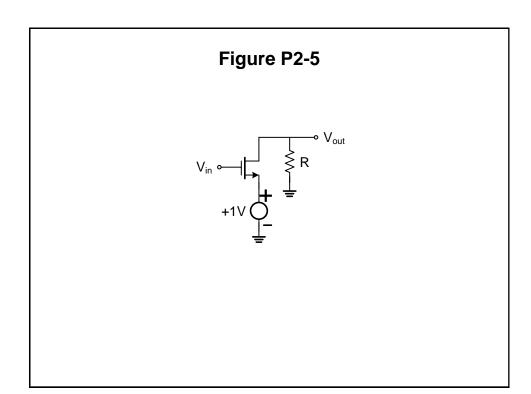
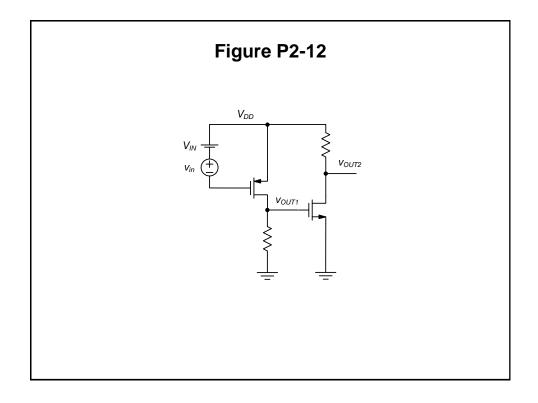
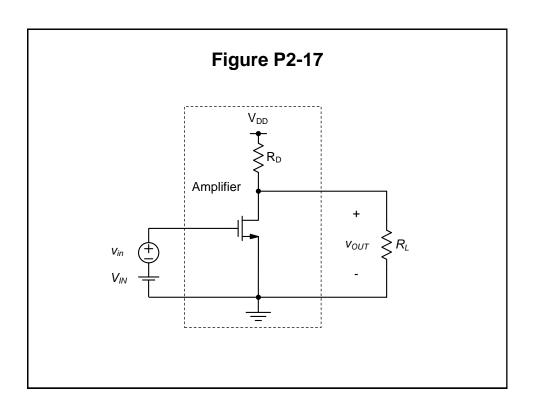


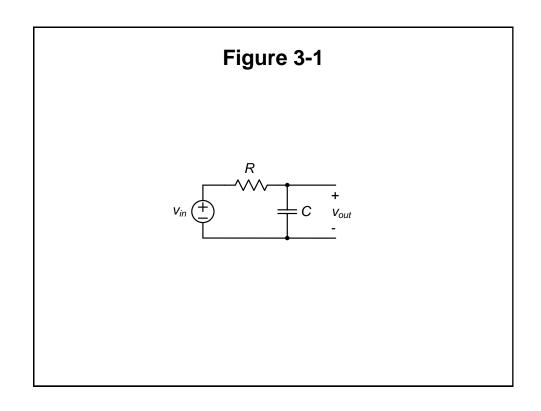
Figure P2-2

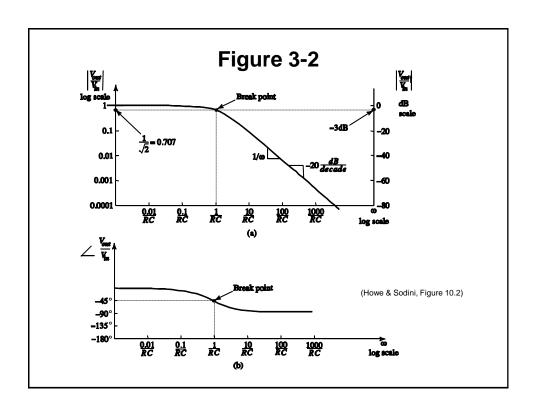
$$M1 \longrightarrow W/L_1 \longrightarrow W/(L_1+L_2)$$
 $M2 \longrightarrow W/L_2$ 

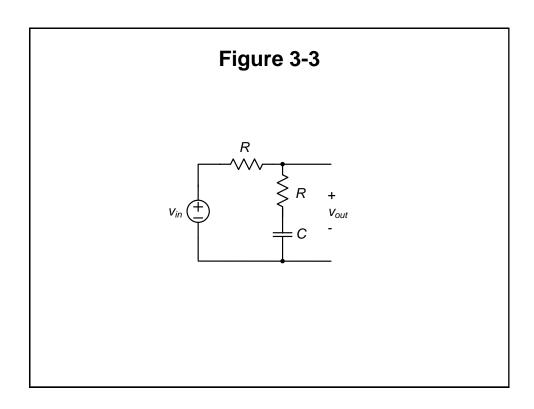


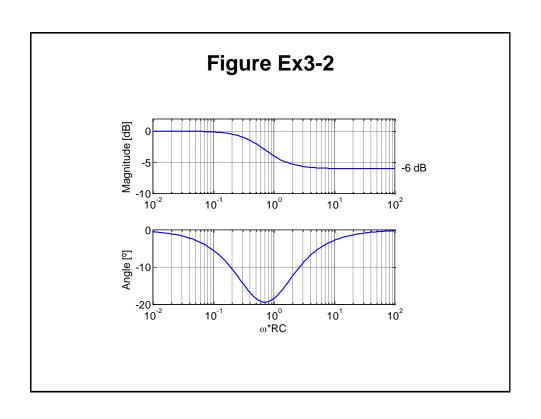


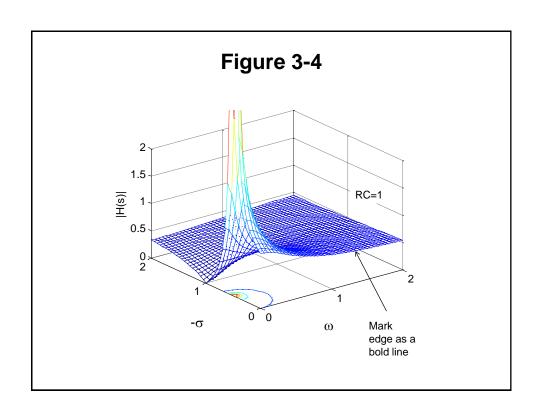


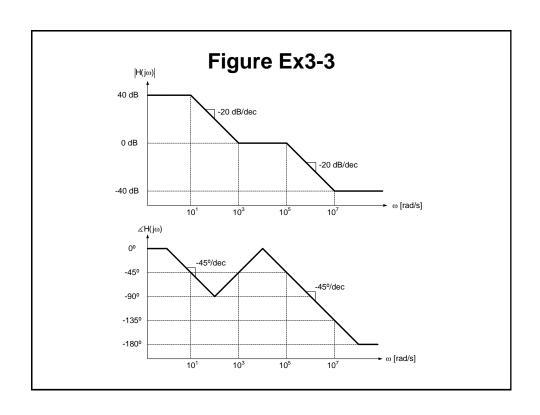


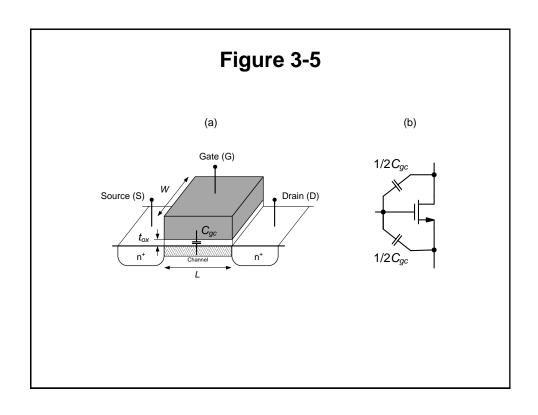


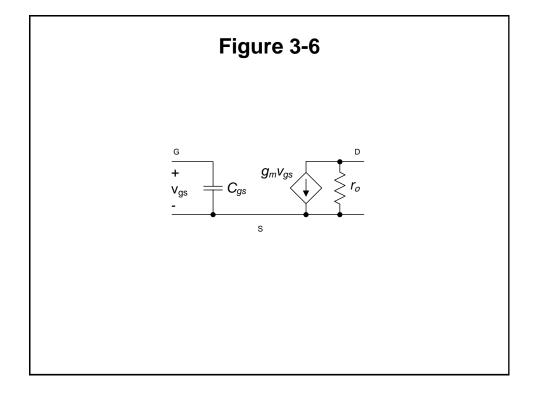


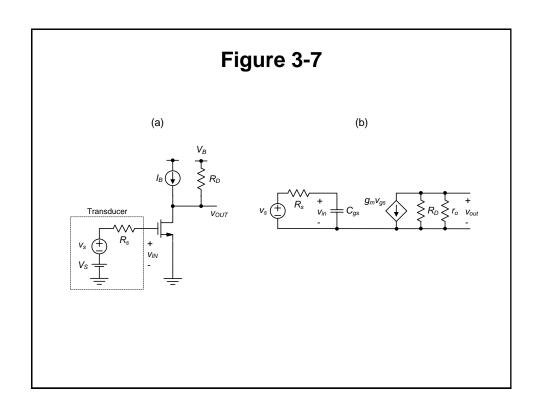


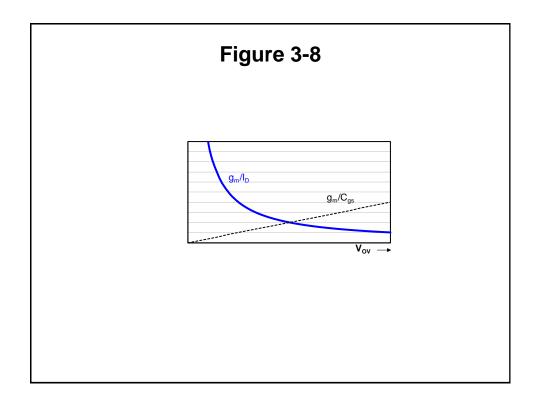


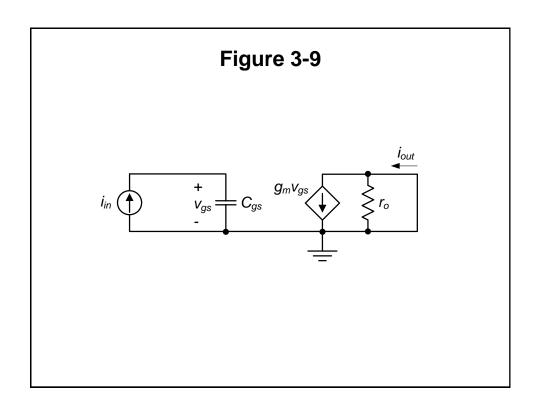


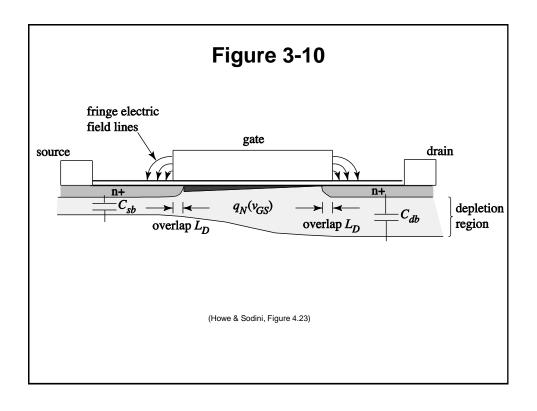


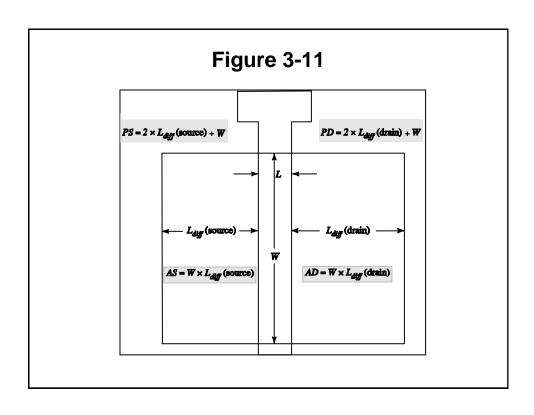


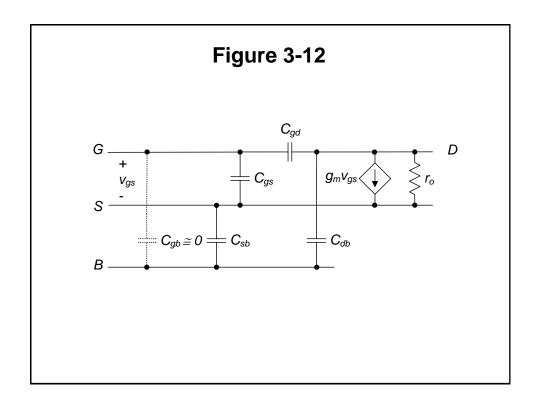


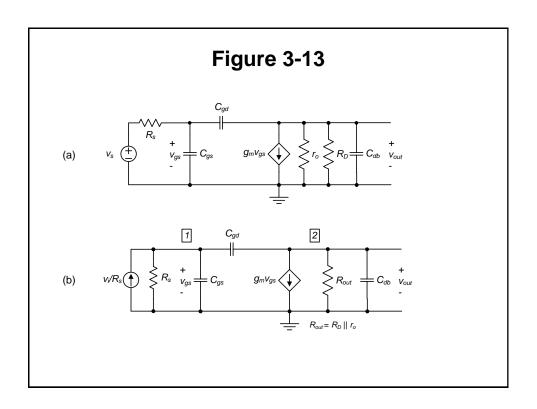


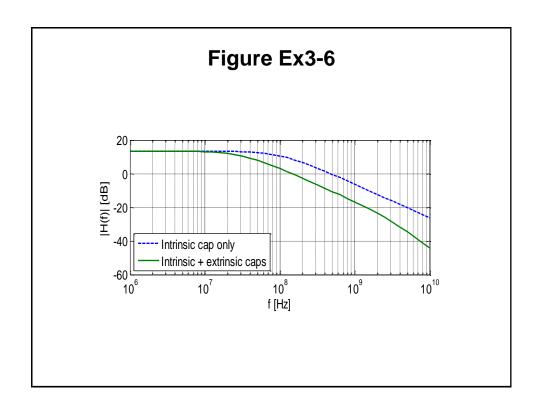


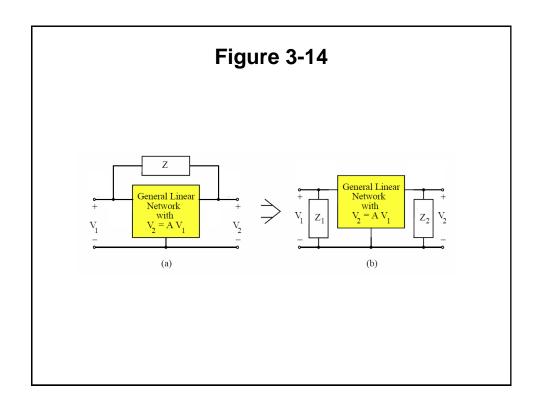


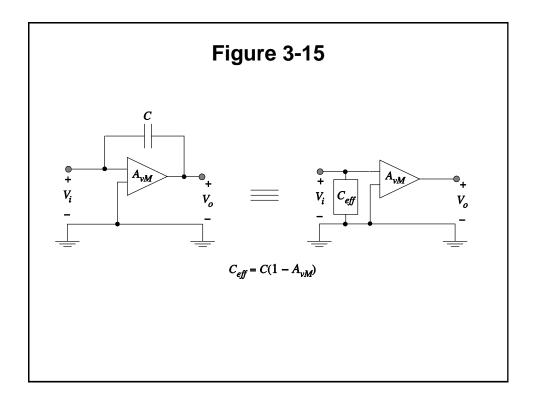


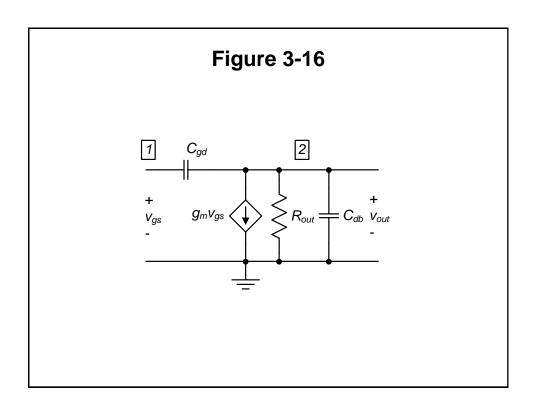


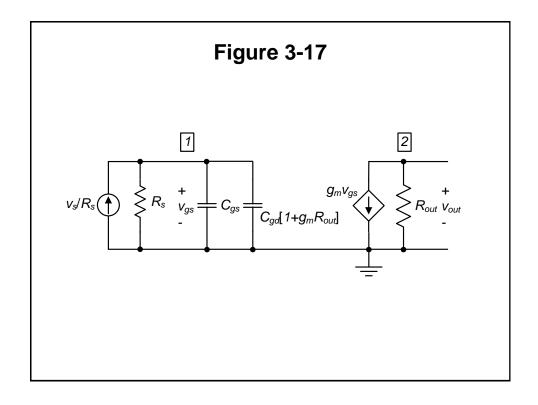


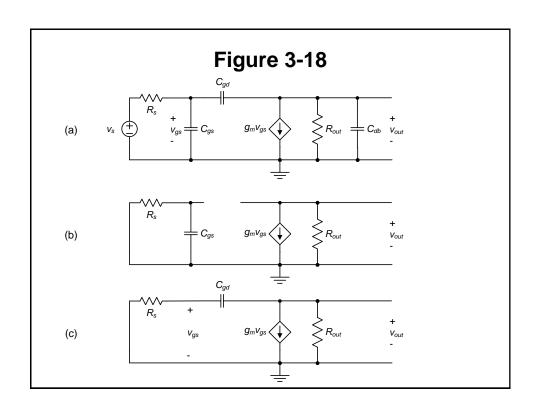


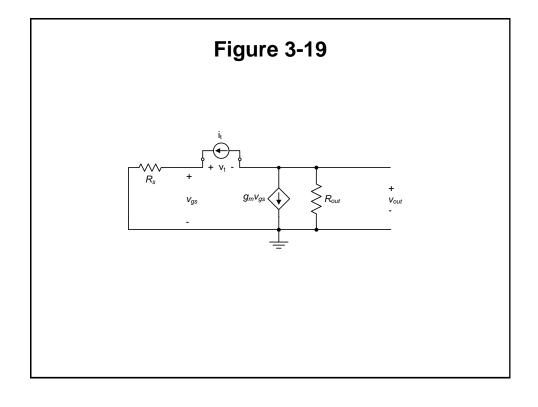




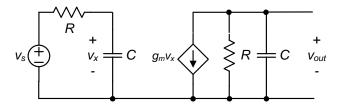




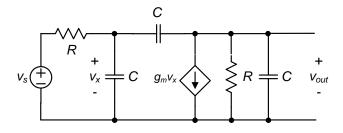


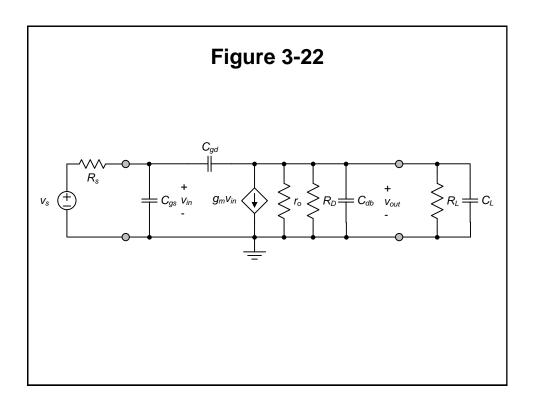


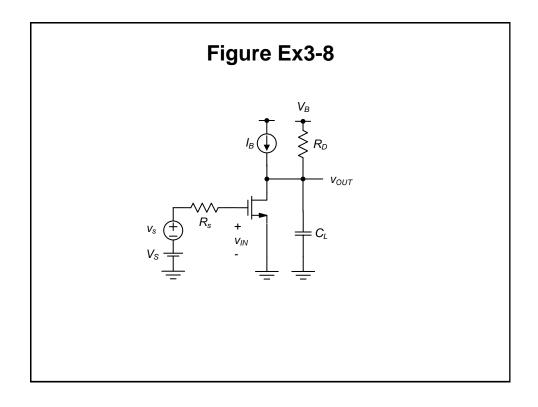


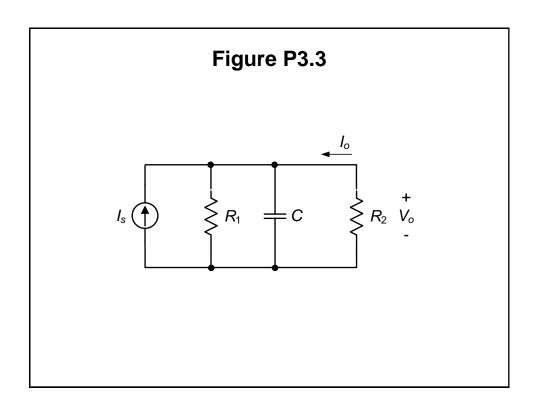


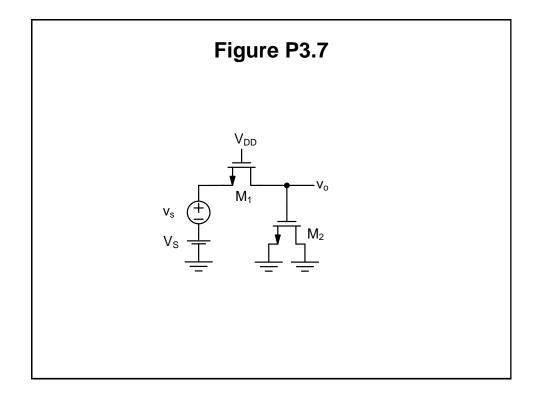
## Figure 3-21

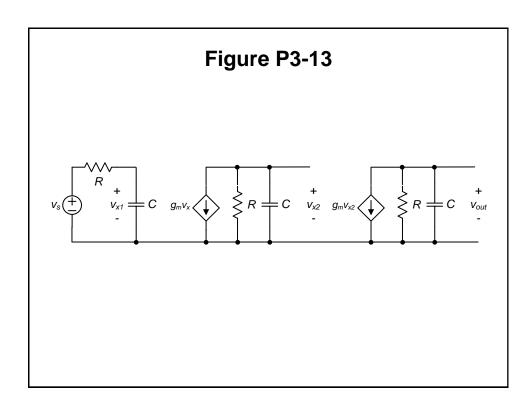


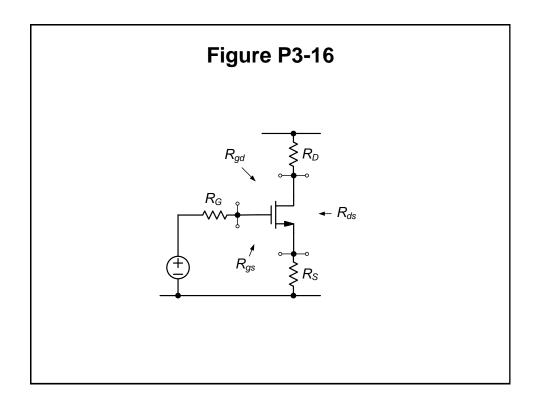


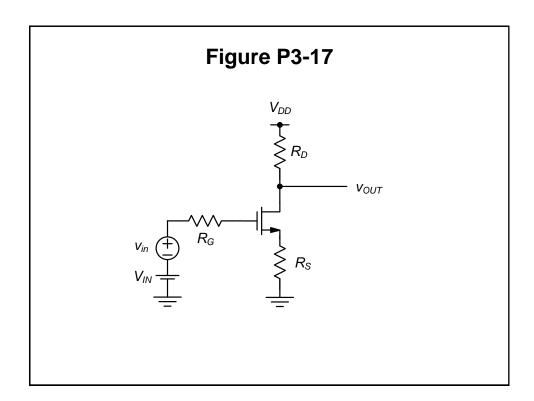


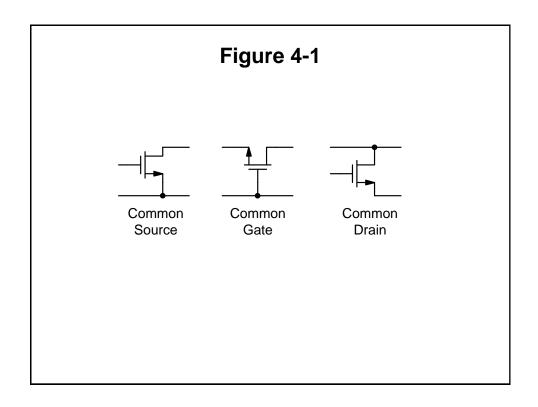


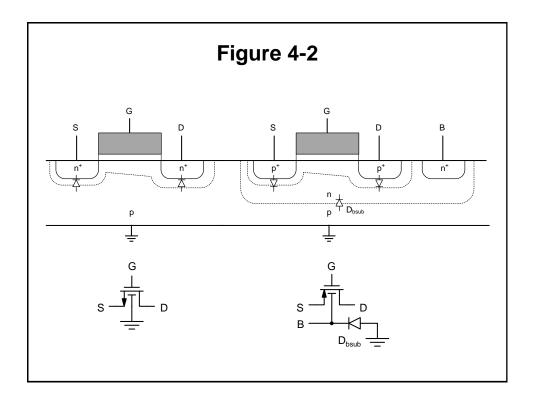


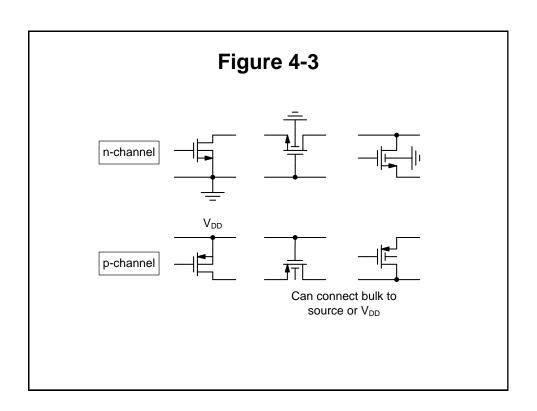


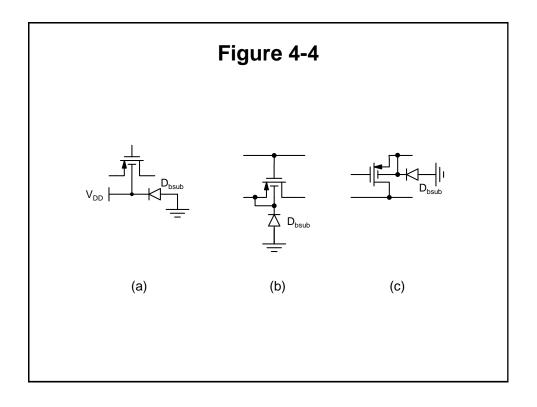


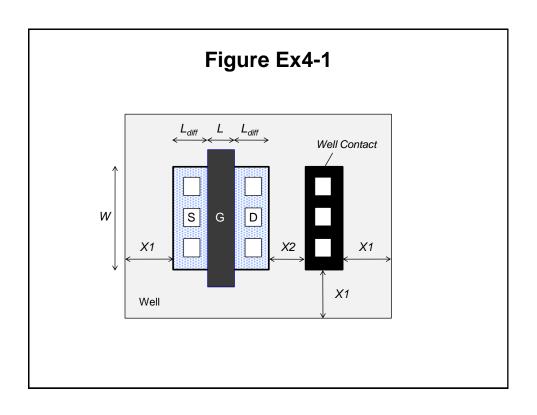


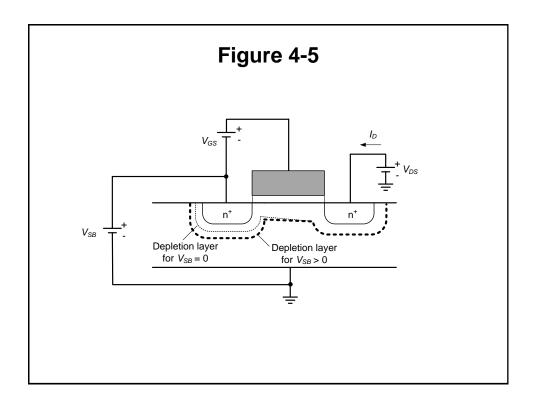


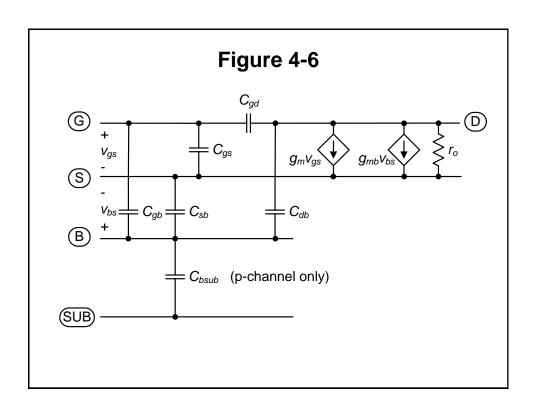


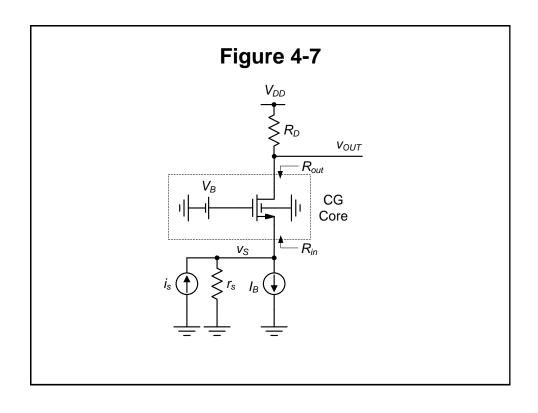


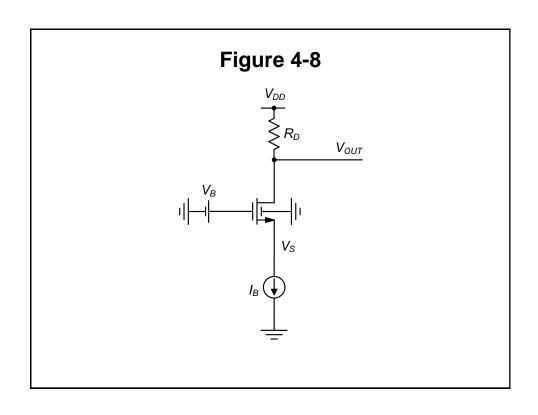


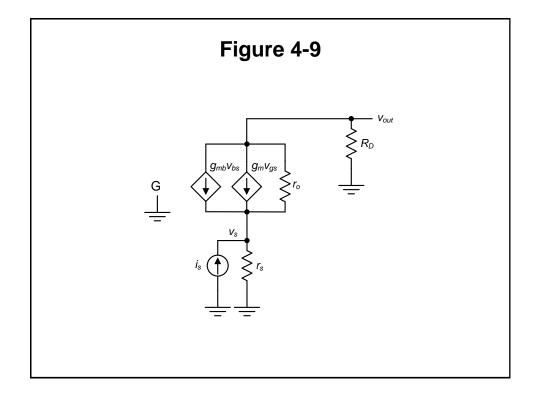


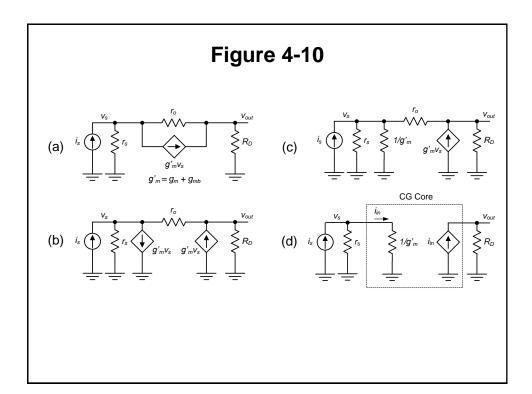


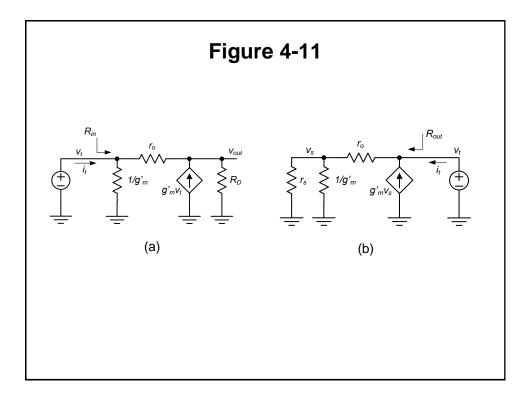


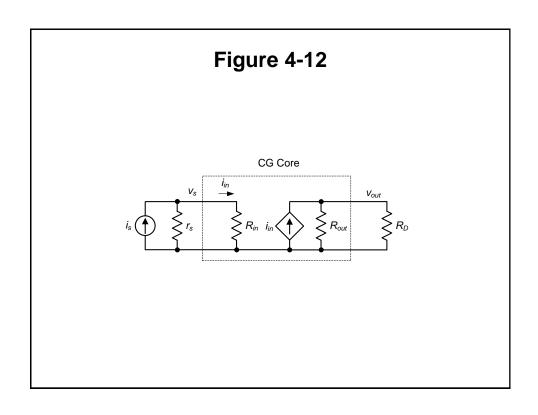


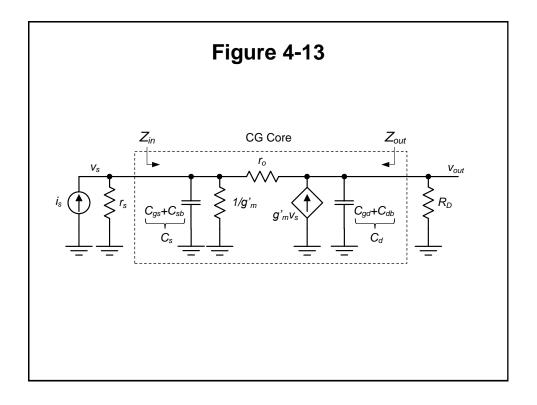


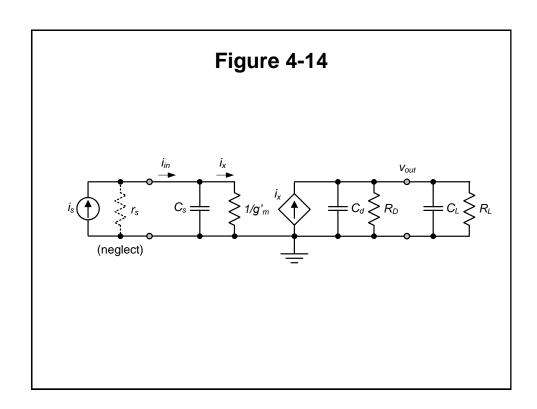


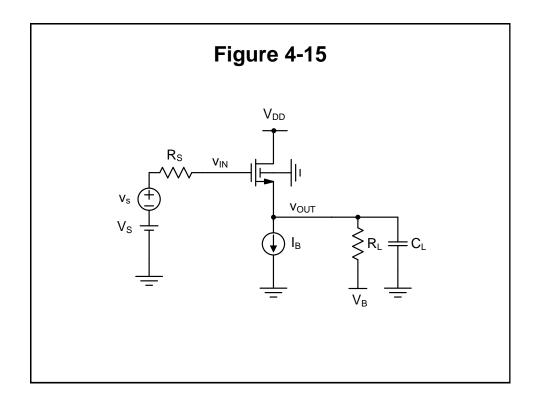


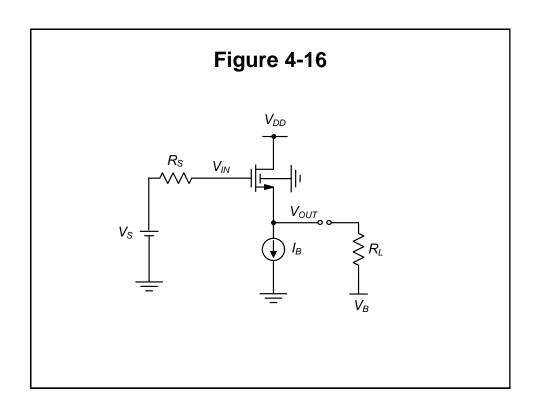


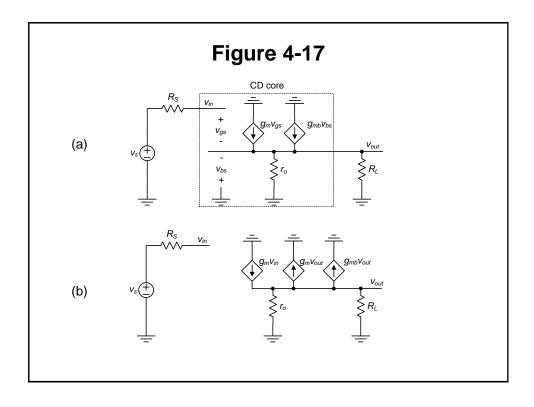




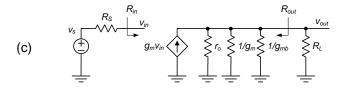


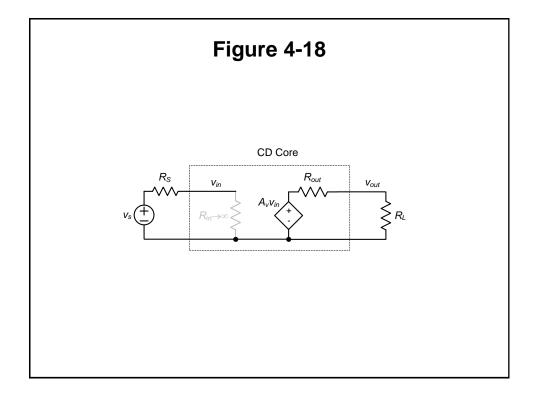


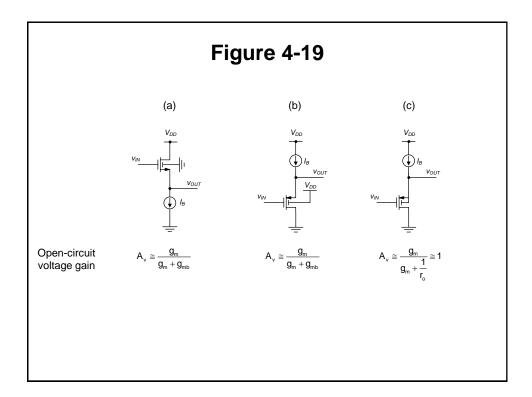


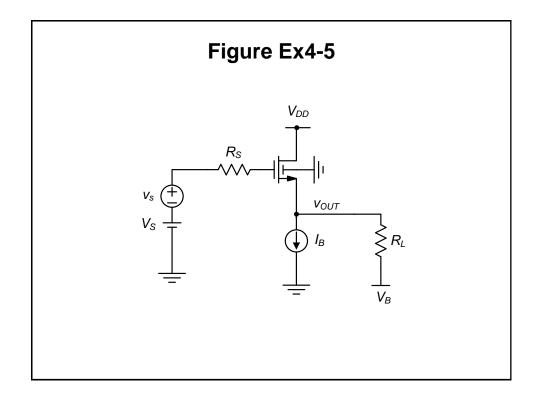


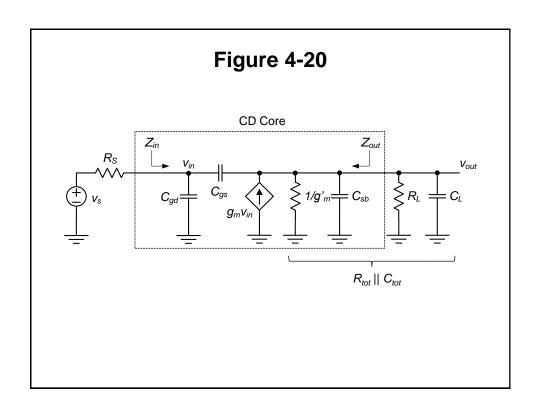
## Figure 4-17 (continued)

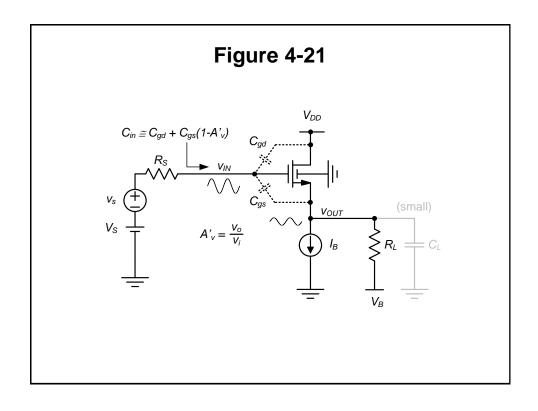


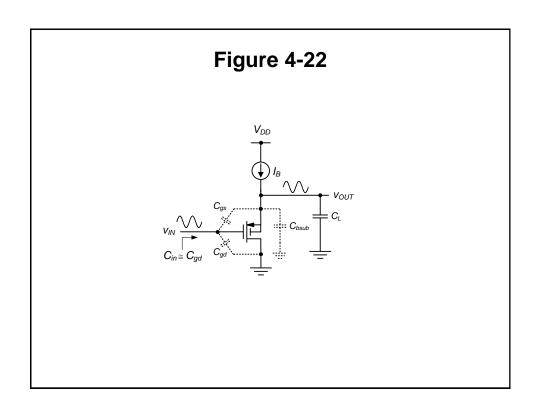


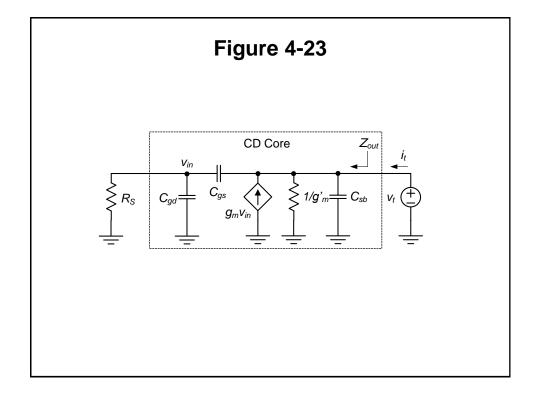


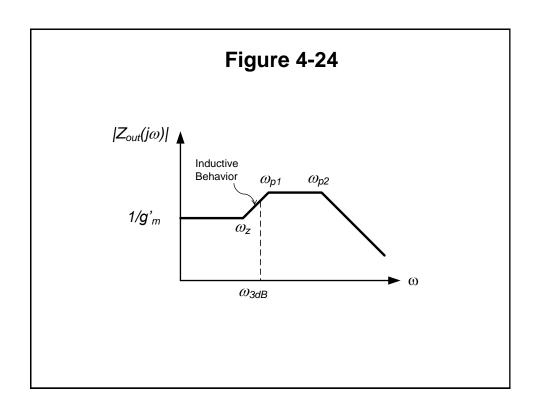


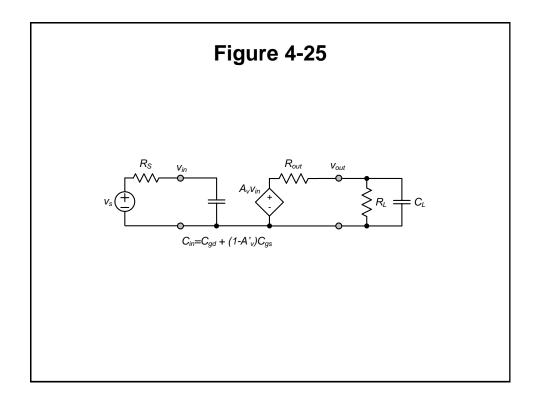




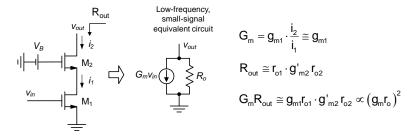


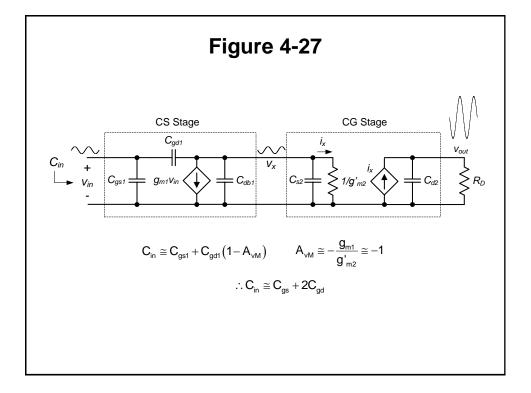


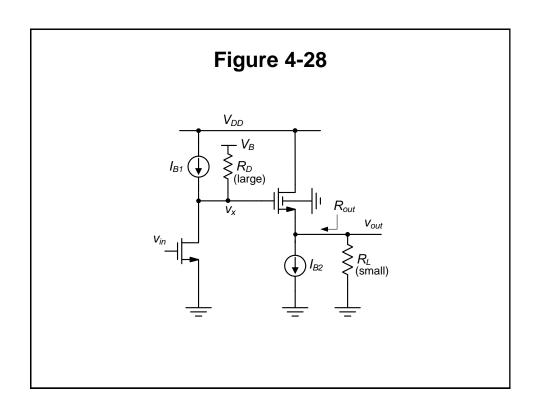


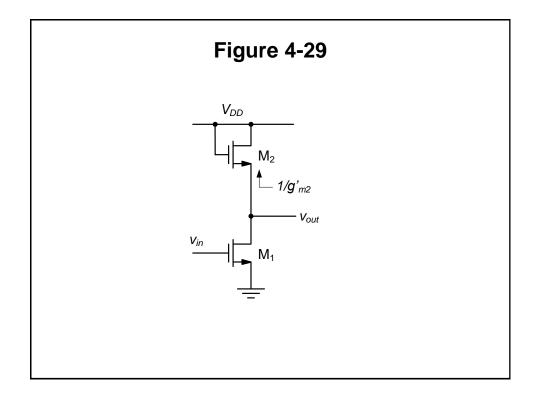


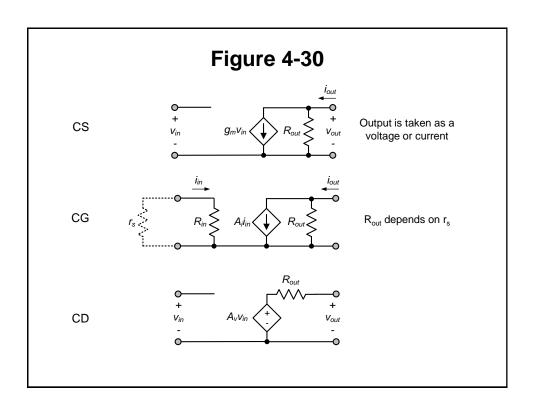
## Figure 4-26

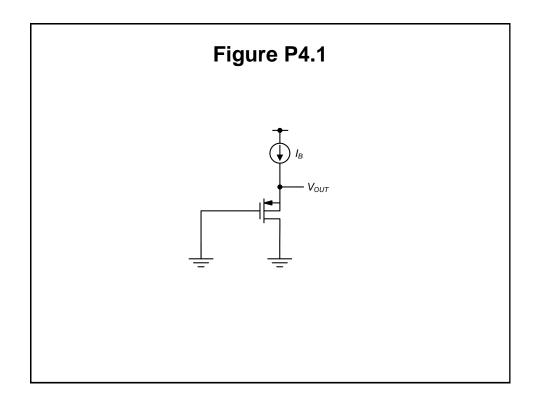


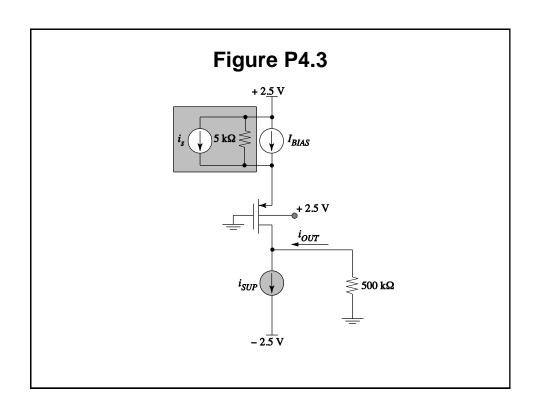


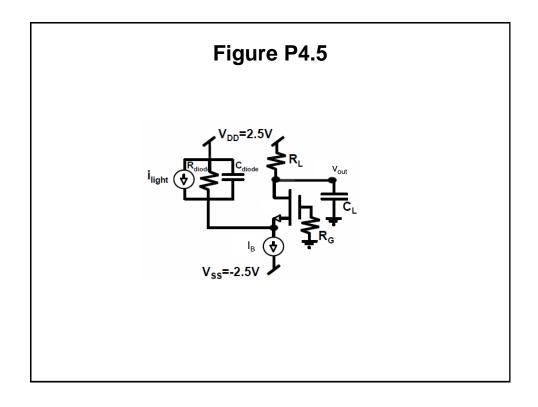


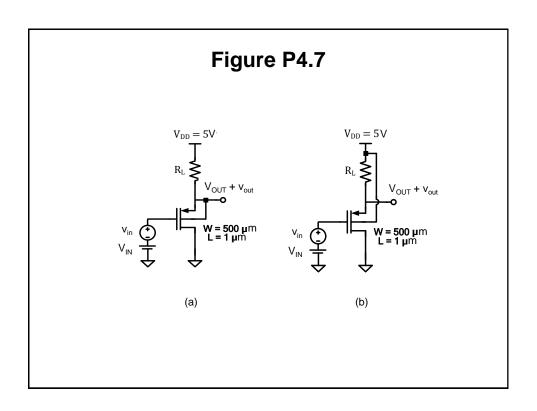


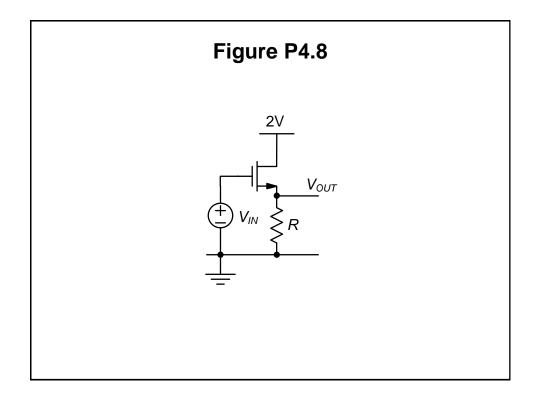


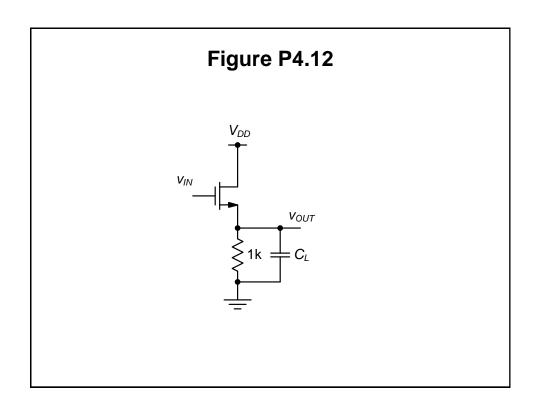


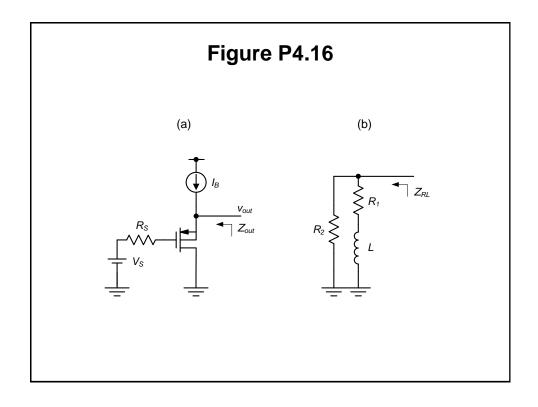


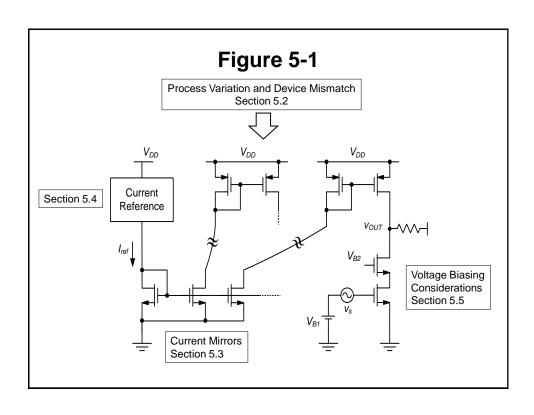


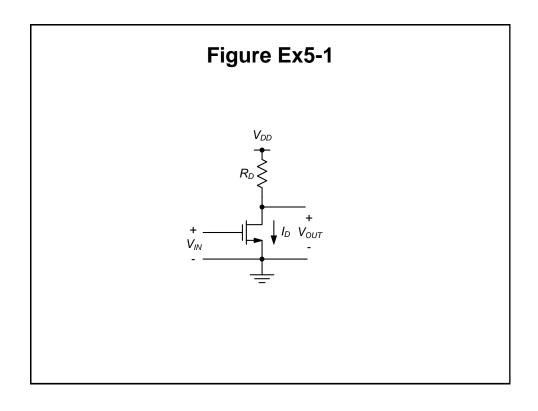


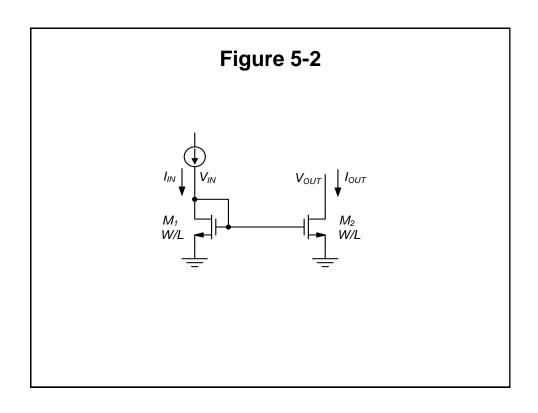


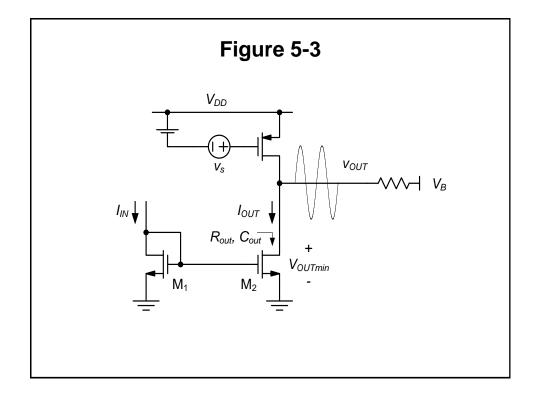


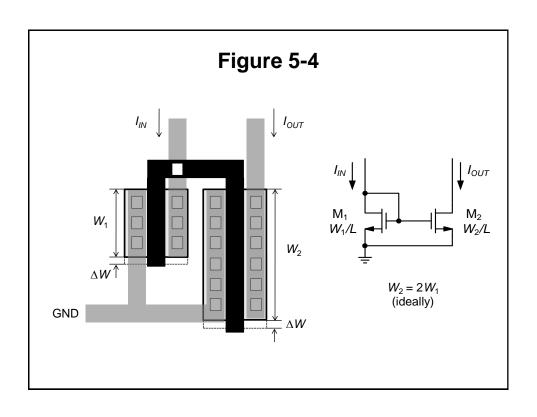


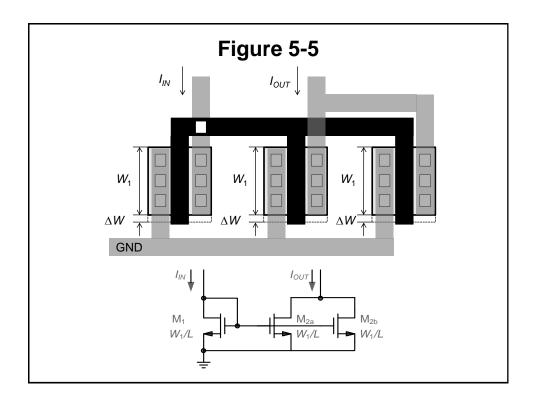


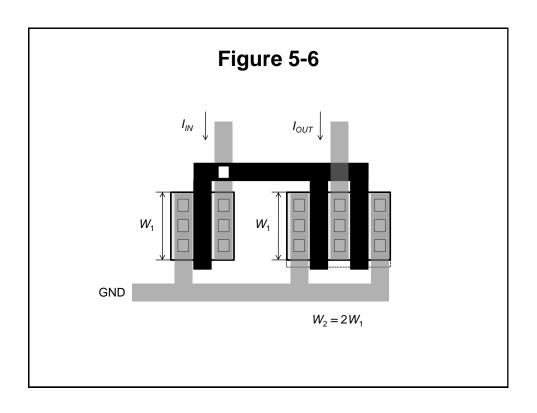


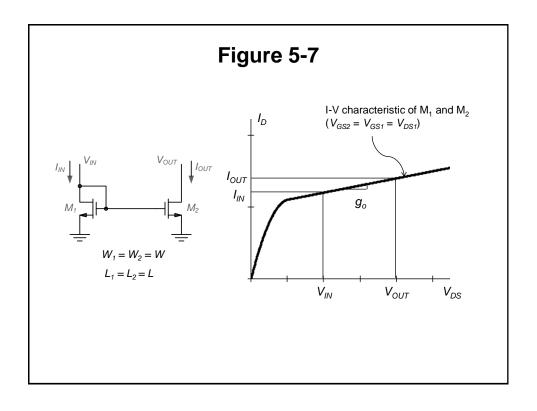


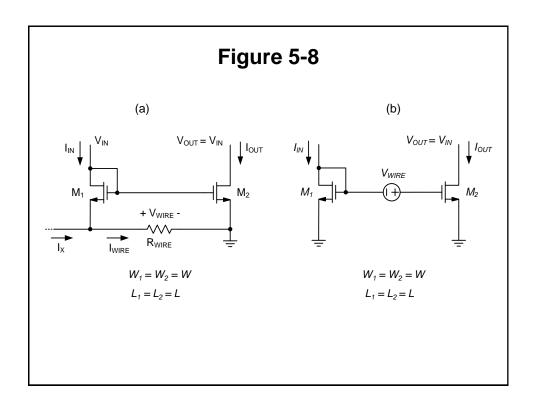


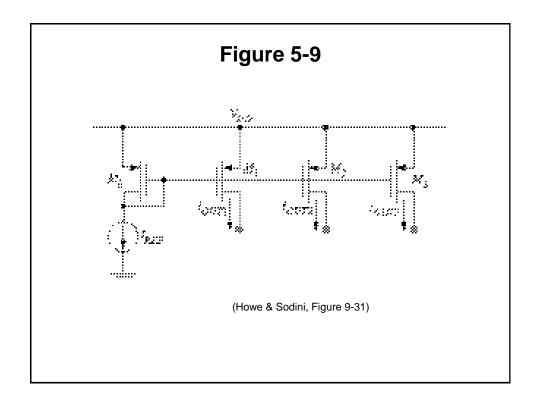


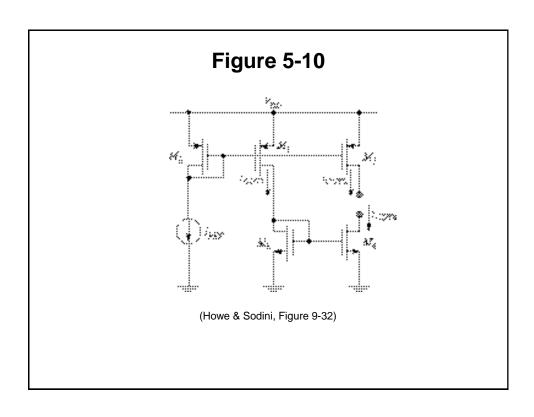


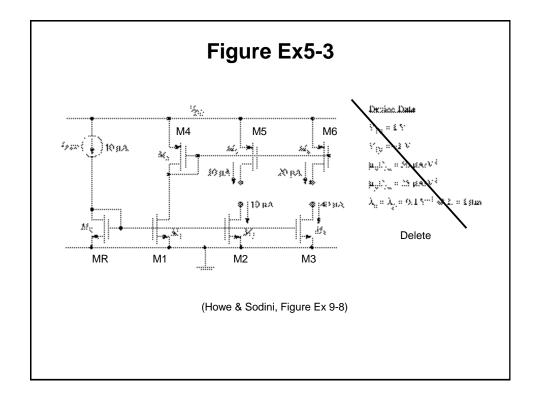


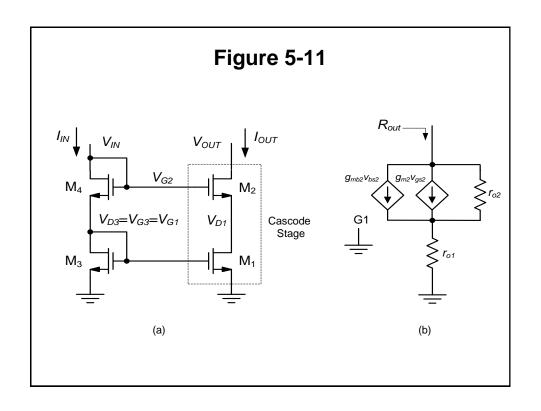


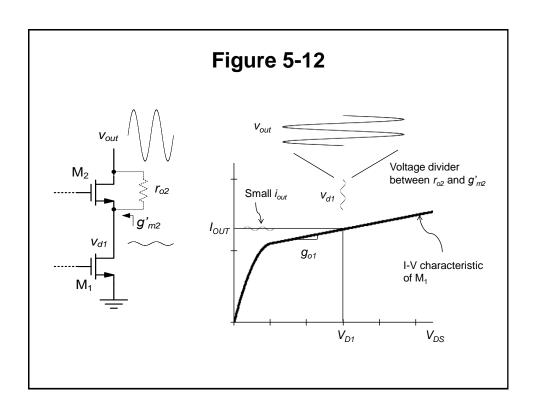


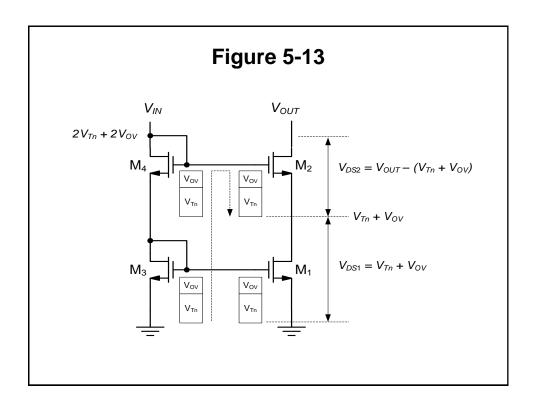


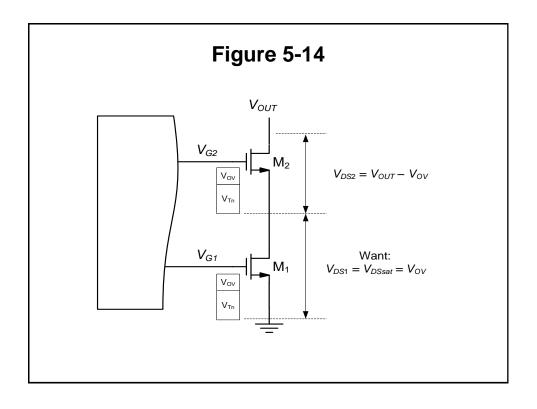


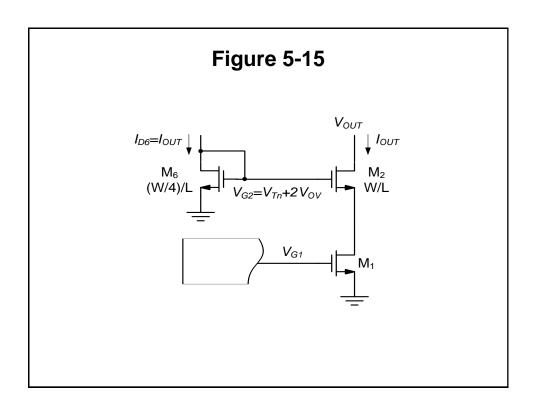


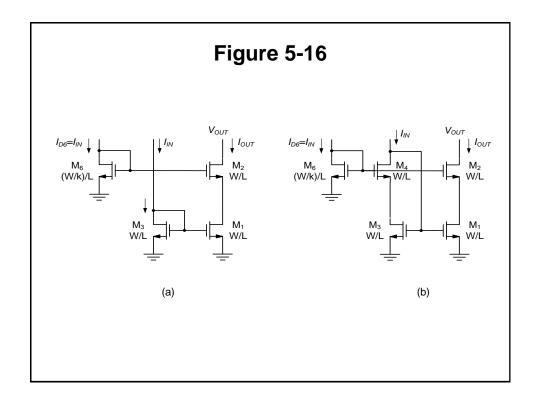


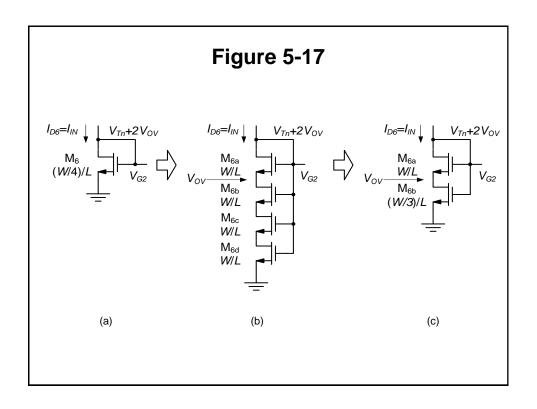


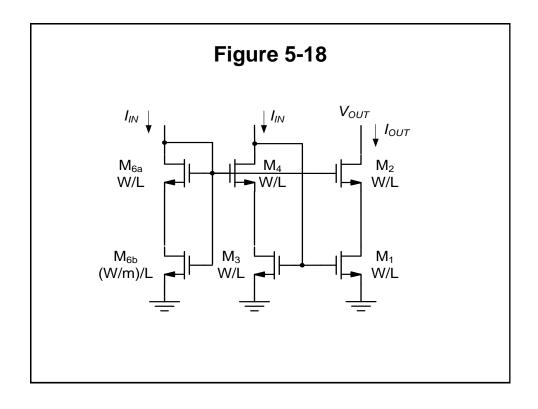


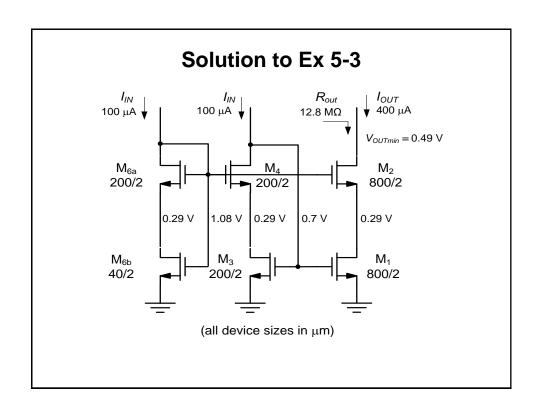


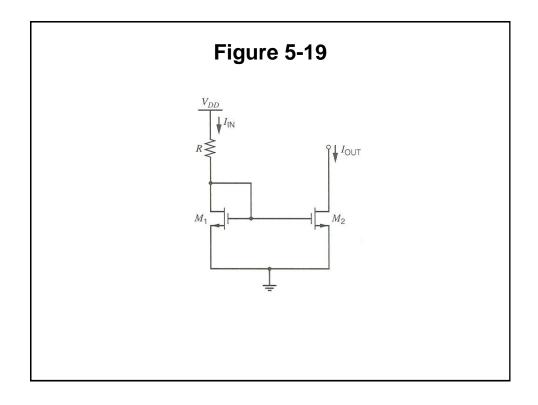


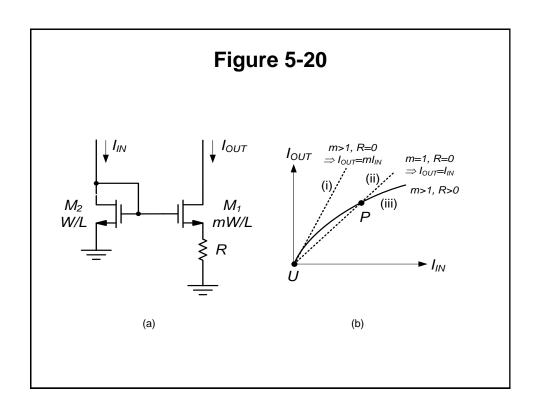


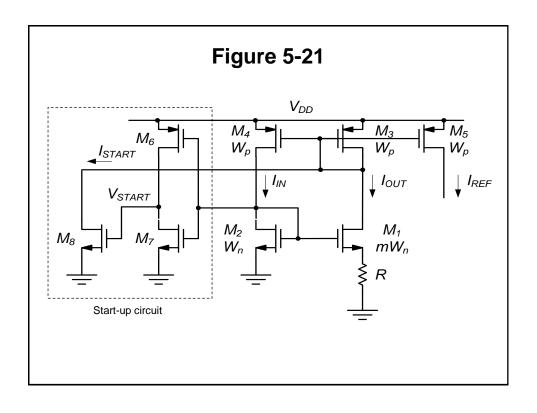


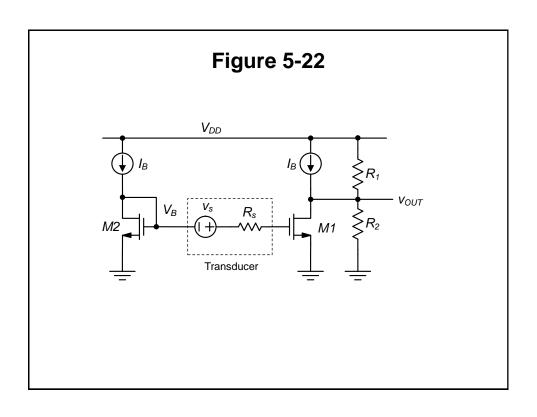


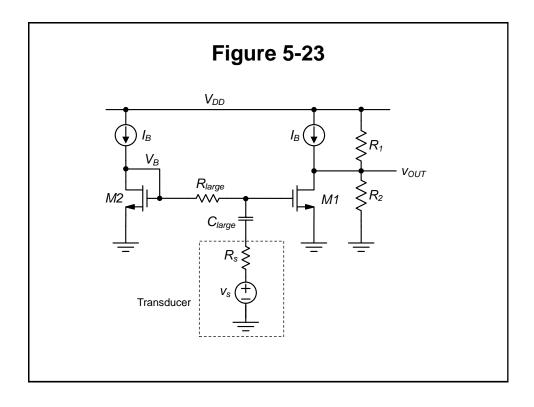


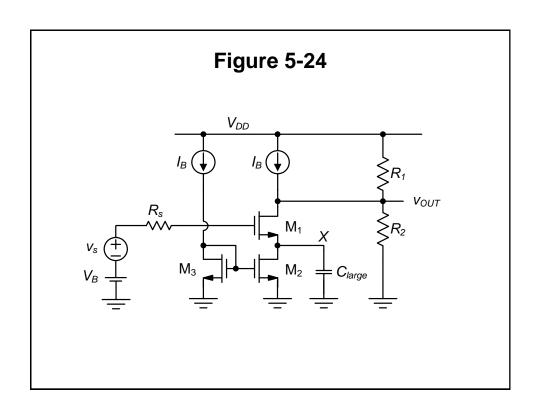


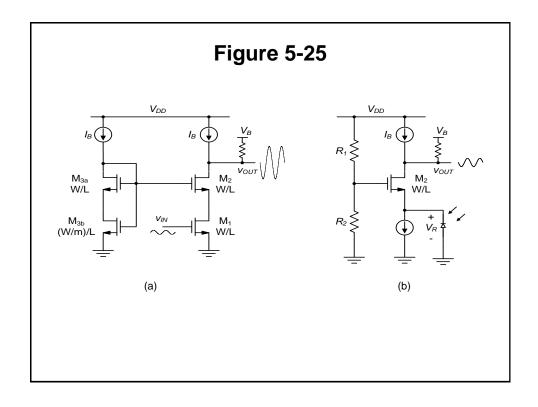


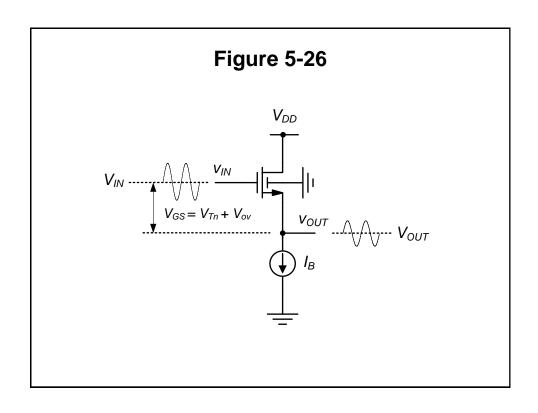


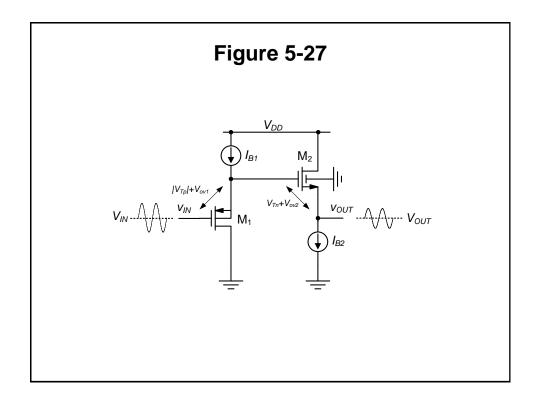


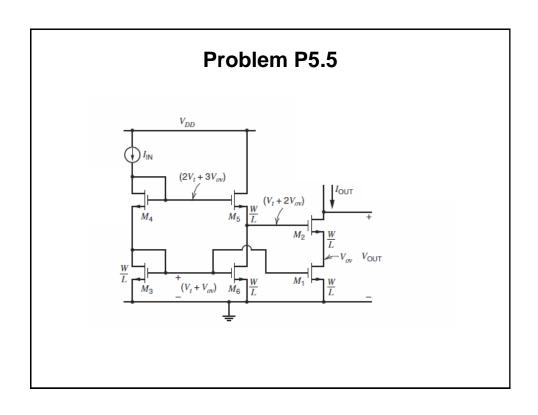


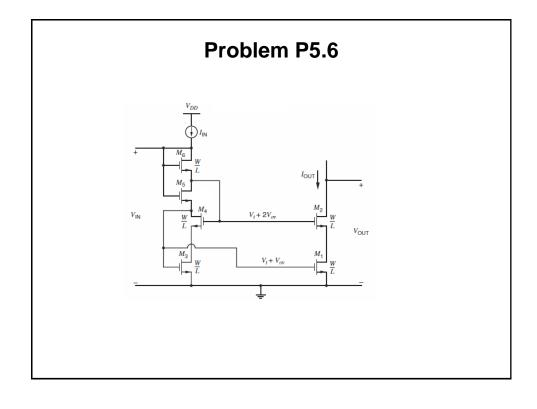




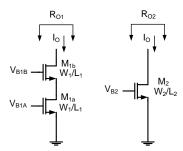




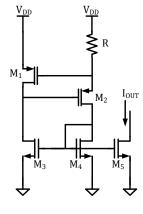


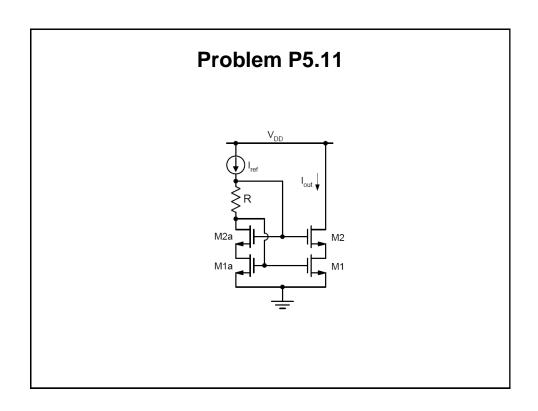


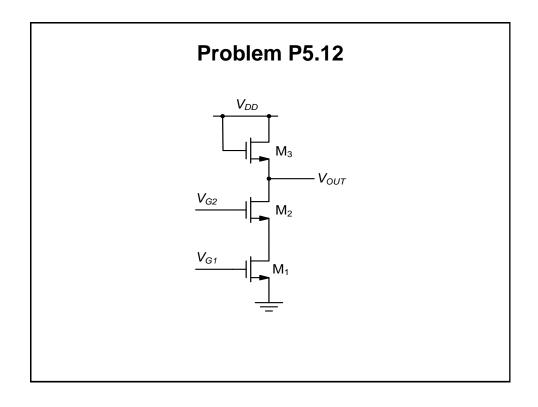
## **Problem P5.9**



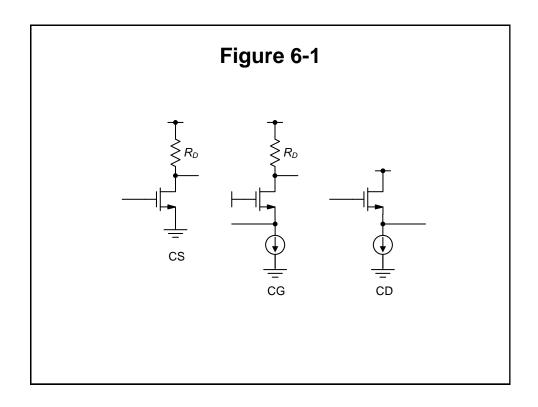
### **Problem P5.10**

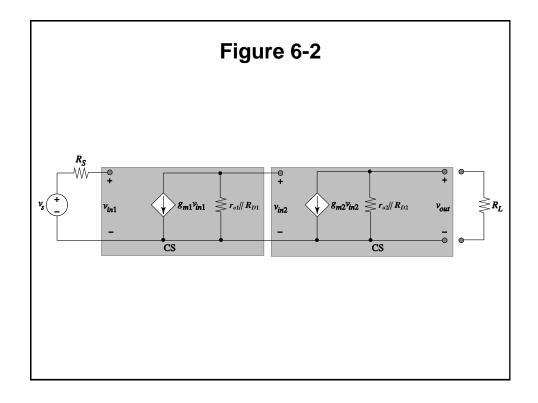


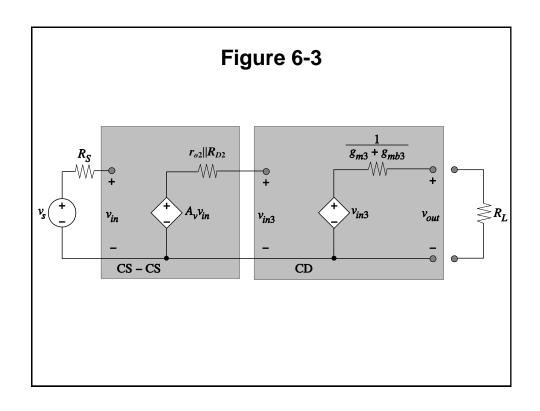


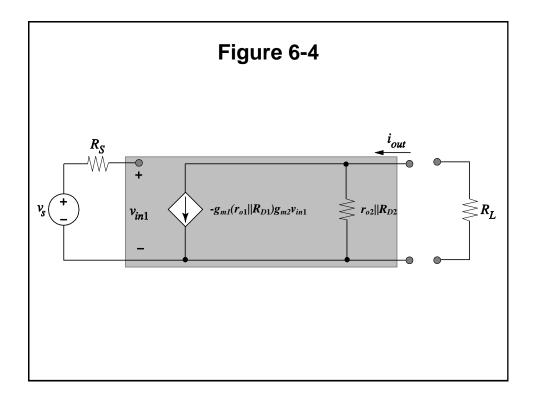


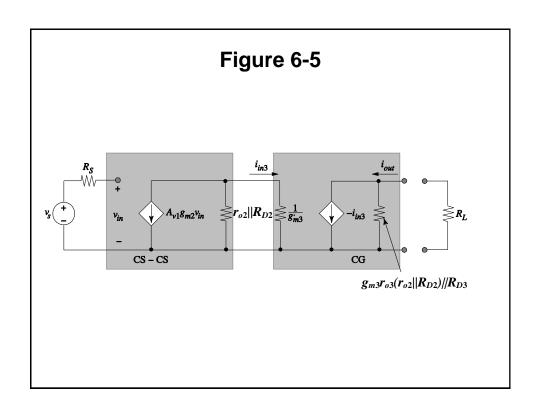
# 

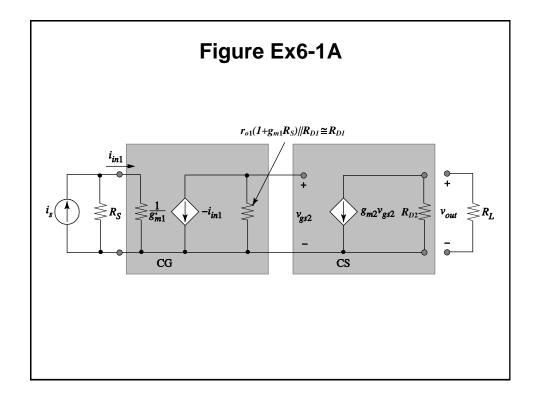


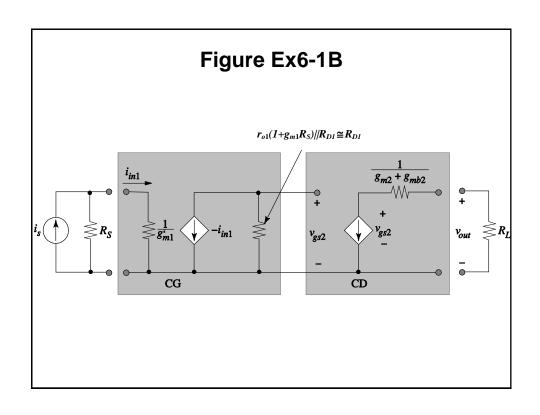












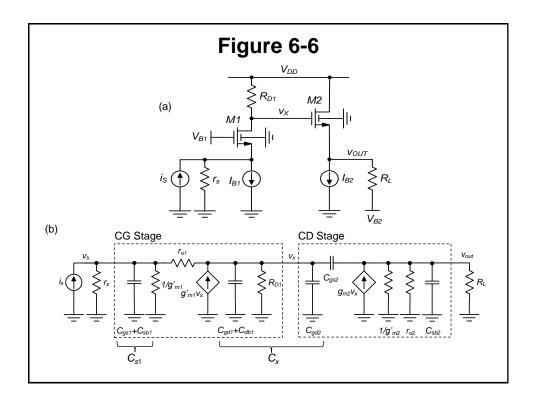
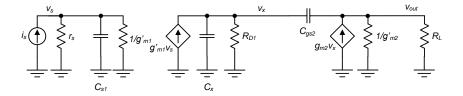
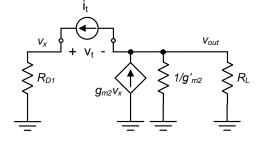


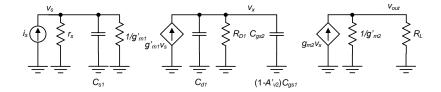
Figure 6-7

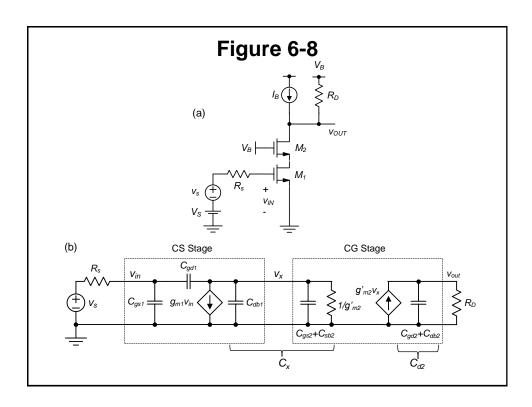


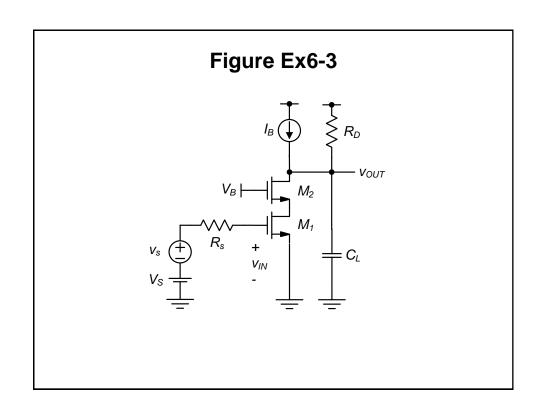
# **Example 6-2 Solution**

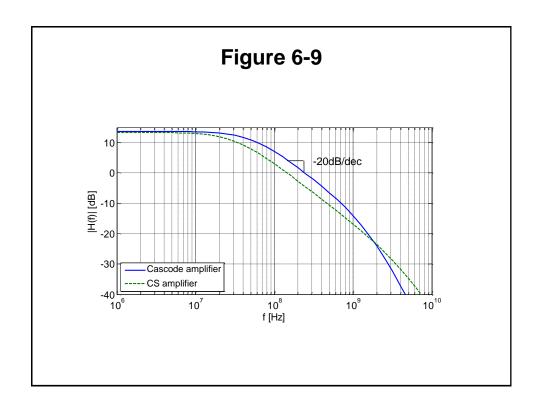


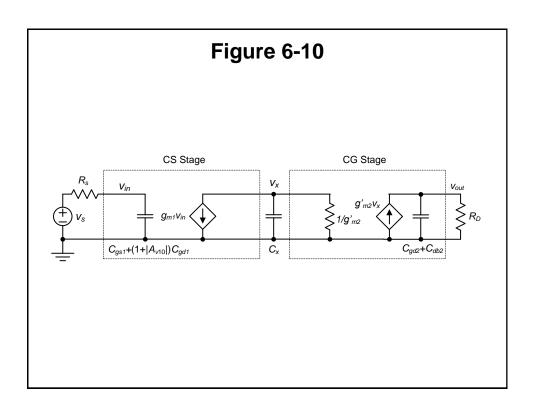
# **Example 6-3 Solution**

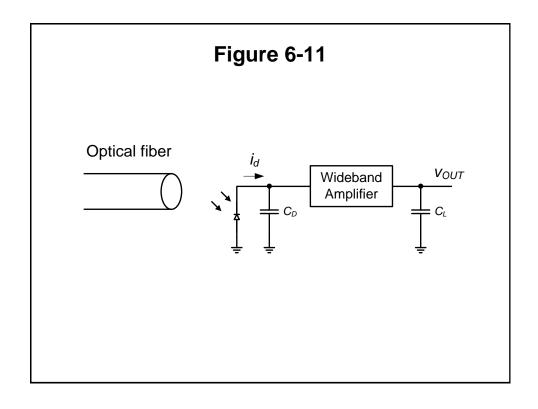


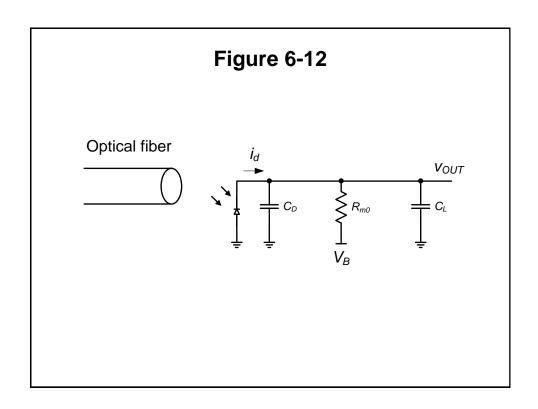


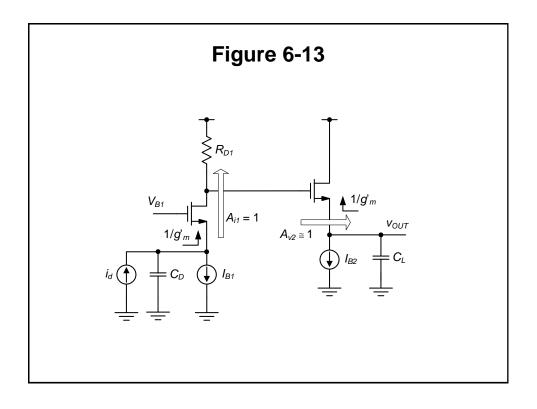


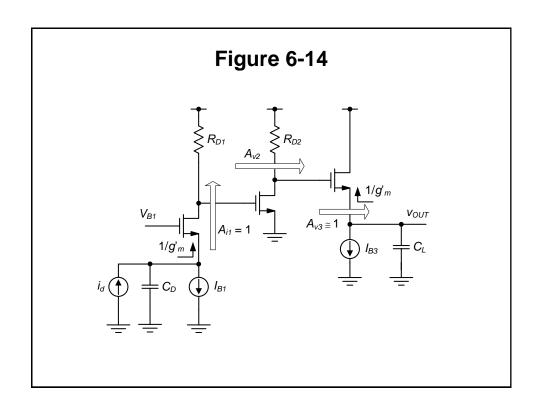


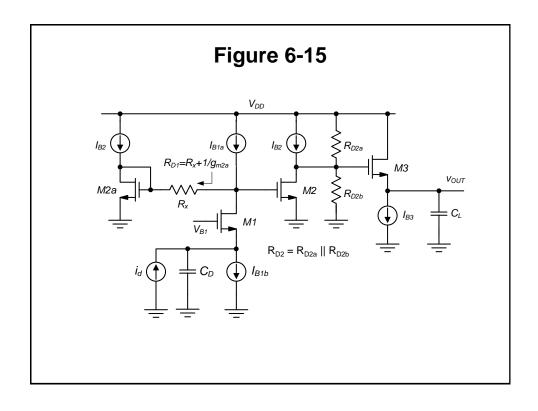


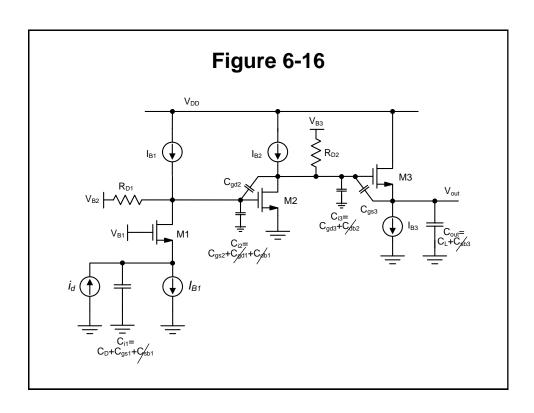












### Figure 6-17

```
********************
% Design script for three-stage transresistance amplifier
                                                                                                 % Compute drain currents
ID1 = IDtot*ID1_IDtot;
% Process technology parameters \begin{aligned} k_{P} & n = 50\text{-}6\text{;} \\ k_{P} & n = 50\text{-}6\text{;} \\ \text{Cox} & = 2.3\text{e}-3\text{;} \\ m_u & = k_{P} & n/\text{Cox;} \\ \text{Cov} & = 0.5\text{e}-9\text{;} \\ \text{gmb\_gm} & = 0.2\text{;} \end{aligned}
                                                                                                 ID3 = IDtot*ID3 IDtot;
                                                                                                 ID2 = IDtot - ID1 - ID3;
                                                                                                 % Calculations for M1
                                                                                                 W1 = 2*ID1/(kp_n/L1*VOV1^2);
Cgs1 = 2/3*W1*L1*Cox + W1*Cov;
% Design specifications R_{\rm B} = 2 {\rm e} 3j CD = 5 {\rm e} - 12j CL = 10 {\rm e} 12j IDtot = 3 {\rm e} - 3j
                                                                                                 tau_in = (Cgs1+CD)/(gml*(1+gmb_gm));
                                                                                                 % Calculations for M3 gm3 = 2*ID3/VOV3;
Cgs3 = 2/3*W3*L3*Cox + W3*Cov;
Cgd3 = W3*Cov;
% Design choices

VOV1 = 0.3;

VOV2 = 0.3;

VOV3 = 0.3;

L1 = 1e-6;

L2 = 1e-6;

L3 = 1e-6;
                                                                                                 Av30 = 1-gmb_gm;
                                                                                                 tau_out = (CL+Cgs3)/(gm3*(1+gmb_gm));
                                                                                                 % Calculations for M2
                                                                                                W2 = 2*ID2/(kp_n/L2*VOV2^2);
Cgs2 = 2/3*W2*L2*Cox + W2*Cov;
% optimization parameters
ID1_IDtot = 0.25;
ID3_IDtot = 0.25;
Av20 = 10;
                                                                                                 Cgd2 = W2*Cov;
RD1 = Rm/Av20/Av30;
                                                                                                 tau core = RD1*(Cgs2 + (1+Av20)*Cgd2) + RD2*(Cgd3+(1-Av30)*Cqs3);
                                                                                                 \ensuremath{\text{\upshape}} Total time constant and bandwidth estimate
                                                                                                 tau_tot = tau_il + tau_core + tau_out
f3dB = 1/2/pi/tau_tot
```

