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## Chapter 4

# A data assimilating state-space model for algal growth under controlled conditions within a photobioreactor

## 4.1 Introduction

Microalgae are tiny organisms..

### 4.2 Methods

## 4.2.1 Data Model: Data description and collection methods

 $O_2$ , pH, DIC and alk observations collected over 4 days.

Gas, temperature, light and dilution rate were used as forcings.

#### 4.2.2 Process model: Carbon chemistry

To calculate the carbon chemistry of the photo-bioreactor, we would ideally use CO2SYS [4] to calculate HCO<sub>3</sub><sup>-</sup>, CO<sub>2</sub>, CO<sub>3</sub> and pH. CO2SYS is a program developed for CO<sub>2</sub> system calculations (CO2SYS) that calculates and returns a detailed state of the carbonate system of oceanographic water samples in seawater and freshwater [4]. It uses two of the four measurable carbonate system parameters (total alkalinity, total inorganic CO<sub>2</sub>, pH, and either fugacity fCO<sub>2</sub> or partial pressure of CO<sub>2</sub>) to calculate the other two parameters at a set of input conditions (temperature and pressure).

To incorporate CO2SYS into LiBbi for solving carbon chemistry on the timescale of the microalgae model, we explicitly define 2 iterations of the Newton-Raphson method for finding approximations to roots of real valued functions. The Newton-Raphson method is an iterative process considering a function, its derivative and an initial starting value. Vital to the convergence of the Newton-Raphson method is a good starting value. To provide a good starting value, we randomly sample from a range of CO2SYS input parameters (temperature = 20-30, salinity = 30-40, DIC = 200-2500, and alkalinity = 1500-3000) and fit an approximating equation to pH as a function of DIC, S and T (alk?). This gives us a close initial starting value for the Newton-Raphson method.

### Converges in 2-3 iterations

Choice of H2CO3 and HCO3- dissociation constants K1 and K2 was Mehrbach (refit BY DICKSON AND MILLERO) [BM: After the iterative approach is finalised, the K1 and K2 constants are adjusted based on measurements taken during the experiment, K1\*1.23 and K2\*0.53 measured during experiment] temperature: 2-35, salinity: 20-40, Seawater scale, Artificial seawater.

The CO2SYS Matlab version [6] was used to produce values of  $CO_2$  and  $HCO_3^-$  across DIC range 200-2500. Approximating equations were fit

Total inorganic  $CO_2$  ( $TCO_2$ ) is the sum of the dissolved  $CO_2$ , the carbonate ( $CO_{3-2}$ ), and the bicarbonate ( $HCO_3^-$ ).

# 4.2.3 Process model: Gas transfer equilibrium concentrations for $O_2$ and $CO_2$

The equilibrium concentration for  $CO_2$  solubility in water  $CO_{2H}$  ( $\mu$ mol/L) is calculated using Henry's law,

$$CO_{2H} = K0_{CO2} * fCO2 * 1.0220 * 1e6$$
 (4.1)

where fCO2 (atm) is the fugacity or approximately the partial pressure of  $CO_2$ , 1.0220 is the density of seawater (kg/L) at salinity 34 ppt and temperature 27°C

[5] [2].  $K0_{CO2}$  (mol/kg<sub>soln</sub>/atm) is the solubility of gas in seawater [BM: ask Chris: solubility of gas? is this right] and is calculated from the fitted van't Hoff equation and the logarithmic Setchenow salinity dependence [7],

$$K0_{CO2} = exp(-60.2409 + 93.4517(100/T_K) + 23.3585 * ln(T_K/100) +$$

$$S(0.023517 - 0.023656(T_K/100) + 0.0047036(T_K/100)^2))$$
(4.2)

where  $T_K$  is the temperature (K) and S is salinity (ppt).

Similarly the equilibrium concentration for  $O_2$  solubility in water  $O_{2H}$  is calculated using Henry's law,

$$O_{2H} = K0_{O2} * fO2 * 1.0220 * 1e - 6 (4.3)$$

where fO2 (atm) is the fugacity or approximately the partial pressure of  $O_2$ , 1.0220 is the density of seawater (kg/L) at salinity 34 ppt and temperature 27°C [5] [2], and  $KO_{O2}$  (mol/kg<sub>soln</sub>/atm) is the solubility of oxygen in seawater with an adjusted salinity dependence [1],

$$K0_{O2} = (exp(-1282.8704 + 36619.96/T_K + 223.1396 * log(T_K) - 0.354707 * T_K + S * (5.957e - 3 - 3.7353/T_K) + 3.68e - 6 * S^2))/0.2094e - 6$$

$$(4.4)$$

where  $T_K$  is the temperature (K) and S is salinity (ppt).

The equilibrium concentrations for  $O_2$  and  $CO_2$  are modelled together with the gas turning on and off during the experiment, as

$$kLA_{O2}\xi(O_{2H} - O_2) \tag{4.5}$$

$$0.893kLA_{O2}\xi(CO_{2H} - CO_2) \tag{4.6}$$

where  $\xi$  is the gas state (1= on, 0= off), and kLA<sub>O2</sub> is the mass transfer coefficient for air (d<sup>-1</sup>), and 0.893 is the ratio between measured O<sub>2</sub> and CO<sub>2</sub> mass transfer constants [3].

#### 4.2.4 Process model: Photosynthesis and respiration

Net photosynthesis

$$dDIC/dt = -P_1 * I * mm + R_1 \tag{4.7}$$

$$dO_2/dt = \frac{P_1 * I * mm - R_1}{R_Q} \tag{4.8}$$

Photosynthesis (P<sub>1</sub>) and respiration (R<sub>1</sub>) are both modelled as random walks, by taking P and R, previously constant parameters, and replacing them by  $P_1(t)$ and  $R_1(t)$ . Here, we take  $P_1(t)$  and  $R_1(t)$  to be such that

$$P_1(t + \Delta t) = P_1(t) + r_P$$

$$R_1(t + \Delta t) = R_1(t) + r_R$$

where  $r_P \sim N(0, \sigma_{r_P})$ ,  $r_R \sim N(0, \sigma_{r_R})$ , and  $\Delta t$  is the length of discrete time-step. For the purpose of the Bayesian analysis here,  $\sigma_{r_P}$  and  $\sigma_{r_R}$  are treated as a parameter to be inferred.

 $R_Q$  is the respiratory quotient, the ratio of  $CO_2$  produced and  $O_2$  consumed by a cell.

PAC is Photosynthetically Active Carbon, this is the type of carbon that the microalgae use for photosynthesis. This can be  $CO_2$ ,  $HCO_3^-$ , or a combination of both, eg  $PAC = CO_2 + HCO_3^-$  if the microalgae are using both carbon dioxide and bicarbonate for photosynthesis.

$$PAC = HCO_3^- \tag{4.9}$$

$$mm = \frac{PAC}{K_m + PAC} \tag{4.10}$$

## 4.2.5 Process model: Ordinary differential equations

Ode's:

Rate flux into cells gas transfer dilution
$$\frac{\partial DIC}{\partial t} = -(P - R) + \hat{Q}^{air}kLa^{air}_{CO_2}(CO_2^{air} - CO_2) + \frac{Q^M}{V}(DIC^M - DIC) \\
+ \hat{Q}^{co2}kLa^{co2}_{CO_2}(CO_2^{co2} - CO_2) + \frac{Q^M}{V}(O_2^M - O_2) \\
\frac{\partial O_2}{\partial t} = \frac{1}{R_Q}(P - R) + \hat{Q}^{air}kLa^{air}_{O_2}(O_2^{air} - O_2) + \frac{Q^M}{V}(O_2^M - O_2) \\
+ \hat{Q}^{co2}kLa^{co2}_{O_2}(O_2^{co2} - O_2) + \frac{Q^M}{V}(TA^M - TA) \\
\frac{\partial TA}{\partial t} = R_R(P) + \frac{Q^M}{V}(TA^M - TA)$$
(4.13)

	Symbol	Description	Prior / Value	Unit
State variable initial conditions	$DIC^0$	Dissolved inorganic carbon		$\mu\mathrm{M/L}$
	$O_2^0$	Oxygen		$\mu\mathrm{M/L}$
ial c	$TA^0$	Total alkalinity		$\mu\mathrm{M/L}$
e init	P <sup>0</sup> Rate of photosynthesis		$\mu \mathrm{M/L/day}$	
riabl	$\mathbb{R}^0$	Rate of respiration		$\mu \mathrm{M/L/day}$
te va	$\mathrm{pH}^0$	-		$\log_{10}(-\text{mol/L H+})$
Sta	$CO_2{}^0$	Carbon dioxide		$\mu\mathrm{M/L}$
	$HCO_3^{-0}$	Bicarbonate		$\mu\mathrm{M/L}$
	$CO_3^{2-0}$	Carbonate		$\mu\mathrm{M/L}$
erms	$\hat{Q}^{air}$	indicator for flow in air line	0 or 1	-
Gas transfer terms	$x_{CO_2}^{air}$	mole fraction of CO <sub>2</sub> atmosphere	400	ppm
trans	$CO_{2H}$	Equilibrium CO <sub>2</sub> concentration	Eq. 4.1	$\mu\mathrm{M/L}$
Gas 1	$CO_2^{air}$	sat $CO_2$ conc with atmosphere $x_{CO_2}^{air}CO_{2H}$		
	$kLa_{CO_2}^{air}$	$La_{CO_2}^{air}$ Mass transfer coefficient for $CO_2$ 0.893 $kLa_{O_2}^{air}$		$\mathrm{day}^{-1}$
	$x_{O_2}^{air}$	mole fraction of $O_2$ atmosphere	0.2094	atm

	$O_{2H}$	Equilibrium $O_2$ concentration	Eq. 4.3	$\mu\mathrm{M/L}$
	$O_2^{air}$	sat $O_2$ conc with atmosphere	$x_{O_2}^{air}O_{2H}$	
	au	half-life of $kLa^{air}_{O_2}$	range(2-20)	$\mathrm{min}^{-1}$
	$kLa^{air}_{O_2}$	Mass transfer coefficient for $O_2$	$\ln(2) * 24 * 60/\tau$	$day^{-1}$
SU	$Q^M$	rate		ml/day
terr	V	Volume of the reactor	500	ml
Dilution terms	$DIC^{M}$	Media dissolved inorganic carbon	1724.20	$\mu\mathrm{M/L}$
Dil	$O_2^M$	Media oxygen concentration	226.65	$\mu\mathrm{M/L}$
	$TA^{M}$	Media total alkalinity	1797.90	$\mu\mathrm{M/L}$
rms	$\hat{Q}^{CO2}$	indicator for dilution	0 or 1	-
Other dilution terms	$x_{O_2}^{CO2}$	mole fraction of	0	-
liluti	$O_2^{CO2}$	sat $CO_2$ conc with $CO_2$	$x_{O_2}^{CO2}O_{2H}$	
her o	$kLa^{CO2}_{O_2}$	mass transfer coefficient		$day^{-1}$
Ŏ	$O_2^{CO2}$			
	$x_{CO_2}^{CO2}$	mole fraction of	1	ppm
	$CO_2^{CO2}$	sat $CO_2$ conc with $CO_2$	$x_{CO_2}^{CO2}CO_{2H}$	
	$kLa_{CO_2}^{CO2}$	mass transfer coefficient	$0.893kLa^{CO2}_{O_2}$	$day^{-1}$
	$CO_2^{CO2}$			

Symbol	Variable	Units
DIC	Dissolved inorganic carbon concentration	$\mu \mathrm{mol/L}$
$O_2$	Oxygen	$\mu \mathrm{mol/L}$
рН	-	$\log_{10}(-\text{mol/L H+})$
$CO_2$	Carbon dioxide	$\mu \mathrm{mol/L}$
$HCO_3^-$	Bicarbonate	$\mu \mathrm{mol/L}$
$CO_3^{2-}$	Carbonate	$\mu \mathrm{mol/L}$
PAC	Photosynthetically active carbon	$\mu \mathrm{mols/L}$
mm	-	-
$\mathrm{kLA}_{O2}$	Mass transfer coefficient for $\mathcal{O}_2$	$d^{-1}$
$\mathrm{CO}_{2H}$	Equilibrium $CO_2$ concentration	$\mu \mathrm{mols/L}$
$\mathrm{K0}_{O2}$	Solubility of gas	$mol/kg_{soln}/atm$
$K0_{CO2}$	Solubility of gas	$mol/kg_{soln}/atm$
TA	Total alkalinity	$\mu \mathrm{mols/L}$
S	Salinity	ppt
fCO2	Fugacity/CO <sub>2</sub> partial pressure	atm
fO2	Fugacity/ $O_2$ partial pressure	atm
$K_m$	Carbon restriction	$\mu \mathrm{mols/L}$
P	Photosynthesis rate	$\mu$ mols/L/day
R	Respiration rate	$\mu$ mols/L/day
$R_R$	Redfield ratio	-
$\mathbf{R}_Q$	Respiratory quotient	-

Table 4.2 : Table of variables and parameters.

Symbol	Variable	Units
I	Light Intensity	normalised to 0-1
Τ	Temperature	• C
$\mathrm{T}_K$	Temperature	K
ξ	gasflow	on/off (1,0)

Table 4.3: Table of Forcings

## 4.2.6 Parameter Model: Priors

Decide whether the parameters vary in time or not. |

Parameter	Prior	Proposal
S	34	*
fCO2	397e-6	*
fO2	0.21	*
$\mathrm{kLA}_{O2}$	LogNormal(log(200.0), 0.5)	$\operatorname{LogNormal}(\operatorname{log}(kLA_{O2}), 0.5 \operatorname{prop}_{std})$
$K_m$	LogNormal(log(200.0), 0.8)	$LogNormal(log(K_m), 0.8prop_{std})$
$R_R$	Uniform(0.0001, 0.2)	$TrunNormal(R_R, 0.2prop_{std}, 0.0001, 0.2)$
$R_Q$	Uniform(0.66, 1)	$TrunNormal(R_Q, 0.2prop_{std}, 0.66, 1.0)$
$\sigma_P$	Normal(0.05, 0.01)	$Normal(\sigma_P, 0.01prop_{std})$
$\sigma_R$	Normal(0.01, 0.001)	$Normal(\sigma_R, 0.001prop_{std})$

Table 4.4 : Table of Parameters, their priors and proposal distributions. \* indicates the parameter was held fixed. (prop<sub>std</sub> =0.1)

## 4.3 Results

#### 4.3.1 Carbon chemistry iterative solution

Total Sulfur

$$TS = \frac{0.14}{96.062} * \frac{S}{1.8065}$$

$$IS = 19.924 * \frac{S}{(1000.0 - 1.005 * S)}$$

$$KS_{int} = -\frac{4276.1}{T_K} + 141.328 - 23.093 * log(T_K) + (-\frac{13856.0}{T_K} + 324.57$$

$$-47.986 * log(T_K)) * \sqrt{IS} + (\frac{35474}{T_K} - 771.54 + 114.723 * log(T_K)) * IS$$

$$-\frac{2698}{T_K} * IS^{1.5} + \frac{1776}{T_K} * IS^2$$

$$KS = exp(KS_{int}) * (1 - 0.001005 * S)$$

Fluorine

$$TF = 0.000067 * S/18.9984/1.80655$$
 
$$KF = exp(-(-\frac{874.0}{T_K} - 0.111 * \sqrt{S} + 9.68))$$
 
$$SWS_{2_T} = \frac{(1 + \frac{TS}{KS})}{(1 + \frac{TS}{KS} + \frac{TF}{KF})}$$
 
$$Free_{2_T} = 1 + \frac{TS}{KS}$$

H2O dissoc

$$KW = exp(148.9802 - \frac{13847.26}{T_K} - 23.6521 * log(T_K)$$
$$+ (\frac{118.67}{T_K} - 5.977 + 1.0495 * log(T_K)) * \sqrt{S} - 0.01615 * S)$$

Boron

$$KB = exp((-8966.90 - 2890.53 * \sqrt{S} - 77.942 * S$$

$$+ 1.728 * S * \sqrt{S} - 0.0996 * S^{2})/T_{K} + 148.0248$$

$$+ 137.1942 * \sqrt{S} + 1.62142 * S$$

$$- (24.4344 + 25.085 * \sqrt{S} + 0.2474 * S) * log(T_{K})$$

$$+ 0.053105 * \sqrt{S} * T_{K})$$

$$TB = 0.0004326 * \frac{S}{35}$$

Carbon eq constants

$$K1 = 10^{\left(-\left(\frac{3633.86}{T_K} - 61.2172 + 9.6777*log(T_K) - 0.011555*S + 0.0001152*S^2\right)\right)} * 1.23$$

$$K2 = 10^{\left(-\left(\frac{471.8}{T_K} + 25.9290 - 3.16967*log(T_K) - 0.01781*S + 0.0001122*S^2\right)\right)} * 0.53$$

1.23 and 0.53 were experiment specific and measured

Initial guess at the pH

$$pH_{init} = 12.26 - 0.0030605 * DIC - 0.043752 * T - 0.013625 * S + 0.00011315 * TA$$
$$+ 1.3463e - 5 * DIC * T + 5.2215e - 7 * DIC * TA$$

Iterations:

For 1 to n iterations:

$$\begin{split} h &= 10^{-pH_{init}} \\ h_{free} &= \frac{h}{Free_{2_T}} \\ f0 &= (DIC*1e - 6*\frac{K1*h + 2*K1*K2}{h*h + K1*h + K1*K2} \\ &- h_{free} + \frac{KW}{h} - Alk*1e - 6 + \frac{TB}{1 + \frac{h}{KB}})*1e6 \\ df0 &= (DIC*1e - 6*\frac{K1 + 2*K1*K2}{h^2 + K1*h + K1*K2} \\ &- DIC*1e - 6*\frac{(K1*h + 2*K1*K2)}{(h^2 + K1*h + K1*K2)^2}*(2*h + K1) \\ &- TB*\frac{1}{(1 + \frac{h}{KB})^2}/KB \\ &- \frac{KW}{h^2} - \frac{1}{Free_{2_T}})*1e6*(-log(10)*10^{-pH}) \\ pH &= pH - \frac{f0}{df0} \\ H &= 10^{-pH} \\ denom &= H^2 + K1*H + K1*K2 \\ CO2 &= \frac{DIC*H^2}{denom} \\ HCO3 &= \frac{DIC*K1*K2}{denom} \\ CO3 &= \frac{DIC*K1*K2}{denom} \end{split}$$

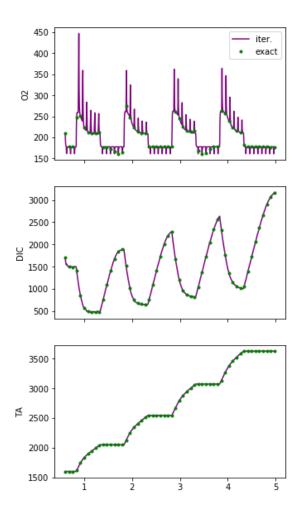


Figure 4.1 : Iterative vs exact solution for state variables  $\mathcal{O}_2,\, DIC,\, \mathrm{and}\,\, TA.$ 

Variable	Iter. 1	Iter. 2	Iter. 3	Iter. 4	Iter. 5
$O_2$	0.308389964	0.016044284	4.18E-05	6.89E-05	7.59E-05
DIC	16.78775711	0.958511825	0.005229318	0.002305054	0.002333411
TA	2.607767674	0.160897272	0.000688102	0.001257725	0.001218981
pH	0.036092734	0.002355758	1.41E-05	6.93E-06	6.93E-06
CO2	2.109401968	0.145719349	0.001222812	0.000866728	0.000866727
HCO3	19.81869214	1.21021115	0.008016765	0.001025002	0.001025139
CO3	20.89660704	1.307061652	0.00867642	0.001102278	0.001102434

Table 4.5: RMSE for 5 iterations of the Newton-raphson carbon chemistry iterative solution.

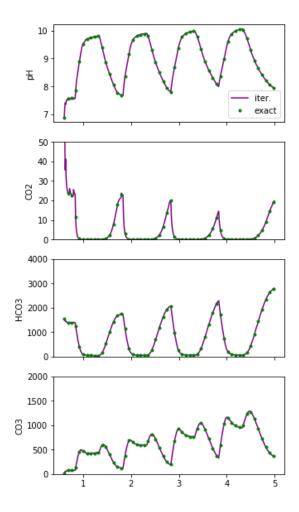


Figure 4.2 : Iterative vs exact solution for carbon chemistry  $CO_2$ ,  $HCO_3$ ,  $CO_3$ , and pH.

## 4.3.2 Posteriors

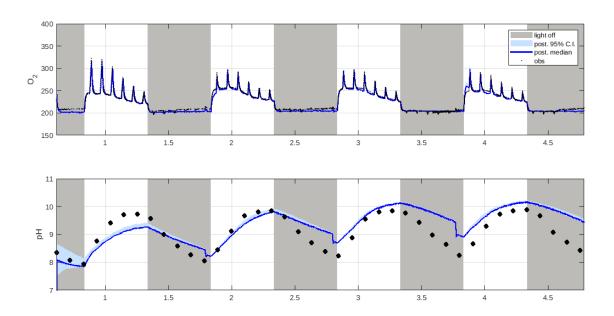


Figure 4.3 : Posteriors for  $O_2$  and pH.

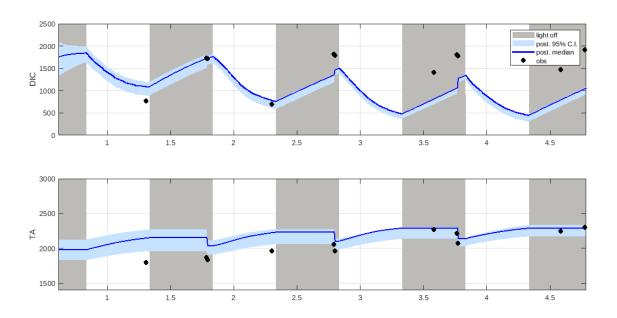


Figure 4.4: Posteriors for DIC and TA.

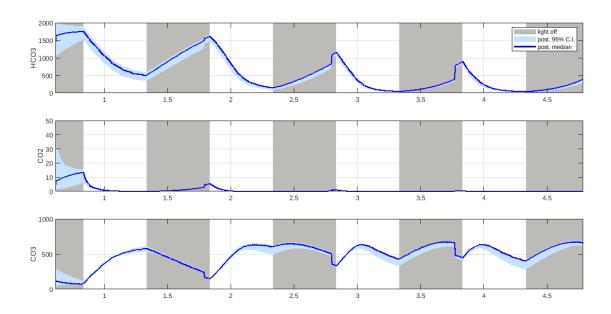


Figure 4.5 : Posteriors for carbon chem.

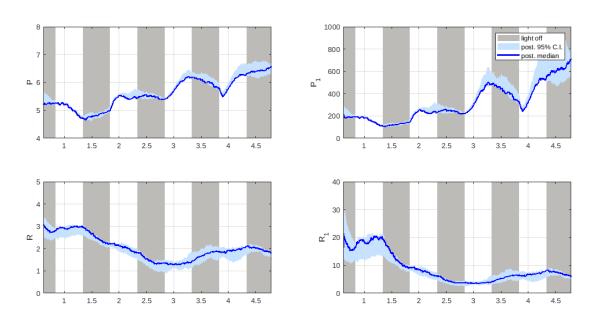


Figure 4.6: Posteriors for photosynthesis and respiration.

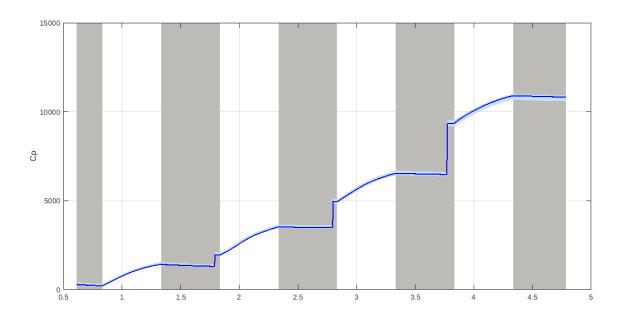


Figure 4.7 : Posterior for  $C_p$ .

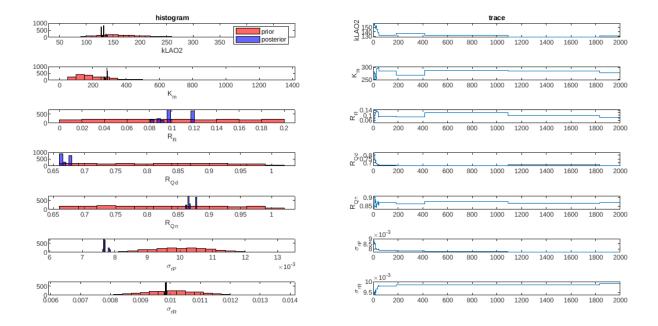


Figure 4.8 : Priors, posteriors and traces for model parameters.

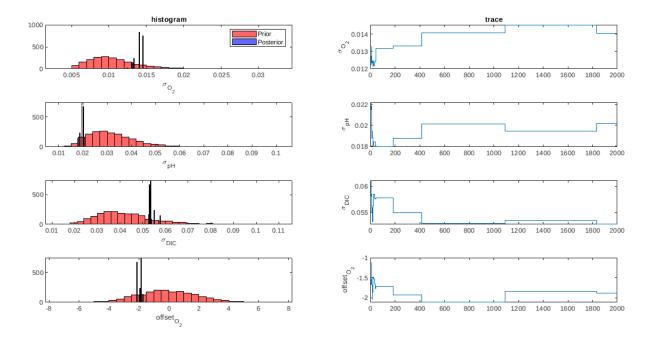


Figure 4.9: Priors, posteriors and traces for obs. error parameters.

## Appendix A

## LiBbi model code

#### LiBbi model file: micro\_iterative.bi

```
1 model micro_iterative {
3 const FO2
                 = 0.2094
4 const FCO2
                 = 397e-6
5 const S
                 = 34.0
6 const V
                 = 500.0
                                          // volume of the
     reactor
                 = 1724.20
7 const DIC_M
                                          // calculated with
     CO2SYS[DIC_M = 1724.20, Alk = 1797.90, T = 27, S = 34]
                = 226.65
8 const 0_2_M
                 = 1797.90
9 const alk_M
10 const tau
                 = 6.0
11 const kLA02_m = log(2.0)*24.0*60.0/tau
12
13 param kLAO2
14 param Km
15 param RR
 param RQ_d
17 param RQ_n
 param sigma_0_2
19 param sigma_pH
20 param sigma_DIC
```

```
_{21} param offset_0_2
22
23 input I
                           // light intensity
                           // temperature (C)
24 input T
  input gas
                           // gas on/off
                           // dilution rate
26 input dil
27
28 state DIC // state variables
29 state 0_2
30 state pH
31 state Cp
32 state mich_ment
33 state O2H_pr
34 state CO2H_pr
35 state R
36 state R1
37 state P
38 state P1
39 state alk
40 state CO2
41 state HCO3
42 state CO3
43 state O_2H
44 state CO2H
45 state h_3
46 state h_free_3
47
48 noise r_R
49 noise r_P
```

```
50
  /* random walk parameter */
51
  param sigma_r_R
  param sigma_r_P
54
55
  obs 02_obs
56 obs pH_obs
  obs DIC_obs
  obs alk_obs
59
  sub parameter {/* prior distribution over parameters */
           ~ log_normal(log(100.0), 0.5)
  Km
61
  kLA02
         ~ log_normal(log(kLAO2_m), 0.3)
           ~ uniform(0.0001, 0.2)
  RR
  RQ_d
          " uniform(0.66, 1.0)
           ~ uniform(0.66, 1.0)
  RQ_n
65
66
   sigma_0_2 ~ log_normal(log(0.03), 0.5)
   sigma_pH ~ log_normal(log(0.03), 0.5)
68
   sigma_DIC \sim log_normal(log(0.03), 0.5)
69
70
   offset_0_2 ~ normal(0, 2.0)
71
72
                   ~ normal(0.01, 0.001)
73 sigma_r_R
                   ~ normal(0.05, 0.01)
74 sigma_r_P
75
76
  const prop_std = 0.1;
78 sub proposal_parameter {
```

```
~ log_normal(log(Km), 0.5*prop_std)
79 Km
           ~ log_normal(log(kLAO2), 0.3*prop_std)
  kLAO2
80
           ~ truncated_normal(RR, 0.2*prop_std, lower = 0.0001,
81 RR
      upper = 0.2)
         ~ truncated_normal(RQ_d, 0.2*prop_std, lower = 0.66,
      upper = 1.0)
83 RQ_n ~ truncated_normal(RQ_n, 0.2*prop_std, lower = 0.66,
      upper = 1.0)
84
85
   sigma_0_2
                    ~ log_normal(log(sigma_0_2), 0.5*prop_std)
86
                    ~ log_normal(log(sigma_pH), 0.5*prop_std)
   sigma_pH
87
   sigma_DIC
                    ~ log_normal(log(sigma_DIC), 0.5*prop_std)
89
   offset_0_2
                    ~ normal(offset_0_2, 2.0*prop_std)
90
91
                    ~ normal(sigma_r_R, 0.001*prop_std)
   sigma_r_R
92
                    ~ normal(sigma_r_P, 0.01*prop_std)
   sigma_r_P
  }
94
95
   sub initial {/* prior distribution over initial conditions,
      given parameters */
   // specify the initial condition model
           ~ normal(log(20.0), 0.4)
98
           ~ log_normal(log(20.0), 0.4)
  R1
99
           ~ normal(log(200.0), 0.4)
100
           ~ log_normal(log(200.0), 0.4)
  Ρ1
101
102
           ~ log_normal(log(300.0), 0.2)
103 Cp
```

```
~ log_normal(log(1750.0), 0.1)
  alk
104
            ~ log_normal(log(1300.0), 0.2)
105 DIC
            ~ log_normal(log(225.0), 0.2)
106 0_2
           ~ log_normal(log(8.5), 0.2)
107
  рΗ
108 CO2
           ~ log_normal(log(3.0), 0.4)
           ~ log_normal(log(1000.0), 0.3)
109
   HC03
110 CO3
           ~ log_normal(log(300.0), 0.4)
           ~ log_normal(log(200.0), 0.2)
111 O_2H
            ~ log_normal(log(10.0), 0.2)
  CO2H
113
  }
114
115
116 //sub transition(delta = 0.0023) { // obs are in days ie
      delta=1.0 for daily solving. delta=0.00069 for solving
      every minute, 0.0014 for every 2 mins, 0.0021 for 3 mins,
      0.0028 for 4mins, delta=0.000011574 for solving every
      second
   sub transition(delta = 0.0021) {
118
   /* processes */
119
120
121 inline TK
                 = T + 273.15
                                             // temp in kelvin
  inline KO_CO2 = exp(-60.2409 + 93.4517*(100.0/TK) + 23.3585*
      log(TK/100.0) + S*(0.023517 - 0.023656*(TK/100) +
      0.0047036*(TK/100.0)*(TK/100.0)))
   CO2H
                  <- K0_C02*FC02*1.0220*1e6
123
124
  inline KO_02 = (exp(-1282.8704 + 36619.96/TK + 223.1396*log)
125
      (TK) -0.354707*TK + S*(5.957e-3 -3.7353/TK) + 3.68e-6*S*S)
```

```
)/(0.2094e-06)
126 O_2H
               <- K0_02*F02*1.0220*1e-6
127
128 inline PAC = HCO3
                                   //PAC=photosynthetically
      active carbon. if the phyto are just using CO2 to
      photosynthesise then PAC=CO2
  inline mm = PAC/(Km + PAC)
129
130
131 // CO2SYS iterative solution
  // set up all the constants
133
134 inline logTK = log(TK)
135 inline S2 = S*S
  inline sqrtS = sqrt(S)
137
138 // total sulphur
139
inline TS = (0.14/96.062)*(S/1.80655)
             = 19.924*S/(1000.0 - 1.005*S)
141 inline IS
142
inline KS_{int} = -4276.1/TK + 141.328 - 23.093*logTK +
      (-13856.0/TK + 324.57 - 47.986*logTK)*sqrt(IS) + (
      35474.0/TK - 771.54 + 114.723*logTK)*IS - 2698.0/TK*IS
      **1.5 + 1776.0/TK*IS**2
  inline KS = \exp(KS_{int})*(1 - 0.001005*S)
144
145
146 // Fluorine
147
148 inline TF
                  = 0.000067*S/18.9984/1.80655
```

```
= \exp(-(-874.0) \text{TK} - 0.111 * \text{sqrtS} + 9.68))
149 inline KF
  inline SWS_2T = (1.0 + TS/KS)/(1.0 + TS/KS + TF/KF)
  inline Free_2_T = 1.0 + TS/KS
151
152
153 // H2O dissoc
154
   inline KW = \exp(148.9802 - 13847.26/TK - 23.6521*logTK +
      (118.67/TK - 5.977 + 1.0495*logTK)*sqrtS - 0.01615*S)
156
  // Boron
158
inline KB = exp((-8966.90 - 2890.53*sqrtS - 77.942*S + 1.728*)
      S*sqrtS - 0.0996*S2)/TK + 148.0248 + 137.1942*sqrtS +
      1.62142*S - (24.4344 + 25.085*sqrtS + 0.2474*S)*logTK +
      0.053105*sqrtS*TK)
  inline TB = 0.0004326*S/35.0
161
162 // Carbon eq constants
163
  inline K1 = 10**(-(3633.86/TK - 61.2172 + 9.6777 *logTK -
164
      0.011555*S + 0.0001152*S**2))*1.23 //1.23 experiment
      specific and measured
inline K2 = 10**(-(471.8/TK + 25.9290 - 3.16967*logTK -
      0.01781*S + 0.0001122*S**2))*0.53
                                         //0.53 experiment
      specific and measured
166
   // end all the constants
167
168
169 // intial guess at the pH (use the approximating equation)
```

```
170
inline pH_init = 12.26 -0.0030605*DIC -0.043752*T -0.013625*S
      + 0.00011315*alk + 1.3463e-05*DIC*T + 5.2215e-07*DIC*alk
172
173 // iteration 1
174
inline h_1 = 10.0**(-pH_init)
inline h_free_1 = h_1/Free_2_T
inline f0_1 = (DIC*1e-6*(K1*h_1 + 2.0*K1*K2)/(h_1*h_1 +
      K1*h_1 + K1*K2) - h_free_1 + KW/h_1 - alk*1e-6 + TB/(1.0 +
      h_1/KB) *1e6
inline df0_1 = (DIC*1e-6*(K1 + 2.0*K1*K2))/(h_1**2.0 + K1*)
      h_1 + K1*K2) - DIC*1e-6*(K1*h_1 + 2.0*K1*K2)/(h_1**2.0 + 6.0*K1*K2)
      K1*h_1 + K1*K2)**2.0*(2.0*h_1 + K1) - TB*1.0/(1.0 + h_1/KB)
      )**2.0/KB - KW/h_1**2.0 - 1.0/Free_2_T)*1e6*(-log(10.0)
      *10.0**(-pH_init))
inline pH_1 = pH_init - f0_1/df0_1
180
181 // iteration 2
182
inline h_2 = 10.0**(-pH_1)
inline h_free_2 = h_2/Free_2_T
185 inline f0_2
                = (DIC*1e-6*(K1*h_2 + 2.0*K1*K2)/(h_2*h_2 +
      K1*h_2 + K1*K2) - h_free_2 + KW/h_2 - alk*1e-6 + TB/(1.0 + B)
       h_2/KB))*1e6
inline df0_2 = (DIC*1e-6*(K1 + 2.0*K1*K2))/(h_2**2.0 + K1*)
      h_2 + K1*K2) - DIC*1e-6*(K1*h_2 + 2.0*K1*K2)/(h_2**2.0 +
      K1*h_2 + K1*K2)**2.0*(2.0*h_2 + K1) - TB*1.0/(1.0 + h_2/KB)
      )**2.0/KB - KW/h_2**2.0 - 1.0/Free_2_T)*1e6*(-log(10.0)
```

```
*10.0**(-pH_1))
inline pH_2 = pH_1 - f0_2/df0_2
188
189 // iteration 3
190
191 h_3
                   <-10.0**(-pH_2)
192 h_free_3
                  <- h_3/Free_2_T
inline f0_3 = (DIC*1e-6*(K1*h_3 + 2.0*K1*K2)/(h_3*h_3 +
      K1*h_3 + K1*K2) - h_free_3 + KW/h_3 - alk*1e-6 + TB/(1.0 + B)
      h_3/KB))*1e6
inline df0_3 = (DIC*1e-6*(K1 + 2.0*K1*K2))/(h_3**2.0 + K1*)
      h_3 + K1*K2) - DIC*1e-6*(K1*h_3 + 2.0*K1*K2)/(h_3**2.0 + 2.0*K1*K2)
      K1*h_3 + K1*K2)**2.0*(2.0*h_3 + K1) - TB*1.0/(1.0 + h_3/KB)
      )**2.0/KB - KW/h_3**2.0 - 1.0/Free_2_T)*1e6*(-log(10.0)
      *10.0**(-pH_2))
                  <- pH_2 - f0_3/df0_3
195 pH
196
197 // iteration 4
198
199 //
          inline h_4 = 10.0**(-pH_3)
          inline h_free_4 = h_4/Free_2_T
200 //
201 //
          inline f0_4 = (DIC*1e-6*(K1*h_4 + 2.0*K1*K2)/(h_4)
      *h_4 + K1*h_4 + K1*K2) - h_free_4 + KW/h_4 - alk*1e-6 + TB
      /(1.0 + h_4/KB))*1e6
202 //
          inline df0_4 = (DIC*1e-6*(K1 + 2.0*K1*K2)/(h_4)
      **2.0 + K1*h_4 + K1*K2) - DIC*1e-6*(K1*h_4 + 2.0*K1*K2)/(
      h_4**2.0 + K1*h_4 + K1*K2)**2.0*(2.0*h_4 + K1) - TB
      *1.0/(1.0 + h_4/KB)**2.0/KB - KW/h_4**2.0 - 1.0/Free_2_T)
      *1e6*(-log(10.0)*10.0**(-pH_3))
```

```
203 //
         inline pH_4 = pH_3 - f0_4/df0_4
204
205 //
          рΗ
                            <- pH_4
206
  // calculate the final concentrations
208
209 inline H
                   = 10.0**(-pH)
210 inline H2
                   = H * H
211 inline denom
                   = (H2 + K1*H + K1*K2)
                   <- DIC*H2/denom
212 CO2
213 HCO3
                   <- DIC*H*K1/denom
214 CO3
                   <- DIC*K1*K2/denom
215
_{216} // end CO2SYS iterative solution
217
218
219 /* R and P as random walks */
220
221 r_R
          ~ normal(0.0, sigma_r_R)
222 R
           <-R+r_R
223 R1
          <- exp(R)
224
r_P \sim normal(0.0, sigma_r_P)
          <- P + r_P
226 P
           <- exp(P)
227 P1
228
229 ode(h = 0.1, atoler = 1.0e-6, rtoler = 1.0e-6, alg = 'RK4(3)
      '){
```

```
230 dDIC/dt = -P1*24.0*I*mm + R1*24.0
             + gas*0.893*kLA02*(CO2H - CO2) + dil/V*(
      DIC_M - DIC)
d0_2/dt = (P1*24.0*I*mm - R1*24.0)/(RQ_d*I + RQ_n*(1.0-I))
         + gas*kLAO2*(0_2H - 0_2)
                                                 + dil/V*(0_2_M
      - 0_2) + offset_0_2
232 dalk/dt = RR*P1*24.0*I*mm
                                                      + dil/V*(
      alk_M - alk)
233 dCp/dt = (P1*24.0*I*mm - R1*24.0)
                                                      + dil/V*(
      Cp)
234
235 }
236
237 mich_ment <- mm
238 O2H_pr <- O_2H
239 CO2H_pr <- CO2H
240
241 }
242
243
244 sub observation {
245
246 02_{obs} ~ log_normal(log(0_2), sigma_0_2)
247 pH_obs ~ log_normal(log(pH), sigma_pH)
248 DIC_obs ~ log_normal(log(DIC), sigma_DIC)
249 alk_obs ~ log_normal(log(alk), sigma_DIC)
250 }
```

```
251 }
```

## LiBbi prior sampling file: prior.conf

```
1 --target prior
2 --model-file micro_iterative.bi
3 --nsamples 500
4 --start-time 0.61304
5 --end-time 4.7866
6 --noutputs 6049
7 --input-file data/input_all_2018_normalised.nc
8 --output-file results/prior_micro_iterative.nc
```

## LiBbi posterior sampling file: posterior.conf

```
--target posterior

--model-file micro_iterative.bi

--input-file data/input_all_2018_normalised.nc

--obs-file data/obs_all_2018.nc

--nsamples 500

--nparticles 1024

--start-time 0.61304

--end-time 4.7866

--noutputs 6049

--output-file results/posterior_micro_iterative.nc

--with-transform-initial-to-param
```



Figure A.1 : Directed Acyclic Graph of the LiBbi model file micro\_iterative.bi

## **Bibliography**

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