

## Task 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in ClassRoom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

| Il tempo oggi in Piacenza<br>Martedì, 03 Dicembre 2019 |   |   |   |  |   |   |   |
|--|---|---|---|--|---|---|---|
|  | 13:00   | 14:00   | 16:00   | 18:00  | 20:00   | 21:00   | 22:00   |
|  |  |  |  |  |  |  |  |
| Temperatura effettiva                                  | 9°C   | 10°C  | 8°C   | 6°C  | 4°C   | 2°C   | 2°C   |
| Temperatura percepita                                  | 7°C   | 10°C  | 6°C   | 4°C  | 2°C   | 0°C   | 0°C   |
| Precipitazioni   | 0 mm  | 0 mm  | 0 mm  | 0 mm   | 0 mm  | 0 mm  | 0 mm  |
| Umidità  | 67 %  | 65 %  | 69 %  | 70 %   | 75 %  | 83 %  | 87 %  |
| Pressione atmosferica                                  | 1025 hPa  | 1025 hPa  | 1025 hPa  | 1026 hPa   | 1027 hPa  | 1027 hPa  | 1028 hPa  |

NOW, it's nearly 20:00.

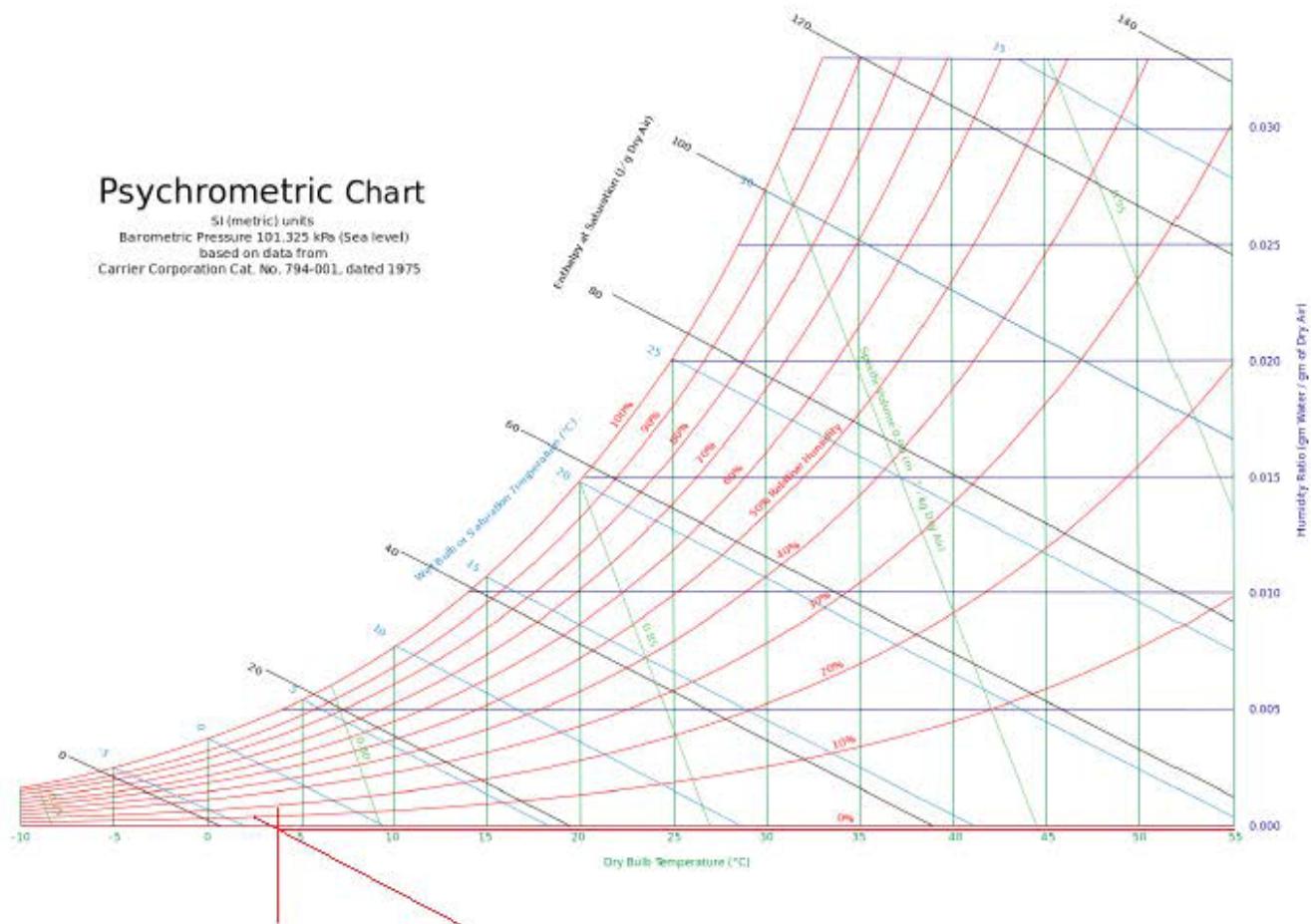
The Relative humidity is 75%,  $\phi$

Air total pressure is 1027 hPa, P=102.7 KPa;

Temperature to be utilized is 4°C, the temperature in Kelvin temperature scale T=277.15K

## Psychrometric Chart

SI (metric) units  
Barometric Pressure 101.325 kPa (Sea level)  
based on data from  
Carrier Corporation Cat. No. 794-001, dated 1975



Using the psychrometric chart, we can see:

The humidity ratio, the absolute humidity  $\omega = 0.0040$

The wet bulb temperature is  $T_{wb} = 2.5^{\circ}\text{C}$

$$\therefore \omega = \frac{0.622P_v}{P_a} = \frac{0.622P_v}{P - P_v} = 0.0040, \quad P = 102.6 \text{ kPa}$$

$$\therefore P_v = 0.665 \text{ kPa}$$

$$\therefore \phi = \frac{m_v}{m_g} = 75\%, \quad \text{for ideal gases } m = \frac{P_v}{R_{sp}T}, \text{ we know that } R_{sp} = 0.4615$$

The volume of Aula  $A=V$

$$m_v = \frac{0.893V}{0.4615 \times 277.15} = 6.98 \times 10^{-3}V$$

$$m_g = \frac{m_v}{75\%} = 9.31 \times 10^{-3}V$$

## Task 2

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

| BRINDISI, Italy  |                        |      |                       |                               |                    |               |            |            |             |   |      |      |      |                       | WMO#: 163200             |  |  |  |
|--|------------------------|------|-----------------------|-------------------------------|--------------------|---------------|------------|------------|-------------|---|------|------|------|-----------------------|--------------------------|--|--|--|
| Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2                    |                        |      | Time Zone: 1.00 (EUW) |                               |                    | Period: 86-10 |            |            | WBAN: 99999 |   |      |      |      |                       |                          |  |  |  |
| Annual Heating and Humidification Design Conditions              |                        |      |                       |                               |                    |               |            |            |             |   |      |      |      |                       |                          |  |  |  |
| Coldest Month  | Heating DB             |      |                       | Humidification DP/MCDB and HR |                    |               |            |            |             | Coldest month WS/MCDB                     |      |      |      | MCWS/PCWD to 99.6% DB |                          |  |  |  |
|  | 99.6%                  | 99%  | DP                    | HR                            | MCDB               | DP            | HR         | MCDB       | WS          | MCDB                                      | WS   | MCDB | MCWS | PCWD                  |                          |  |  |  |
| (1)  | (a)                    | (b)  | (c)                   | (d)                           | (e)                | (f)           | (g)        | (h)        | (i)         | (j)                                       | (k)  | (l)  | (m)  | (n)                   | (o)                      |  |  |  |
| (1)  | 2                      | 2.9  | 4.1                   | -5.1                          | 2.5                | 7.2           | -3.0       | 3.0        | 7.4         | 13.4                                      | 10.2 | 12.4 | 10.6 | 3.4                   | 250                      |  |  |  |
| Annual Cooling, Dehumidification, and Enthalpy Design Conditions |                        |      |                       |                               |                    |               |            |            |             |   |      |      |      |                       | (1)                      |  |  |  |
| Hottest Month  | Hottest Month DB Range |      |                       | Cooling DB/MCWB               |                    |               |            |            |             | Evaporation WB/MCDB                       |      |      |      | MCWS/PCWD to 0.4% DB  |                          |  |  |  |
|  | DB                     | MCWB | DB                    | MCWB                          | DB                 | MCWB          | WB         | MCDB       | WB          | MCDB                                      | WB   | MCDB | MCWS | PCWD                  |                          |  |  |  |
| (2)  | (a)                    | (b)  | (c)                   | (d)                           | (e)                | (f)           | (g)        | (h)        | (i)         | (j)                                       | (k)  | (l)  | (m)  | (n)                   | (o)                      |  |  |  |
| (2)  | 8                      | 7.1  | 32.8                  | 23.6                          | 31.1               | 24.3          | 29.9       | 24.3       | 27.2        | 29.7                                      | 26.3 | 29.0 | 25.6 | 28.3                  | 4.2                      |  |  |  |
| Dehumidification DP/MCDB and HR                                  |                        |      |                       |                               |                    |               |            |            |             |   |      |      |      |                       | Hours 8 to 4 & 12.8/20.6 |  |  |  |
| DP   | 0.4%                   | 1%   | 2%                    | DP                            | HR                 | MCDB          | DP         | HR         | MCDB        | Enth                                      | MCDB | Enth | MCDB | Enth                  | MCDB                     |  |  |  |
|  | (a)                    | (b)  | (c)                   | (d)                           | (e)                | (f)           | (g)        | (h)        | (i)         | (j)                                       | (k)  | (l)  | (m)  | (n)                   | (o)                      |  |  |  |
| (3)  | 26.3                   | 21.8 | 29.2                  | 25.4                          | 20.7               | 28.5          | 24.7       | 19.7       | 27.9        | 86.0                                      | 30.1 | 82.2 | 29.1 | 78.5                  | 28.3                     |  |  |  |
| Extreme Annual Design Conditions                                 |                        |      |                       |                               |                    |               |            |            |             |   |      |      |      |                       | (3)                      |  |  |  |
| Extreme Annual WS  |                        |      | Extreme Max WB        | Extreme Annual DB             |                    |               |            |            |             | n-Year Return Period Values of Extreme DB |      |      |      |                       |                          |  |  |  |
| 1%   | 2.5%                   | 5%   |                       | Mean                          | Standard deviation | n=5 years     | n=10 years | n=20 years | n=50 years  | Min                                       | Max  | Min  | Max  | Min                   | Max                      |  |  |  |
| (4)  | (a)                    | (b)  | (c)                   | (d)                           | (e)                | (f)           | (g)        | (h)        | (i)         | (j)                                       | (k)  | (l)  | (m)  | (n)                   | (o)                      |  |  |  |
| (4)  | 11.3                   | 9.9  | 8.7                   | 31.4                          | 0.4                | 37.3          | 1.4        | 3.0        | -0.6        | 39.4                                      | -1.4 | 41.1 | -2.2 | 42.8                  | -3.2                     |  |  |  |

Noc=2

Height=2.5m<sup>2</sup>

Conditioned Floor Area=200m<sup>2</sup>

**Internal Gains:**

$$\dot{Q}_{igsensible} = 136 + 2.2A_{cf} + 22N_{oc} = 136 + 2.2 \times 200 + 22 \times 2 = 620W$$

$$\dot{Q}_{iglatent} = 20 + 0.22A_{cf} + 12N_{oc} = 20 + 0.22 \times 200 + 12 \times 2 = 88W$$

**Infiltration:**

**Table 3 Unit Leakage Areas**

| <b>Construction</b> | <b>Description</b>                                     | $A_{ul}$ , $\text{cm}^2/\text{m}^2$ |
|---------------------|--|-------------------------------------|
| Tight               | Construction supervised by air-sealing specialist      | 0.7                                 |
| Good                | Carefully sealed construction by knowledgeable builder | 1.4                                 |
| Average             | Typical current production housing                     | 2.8                                 |
| Leaky               | Typical pre-1970 houses                                | 5.6                                 |
| Very leaky          | Old houses in original condition                       | 10.4                                |

| <b>Situation</b>  | <b>Include</b>                                   | <b>Exclude</b>       |
|---|--|----------------------|
| Ceiling/roof combination (e.g., cathedral ceiling without attic)    | Gross surface area                               |                      |
| Ceiling or wall adjacent to attic                                   | Ceiling or wall area                             | Roof area            |
| Wall exposed to ambient   | Gross wall area<br>(including fenestration area) |                      |
| Wall adjacent to unconditioned buffer space (e.g., garage or porch) | Common wall area                                 | Exterior wall area   |
| Floor over open or vented crawlspace                                | Floor area                                       | Crawlspace wall area |
| Floor over sealed crawlspace  | Crawlspace wall area                             | Floor area           |
| Floor over conditioned or semiconditioned basement                  | Above-grade basement wall area                   | Floor area           |
| Slab floor  |  | Slab area            |

$$A_{ul}(\text{GOOD CONSTRUCTION}) = 1.4 \text{ cm}^2/\text{m}^2$$

$$A_{es} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$$

$$A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

The cooling temperature in Brindisi is  $T_{cooling} = 24^\circ\text{C}$  and heating temperature  $T_{heating} = 20^\circ\text{C}$  in Brindisi

$$\Delta T_{cooling} = 31.1 - 24 = 7.1^\circ\text{C} = 7.1K$$

$$\Delta T_{heating} = 20 - (-4.1) = 24.1^\circ\text{C} = 24.1K$$

$$DR = 7.1^\circ\text{C} = 7.1K$$

$$IDF_{heating} = 0.073 \text{ L/s} \cdot \text{cm}^2$$

$$IDF_{cooling} = 0.033 \text{ L/s} \cdot \text{cm}^2$$

$$\dot{V}_{infiltration\ heating} = A_L \times IDF_{heating} = 481.6 \times 0.073 = 35.157 \text{ L/S}$$

$$\dot{V}_{infiltration\ cooling} = A_L \times IDF_{cooling} = 481.6 \times 0.033 = 15.89 \text{ L/}$$

$$\dot{V}_{ventilation} = 0.05A_{cf} + 3.5(N_{br} + 1) = 0.05 \times 200 + 3.5 \times (1 + 1) = 17 \text{ L/S}$$

$$\dot{V}_{inf-ventilation\ heating} = 35.157 + 17 = 52.157 \text{ L/S}$$

$$\dot{V}_{inf-ventilation\ cooling} = 15.89 + 17 = 32.893 \text{ L/S}$$

$$C_{sensible} = 1.23, C_{latent} = 3010, \Delta\omega_{cooling} = 0.0039$$

$$\dot{Q}_{inf-ventilation\ cooling\ sensible} = C_{sensible} \times \dot{V} \times \Delta T_{cooling} = 1.23 \times 32.893 \times 7.1 = 287.25W$$

$$\dot{Q}_{inf-ventilation\ heating\ sensible} = C_{sensible} \times \dot{V} \times \Delta T_{heating} = 1.23 \times 52.157 \times 24.1 = 1546.09W$$

$$\dot{Q}_{inf-ventilation\ cooling\ latent} = C_{latent} \times \dot{V} \times \Delta\omega_{cooling} = 3010 \times 32.893 \times 0.0039 = 386.13W$$