

# Hand-eye calibration

Umberto Castellani

Robotics, vision and control

# Overall aim

The overall aim of **hand-eye calibration** procedure is to find the **camera-to-robot** transformation.

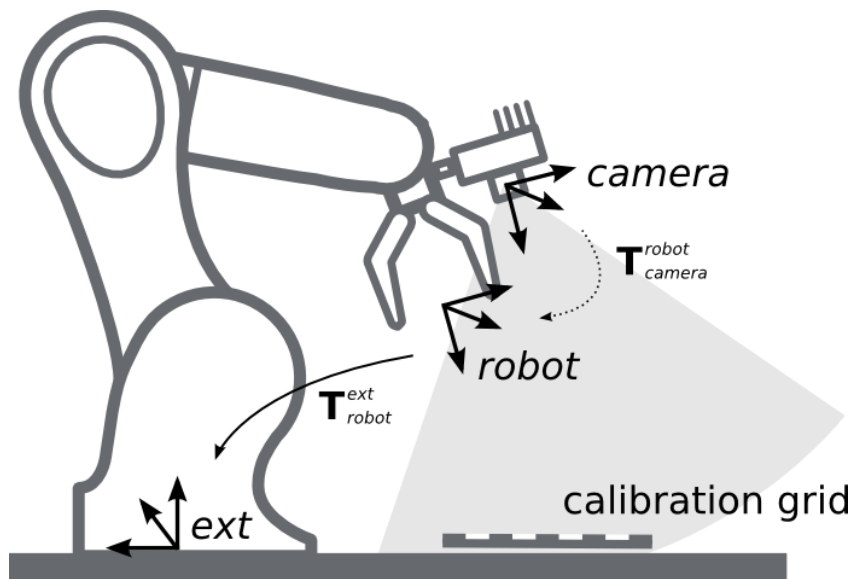
In the basic scenarios:

- The scene is composed by one object, one camera (e.g., RGBD device), and a robot arm with a gripper,
- The camera observes the object in the scene, detect the object position and tell the robot where to pick it.

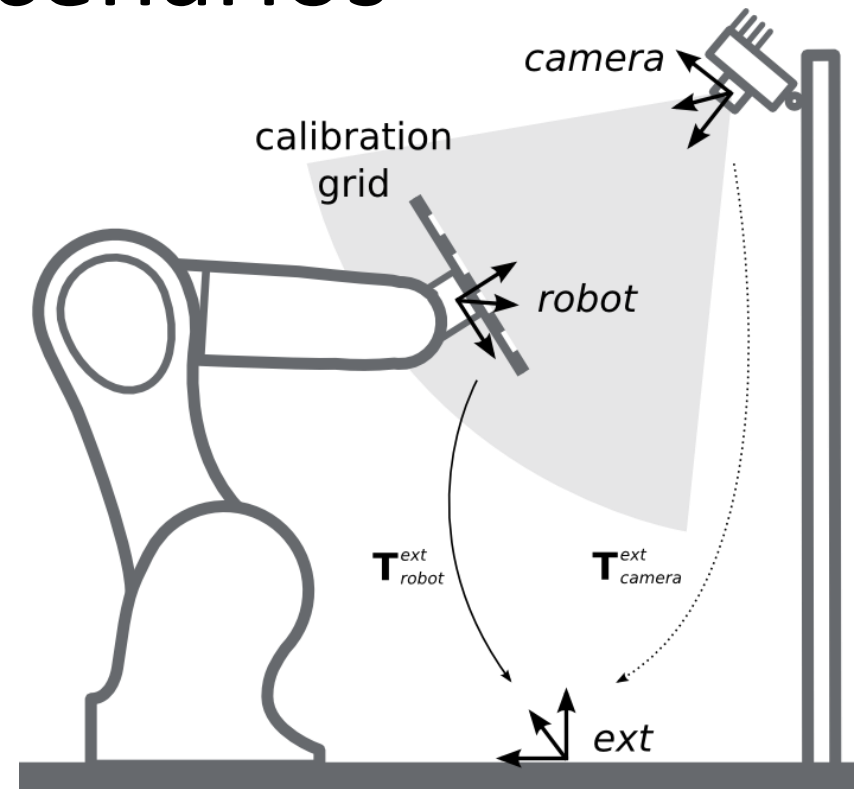


The camera has to know the robot position to transform the object coordinates from the camera to the robot reference system !

# Different scenarios



camera attached to the end-effector

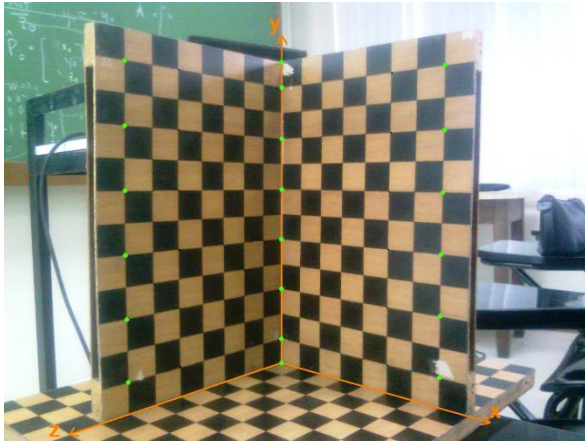


static camera

<https://answers.opencv.org/answers/204935/revisions/>

# System calibration

A calibration object is used



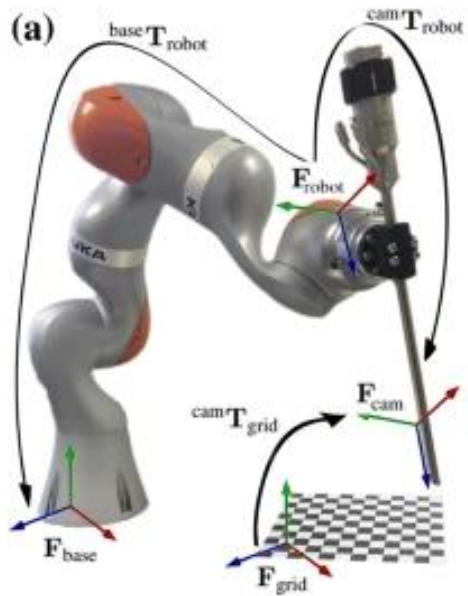
- The aim of calibration object is to easily detect 3D-2D correspondences,
- Sometimes we ask the end-effector to touch the interest points of the calibration object,
- The calibration object may define the world reference system.

# Calibration System

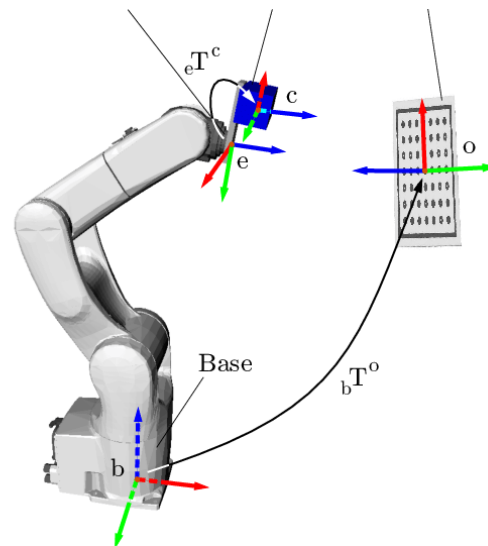
Different calibration scenarios:

- Chessboard mounted on the end-effector (we need to estimate also the transformation between the end-effector and the chessboard).
- Fixed Chessboard with camera mounted to the end effector (we need to estimate also the transformation between end-effector and camera)

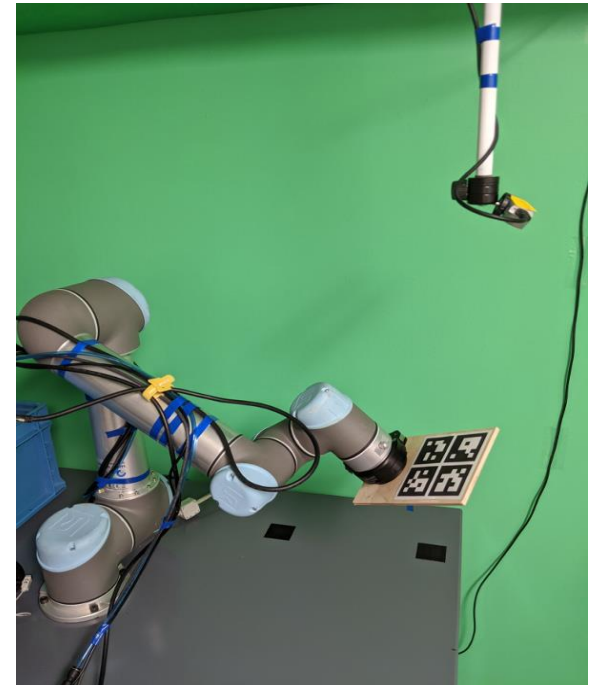
# Calibration system



End-effector touches the calibration object



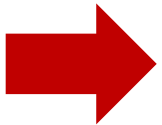
Fixed calibration object and camera mounted to the end-effector



Fixed camera and calibration object mounted to the end-effector

# Transformations

- Each system involves different reference systems:
  - Calibration object (i.e., chessboard),
  - Camera,
  - Robot (base),
  - Gripper



We can compute matrix transformations to move among the reference systems

# Problem solution

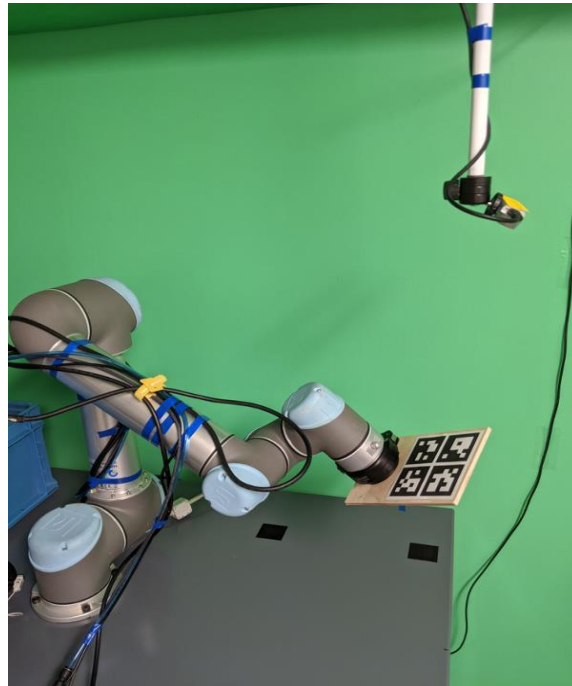
- We need to combine the various transformations in order to obtain reasonable equations to estimate our unknowns,
- We need to define a suitable optimization problem,
  - We should solve the optimization problem in closed-form, or...
  - We should employ an iterative (numerical) method.



The literature on hand-eye calibration differs on the definition of the optimization problem according to the involved Transformations (and the respective scenarios)



# Case 1



Fixed camera and calibration  
object mounted to the end-  
effector

# Involved transformation

- For this scenario we define the respective **transformation chain**, here we have a fixed camera scenario:

$$p\_cam = K * BaseT * armPose * gripT * P\_ch$$

where

- $p\_cam$  = pixel coordinates,
- $K$  = camera projection matrix,
- $BaseT$  = robot to camera transform,
- $armPose$  = end-effector to robot transform,
- $gripT$  = chessboard to end-effector transform,
- $P\_ch$  = 3D coordinates of points on the chessboard

# Involved transformation

- For this scenario we define the respective **transformation chain**, here we have a fixed camera scenario:

$$p\_cam = K * BaseT * armPose * gripT * P\_ch$$

where

- $p\_cam$  = pixel coordinates (observed by image processing),
- $K$  = camera projection matrix (estimated as pre-processing),
- $BaseT$  = robot to camera transform (unknown),
- $armPose$  = end-effector to robot transform (given),
- $gripT$  = chessboard to end-effector transform (unknown),
- $P\_ch$  = 3D coordinates of points on the chessboard (given).

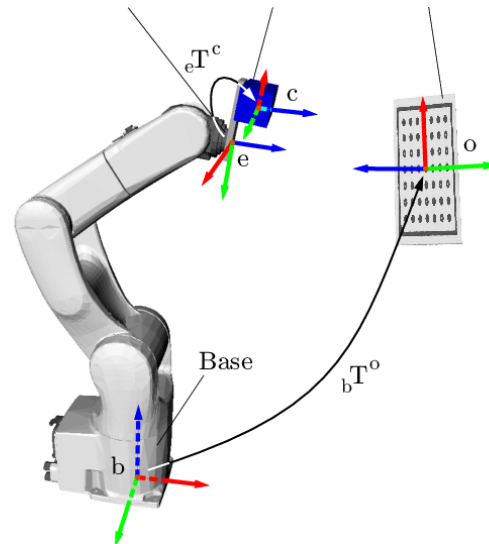
# Estimated solution

- For this example we solve a generic optimization problem by collecting a set of equations derived by the transformation chain,
- We can refer to this code:

<https://github.com/ZacharyTaylor/Camera-to-Arm-Calibration>

- The most important part is the 'ProjectError' function.

# Case 2

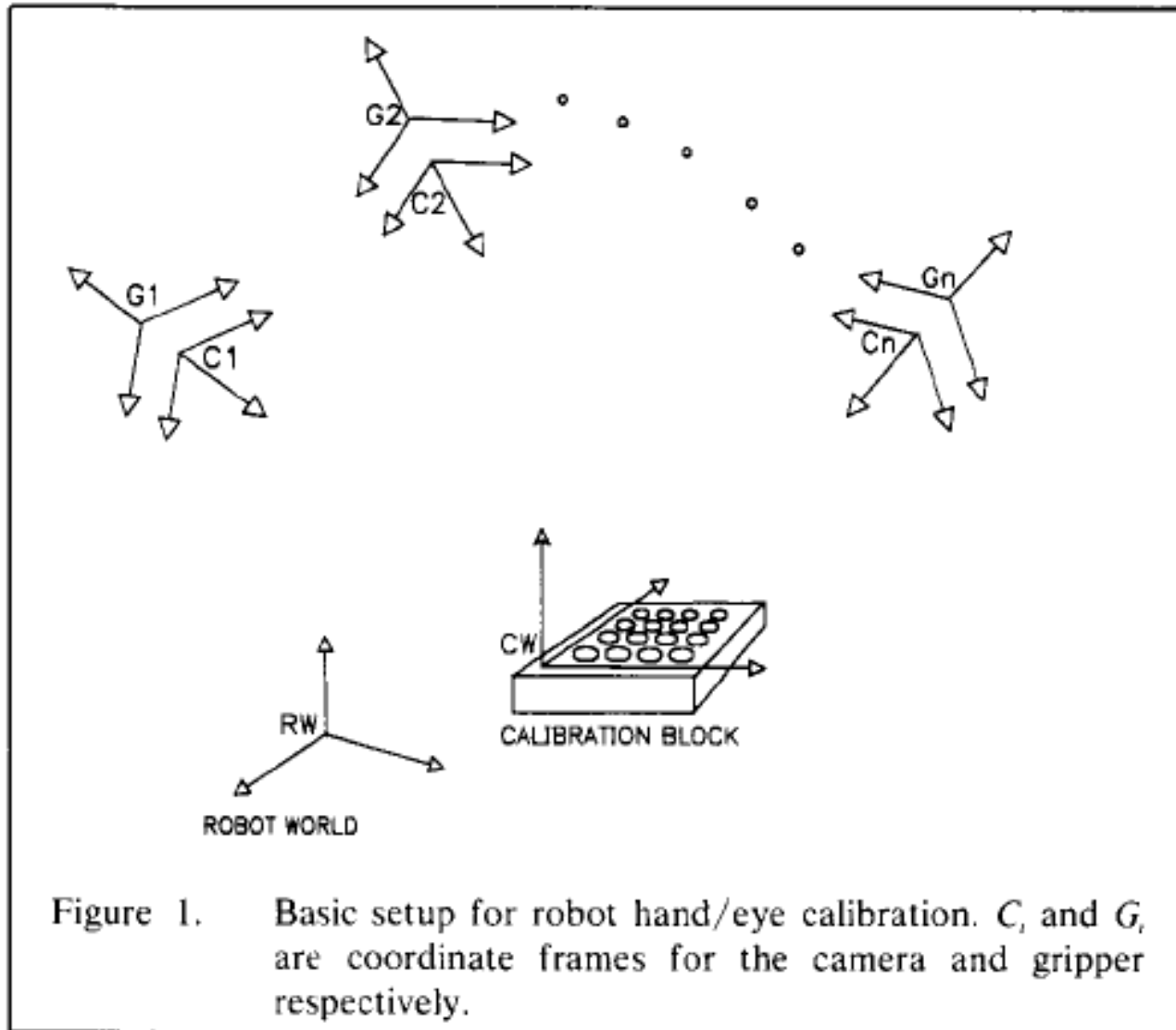


**Fixed calibration object  
and camera mounted to  
the end-effector**

# Calibration setup

- The robot carrying a camera makes a series of motions with the camera acquiring a picture of a calibration object at each motion.
- The involved reference systems are:
  - $G_i$ : the gripper coordinate system, i.e., the coordinate frame fixed on the robot gripper.
  - $C_i$ : the camera coordinate system, i.e., the coordinate frame fixed on the camera.
  - $R_w$ : robot world coordinate system, i.e., the coordinate frame fixed on the robot.
  - $C_w$ : the calibration world coordinate system. This frame is located on the calibration object used to calibrate the camera.

# Calibration setup

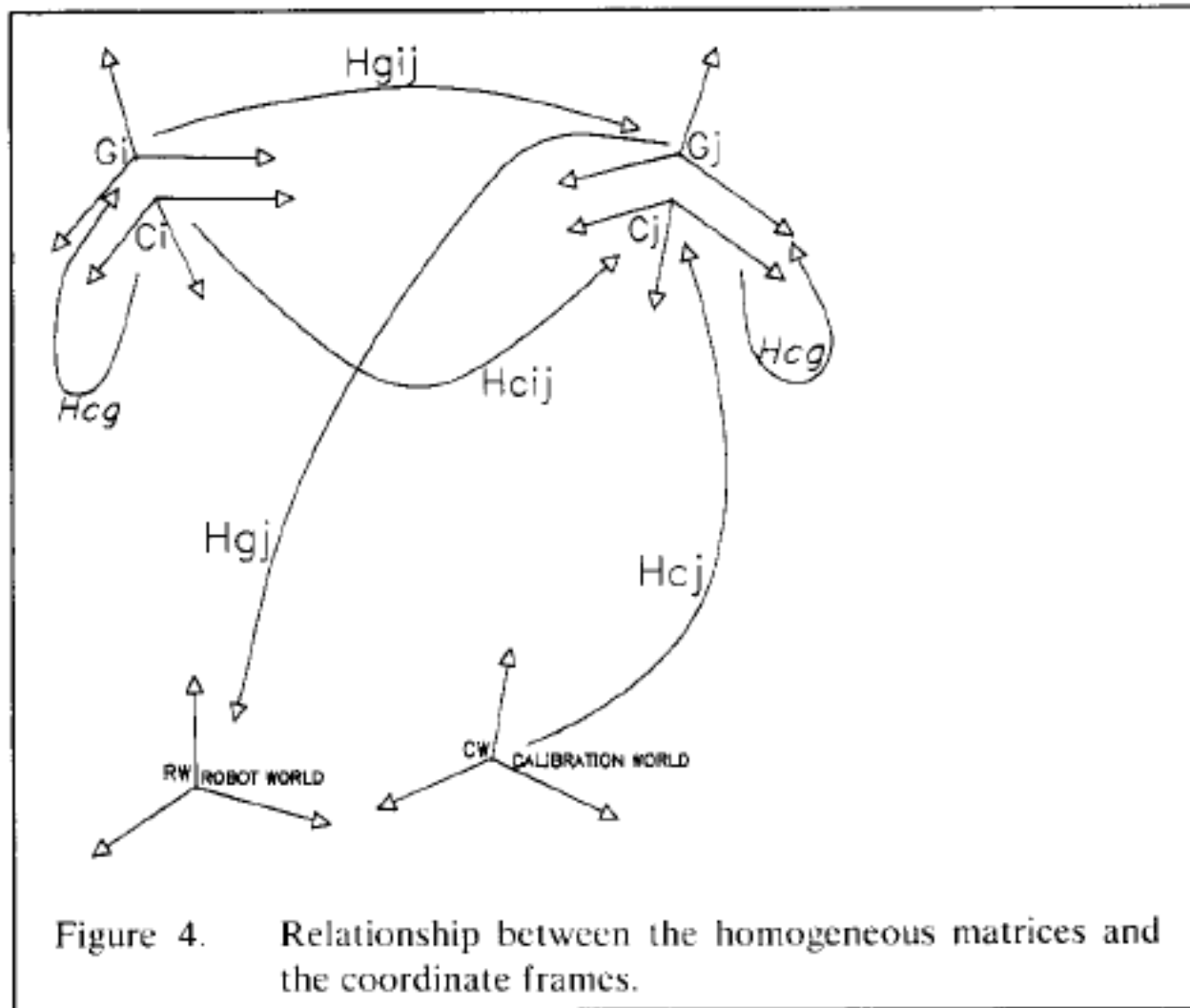


# Transformations

- We involve the following transformations:
  - $H_g^i$ : from  $G_i$  to  $R_w$ , available from robot control.
  - $H_c^i$ : from  $C_w$  to  $C_i$ , available from camera calibration as extrinsic parameters.
  - $H_g^{(i,j)}$ : from gripper position  $G_i$  to gripper position  $G_j$ .
  - $H_c^{(i,j)}$ : from camera position  $C_i$  to camera position  $C_j$ .
  - $H_{cg}$ : from camera frame to gripper frame. This transformation is fixed for all positions since the gripper and the camera are moving together. This transformation is the unknown.



# Transformation



# Interesting equations

- We can recover the following relations:

$$H_g^{(i,j)} = (H_g^j)^{-1} H_g^i$$

$$H_c^{(i,j)} = H_c^j (H_c^i)^{-1}$$

More interesting:  $\longrightarrow H_g^{(i,j)} = H_{cg} H_c^{(i,j)} (H_{cg})^{-1}$



$$H_g^{(i,j)} H_{cg} = H_{cg} H_c^{(i,j)}$$

Unknown

# End eye calibration equation

- This class of equations are of the form:

$$AX = XB$$

- In our case we can decompose the problem in rotation and translation components as:

$$R_A R_X = R_X R_B \quad (R_A - I)t_x = R_X t_b - t_a$$

# Tsai's method

- Tsai proposed a further variation of the rotation matrix representation from the rotation axis  $\mathbf{v}$ :

$$R = \left(1 - \frac{\|\mathbf{v}\|^2}{2}\right)I + \frac{1}{2} \left( \mathbf{v}\mathbf{v}^\top + \sqrt{4 - \|\mathbf{v}\|^2} [\mathbf{v}]_\times \right)$$

Where:  $\|\mathbf{v}\| = 2 \sin\left(\frac{\theta}{2}\right)$



This representation is particularly convenient because it is without any trigonometric function

# Tsai's method

The main procedure is summarized to the following main steps:

1. For each pair of station  $(i, j)$  set up a system of linear equations with  $\mathbf{v}'_{cg}$  as unknown, with  $\mathbf{v}'_{cg}$  is a properly rescaled version of  $\mathbf{v}_{cg}$  to satisfy certain properties (see later):

$$[\mathbf{v}_g^{(i,j)} + \mathbf{v}_c^{(i,j)}] \times \mathbf{v}'_{cg} = (\mathbf{v}_c^{(i,j)} - \mathbf{v}_g^{(i,j)})$$

2. Compute  $\vartheta_{cg} = 2 \tan^{-1} \|\mathbf{v}'_{cg}\|$  (this step is not necessary).

# Tsai's method

The main procedure is summarized to the following main steps:

3. Compute: 
$$\mathbf{v}_{cg} = \frac{2\mathbf{v}'_{cg}}{\sqrt{1 + \|\mathbf{v}'_{cg}\|^2}}$$

Then from  $\mathbf{v}_{cg}$  we can recover  $R_{cg}$  using:

$$R = \left(1 - \frac{\|\mathbf{v}\|^2}{2}\right)I + \frac{1}{2} \left( \mathbf{v}\mathbf{v}^\top + \sqrt{4 - \|\mathbf{v}\|^2} [\mathbf{v}]_\times \right)$$

Finally, the translation vector  $\mathbf{t}_{cg}$  is recovered by solving:

$$(R_g^{(i,j)} - 1)\mathbf{t}_{cg} = R_{cg}\mathbf{t}_c^{(i,j)} - \mathbf{t}_g^{(i,j)}$$

# Tsai's method

- DEMO:**

Working with rotation first:  $R_g^{(i,j)} = R_{cg} R_c^{(i,j)} R_{cg}^\top$

**Property 1:** *The eigenvector matrix of  $R_g^{(i,j)}$  can be transformed from that of  $R_c^{(i,j)}$  using  $R_{cg}$*

$$R_g^{(i,j)} R_{cg} = R_{cg} R_c^{(i,j)}$$



$$\begin{aligned} R_g^{(i,j)} R_{cg} \mathbf{v}_c^{(i,j)} &= R_{cg} R_c^{(i,j)} \mathbf{v}_c^{(i,j)} \\ R_g^{(i,j)} \boxed{R_{cg} \mathbf{v}_c^{(i,j)}} &= \boxed{R_{cg} \mathbf{v}_c^{(i,j)}} \\ R_g^{(i,j)} \mathbf{v}_g^{(i,j)} &= \mathbf{v}_g^{(i,j)} \end{aligned}$$

Rotation axis  
(by definition)



# Tsai's method

- **DEMO:**

Working with rotation first:  $R_g^{(i,j)} = R_{cg} R_c^{(i,j)} R_{cg}^\top$

**Property 1:** *The eigenvector matrix of  $R_g^{(i,j)}$  can be transformed from that of  $R_c^{(i,j)}$  using  $R_{cg}$*

$$R_g^{(i,j)} R_{cg} = R_{cg} R_c^{(i,j)}$$



$$\mathbf{v}_g^{(i,j)} = R_{cg} \mathbf{v}_c^{(i,j)}$$



# Tsai's method

- **DEMO:**

**Property 2 :** *The rotation axis of  $R_{cg}$  is perpendicular to the vector joining the ends of the rotation axis for  $R_g^{(i,j)}$  and  $R_c^{(i,j)}$*

$$\mathbf{v}_{cg} \perp (\mathbf{v}_g^{(i,j)} - \mathbf{v}_c^{(i,j)})$$

# Tsai's method

- **DEMO:**  $\mathbf{v}_{cg} \perp (\mathbf{v}_g^{(i,j)} - \mathbf{v}_c^{(i,j)})$



$$\begin{aligned}(\mathbf{v}_g - \mathbf{v}_c)^\top \mathbf{v}_{cg} &= (\mathbf{v}_g - \mathbf{v}_c)^\top R_{cg}^\top R_{cg} \mathbf{v}_{cg} \\&= (R_{cg}(\mathbf{v}_g - \mathbf{v}_c)^\top)^\top R_{cg} \mathbf{v}_{cg} \\&= (R_{cg} \mathbf{v}_g - R_{cg} \mathbf{v}_c)^\top \mathbf{v}_{cg} \\&= (R_{cg} \mathbf{v}_g - \mathbf{v}_g)^\top \mathbf{v}_{cg} \\&= ((R_{cg} - I) \mathbf{v}_g)^\top \mathbf{v}_{cg} \\&= \mathbf{v}_g^\top (R_{cg} - I)^\top \mathbf{v}_{cg} \\&= \mathbf{v}_g^\top (R_{cg}^\top - I) \mathbf{v}_{cg} \\&= \mathbf{v}_g^\top (R_{cg}^\top \mathbf{v}_{cg} - \mathbf{v}_{cg}) \\&= \mathbf{v}_g^\top (\mathbf{v}_{cg} - \mathbf{v}_{cg}) \\&= 0 \quad \blacksquare\end{aligned}$$

\* Here we omit (i,j)  
to clarify notation

# Tsai's method

- **DEMO:**

**Property 3:**  $(\mathbf{v}_g - \mathbf{v}_c)$  is collinear with  $(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}_{cg}$ .

This means that  $(\mathbf{v}_g - \mathbf{v}_c)$  is simultaneously orthogonal to  $\mathbf{v}_{cg}$  (according to Property 2) and also to  $(\mathbf{v}_g + \mathbf{v}_c)$ . This can be shown considering that  $(\mathbf{v}_g + \mathbf{v}_c)$  and  $(\mathbf{v}_g - \mathbf{v}_c)$  are the minor and major diagonals of the parallelogram defined by the cross product (see picture). This provides this important constraint:

$$(\mathbf{v}_g - \mathbf{v}_c) = s \cdot (\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}_{cg}$$

# Tsai's method

- **DEMO:**

**Property 4:** *we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .*

This means that vectors  $(\mathbf{v}_g - \mathbf{v}_c)$  and  $(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}'_{cg}$  have the same length (other than being collinear). Let be  $\alpha$  the angle between  $\mathbf{v}'_{cg}$  and  $(\mathbf{v}_g + \mathbf{v}_c)$ . Then by definition we have:

$$\|(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}'_{cg}\| = \|(\mathbf{v}_g + \mathbf{v}_c)\| \cdot \|\mathbf{v}'_{cg}\| \cdot \cos \alpha$$

# Tsai's method

- **DEMO:**

**Property 4:** *we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .*

Here we focuses on the term  $\|\mathbf{v}'_{cg}\|$ , from step 3 of the main Tsai's procedure we can derive that:

$$\mathbf{v}'_{cg} = \frac{\mathbf{v}_{cg}}{\sqrt{4 - \|\mathbf{v}_{cg}\|^2}}$$

# Tsai's method

- DEMO:**

**Property 4:** we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .

Here we focus on the term  $\|\mathbf{v}'_{cg}\|$ , from step 3 of the main Tsai's procedure we can derive that:

$$\mathbf{v}'_{cg} = \frac{\mathbf{v}_{cg}}{\sqrt{4 - \|\mathbf{v}_{cg}\|^2}} \quad \Rightarrow \quad \|\mathbf{v}'_{cg}\| = \left\| \frac{\mathbf{v}_{cg}}{\sqrt{4 - \|\mathbf{v}_{cg}\|^2}} \right\|$$

$$= \frac{\|\mathbf{v}_{cg}\|}{\sqrt{4 - 4 \sin^2 \frac{\theta_{cg}}{2}}} \quad \boxed{\|\mathbf{v}\| = 2 \sin \left( \frac{\theta}{2} \right)}$$

$$= \frac{2 \sin \frac{\theta_{cg}}{2}}{\sqrt{4 - 4 \sin^2 \frac{\theta_{cg}}{2}}}$$

$$= 2 \sin \frac{\theta_{cg}}{2} \cdot \frac{1}{2 \cos \frac{\theta_{cg}}{2}}$$

$$= \tan \frac{\theta_{cg}}{2}$$

$$4 \sin^2 \alpha + 4 \cos^2 \alpha = 4,$$

therefore  $4 \cos^2 \alpha = 4 - 4 \sin^2 \alpha$

and  $\sqrt{4 - 4 \sin^2 \alpha} = 2 \cos \alpha$

# Tsai's method

- **DEMO:**

**Property 4:** *we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .*

$$\begin{aligned}\|(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}'_{cg}\| &= \|(\mathbf{v}_g + \mathbf{v}_c)\| \cdot \tan \frac{\theta_{cg}}{2} \cdot \sin \alpha \\ &= 2\|OB\| \cdot \sin \alpha \cdot \tan \frac{\theta_{cg}}{2} \\ &= 2\|AB\| \cdot \tan \frac{\theta_{cg}}{2} \\ &= 2\|CB\| \\ &= \|CG\| \\ &= \|(\mathbf{v}_g - \mathbf{v}_c)\| \\ &\blacksquare\end{aligned}$$

# Tsai's method

- **DEMO:**

Property 4:

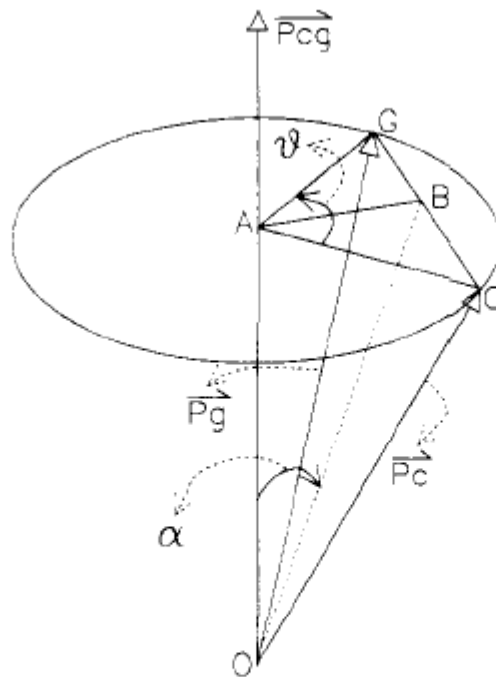


Figure 5. Geometrical relationships between  $P_{cg}$ ,  $P_i$  and  $P_c$ .  $P_c$  rotates  $P_i$  into  $P_{cg}$ . The plane containing the circle is perpendicular to  $P_{cg}$ , and point B is the midpoint of point C and G.



# Tsai's method

- **DEMO:**

**Property 4:** *we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .*

$$\begin{aligned} \|(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}'_{cg}\| &= \underbrace{\|(\mathbf{v}_g + \mathbf{v}_c)\|}_{\text{green}} \cdot \tan \frac{\theta_{cg}}{2} \cdot \sin \alpha \\ &= \underbrace{2\|OB\|}_{\text{green}} \cdot \sin \alpha \cdot \tan \frac{\theta_{cg}}{2} \\ &= 2\|AB\| \cdot \tan \frac{\theta_{cg}}{2} \\ &= 2\|CB\| \\ &= \|CG\| \\ &= \|(\mathbf{v}_g - \mathbf{v}_c)\| \end{aligned}$$

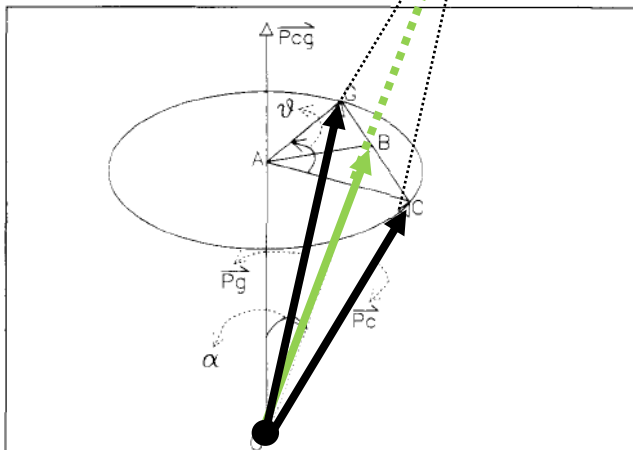


Figure 5. Geometrical relationships between  $P_v$ ,  $P$  and  $P_v'$ .  $P_v$  rotates  $P$  into  $P_v'$ . The plane containing the circle is perpendicular to  $P_v'$ , and point B is the midpoint of point C and G.

# Tsai's method

- DEMO:**

**Property 4:** *we can define  $\mathbf{v}'_{cg}$  such that  $s = 1$ .*

$$\begin{aligned}
 \|(\mathbf{v}_g + \mathbf{v}_c) \times \mathbf{v}'_{cg}\| &= \|(\mathbf{v}_g + \mathbf{v}_c)\| \cdot \tan \frac{\theta_{cg}}{2} \cdot \sin \alpha \\
 &= 2\|OB\| \cdot \sin \alpha \cdot \tan \frac{\theta_{cg}}{2} \\
 &= 2\|AB\| \cdot \tan \frac{\theta_{cg}}{2} \\
 &= 2\|CB\| \\
 &= \|CG\| \\
 &= \|(\mathbf{v}_g - \mathbf{v}_c)\|
 \end{aligned}$$

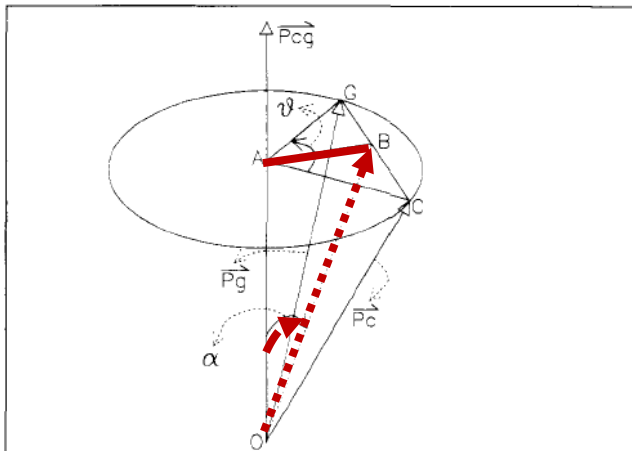


Figure 5. Geometrical relationships between  $P_g$ ,  $P_c$  and  $P_e$ .  $P_e$  rotates  $P_c$  into  $P_g$ . The plane containing the circle is perpendicular to  $P_{cg}$ , and point B is the midpoint of point C and G.

# Tsai's method

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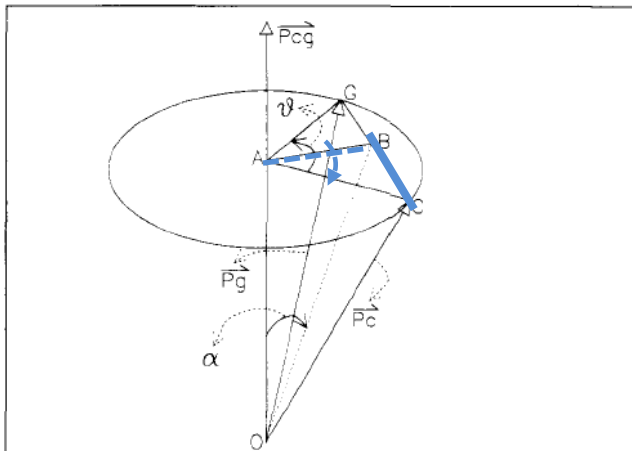


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 &= 2\|AB\| \cdot \tan \frac{\theta_{cg}}{2} \\
 &= \underline{2\|CB\|} \\
 &= \underline{\|CG\|} \\
 &= \|(\mathbf{v}_g - \mathbf{v}_c)\|
 \end{aligned}$$

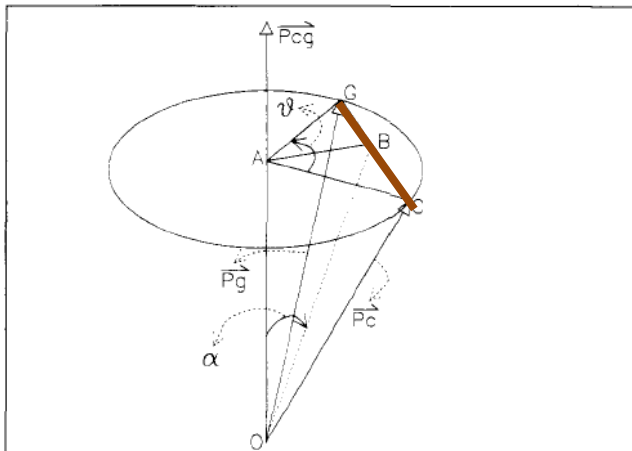


Figure 5. Geometrical relationships between  $P_g$ ,  $P_c$  and  $P_e$ .  $P_e$  rotates  $P_c$  into  $P_g$ . The plane containing the circle is perpendicular to  $P_g$ , and point B is the midpoint of point C and G.

# Tsai's method

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 \end{aligned}$$

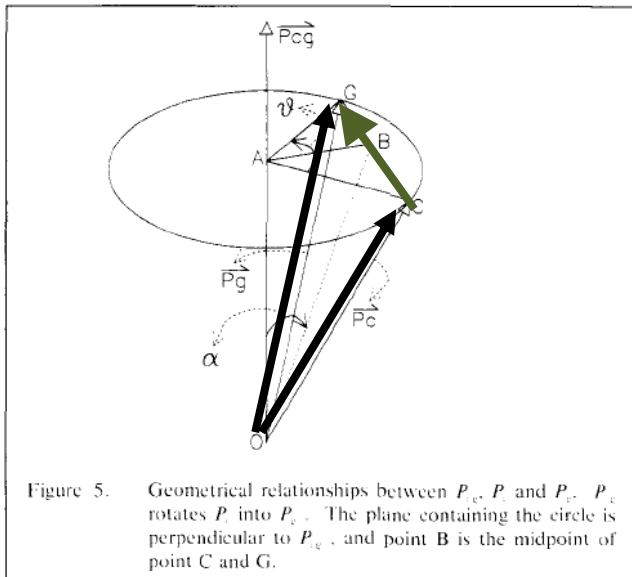


Figure 5. Geometrical relationships between  $P_g$ ,  $P_c$  and  $P_e$ .  $P_e$  rotates  $P_c$  into  $P_g$ . The plane containing the circle is perpendicular to  $P_g$ , and point B is the midpoint of point C and G.

# Tsai's method

Moreover, we can recover the rotation angle  $\theta_{cg}$  from the rotation angle  $\theta'_{cg}$  considering that  $\|\mathbf{v}'_{cg}\| = \tan \frac{\theta_{cg}}{2}$  but also  $\|\mathbf{v}'_{cg}\| = 2 \sin \frac{\theta'_{cg}}{2}$ . We can combine these relations to get:

$$\begin{aligned}\tan \frac{\theta_{cg}}{2} &= 2 \sin \frac{\theta'_{cg}}{2} \\ \frac{\theta_{cg}}{2} &= \tan^{-1} \left( 2 \sin \frac{\theta'_{cg}}{2} \right) \\ \theta_{cg} &= 2 \tan^{-1} \left( 2 \sin \frac{\theta'_{cg}}{2} \right) \\ \theta_{cg} &= 2 \tan^{-1} \|\mathbf{v}'_{cg}\|\end{aligned}$$

that was introduced on the optional step 2 of the Tsai's procedure.