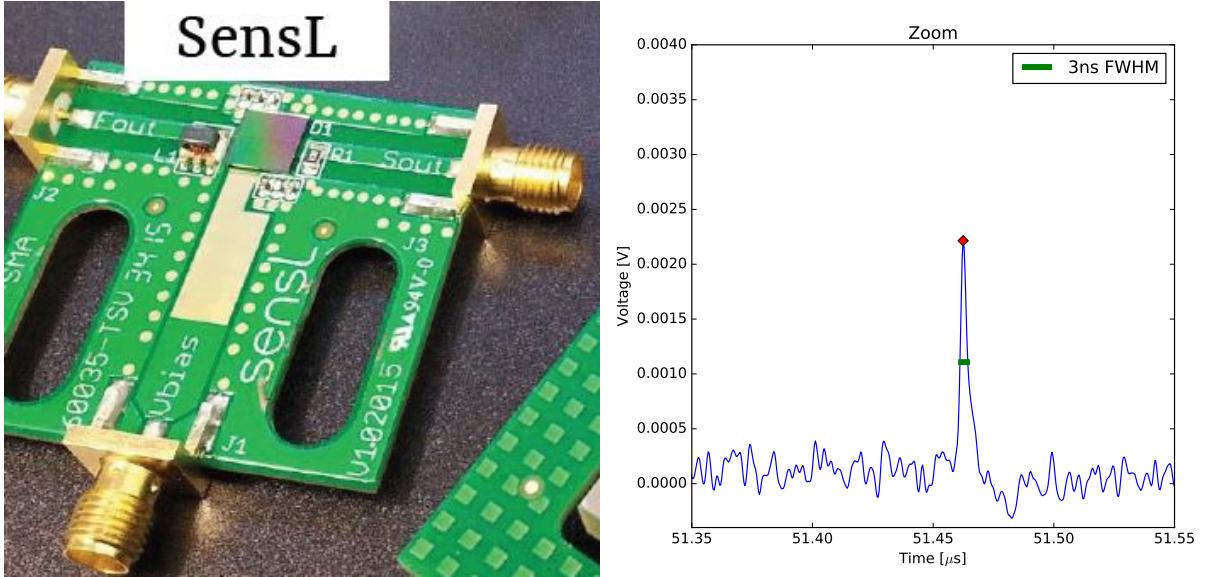


Figure 32: SensL Test Array and pulse shape at bias-voltage = 29V0

### 5.5.1 Gain

Evaluating the SensL pulse area spectra showed the 1 p.e. position and  $\Delta$ p.e. overlapping, so using the older analysis iteration introduced no error when evaluating the gain of the SensL device. It is clearly linear over a wide temperature range from -5°C to 35°C over an over-voltage ranging from 2V up to 8V. When plotted versus over-voltage the spread of the gain is even tighter, while still following the expected behaviour of decreasing with increasing temperature.

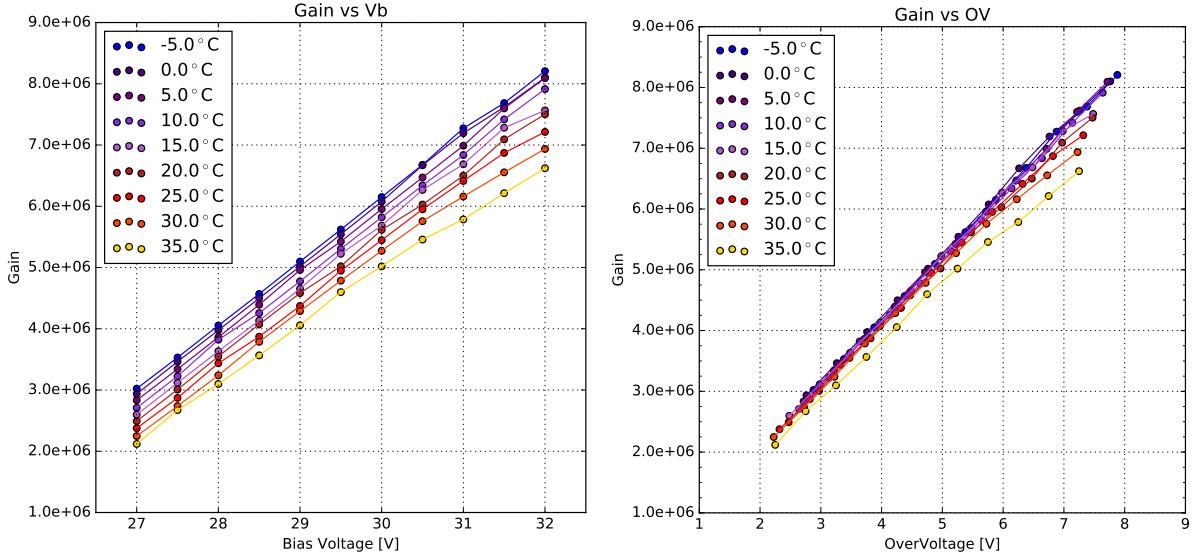


Figure 33: Gain of the SensL FJ-60035 test array

### 5.5.2 Dark Count Rate and Optical Cross Talk

The Dark Count Rate also shows the expected behaviour. At very low temperatures the changes in rate over the over-voltage range is minimal. Increasing the temperature shows a rapid increase in thermally induced dark counts. The Optical Cross Talk on the other hand is independent of the device temperature, also as expected.

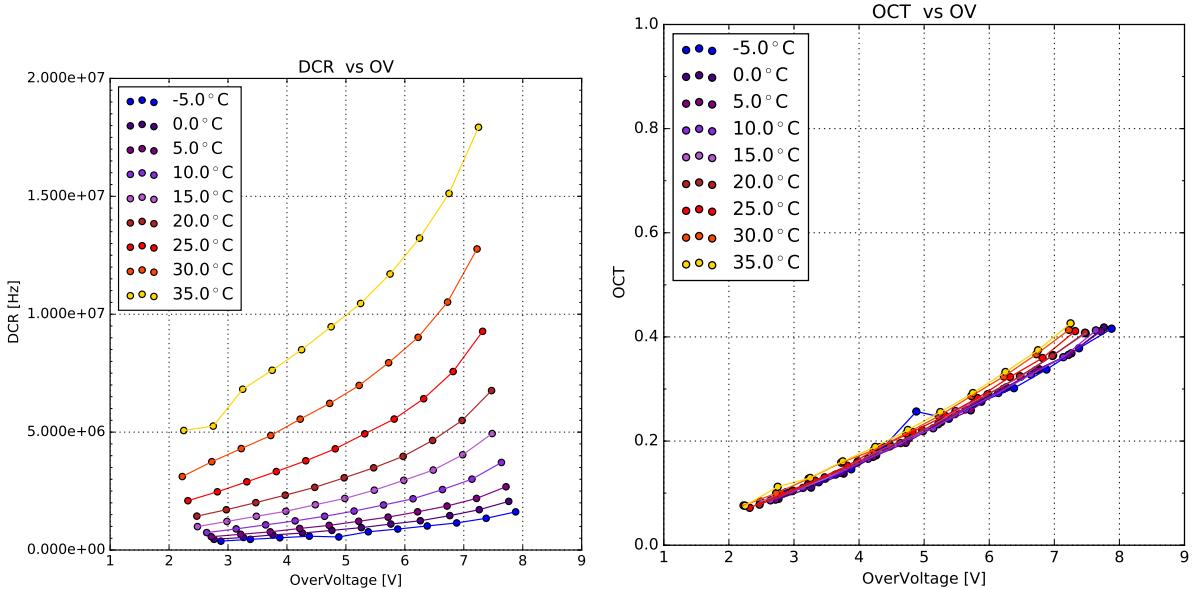


Figure 34: Dark Count Rate and Optical Cross Talk of the SensL test array

## 6 Comparison

A comparison of the performance of all devices is the significant step for choosing the Silicon Photomultiplier later to be used in CHEC-S. In order to do this, all measured characteristics are compared versus over-voltage. Operation of the CHEC-S camera in GCT will come down to a decision between two operational points. The first point will be marked by an Optical Cross Talk of under 15%. Every other attribute of the Silicon Photomultiplier at this over-voltage is then compared. This point will trade off precision for efficiency, a lower Optical Cross Talk makes real event detection easier, on the other hand, a lower Photon Detection Efficiency may forfeit a lot of data.

The second point of operation is marked at the highest achievable Photon Detection Efficiency. My conducted measurements do not involve this, therefore the point of highest Photon Detection Efficiency is marked by the results of other conducted measurements, that are comparable 37. This point will assure the highest detection of event photons, but will trade that for an increase in detector noise, due to the higher Dark Count Rate and more importantly Optical Cross Talk.

Comparing results to other groups, using different experimental setups and procedures and therefore also entirely different analysis techniques. Comparing against results from the University of Leicester, the University of Nagoya and the University of Catania, all of which are conducting fixed window readout of the SiPM after an expected light-pulse from a flasher-LED or a laser.

### 6.1 Dark Count Rate

Comparing the Dark Count Rate of the measured devices and results from the other groups is shown in Figure 35.

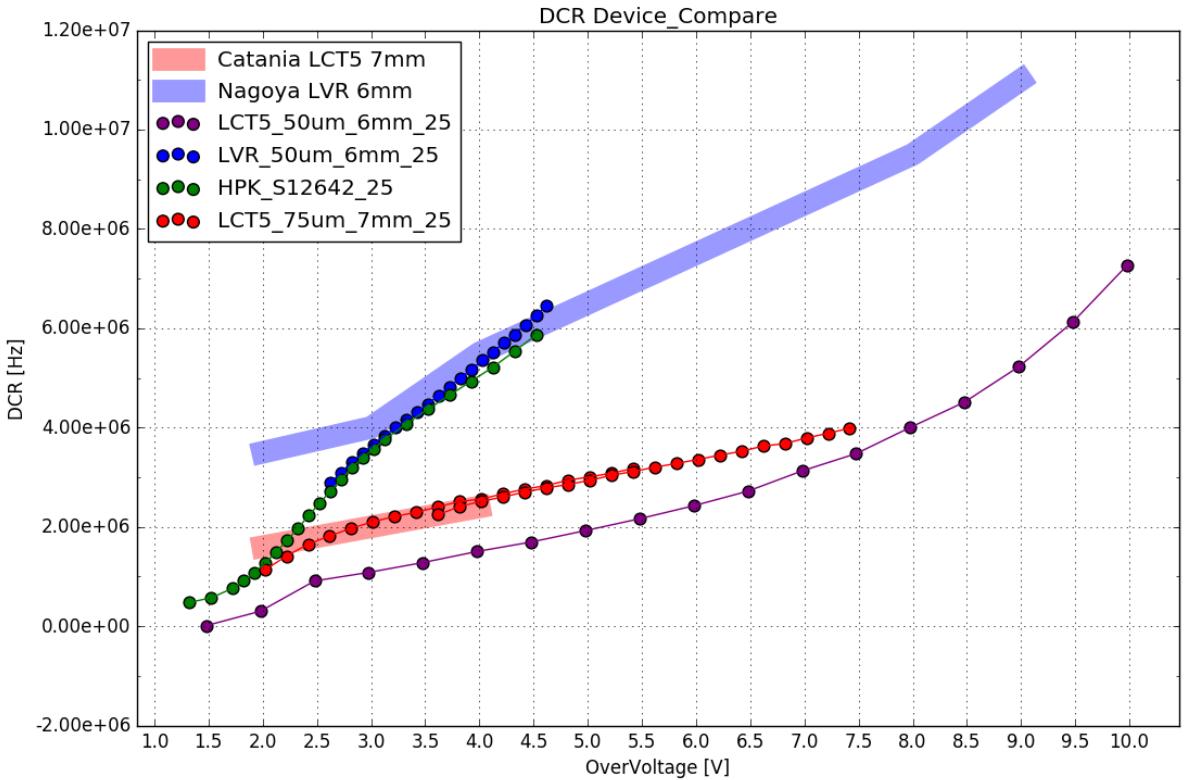


Figure 35: Dark Count Rate comparison of measured devices

### 6.2 Optical Cross Talk

TODO

### 6.3 Photon Detection Efficiency

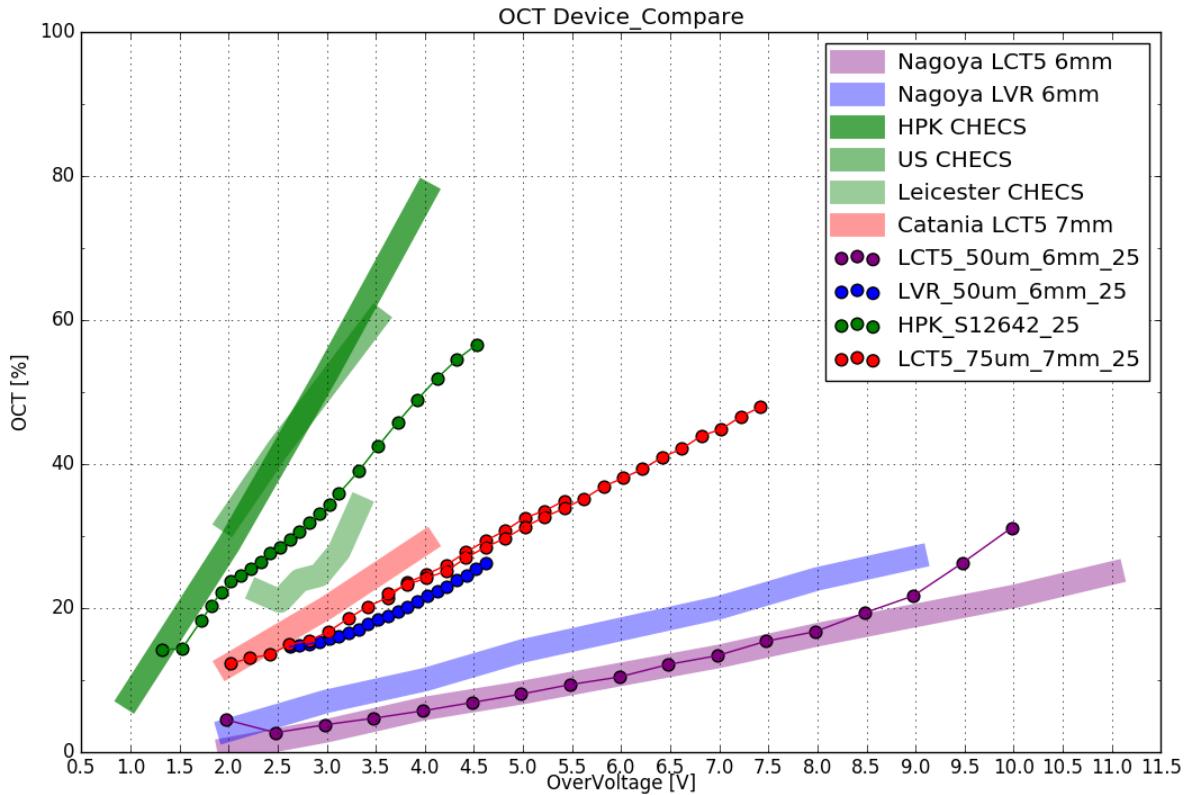


Figure 36: Cross Talk comparison of measured devices

## 7 Glossary

1. CTA - Cherenkov Telescope Array
2. HPK - Hamamatsu Photonics K.K.

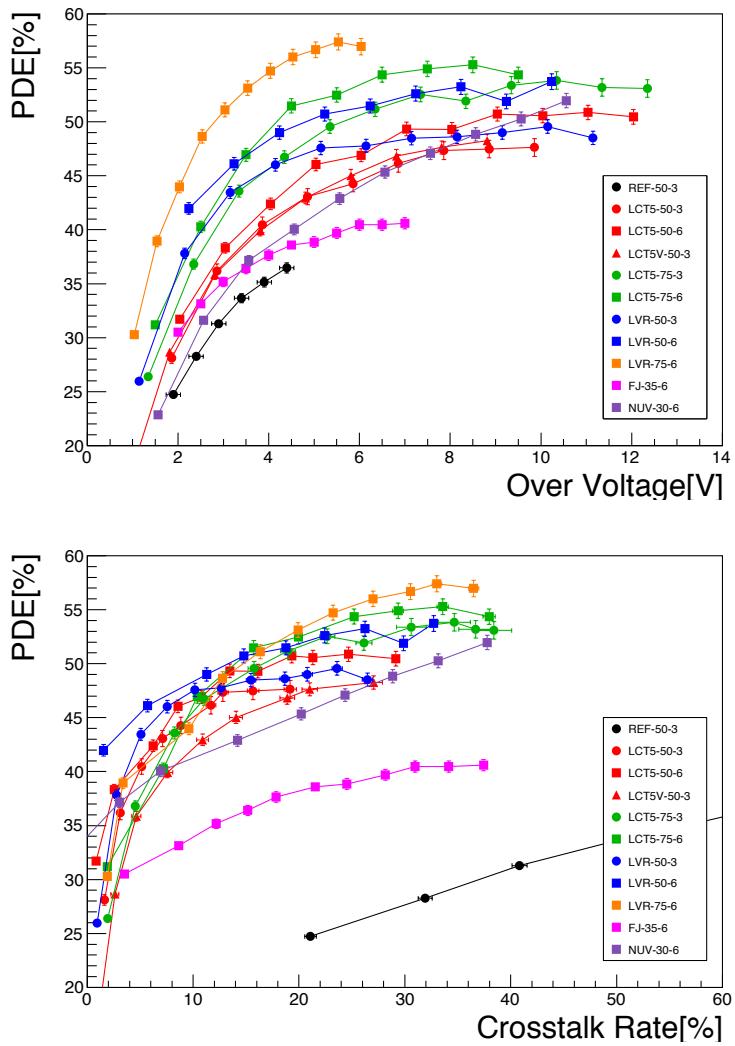


Figure 37: Photon Detection Efficiency Comparison Plots from the University of Nagoya

8 supplementary plots

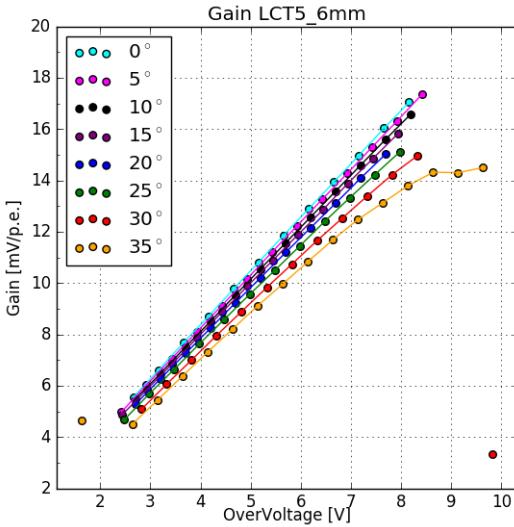


Figure 38: Gain of the HPK S13360 pixel, plotted against over-, bias-voltage and temperature.

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## 9 Appendix

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### 9.1 HPK S12642 Pixel Comparison versus bias-voltage

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### 9.2 Pulse Area Spectra of different integration windows

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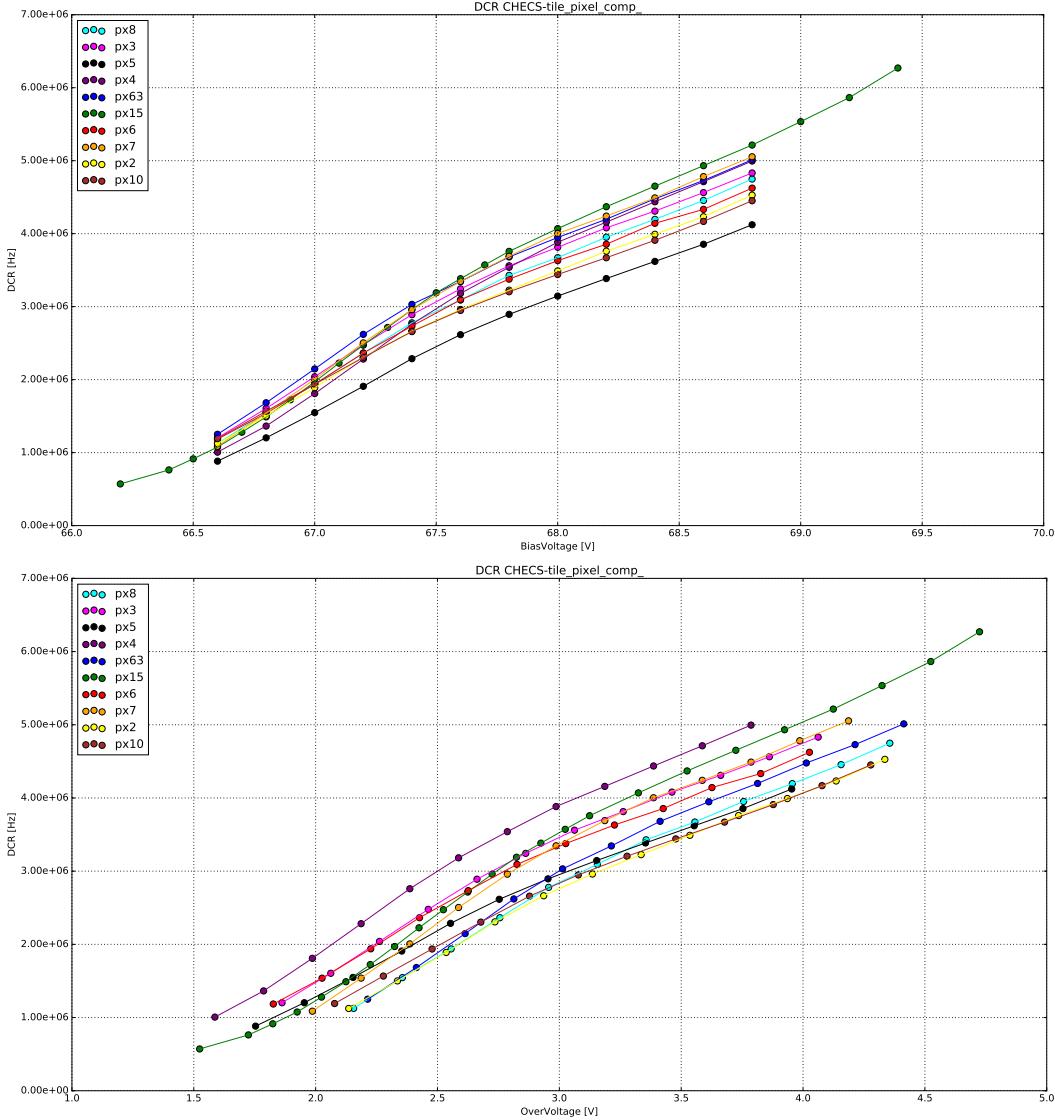


Figure 39:

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10. <http://www.ung.si/en/research/laboratory-for-astroparticle-physics/projects/cta/>

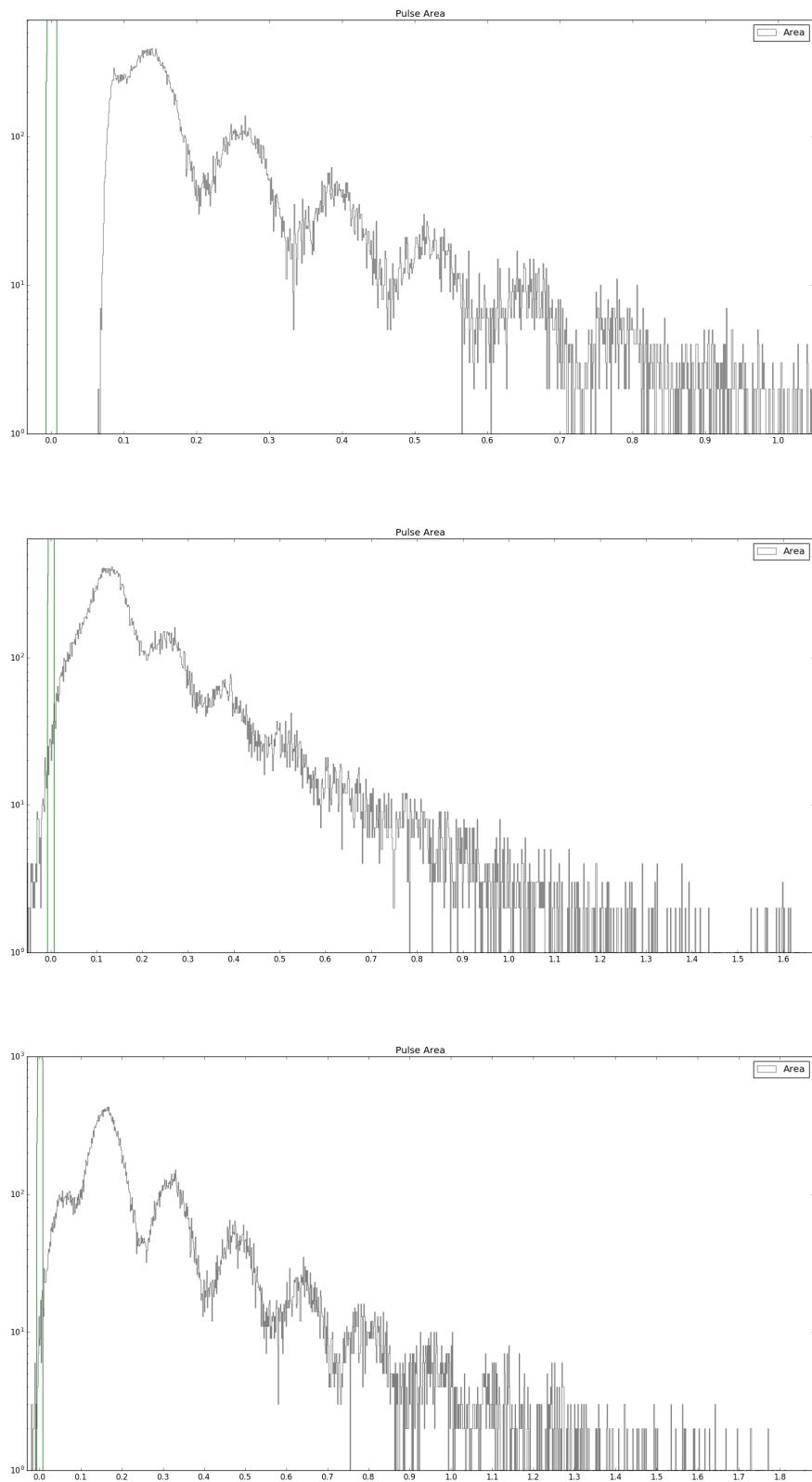


Figure 40: