



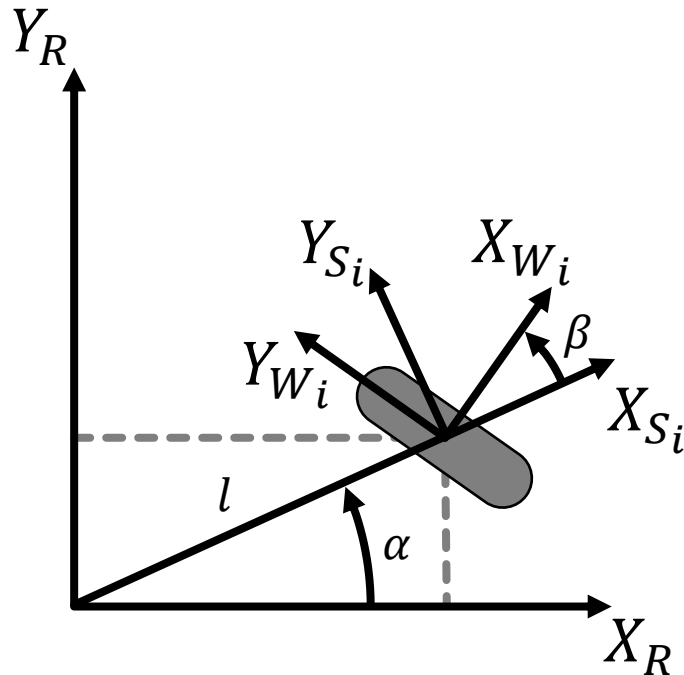
Wheeled Locomotion | Wheeled Kinematics

Autonomous Mobile Robots

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Review: Standard wheel



- The constraints imposed by a single wheel, W_i , can be expressed as follows

- Rolling constraint

$$J_{1,i}(\beta_{s,i})R(\theta)\dot{\xi}_I - \dot{\phi}_i r_i = 0$$

- No-sliding constraint

$$C_{1,i}(\beta_{s,i})R(\theta)\dot{\xi}_I = 0$$

Differential Kinematics

- Given a wheeled robot, each wheel imposes n constraints
- Only fixed and steerable standard wheels impose no-sliding constraints
- Suppose a robot has n wheels of radius r_i , the individual wheel constraints can be concatenated in matrix form:
 - Rolling constraints

$$J_1(\beta_S)R(\theta)\dot{\xi}_I - J_2\dot{\phi} = 0, \quad J_1(\beta_S) = \begin{bmatrix} J_{1f} \\ J_{1s}(\beta_S) \end{bmatrix}, \quad J_2 = \text{diag}(r_1, \dots, r_N), \quad \dot{\phi} = \begin{bmatrix} \dot{\phi}_1 \\ \vdots \\ \dot{\phi}_N \end{bmatrix}$$

- No-sliding constraints

$$C_1(\beta_S)R(\theta)\dot{\xi}_I = 0, \quad C_1(\beta_S) = \begin{bmatrix} C_{1f} \\ C_{1s}(\beta_S) \end{bmatrix}$$

Differential Kinematics

- Stacking the rolling and no-sliding constraints gives an expression for the differential kinematics

$$\begin{bmatrix} J_1(\beta_s) \\ C_1(\beta_s) \end{bmatrix} R(\theta) \dot{\xi}_I = \begin{bmatrix} J_2 \\ 0 \end{bmatrix} \dot{\phi}$$

- Solving this equation for $\dot{\xi}_I$ yields the **forward differential kinematics** equation needed for computing wheel odometry
- Solving this equation for $\dot{\phi}$ yields the **inverse differential kinematics** equation needed for control

Degree of Maneuverability

- The maneuverability of a robot is measured by different metrics
- Mobility – restricted by no-sliding constraints
 - δ_m : degree of mobility
- Steerability – additional freedom due to steering mechanisms
 - δ_s : degree of steerability

Degree of Mobility

- To avoid any lateral slip, the motion vector needs to satisfy:

$$C_1(\beta_S)R(\theta)\dot{\xi}_I = 0, \quad C_1(\beta_S) = \begin{bmatrix} C_{1f} \\ C_{1s}(\beta_S) \end{bmatrix}$$

- Hence, $R(\theta)\xi_I$ must belong to the null space, N , of $C_1(\beta_S)$
 - The null space of $C_1(\beta_S)$ is the set of all vectors, n , such that $C_1(\beta_S)n = 0$
 - Intuitively, this means that all the axes associated with the no-slip constraints from all standard wheels converge at a single point—the instantaneous center of rotation

Degree of Mobility

- The larger the rank of $C_1(\beta_s)$, the more constrained a robot's mobility. The degree of mobility, δ_m , reflects this:

$$\delta_m = \dim N[C_1(\beta_s)] = 3 - \text{rank}[C_1(\beta_s)]$$

- For a robot with no standard wheels:

$$\text{rank}[C_1(\beta_s)] = 0, \quad \delta_m = 3$$

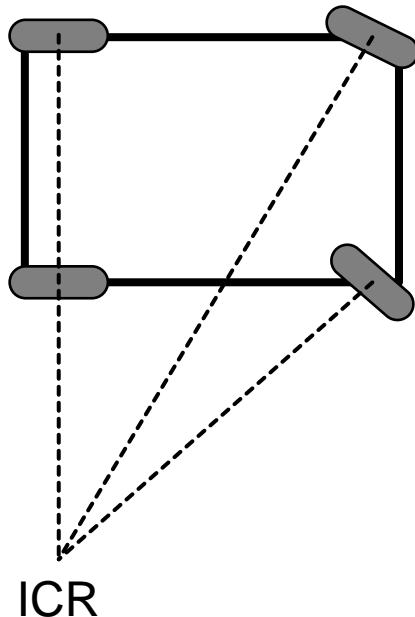
- For a robot with all directions constrained

$$\text{rank}[C_1(\beta_s)] = 3, \quad \delta_m = 0$$

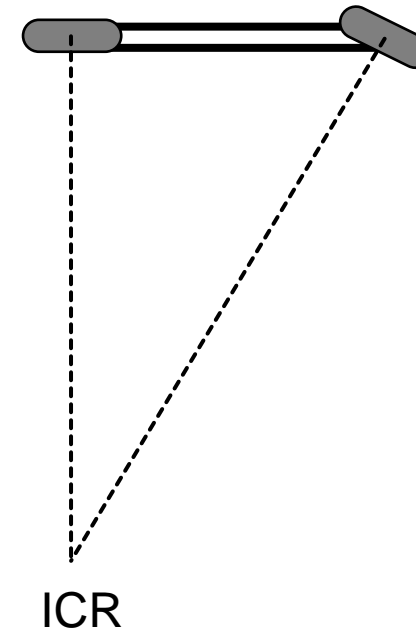
Degree of Mobility

- Instantaneous Center of Rotation (ICR)
 - For any robot with $\delta_m = 2$, the ICR is constrained to lie on a line
 - For any robot with $\delta_m = 3$, the ICR can be any point on the 2D plane

Ackerman Steering, $\delta_m = 2$



Bicycle, $\delta_m = 2$

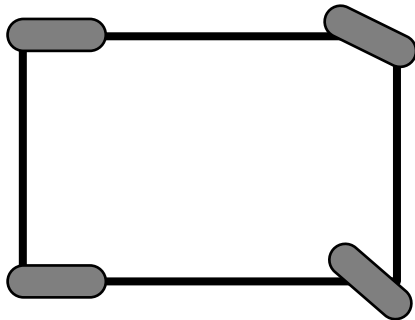


Degree of Steerability

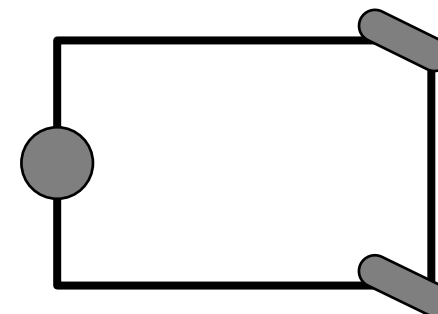
- Degree of steerability,
 - Represents an indirect degree of motion
 - The particular orientation at any instant imposes a kinematic constraint
 - The ability to change that orientation leads to an additional degree of maneuverability

$$\delta_s = \text{rank}[C_{1s}(\beta_s)], \quad 0 \leq \delta_s \leq 2$$

Ackermann Steering, $\delta_s = 1$



Two Steer, $\delta_s = 2$

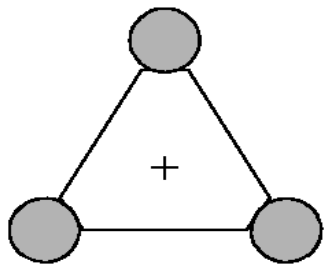


Degree of Maneuverability

- The Degree of Maneuverability, δ_M , combines mobility and steerability

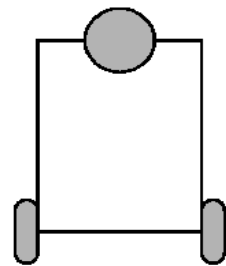
$$\delta_M = \delta_m + \delta_s$$

- Examples



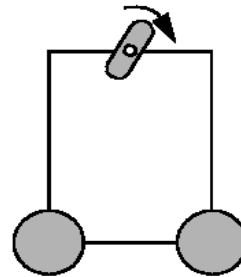
Omnidirectional

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 3 \\ \delta_s &= 0\end{aligned}$$



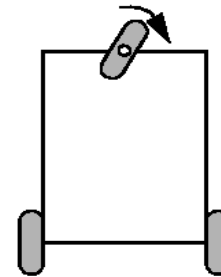
Differential

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 2 \\ \delta_s &= 0\end{aligned}$$



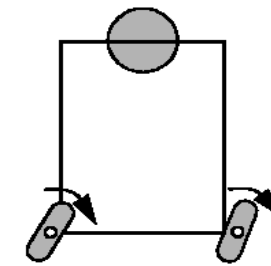
Omni-Steer

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 2 \\ \delta_s &= 1\end{aligned}$$



Tricycle

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 1 \\ \delta_s &= 1\end{aligned}$$



Two-Steer

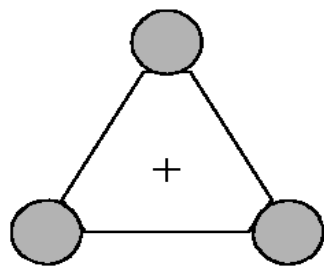
$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 1 \\ \delta_s &= 2\end{aligned}$$

Degree of Maneuverability

- The Degree of Maneuverability, δ_M , combines mobility and steerability

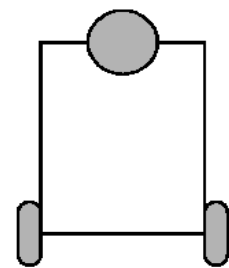
$$\delta_M = \delta_m + \delta_s$$

- Note: Two robots with the same δ_M may not be equivalent **instantaneously**



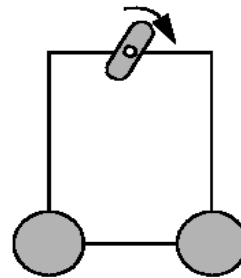
Omnidirectional

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 3 \\ \delta_s &= 0\end{aligned}$$



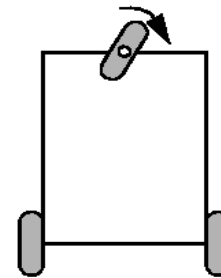
Differential

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 2 \\ \delta_s &= 0\end{aligned}$$



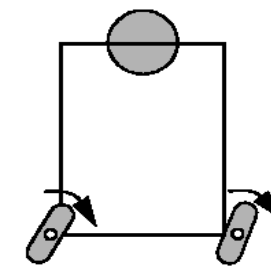
Omni-Steer

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 2 \\ \delta_s &= 1\end{aligned}$$



Tricycle

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 1 \\ \delta_s &= 1\end{aligned}$$



Two-Steer

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 1 \\ \delta_s &= 2\end{aligned}$$

Degree of Maneuverability

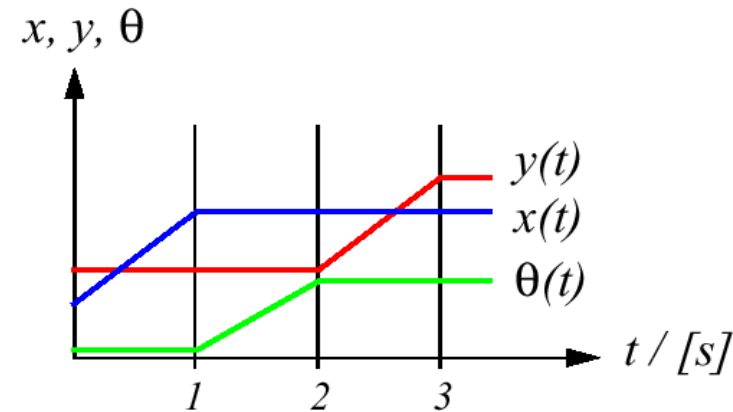
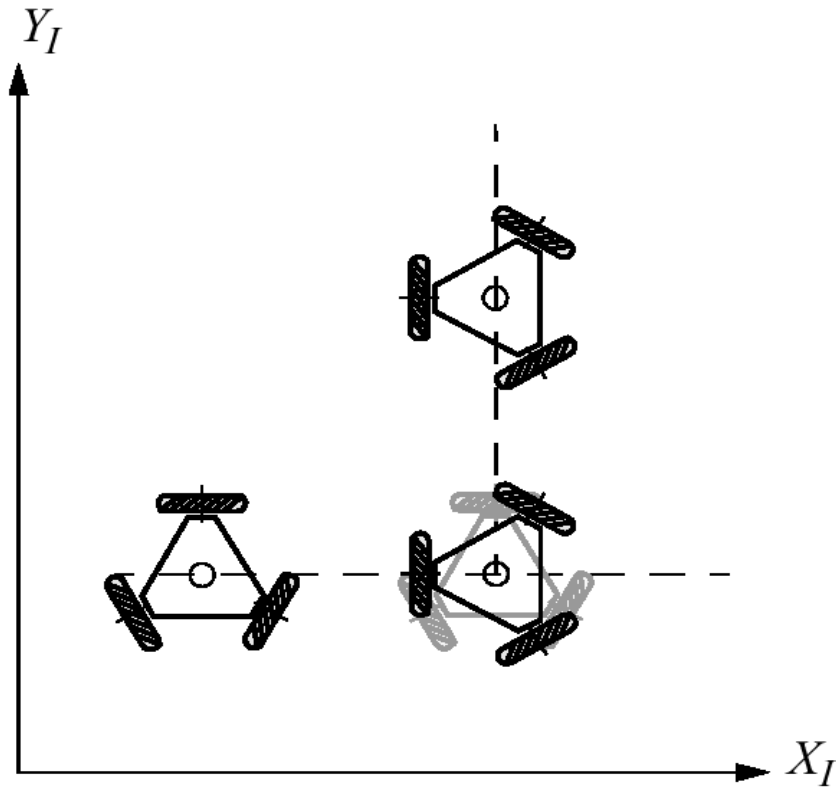
Omni-Drive Example

- Three fixed Swedish wheels

$$\delta_M = 3$$

$$\delta_m = 3$$

$$\delta_s = 0$$



Degree of Maneuverability

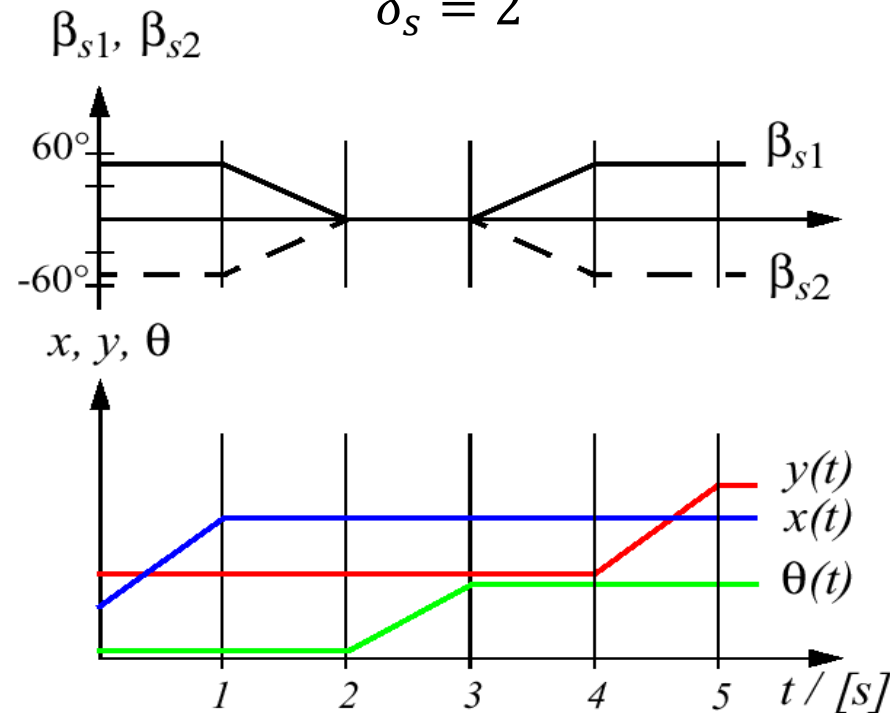
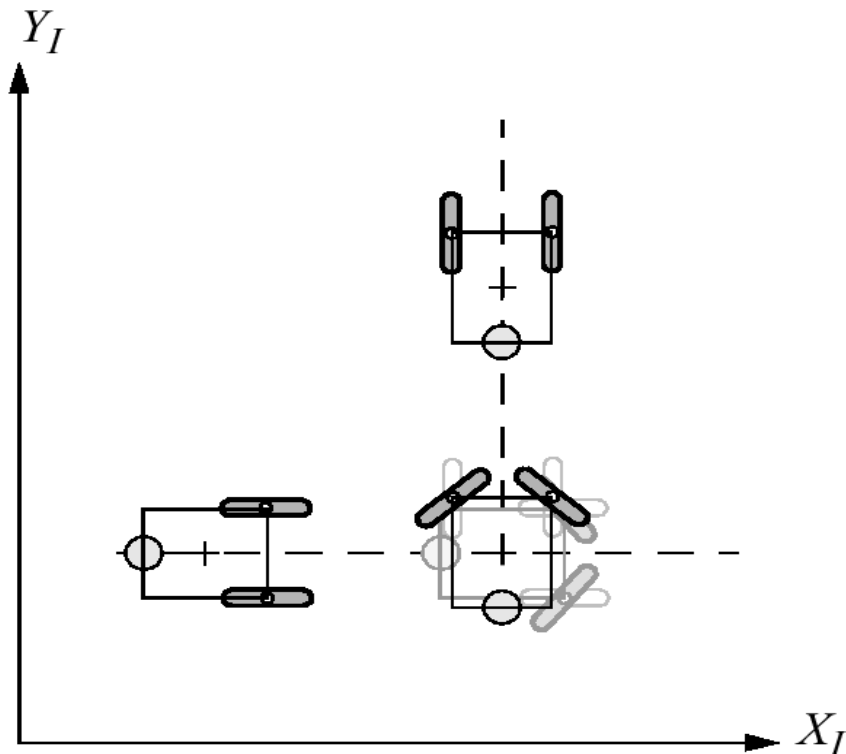
Two-Steer Example

- Two steerable standard wheels

$$\delta_M = 3$$

$$\delta_m = 1$$

$$\delta_s = 2$$



Summary

- Stacking individual wheel constraints gives an equation that may be manipulated to derive the forward and inverse differential kinematics equations for a wheeled mobile robot

$$\begin{bmatrix} J_1(\beta_s) \\ C_1(\beta_s) \end{bmatrix} R(\theta) \dot{\xi}_I = \begin{bmatrix} J_2 \\ 0 \end{bmatrix} \dot{\phi}$$

- Analysis of the component parts of this equation lets us classify wheeled mobile robots in terms of maneuverability—a combination of mobility and steerability