1 Calculation of receiver position

1.1 Satellite and receiver clocks are synchronized

$$transittime^{(k)} = rxtime - txtime^{(k)}$$
 (1)

$$r^{(k)} = (rxtime - txtime^{(k)}) * c$$
 (2)

$$r^{(k)} = \sqrt{(x - x^{(k)})^2 + (y - y^{(k)})^2 + (z - z^{(k)})^2}$$
(3)

$$\sqrt{(x-x^{(k)})^2 + (y-y^{(k)})^2 + (z-z^{(k)})^2} = (rxtime - txtime^{(k)}) * c$$
 (4)

 $\begin{array}{ll} txtime^{(k)} = \text{time of transmission (measured by } k^{th's} \text{ satellite clock)} \\ rxtime & = \text{time of reception (measured by receiver clock)} \\ r^{(k)} & = \text{real (geometrical) range} \end{array}$

1.2 Satellite and receiver clocks are not synchronized

$$\rho^{(k)} = ((rxtime + \Delta t) - (txtime^{(k)} + \delta t^{(k)})) * c$$

$$(5)$$

$$\rho^{(k)} = (rxtime - txtime^{(k)}) * c - \delta t^{(k)} * c + \Delta t * c$$
(6)

$$\rho^{(k)} = r^{(k)} - \delta t^{(k)} * c + \Delta t * c \tag{7}$$

$$\rho^{'(k)} = \rho^{(k)} + \delta t^{(k)} * c = r^{(k)} + \Delta t * c$$
(8)

 $txtime^{(k)} = time of transmission (relative to gps system time)$

rxtime = time of reception (relative to gps system time)

 $\rho^{(k)}$ = pseudorange

 $\delta t^{(k)}$ = advance of the $k^{th's}$ satellite clock with respect to system time

 Δt = advance of the receiver clock with respect to system time

1.3 Time to solve navigation equations

Let's introduce function $f^{(k)} = f^{(k)}(x, y, z, \Delta t)$ of four variables

$$f^{(k)}(x, y, x, \Delta t) = \sqrt{(x - x^{(k)})^2 + (y - y^{(k)})^2 + (z - z^{(k)})^2} + \Delta t * c$$
 (9)

Above function can be expanded about the point $(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)$ using the Taylor series. It is deliberately truncated after the first-order partial derivatives to eliminate non-linear terms.

$$f^{(k)}(x, y, x, \Delta t) \approx f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t) + \frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial x} \Delta x + \frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial y} \Delta y + \frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial z} \Delta z + \frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial (\Delta t)} \Delta (\Delta t)$$

$$(10)$$

The partial derivatives evaluate as follows:

$$\frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial x} = \frac{\hat{x} - x^{(k)}}{\hat{r}}$$
(11)

$$\frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial y} = \frac{\hat{y} - y^{(k)}}{\hat{r}}$$
(12)

$$\frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial z} = \frac{\hat{z} - z^{(k)}}{\hat{r}}$$
(13)

$$\frac{\partial f^{(k)}(\hat{x}, \hat{y}, \hat{z}, \hat{\Delta}t)}{\partial (\Delta t)} = c \tag{14}$$

where

$$\hat{r} = \sqrt{(\hat{x} - x^{(k)})^2 + (\hat{y} - y^{(k)})^2 + (\hat{z} - z^{(k)})^2}$$
(15)

We shall have already noticed that our $f^{(k)}$ has the same form as our pseudorange $\rho^{'(k)}$. Thus we can write

$$\rho^{'(k)} = \rho^{'(k)} + \frac{\hat{x} - x^{(k)}}{\hat{x}} \Delta x + \frac{\hat{y} - y^{(k)}}{\hat{x}} \Delta y + \frac{\hat{z} - z^{(k)}}{\hat{x}} \Delta z + c * \Delta(\Delta t) \quad (16)$$

If we introduce new variables as follows

$$\Delta \rho^{'(k)} = \rho^{'(k)} - \rho^{'(k)} \tag{17}$$

$$a_x^{(k)} = \frac{\hat{x} - x^{(k)}}{\hat{r}} \tag{18}$$

$$a_y^{(k)} = \frac{\hat{y} - y^{(k)}}{\hat{r}} \tag{19}$$

$$a_z^{(k)} = \frac{\hat{z} - z^{(k)}}{\hat{r}} \tag{20}$$

Then we can rewrite equation (16) in a simpler form as

$$\Delta \rho^{'(k)} = a_x^{(k)} \Delta x + a_y^{(k)} \Delta y + a_z^{(k)} \Delta z + c * \Delta(\Delta t) \tag{21} \label{eq:21}$$

So, we have 4 unknowns: $\Delta x, \Delta y, \Delta z$ and $\Delta(\Delta t)$. Thus we need pseudorange measurements from 4 satellites which will give us set of four linear equations

$$\Delta \rho^{'(1)} = a_x^{(1)} \Delta x + a_y^{(1)} \Delta y + a_z^{(1)} \Delta z + c * \Delta(\Delta t)$$
 (22)

$$\Delta \rho^{'(2)} = a_x^{(2)} \Delta x + a_y^{(2)} \Delta y + a_z^{(2)} \Delta z + c * \Delta(\Delta t)$$
 (23)

$$\Delta \rho^{'(3)} = a_x^{(3)} \Delta x + a_y^{(3)} \Delta y + a_z^{(3)} \Delta z + c * \Delta(\Delta t)$$
 (24)

$$\Delta \rho'^{(4)} = a_x^{(4)} \Delta x + a_y^{(4)} \Delta y + a_z^{(4)} \Delta z + c * \Delta(\Delta t)$$
 (25)

Those equations can be rewritten using matrix notation

$$\Delta \boldsymbol{\rho}' = \begin{pmatrix} \Delta \rho^{'(1)} \\ \Delta \rho^{'(2)} \\ \Delta \rho^{'(3)} \\ \Delta \rho^{'(4)} \end{pmatrix}$$
 (26)

$$\boldsymbol{H} = \begin{pmatrix} a_x^{(1)} & a_y^{(1)} & a_z^{(1)} & 1\\ a_x^{(2)} & a_y^{(2)} & a_z^{(2)} & 1\\ a_x^{(3)} & a_y^{(3)} & a_z^{(3)} & 1\\ a_x^{(4)} & a_y^{(4)} & a_z^{(4)} & 1 \end{pmatrix}$$
(27)

$$\Delta s = \begin{pmatrix} \Delta x \\ \Delta y \\ \Delta z \\ c * \Delta(\Delta t) \end{pmatrix} \tag{28}$$

And finally

$$\Delta \rho' = H \Delta s \tag{29}$$

Naturally (30) has the following solution

$$\Delta s = H^{-1} \Delta \rho' \tag{30}$$