

Max 50 used
May be fine
depending on
damping
values

redundant

ways to
unbalance

assigned
correct
+ essentially
cut for
our cases.

all 50.

need to
update in my calculations

23073 - Modified Discharge Boom 04155/05050
VORTEX SHEDDING

INPUTS

Member PIPE 405.4 0.0 x 9.5 wall thk

D = 16 Pipe Diameter, in

I = 560.71 in⁴

S = 70.09 in³

w = 62.48 lb/ft

μ = 0.0135 lb*sec²/in²

E = 2.90E+07 lb/in²

L = 569 Length of Unsupported Structure, in

t = 0.37 Wall Thickness, in

A = 18.361 in²

β = 0.01 Damping Ratio (ζ) (Supplement to the National Building Code of Canada 1990, Pg 146, 22. Steel frames)

H = 14.45 Height of the Structure, m

Lu = 1/3 * L For Mode 2

Mode 1 (fixed-hinged) A = 15.4

Mode 1 (fixed-fixed) A = 22.4

Mode 2 (fixed-hinged) A = 50

Op. Wind = 20 m/s

q = 240 N/m²

St. Wind = 62 m/s

q = 2381 N/m²

OUTPUTS

ω₀ = A*(EI/(μL³))^{0.5} Natural Frequency, rad/sec (Harris, C.M. - Shock and Vibration Handbook 5th Edition pg 1.13)

where E = Young's Modulus, lb/in²

I = Area Moment of Inertial of Beam Cross Section, in⁴

L = Length of Beam, in

μ = mass per unit length of beam, lb-sec²/in²

A = Coefficient from Table

V₀ = (1/5) * ω₀ * D Mean Wind Speed, m/s (Supplement to the National Building Code of Canada 1990, Pg 149, Eq. 11)

where S = Strouhal Number (Supplement to the National Building Code of Canada 1990, Pg 149, Eq. 11a, 11b, 11c)

D = Diameter, in

ω₀ = Angular Natural Frequency (No Axial Force), Hz

F_L = C_L/(λ^{0.5} * (β - C_L(ρD³/M)^{0.5}) * q₀ * D Static Force Approximation From Dynamic Vortex Effect, N/m (Supplement to the National Building Code of Canada 1990, Pg 150, Eq. 12)

where C_L = Constant 1

λ = Aspect Ratio (H/D) = 35.57

β = Critical Damping Ratio as Defined for Equation (9) If: C_L(ρD³/M) > β Then Large Amplitued Motions, Up to 1 x D, May Result

C_L = Constant 2

ρ = Density of Air = 1.2 kg/m³

D = Diameter, m

M = Average Mass per Unit Length Over the Top One-Third of the Structure, kg/m

q₀ = Velocity Pressure Corresponding to V₀, Where V₀ is in m/s = 0.6 * V₀^{1.2} in Pa

No Axial Force (Non-Operating, Parked in Bolster)		
Mode 1 (fixed-hinged)	Mode 1 (fixed-fixed)	Mode 2 (fixed-hinged)
ω ₀ = 52.21 rad/sec ω ₀ = 8.31 Hz ω ₀ *D ² = 1.372 m ² /sec V ₀ = 16.89 m/s Bad	ω ₀ = 75.95 rad/sec ω ₀ = 12.09 Hz ω ₀ *D ² = 1.996 m ² /sec V ₀ = 24.56 m/s Bad	ω ₀ = 169.52 rad/sec ω ₀ = 26.98 Hz ω ₀ *D ² = 4.456 m ² /sec V ₀ = 54.82 m/s Bad
Vel. Pressure, q ₀ = 171.08 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 374.51 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 18.73 kN/m Moment = 489.02 kN-m Stress = 425.77 MPa	Vel. Pressure, q ₀ = 361.95 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 792.36 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 39.62 kN/m Moment = 1034.62 kN-m Stress = 900.80 MPa	Vel. Pressure, q ₀ = 1803.42 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 3947.91 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 197.40 kN/m Moment = 1718.31 kN-m Stress = 1496.06 MPa

Unloaded Cylinder, Luffing Structure Load (Supported in Bolster, Storm Wind)		
Mode 1 (fixed-hinged)	Mode 1 (fixed-fixed)	Mode 2 (fixed-hinged)
ω ₀ = 8.33 Hz ω ₀ *D ² = 1.375 m ² /sec V ₀ = 16.92 m/s Bad	ω ₀ = 12.11 Hz ω ₀ *D ² = 2.001 m ² /sec V ₀ = 24.61 m/s Bad	ω ₀ = 27.00 Hz ω ₀ *D ² = 4.459 m ² /sec V ₀ = 54.85 m/s Bad
Vel. Pressure, q ₀ = 171.82 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 376.15 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 18.81 kN/m Moment = 491.15 kN-m Stress = 427.62 MPa	Vel. Pressure, q ₀ = 363.53 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 795.81 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 39.79 kN/m Moment = 1039.12 kN-m Stress = 904.72 MPa	Vel. Pressure, q ₀ = 1805.38 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 3952.21 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 197.61 kN/m Moment = 1720.18 kN-m Stress = 1497.69 MPa

Effect of Axial Load (Harris, C.M. - Shock and Vibration Handbook 5th Edition pg 7.21)

ω₀ = ω₀ (1 ± α²/n²)^{0.5} Natural Frequency with Axial Force, Hz

α = FL²/EI n²

ω₀ = Natural Frequency with no axial force, Hz

n = Mode Number

F = 32710 lbs, Unloaded Cylinder, Luffing Structure Load (+ tensile force - compressive force)

α = 0.056

F = 249538 lbs, Dead Load Only (+ tensile force - compressive force)

α = 0.504

F = 297872 lbs, DL + Normal Operating Material (+ tens - comp)

α = 0.601

Single Degree of Freedom (SDOF) Dynamic Modification Factor (DMF) from "The Nature of Wind Loads and Dynamic Response" Boggs and Dragovich 2006 - Figure 7

Max Non-Operating Wind = 63 m/s		
ω ₀ *D ²	>0.75	<0.75 and >0.5
Yes	No	No
ω ₀ = 31.00	48.65	25.84
ω ₀ *D ² = 5.12	8.03	4.27
V ₀ = 63.00	63.00	63.00

Max Operating Wind = 20 m/s		
ω ₀ *D ²	>0.75	<0.75 and >0.5
Yes	No	No
ω ₀ = 9.84	13.38	8.20
ω ₀ *D ² = 1.63	2.21	1.35
V ₀ = 20.00	20.00	20.00

Effect of Axial Load (Dead Load Only <Operating Case>)

Mode 1 (fixed-hinged)	Mode 1 (fixed-fixed)	Mode 2 (fixed-hinged)
ω ₀ = 9.30 Hz ω ₀ *D ² = 1.537 m ² /sec V ₀ = 18.91 m/s Bad	ω ₀ = 13.53 Hz ω ₀ *D ² = 2.235 m ² /sec V ₀ = 27.50 m/s OK	ω ₀ = 27.82 Hz ω ₀ *D ² = 4.595 m ² /sec V ₀ = 56.53 m/s OK
Vel. Pressure, q ₀ = 214.45 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 469.46 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 23.47 kN/m Moment = 612.99 kN-m Stress = 533.71 MPa	Vel. Pressure, q ₀ = 453.72 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 993.24 N/m f/f ₀ = 0.73 H(f) = 2.3 DMF (Figure 7) UDL = 2.28 kN/m Moment = 59.66 kN-m Stress = 51.94 MPa	Vel. Pressure, q ₀ = 1917.72 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 4198.12 N/m f/f ₀ = 0.35 H(f) = 1.2 DMF (Figure 7) UDL = 5.04 kN/m Moment = 43.85 kN-m Stress = 38.18 MPa

Effect of Axial Load (Dead Load + Normal Operating Material <Operating Case>)

Mode 1 (fixed-hinged)	Mode 1 (fixed-fixed)	Mode 2 (fixed-hinged)
ω ₀ = 9.70 Hz ω ₀ *D ² = 1.601 m ² /sec V ₀ = 19.70 m/s Bad	ω ₀ = 14.10 Hz ω ₀ *D ² = 2.329 m ² /sec V ₀ = 28.66 m/s OK	ω ₀ = 28.17 Hz ω ₀ *D ² = 4.653 m ² /sec V ₀ = 57.25 m/s OK
Vel. Pressure, q ₀ = 232.88 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 508.80 N/m f/f ₀ = 1.00 H(f) = 50 DMF (Figure 7) UDL = 25.49 kN/m Moment = 655.57 kN-m Stress = 579.57 MPa	Vel. Pressure, q ₀ = 492.71 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 1078.60 N/m f/f ₀ = 0.70 H(f) = 2 DMF (Figure 7) UDL = 2.16 kN/m Moment = 56.33 kN-m Stress = 49.05 MPa	Vel. Pressure, q ₀ = 1966.28 N/m ² C _L = 3.00 C ₂ = 0.6 C _L (ρD ³ /M) = 0.0013 OK F _L = 4304.44 N/m f/f ₀ = 0.35 H(f) = 1.2 DMF (Figure 7) UDL = 5.17 kN/m Moment = 44.96 kN-m Stress = 39.15 MPa