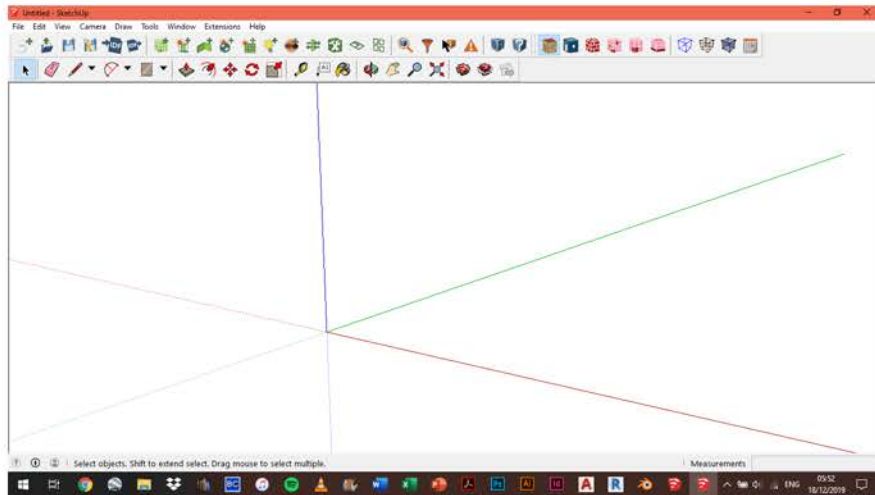


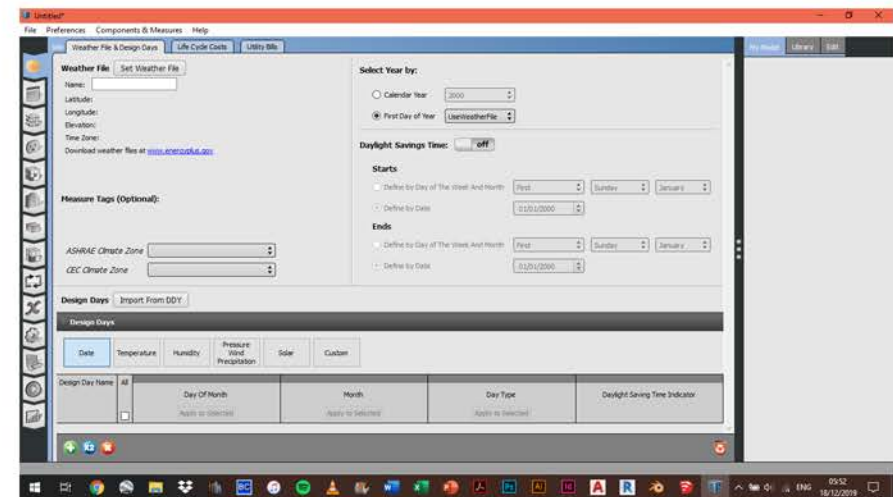
# INTRODUCTION

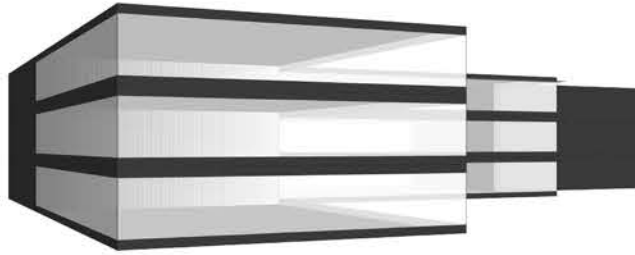
THE Open Studio SOFTWARE



DESIGN OF THE BUILDING

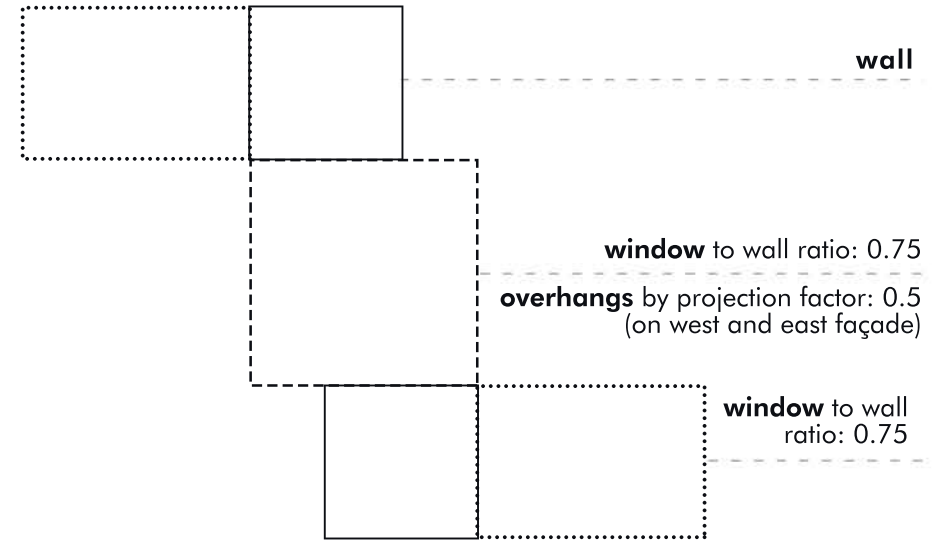
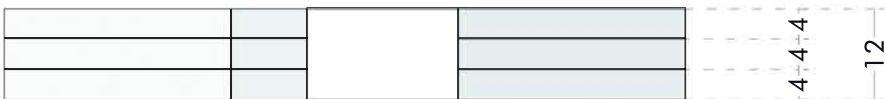
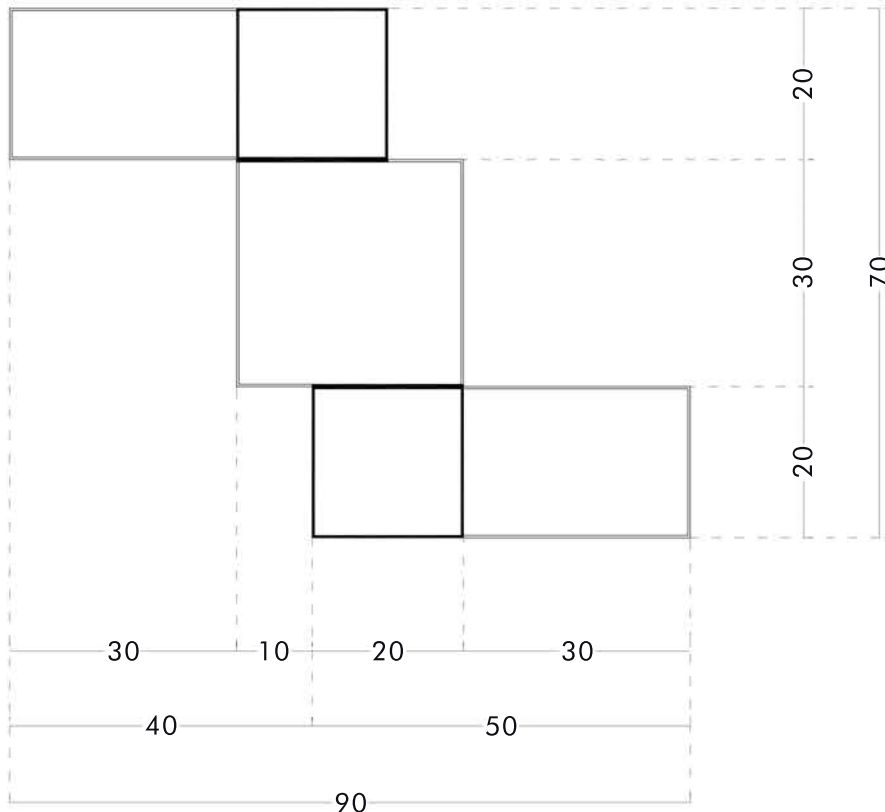
ANALYSIS OF THE BUILDING PERFORMANCE





# THE BUILDING

## GEOMETRY AND CHARACTERISTICS



### TOTAL EXTERNAL WALL AREA CALCULATION

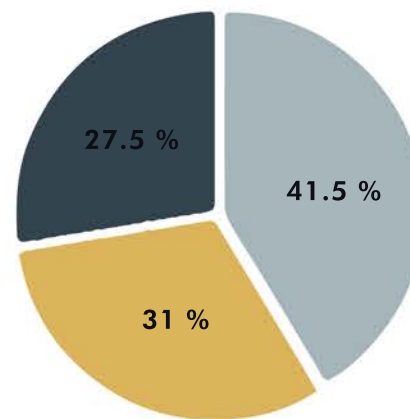
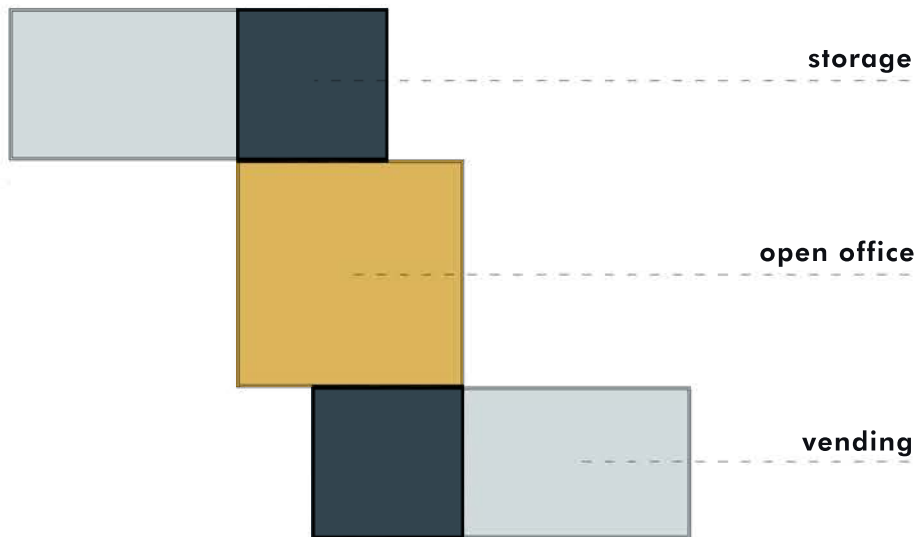
Let's start by considering just the first storey

STORAGE: area of storage façade = area of storage external wall  
Area of storage external wall =  $20\text{m} \times 4\text{m} \times 4 = 320\text{ m}^2$

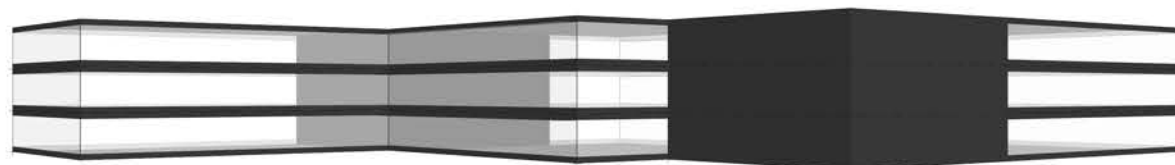
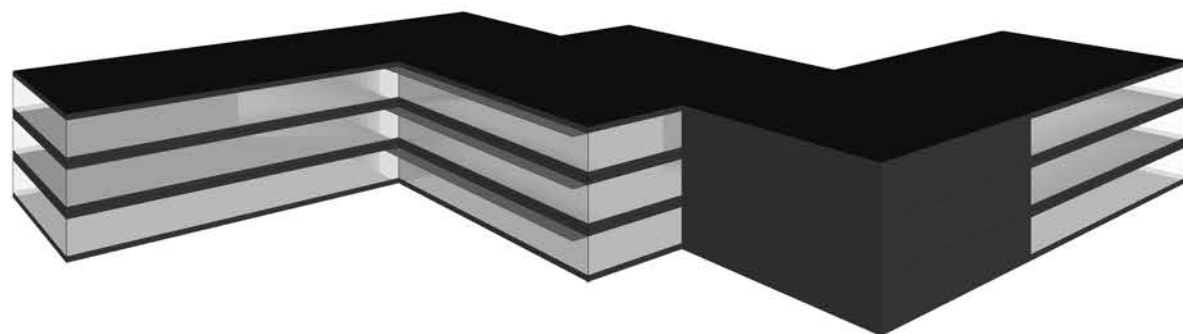
OPEN OFFICE AND VENDING: window to wall ratio 0.75  
Area of open office and vending façade =  $(30\text{m} \times 4\text{m} \times 6) + (20\text{m} \times 4\text{m} \times 2) + (10\text{m} \times 4\text{m} \times 2) = 960\text{ m}^2$   
Area of open office and vending external wall =  $960\text{ m}^2 \times 25/100 = 240\text{ m}^2$

Total external wall area for one storey =  $320\text{ m}^2 + 240\text{ m}^2 = 560\text{ m}^2$   
All the storeys are the same

**Total external wall area** =  $560\text{ m}^2 \times 3 = 1680\text{ m}^2$



- storage - 2400 sqm
- open office - 2700 sqm
- vending - 3600 sqm



# THE LOCATION

NYC - STOCKHOLM - ALEXANDRIA



## LOCATION

United States of America

LATITUDE: **40.78**

LONGITUDE: **-73.97**

ELEVATION: **57 m/sealevel**

## WORST CASE SCENARIOS

WINTER DESIGN DAY: **21.01**

MINIMUM DRY BULB TEMPERATURE: **-10.7 °C**

SUMMER DESIGN DAY: **21.07**

MAXIMUM DRY BULB TEMPERATURE: **31.1 °C**



## LOCATION

Sweden | Europe

LATITUDE: **59.65**

LONGITUDE: **17.95**

ELEVATION: **61 m/sealevel**

## WORST CASE SCENARIOS

WINTER DESIGN DAY: **21.02**

MINIMUM DRY BULB TEMPERATURE: **-17.8 °C**

SUMMER DESIGN DAY: **21.07**

MAXIMUM DRY BULB TEMPERATURE: **27.1 °C**



## LOCATION

Egypt | Africa

LATITUDE: **31.2**

LONGITUDE: **29.95**

ELEVATION: **7 m/sealevel**

## WORST CASE SCENARIOS

WINTER DESIGN DAY: **21.01**

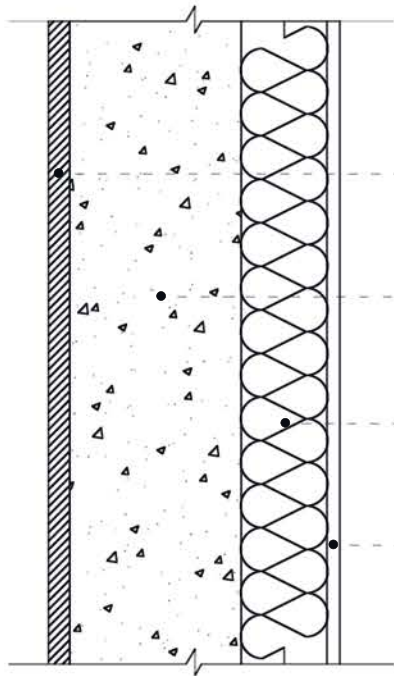
MINIMUM DRY BULB TEMPERATURE: **6.9 °C**

SUMMER DESIGN DAY: **21.08**

MAXIMUM DRY BULB TEMPERATURE: **33 °C**

# THE WALLS

## COMPOSITION AND U-VALUE



### 1. BASE CASE STUDY

**wood** 2.5 cm

$$R = 0.22 \text{ m}^2\text{C/W}$$

**h. concrete** 20 cm

$$R = 0.12 \text{ m}^2\text{C/W}$$

**glass fiber insulation** 9 cm

$$R = 2.52 \text{ m}^2\text{C/W}$$

**gypsum** 1.3 cm

$$R = 0.079 \text{ m}^2\text{C/W}$$

### OVERALL HEAT TRANSFER COEFFICIENT (U-factor) CALCULATION

$U = 1/R$  (overall unit thermal resistance)

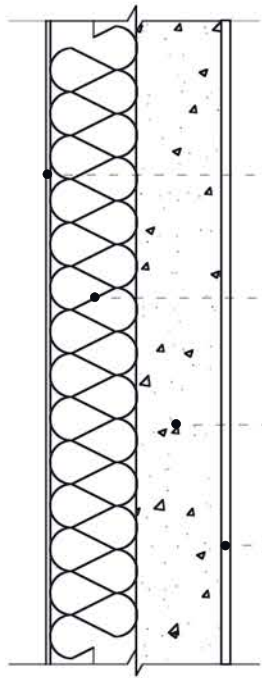
[Glass fiber insulation 2.5 cm:  $R = 0.70 \text{ m}^2\text{C/W}$

Glass fiber insulation 9 cm:  $R = (0.70/2.5) \times 9 = 2.52 \text{ m}^2\text{C/W}$ ]

$$R_{\text{TOTAL}} = (0.22 + 0.12 + 2.52 + 0.079) \text{ m}^2\text{C/W} = 2.94 \text{ m}^2\text{C/W}$$

$$U_{\text{TOTAL1}} = 1 / 2.94 \text{ m}^2\text{C/W} = \mathbf{0.34 \text{ W/m}^2\text{C}}$$

$$U_{\text{TOTAL1}} \times A_{\text{TOTALWALL}} = 0.34 \text{ W/m}^2\text{C} \times 1680 \text{ m}^2 = 571.43 \text{ W/}^\circ\text{C}$$



## 2. LIGHTER WALL

**metal** 0.5 cm

**R** = 0 m<sup>2</sup>C/W

**glass fiber insulation** 9 cm

**R** = 2.52 m<sup>2</sup>C/W

**l. concrete** 10 cm

**R** = 0.27 m<sup>2</sup>C/W

**plywood** 1.3 cm

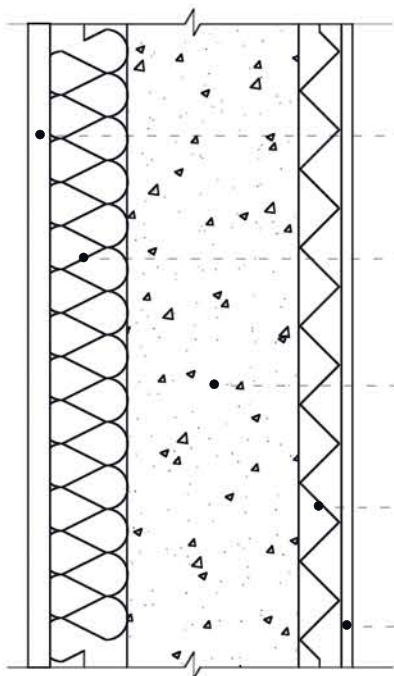
**R** = 0.11 m<sup>2</sup>C/W

## OVERALL HEAT TRANSFER COEFFICIENT (U-factor) CALCULATION

$$R_{\text{TOTAL}} = (0 + 2.52 + 0.27 + 0.11) \text{ m}^2\text{C/W} = 2.9 \text{ m}^2\text{C/W}$$

$$U_{\text{TOTAL2}} = 1/2.9 \text{ m}^2\text{C/W} = \mathbf{0.35 \text{ W/m}^2\text{C}}$$

$$U_{\text{TOTAL1}} \times A_{\text{TOTALWALL}} = 0.35 \text{ W/m}^2\text{C} \times 1680 \text{ m}^2 = 579.31 \text{ W/}^\circ\text{C}$$



## 3. THICKER WALL

**plaster** 2.5 cm

**R** = 0.037 m<sup>2</sup>C/W

**glass fiber insulation** 9 cm

**R** = 2.52 m<sup>2</sup>C/W

**h. concrete** 20 cm

**R** = 0.12 m<sup>2</sup>C/W

**acoustic insulation** 5 cm

**R** = 0.32 m<sup>2</sup>C/W

**gypsum** 1.3 cm

**R** = 0.079 m<sup>2</sup>C/W

## OVERALL HEAT TRANSFER COEFFICIENT (U-factor) CALCULATION

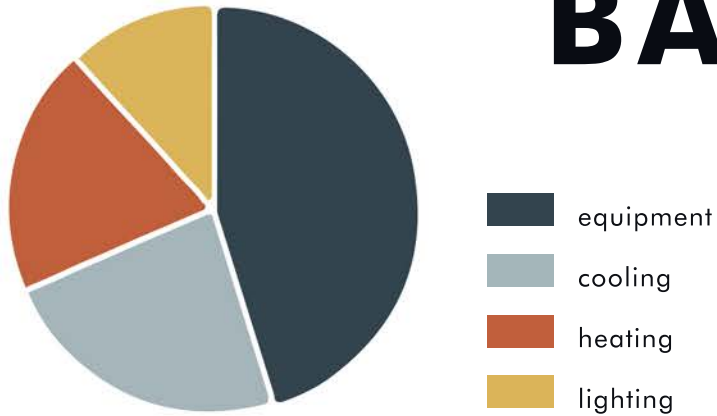
$$R_{\text{TOTAL}} = (0.037 + 2.52 + 0.12 + 0.32 + 0.079) \text{ m}^2\text{C/W} = 3.08 \text{ m}^2\text{C/W}$$

$$U_{\text{TOTAL1}} = 1 / 3.08 \text{ m}^2\text{C/W} = \mathbf{0.33 \text{ W/m}^2\text{C}}$$

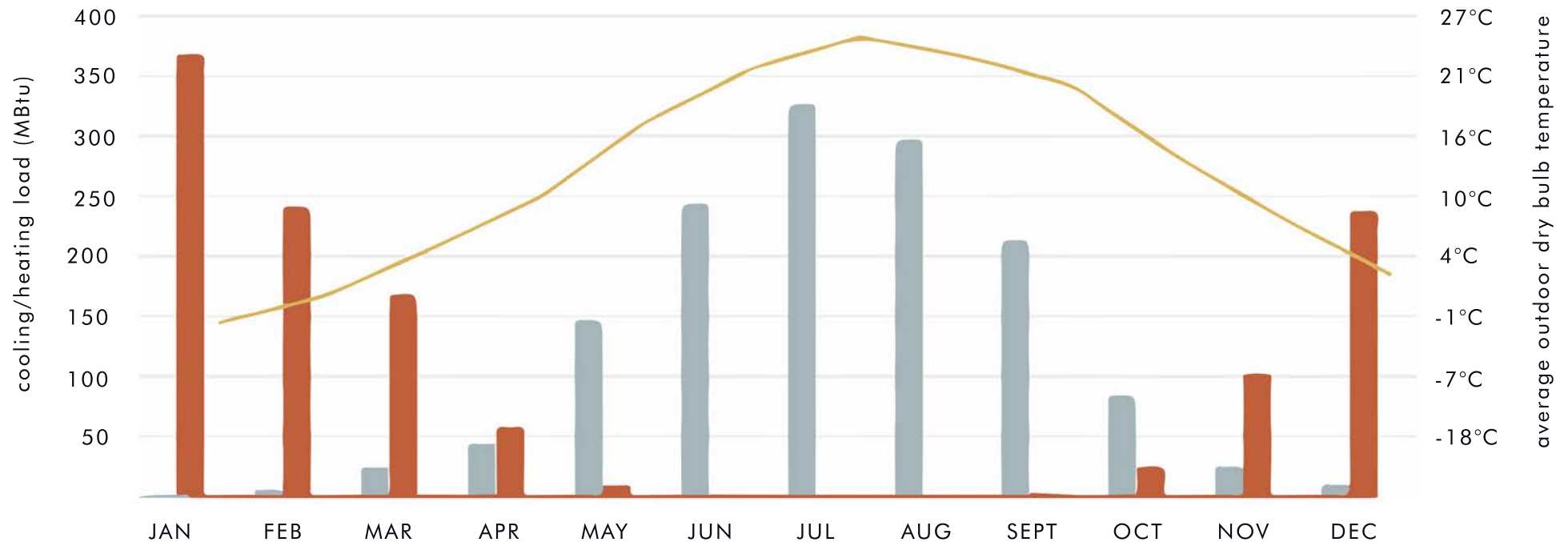
$$U_{\text{TOTAL1}} \times A_{\text{TOTALWALL}} = 0.33 \text{ W/m}^2\text{C} \times 1680 \text{ m}^2 = 545.45 \text{ W/}^\circ\text{C}$$

# BASE CASE STUDY

NYC - WALL1



## ENERGY USE - ANNUAL OVERVIEW



## HVAC MONTHLY LOAD PROFILE

# THE RESULTS

## CONFRONTATION AND CONCLUSIONS

### WALL 1

	NYC	Stockholm	Alexandria
HEATING [GJ]	1272,45	2046,03	69,2
COOLING [GJ]	1489,63	591,1	2950,96
TOTAL [GJ]	2762,08	2637,13	3020,16

### WALL 2

	NYC	Stockholm	Alexandria
HEATING [GJ]	1256,67	2042,18	66,5
COOLING [GJ]	1487,56	584,96	2953,28
TOTAL [GJ]	2744,23	2627,14	3019,78

### WALL 3

	NYC	Stockholm	Alexandria
HEATING [GJ]	1252,59	2018,16	66,18
COOLING [GJ]	1490,49	591,18	2955,52
TOTAL [GJ]	2743,08	2609,34	3021,7

The results reflect the different climates of the cities

The best performance of the walls is in Stockholm

THE BEST WALL IS WALL 3