Master's thesis in
Applied Computer Science

CoolingGen

A parametric 3D-modeling software for turbine
blade cooling geometries using NURBS

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I hereby declare that this thesis has been written by myself and no other
resources than those mentioned have been used.

Göttingen, October 7, 2022

Abstract

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Contents

1 Introduction

1.1 Motivation

1.2 State of the Art

1.3 Problem Statement

2 Geometric Methods

As stated before, Non-Uniform Rational B-splines (NURBS) curves and surfaces are used to model geometries in CoolingGen. In this chapter we will first introduce Beziér curves. We will then generalize Beziér curves to obtain B-spline curves and surfaces. Applying an embedding map and a projection map to B-spline curves and surfaces, we acquire NURBS curves and surfaces, which are a generalization of B-spline curves and surfaces. Furthermore, CoolingGen uses special geometric algorithms such as point inversion, ray marching, curve intersection, offset curve creation and fillet creation, which we will also present.

2.1 Bézier Curves

Bézier curves are named after the French engineer Pierre Bézier, who famously utilized them in the 1960s to design car bodies for the automobile manufacturer Renault [Béz68]. Today, they are used in a wide variety of vector graphics applications (i.e. in font representation on computers). At first glance, the definition of the Bézier curve might seem cumbersome, but given the mathematical foundation and a few graphical representations, it becomes apparent why they are such a powerful tool in computer-aided design.

(a) Degree 1.   (b) Degree 2.   (c) Degree 3.

Figure 2.1: Beziér curves of different degrees (orange) and their control points (blue).

2.1.1 Definition

Definition 2.1.1. The *Bernstein basis polynomials* of degree n on the interval $[t_0, t_1]$ are defined as

$$b_{n,k,[t_0,t_1]}(t) := \frac{\binom{n}{k}(t_1 - t)^{n-k}(t - t_0)^k}{(t_1 - t_0)^n}, \tag{2.1}$$

for $k \in \{0, \ldots, n\}$.

Definition 2.1.2. A *Bézier curve* of degree n is a parametric curve $B_{P,[t_0,t_1]} : [t_0, t_1] \to \mathbb{R}^d$ that has a representation

$$B_{P,[t_0,t_1]}(t) = \sum_{k=0}^{n} b_{n,k,[t_0,t_1]}(t) P_k = \sum_{k=0}^{n} \frac{\binom{n}{k}(t_1 - t)^{n-k}(t - t_0)^k}{(t_1 - t_0)^n} P_k. \tag{2.2}$$

We call the elements of the set $P = \{P_0, P_1, \ldots, P_n\} \subset \mathbb{R}^d$ the *control points* of B_P.

Remark. Let $t_0 = 0$ and $t_1 = 1$. Then 2.2 simplifies to

$$b_{n,k}(t) := b_{n,k,[0,1]}(t) = \binom{n}{k}(1-t)^{n-k}t^k$$

and 2.1 simplifies to

$$B_P(t) := B_{P,[0,1]}(t) = \sum_{k=0}^{n}\binom{n}{k}(1-t)^{n-k}t^k P_k. \tag{2.3}$$

This case is the only case considered in this thesis.

In a Beziér curve of a given degree, the control points completely determine the shape of the curve. This behavior can be observed in Figure 2.1. However, changing one control point affects the whole curve, since for n control points the degree of the Beziér curve is always $n - 1$. This behavior also becomes apparent using de Casteljau's algorithm for the computation of points on the Beziér curve.

2.1.2 De Casteljau's Algorithm

The computation of Equation 2.3 is usually performed using de Casteljau's algorithm. This is because the algorithm yields a simple implementation and lower complexity than straightforwardly computing Equation 2.3. The algorithm was proposed by Paul de Faget de Casteljau for the automobile manufacturer Citroën in the 1960s.

Algorithm 1 de Casteljau's algorithm

1: **Input**
2:    $P = \{P_0, P_1, ..., P_n\}$ set of control points
3:    t real number
4: **Output**
5:    $P_0^{(n)} = B_P(t)$ the point on the Beziér curve w.r.t. to t
6: **procedure** DECASTELJAU(P, t)
7:    $P^{(0)} \leftarrow P$
8:    **for** $j = 1, 2, ..., n$ **do**
9:       **for** $k = 0, 1, ..., n - j$ **do**
10:         $P_k^{(j)} \leftarrow (1-t) \cdot P_k^{(j-1)} + t \cdot P_{k+1}^{(j-1)}$
11:    **return** $P_0^{(n)}$

Theorem 2.1.3. Algorithm 1 computes $B_P(t)$.

Proof. By induction. Let $n = 1$. Then

$$P_0^{(1)} = (1-t) \cdot P_0 + t \cdot P_1.$$

By employing the induction hypothesis

$$P_j^{(n)} = \sum_{k=j}^{n+j} \binom{n}{k} (1-t)^{n-k} t^k P_{j+k}$$

for some $n \in \mathbb{N}$, we can infer that

$$
\begin{aligned}
P_0^{(n+1)} &= (1-t) \cdot P_0^{(n)} + t \cdot P_1^{(n)} \\
&= (1-t) \cdot \sum_{k=0}^{n} \binom{n}{k} (1-t)^{n-k} t^k P_k + t \cdot \sum_{k=1}^{n+1} \binom{n}{k} (1-t)^{n-k} t^k P_{k+1} \\
&= \sum_{k=0}^{n+1} \binom{n+1}{k} (1-t)^{n+1-k} t^k P_k,
\end{aligned}
$$

which is equal to $B_P(t)$ for degree $n+1$. $\qquad\square$

A visual representation of Algorithm 1 yields a triangular scheme. To compute one point on a Beziér curve B_P with degree n, one has to perform $\frac{n^2-n}{2}$ vector additions and $n^2 - n$ scalar multiplications.
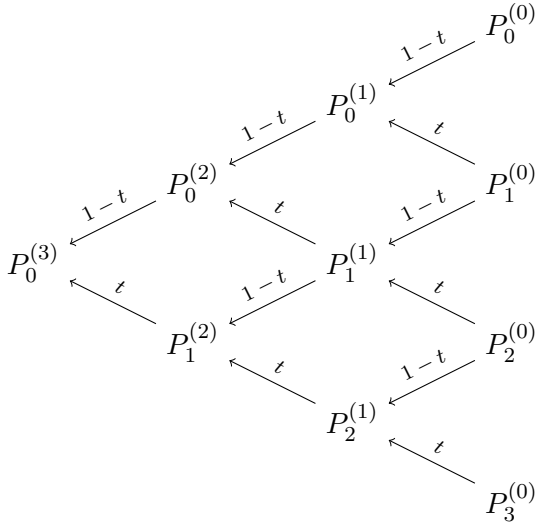
(a) Algorithmic visualization.　　　　(b) Geometric visualization of $B_P(\frac{3}{5})$.

Figure 2.2: Visual representations of de Casteljau's algorithm.

Interestingly, the representation of the algorithm in Figure 2.2 also gives rise to an intuitive visualization of the geometric shape of the Beziér curve B_P. For all $i \in \{0, ..., n\}$ and all $j \in \{0, ..., n-i\}$, the point $P_j^{(i+1)}$ is the convex combination (always w.r.t. t) of $P_j^{(i)}$ and $P_{j+1}^{(i)}$. Thus $P_j^{(i+1)}$ always lies on the line segment between $P_j^{(i)}$ and $P_{j+1}^{(i)}$, as can be observed in the example in Figure 2.2.

2.1.3 Properties

Other than being remarkably intuitive, Beziér curves have a lot of covenient properties. In computer-aided design software, most graphical user interfaces rely on the principle of letting the user interactively drag and drop the control points with a mouse, granting them control over the shape of the whole Beziér curve. The following theorems further illustrate why this is a good concept.

Theorem 2.1.4. $B_P(0) = P_0$ and $B_P(1) = P_n$.

Proof. Explicit computation yields

$$B_P(0) = \sum_{k=0}^{n} \binom{n}{k} t^k P_k = \binom{n}{0} P_0 = P_0$$

and

$$B_P(1) = \sum_{k=0}^{n} \binom{n}{k} (1-t)^{n-k} P_k = \binom{n}{n} P_n = P_n.$$

$\square$

Theorem 2.1.5. Let $T \in \mathbb{R}^{3 \times 3}$. Then $B_{TP}(t) = TB_P(t)$ where $TP := \{TP_0, TP_1, ..., TP_n\}$.

Proof. For all $t \in [0, 1]$ we can directly compute

$$TB_P(t) = \sum_{k=0}^{n} \binom{n}{k} (1-t)^{n-k} t^k TP_k = B_{TP}(t).$$

$\square$

Theorem 2.1.6. $B_P(t)$ lies in the convex hull of P for all $t \in [0, 1]$.

Proof. By the algorithm of de Casteljau (1), we know that $P_j^{(i)} = (1-t) \cdot P_j^{(i-1)} + t \cdot P_{j+1}^{(i-1)}$ for all $t \in [0, 1]$. Therefore, $P^{(i)}$ lie in the convex hull of $P^{(i-1)}$. But then $B_P(t) = P_0^{(n)}$ always lies in the convex hull of $P^{(0)} = P$ by induction. $\square$

Theorem 2.1.4 guarantees the control over the end points of the the curve, whereas Theorem 2.1.6 ensures that the Beziér curve lies close to the control points. Theorem 2.1.5 shows that transformations such as rotations and projections can be applied directly to the control points instead of the points on the curve.

Simple as their appearance may be, Beziér curves fall short of representing some of the most common geometric shapes. Given a finite number of control points, we can never make $B_P(t)$ a circular arc, although a circle has a very simple parametric form. One of their greatest perks, the ability to describe a shape with a low number of of control points, is simultaneously one of their greatest shortcoming. This is most likely the reason why Beziér curves are not the state of the art in technical engineering applications. However, Beziér curves certainly do provide an intuition for Non-Uniform Rational B-Splines or NURBS, which is their prevailing counterpart.

2.2 Non-Uniform Rational B-splines (NURBS)

NURBS are a state of the art tool for curve and surface modelling. There is a somewhat common joke that describes the acronym NURBS as *"Nobody Understands Rational B-Splines"* (source?). In this section, we invalidate this punch line. First of all, we discuss B-splines, then we construct B-spline curves and surfaces and then we apply simple transformations to the B-spline curves and surfaces to acquire NURBS curves and surfaces.

2.2.1 Definition

Similarly to how Beziér curves are defined on the Bernstein polynomial basis, NURBS are defined on basis functions called basis splines or, more commonly, B-splines.

Definition 2.2.1. A *knot sequence* $(t_m)_{m=-\infty}^{\infty} \subset \mathbb{R}$ is a sequence with $t_m \leq t_{m+1}$ for all $m \in \mathbb{Z}$.

Definition 2.2.2. The *B-splines of degree* 0 on a knot sequence (t_m) are defined as

$$N_{1,k}^{(t_m)}(t) := \begin{cases} 1 & \text{if } t \in [t_k, t_{k+1}), \\ 0 & \text{else.} \end{cases} \tag{2.4}$$

The *B-splines of degree* $p - 1$ with $p > 1$ are given by the *Cox-de-Boor recursion formula*

$$N_{p,k}^{(t_m)}(t) := \omega_{p-1,k}^{(t_m)}(t)\, N_{p-1,k}^{(t_m)}(t) + (1 - \omega_{p-1,k+1}^{(t_m)}(t))\, N_{p-1,k+1}^{(t_m)}(t), \tag{2.5}$$

where

$$\omega_{p,k}^{(t_m)}(t) := \begin{cases} \frac{t - t_k}{t_{k+p} - t_k} & \text{if } t_{k+p} \neq t, \\ 0 & \text{else.} \end{cases} \tag{2.6}$$

Remark. Instead of $N_{p,k}^{(t_m)}$ we write $N_{p,k}$ and explicitly refer to (t_m) when necessary. We restrict the domain of definition of $N_{p,k}$ to $[0,1]$ by setting $\lim_{m\to-\infty} t_m = 0$ and $\lim_{m\to\infty} t_m = 1$.

Definition 2.2.3. A *B-spline curve* of degree $p - 1$ over a set of control points

$$P = \{P_0, P_1, ... P_n\} \subset \mathbb{R}^d$$

and a knot sequence (t_m) is defined as

$$S_P(t) = \sum_{k=0}^{n} N_{p,k}(t) P_k.$$

Definition 2.2.4. A *NURBS curve* $C_P(t)$ of degree $p - 1$ with the control points

$$P = \{P_0, P_1, ..., P_n\} \subset \mathbb{R}^d,$$

the control weights $w = (w_0, w_1, ... w_n) \subset \mathbb{R}$ and a knot sequence (t_m) is defined as

$$C_P(t) = \frac{\sum_{k=0}^{n} N_{p,k}(t) w_k P_k}{\sum_{k=0}^{n} N_{p,k}(t) w_k}. \tag{2.7}$$

Remark. Let $P \subset \mathbb{R}^d$. A NURBS curve can alternatively be understood as a projection of a B-spline curve on a transformed set of control points. For this purpose we define the embedding into the weighted vector space

$$\Phi_w : \mathbb{R}^d \to \mathbb{R}^{d+1}$$

that maps each control point $P_k = (p_1, ..., p_d) \in \mathbb{R}^d$ onto $(w_k p_1, ..., w_k p_d, w_k) \in \mathbb{R}^{d+1}$. We also have to define the projection map

$$\Phi^\dagger : \mathbb{R}^{d+1} \to \mathbb{R}^d$$

that maps each point on the B-spline curve $S_{\Phi(P)}(t) = (s_1, ..., s_d, s_{d+1})$ onto $(\frac{s_1}{s_{d+1}}, ..., \frac{s_d}{s_{d+1}})$. We can then define the NURBS curve as

$$C_P(t) = \Phi^\dagger(S_{\Phi_w(P)}(t))$$

which we will make use of later on.

Theorem 2.2.5. Let $w \equiv 1$. Then $S_P \equiv \Phi^\dagger(S_{\Phi_w(P)})$. In other words, NURBS curves are a generalization of B-spline curves.

Proof. Since in this case $\Phi_w((p_1, ..., p_d)) = (p_1, ..., p_d, 1)$, we have

$$\Phi^\dagger(S_{\Phi_w(P)}(t)) = \Phi^\dagger(\Phi_w(S_P(t))) = S_P(t).$$
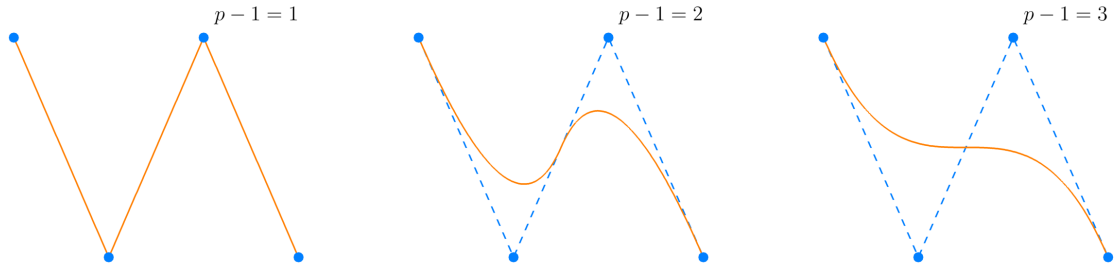
$\square$

Figure 2.3: A set of control points and three NURBS curves of different degrees.

Now that we have defined B-spline curves and NURBS curves, we can define B-spline surfaces and NURBS surfaces in a similar manner. To do this, we require a grid of knots represented by two knot sequences $(u_m)_{m=-\infty}^\infty$ and $(v_m)_{m=-\infty}^\infty$ which satisfy the same conditions as (t_m) did before. Instead of a one-dimensional set of control points, the surface definition relies on a two-dimensional set of control points. Notice that this grants us control

Definition 2.2.6. A *B-spline surface* $S_P(u, v)$ of degree $(p-1, q-1)$ over a set of control points $P = \{P_{i,j} : (i,j) \in \{0, 1, ..., n_u\} \times \{0, 1, ..., n_v\}\} \subset \mathbb{R}^d$ on the knot grid $(u_m), (v_m)$ is defined as

$$S_P(u, v) = \sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) P_{k_u, k_v},$$

where $N_{p,k_u}(u) := N_{p,k_u}^{(u_m)}(u)$ and $N_{q,k_v}(v) := N_{q,k_v}^{(v_m)}(v)$.

7

Definition 2.2.7. A *NURBS surface* $C_P(u, v)$ of degree $(p-1, q-1)$ over a set of control points $P = \{P_{i,j} : (i,j) \in \{0, 1, ..., n_u\} \times \{0, 1, ..., n_v\}\} \subset \mathbb{R}^d$, the control weights $w = \{w_{i,j} : (i,j) \in \{0, 1, ..., n_u\} \times \{0, 1, ..., n_v\}\} \subset \mathbb{R}$ and the knot grid $(u_m), (v_m)$ is defined as

$$C_P(u, v) = \frac{\sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) w_{k_u,k_v} P_{k_u,k_v}}{\sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) w_{k_u,k_v}},$$

where $N_{p,k_u}(u) := N_{p,k_u}^{(u_m)}(u)$ and $N_{q,k_v}(v) := N_{q,k_v}^{(v_m)}(v)$.

Remark. As with NURBS curve, we have the analogous result

$$C_P(u, v) = \Phi^\dagger(S_{\Phi_w(P)}(u, v))$$
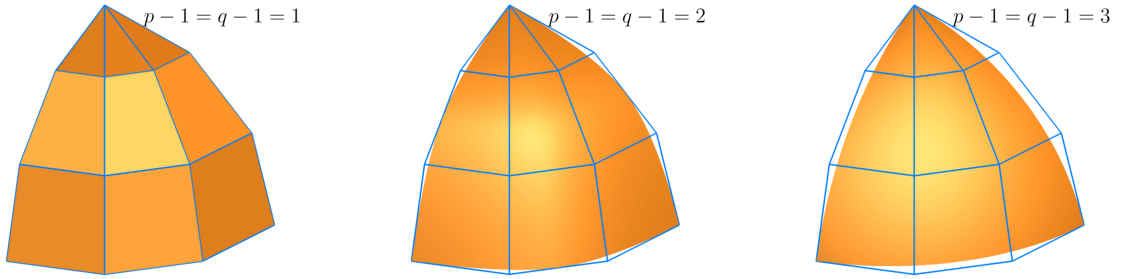
for NURBS surfaces.

Figure 2.4: A set of control points and three NURBS surfaces of different degrees.

The notion of the knot sequence (t_m) is commonly computationally simplified to that of a knot vector τ, since τ only contains a finite number of elements. For our purposes, we let

$$\tau = (\underbrace{t_0, ..., t_{p-1}}_{=0}, t_p, ..., t_n, \underbrace{t_{n+1}, ..., t_{n+p}}_{=1}),$$

where $t_k = 0$ for $k \in \{0, ..., p-1\}$ and $t_k = 1$ for $k \in \{n+1, ..., n+p\}$. We still require the monotony property $t_k \leq t_{k+1}$ for all $k \in \{0, ..., n+p\}$.

2.2.2 De Boor's Algorithm

To efficiently calculate points on a B-spline object, Carl-Wilhelm Reinhold de Boor devised an efficient algorithm, the construction of which demonstrates its correctness. Together with the embedding Φ_w and the projection $\Phi^\dagger$ from the Remark for Definition 2.2.4, this algorithm can also be used to calculate points on a NURBS object.

Let $P = \{P_0, P_1, ..., P_n\}$ a set of control points, (t_m) a knot sequence and $p-1$ the degree of the B-spline curve $S(t)$. Then by the Cox-de-Boor recursion formula, we find

$$\begin{aligned} S(t) &= \sum_{k=0}^{n} N_{p,k}(t) P_k \\ &= \sum_{k=1}^{n} \omega_{p-1,k}(t) N_{p-1,k}(t) P_k + \sum_{k=0}^{n} (1 - \omega_{p-1,k+1}(t)) N_{p-1,k+1}(t) P_k. \end{aligned}$$

Changing the limits of the second term, we can summarize the two terms as

$$S(t) = \sum_{k=1}^{n} N_{p-1,k}(t) \underbrace{\left[\omega_{p-1,k}(t)\, P_k \; + \; (1 - \omega_{p-1,k}(t))\, P_{k-1} \right]}_{=:P_k^{(1)}(t)}$$

$$= \sum_{k=1}^{n} N_{p-1,k}(t)\, P_k^{(1)}(t).$$

Recursively defining

$$P_k^{(j)}(t) := \begin{cases} \omega_{p-j,k}\, P_k^{(j-1)}(t) \; + \; (1 - \omega_{p-j,k})\, P_{k-1}^{(j-1)}(t) & \text{if } j > 0, \\ P_k & \text{else,} \end{cases} \tag{2.8}$$

we can repeat this process up to $p - 2$ more times, finding

$$S(t) = \sum_{k=p-1}^{n} N_{1,k}(t)\, P_k^{(p-1)}(t) = P_l^{(p-1)}(t)$$

for $t \in [t_l, t_{l+1})$. We can thus use the recursive definition in Equation 2.8 as the key step of our algorithm to compute $S(t)$. It becomes apparent that the points calculated on a B-spline curve are in fact also a cumulated convex combination of control points, just as it is the case with Beziér curves. As zero-values for $\omega_{i,j}$ (or $1 - \omega_{i,j}$) can be completely omitted by checking multiplicity, we arrive at the following algorithm:
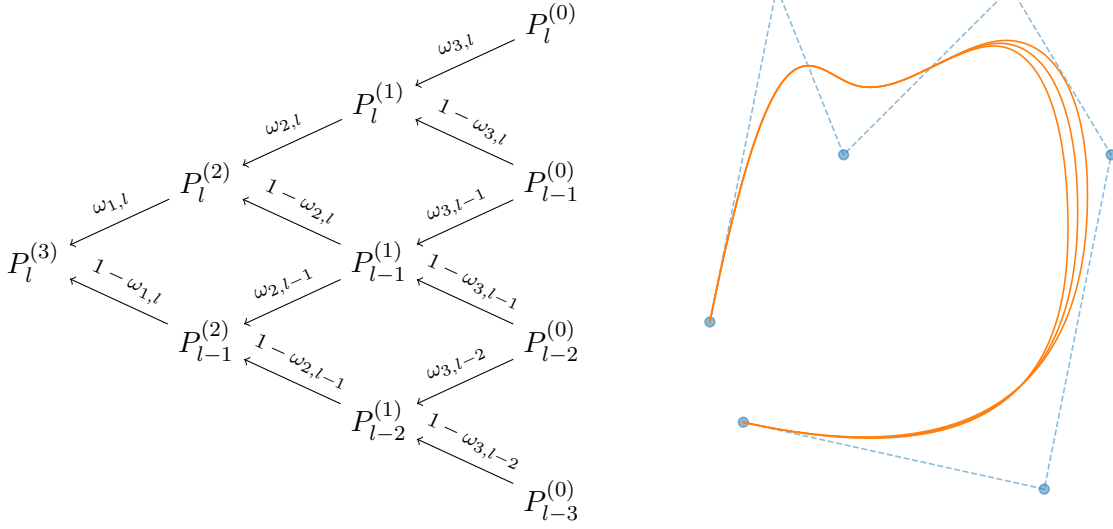

Algorithm 2 de Boor's algorithm for curves

1: **Input**
2:      $P = \{P_0, P_1, ..., P_n\}$ set of control points of the B-spline curve
3:      $\tau = (t_0, t_1, ..., t_{n+p})$ knot vector of the B-spline curve
4:      $p - 1$ degree of the B-spline curve
5:      $t \in [t_0, t_{n+p})$ real number

6: **Output**
7:      $S_P(t)$ the point on the B-spline curve w.r.t. to t

8: **procedure** DEBOORCURVE(P, p, τ, t)
9:      Find l such that $t \in [t_l, t_{l+1})$
10:      Let m be the multiplicity of t in the knot vector τ
11:      $P^{(0)} \leftarrow P$
12:      **for** $j = 1, 2, ..., p - m - 1$ **do**
13:          **for** $k = l - p + j + 1, ..., l - m$ **do**
14:          $\omega_{p-j,k} \leftarrow \frac{t - t_k}{t_{k+p-j} - t_k}$
15:          $P_k^{(j)} \leftarrow (1 - \omega_{p-j,k}) \cdot P_{k-1}^{(j-1)} + \omega_{p-j,k} \cdot P_k^{(j-1)}$
16:      **return** $P_{l-m}^{(p-m-1)} = C_P(t)$

(a) Visualization of de Boor's algorithm on a curve $S_P(t)$ with degree 3, where t does not appear in the knot vector τ (in other words, $m = 0$.

(b) Degree 3 NURBS curve $\Phi^\dagger(S_{\Phi_w(P)}(t))$ for different values of a single entry of the control weight vector w.

Figure 2.5: Calculating points on a NURBS curve.

To calculate one point on the B-spline curve S_P of degree p, we require at most $\frac{p^2-p}{2}$ vector additions and $p^2 - p$ scalar multiplications, which is quite similar to what we found for Beziér curves. However, we also need to calculate $\omega_{j,k}$ at every step, which in total sums up to $p^2 - p$ real additions and $\frac{p^2-p}{2}$ real multiplications.

By writing the definition of the B-spline surface as

$$S_P(u,v) = \sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) P_{k_u,k_v} = \sum_{k_u=0}^{n_u} N_{p,k_u}(u) \underbrace{\left(\sum_{k_v=0}^{n_v} N_{q,k_v}(v) P_{k_u,k_v} \right)}_{:= q_{k_u}(v)},$$

we can observe that Algorithm 2 can be utilized to calculate points on B-splines surfaces. To do this, we run the de Boor's algorithm to calculate $q_{k_u}(v)$.

Algorithm 3 de Boor's algorithm for surfaces
1:	**Input**	
2:	$P = \{P_{i,j}\}$	set of control points with $n_1 \cdot n_2$ elements
3:	$\tau_u = (u_0, u_1, ..., u_{n_u+p})$	first knot vector of the B-spline curve
4:	$\tau_v = (v_0, v_1, ..., v_{n_v+q})$	second knot vector of the B-spline curve
5:	$p-1$	first degree of the B-spline curve
6:	$q-1$	second degree of the B-spline curve
7:	$u \in [u_0, u_{n_u+p})$	first real number
8:	$v \in [v_0, v_{n_v+q})$	second real number
9:	**Output**	
10:	$S_P(u,v)$	the point on the B-spline curve w.r.t. to u, v

11: **procedure** DEBOORSURFACE($P, p, q, \tau_u, \tau_v, u, v$)
12:      Find l such that $u \in [u_l, u_{l+1})$
13:      Let m be the multiplicity of u in the knot vector τ_u
14:      **for** $k = l - p + 1, , ..., l - m - 1$ **do**
15:          $Q_k \leftarrow$ deBoorCurve($P_{k,\cdot}, q, \tau_v, v$)
16:      **return** deBoorCurve(Q, p, τ_u, u)

Utilizing the notation with the embedding map Φ_w and the projection map $\Phi^\dagger$, we can calculate points on NURBS objects with these two algorithms. To do this, we employ the following steps on a set of control points P and the weights w:

1. Calculate $P_w = \Phi_w(P)$.

2. Use de Boor's algorithm to calculate points on S_{P_w}.

3. Project points onto $\mathbb{R}^d$ by applying $\Phi^\dagger$ to S_{P_w} to find C_P.

2.2.3 Properties

In this section, we will see that B-spline curves and NURBS curves share some (although not all) useful properties with Beziér curves.

Theorem 2.2.8. Let S_P a B-spline curve and C_P a NURBS curve. Then $S_P(0) = P_0$ and $S_P(1) = P_n$ and therefore $C_P(0) = P_0$ and $C_P(1) = P_n$.

Proof. By using Algorithm 2, we have $m = p$ and return P_l without calculation, which is P_0 in the case of $t = 0$ and P_n in the case of $t = 1$. Then by $C_P(t) = \Phi^\dagger(S_{\Phi_w(P)}(t))$, we have $C_P(0) = \Phi^\dagger\Phi_w(P_0) = P_0$ and $C_P(1) = \Phi^\dagger\Phi_w(P_n) = P_n$. $\qquad\square$

Theorem 2.2.9. Let $T \in \mathbb{R}^{d \times d}$. Let S_P be a B-spline curve or surface and C_P a NURBS curve or surface. Then $S_{TP} = TS_P$ and $C_{TP} = TC_P$.

Proof. By linearity of T we can compute

$$S_{TP}(t) = \sum_{k=0}^{n} N_{p,k}(t) T P_k = T\left(\sum_{k=0}^{n} N_{p,k}(t) P_k\right) = TS_P(t)$$

for B-spline curves and

$$C_{TP}(t) = \frac{\sum_{k=0}^{n} N_{p,k}(t) w_k TP_k}{\sum_{k=0}^{n} N_{p,k}(t) w_k} = T\left(\frac{\sum_{k=0}^{n} N_{p,k}(t) w_k P_k}{\sum_{k=0}^{n} N_{p,k}(t) w_k}\right) = TC_P(t)$$

for NURBS curves. Similarly, we can compute

$$S_{TP}(u,v) = \sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) TP_{k_u,k_v} = TS_P(u,v)$$

for B-spline surfaces and

$$C_{TP}(u,v) = \frac{\sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) w_{k_u,k_v} TP_{k_u,k_v}}{\sum_{k_u=0}^{n_u} \sum_{k_v=0}^{n_v} N_{p,k_u}(u) N_{q,k_v}(v) w_{k_u,k_v}} = TC_P(u,v)$$

for NURBS surfaces. $\qquad \square$

Theorem 2.2.10. A B-spline curve or surface S_P lies in the convex hull of its control points P.

Proof. Using Equation 2.8, we can see that every iteration of Algorithm 2 produces a set of points which all lie in the convex hull of the last iteration. Therefore, $S_P(t) = P_l^{(p-1)}$ lies in the convex hull of $P^{(0)}$ for all l. $\qquad \square$

Remark. This theorem does not hold for NURBS curves and surfaces C_P.

For a given degree p, B-spline and NURBS curves can have any number $n > p + 1$ of control points. This makes them a much more flexible tool than their Beziér counterpart. Yet Beziér, B-splines and NURBS curves still share a lot of nice properties, which makes them, once implemented, easy to use.

2.3 Common Methods on Curves and Surfaces

In this section, the most important tools of CoolingGen are presented. However simple the modification of NURBS objects through their control points may be, common and useful operations such as the calculation of intersection points, the projection of an arbitrary point in space onto a curve and finding useful offset curves and fillets are major challenges. (Insert SIAM journal citation about how much cost bad intersection algorithms generated).

This comes down to the fact that many of the problem statements are (generally) non-convex minimization problems. However, these problems can often be greatly simplified by asserting properties of underlying geometric patterns that arise in specific procedures.

2.3.1 Point Inversion

Let $\gamma(t) \subset \mathbb{R}^d$ a curve, $t \in [0,1]$, and let $Q \in \mathbb{R}^d$ a point. We want to find an element in the set

$$T^* := \arg\min_{t \in [0,1]} D(\gamma(t), Q),$$

where $D(\cdot, \cdot)$ is the Euclidean distance between two points. Notice that

$$\min_{t \in [0,1]} D(\gamma(t), Q) = D(\gamma(t^*), Q),$$

is the distance between the curve γ and the point Q, and is constant for all $t^* \in T^*$.
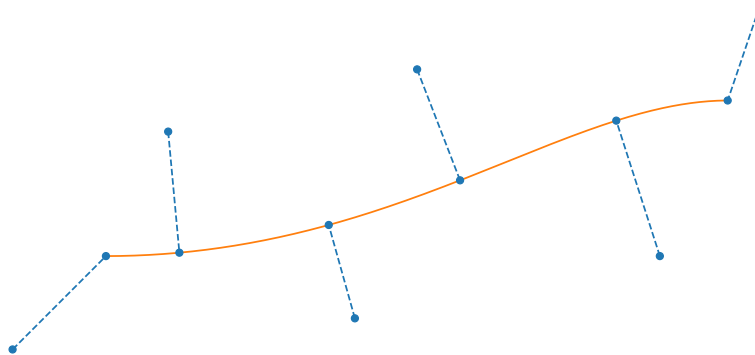

Figure 2.6: Point inversion. Each blue point on the orange curve is the projection of the point connected to it with a dotted line.

Definition 2.3.1. The distance between a curve $\gamma \subset \mathbb{R}^d$ and a point $Q \in \mathbb{R}^d$ is given by

$$D(Q, \gamma) := D(\gamma, Q) := \min_t D(\gamma(t), Q).$$

Remark. If $D(Q, \gamma) = 0$, then by the point-separating property of the Euclidean norm, Q lies on the curve γ.

Theorem 2.3.2. Let $\gamma(t) \subset \mathbb{R}^d$ a curve, $t \in [0, 1]$ and let $Q \in \mathbb{R}^d$. If γ has no self-intersections and

$$\min_{t \in [0,1]} D(\gamma(t), Q) = 0$$

then T^* is a single element set.

Proof. If γ has no self-intersections, then no two parameters of γ will map onto the same point. Therefore, γ is injective. We know t^* exists such that $D(\gamma(t^*), Q) = 0$, which by the point-separating property of the Euclidean norm is equivalent to $Q = \gamma(t^*)$. By injectivity, this t^* is unique. $\qquad\square$

Minimizing distance functions for general curves is a problem that is hard to solve. We therefore make some assumptions about the point-curve distance function $\phi(t) := D(\gamma(t), Q)$ that we are going to minimize in order to find one target parameter $t^* \in T^*$. If ϕ is convex and differentiable, then the problem statement has a well-known and easy to implement solution, namely Newton's method, which for an initial guess $t^{(0)}$ is given by the iteration

$$t^{(n+1)} = t^{(n)} - \frac{\phi(t^{(n)})}{\phi'(t^{(n)})}.$$

Here, $\phi'(t)$ is the derivative of $\phi(t)$ with respect to t, which for a small value of $\epsilon > 0$ can be approximated by the right-sided difference quotient

$$\phi_r'(t) = \frac{\phi(t + \epsilon) - \phi(t)}{\epsilon}.$$

However, to ensure differentiability of ϕ adjacent to t, it is recommended to compare the value of the right-sided difference quotient to

$$\phi_l'(t) = \frac{\phi(t) - \phi(t - \epsilon)}{\epsilon},$$

which is the left-sided difference-quotient. If $\phi_r'(t) = \phi_l'(t)$, then we can assume $\phi_l'(t) \approx \phi(t) \approx \phi_r'(t)$.

Although in CoolingGen, we often cannot make the assumption of differentiability or convexity of ϕ. We therefore employ a pragmatic scheme and assume continuity, piecewise differentiability and piecewise convexity of ϕ and run Newton's method on a small subinterval $[l, u] \subset [0, 1]$.

To find $[l, u]$, we sample the curve γ at a set of points $\{t_0, t_1, ..., t_n\}$ with $t_i = \frac{i}{n}$ and seek

$$m = \underset{t \in \{t_0, t_1, ..., t_n\}}{\arg \min} \phi(t).$$

We let $l = m - \frac{1}{n}$ and $u = m + \frac{1}{n}$. Next, we can use Newton's method with the start value m to find

$$t^* = \underset{t \in [l, u]}{\arg \min} \phi(t).$$

This scheme will only converge to the global minimum of ϕ for large enough $n \in \mathbb{N}$.

We describe the procedure in pseudo-code. The start and boundary value search is described by the following algorithm.

Algorithm 4 Start value search

1: **Input**
2:      N number of samples for initial value search
3: **procedure** FINDPOINTINVERSIONINITVALUES(γ, Q)
4:      $m \leftarrow 0$
5:      **for** $k = 1, ..., N$ **do**
6:          $t \leftarrow \frac{k}{N}$
7:          **if** $D(Q, \gamma(m)) > D(Q, \gamma(t))$ **then** $m \leftarrow t$
8:      **return** $m - \frac{i}{N}, m + \frac{i}{N}, m$

Using the start and boundary values, we apply Newton's method for M iterations to find our target value, which is returned upon completion.

Algorithm 5 Point Inversion

1: **Input**
2:     M number of iterations
3: **procedure** POINTINVERSION(γ, Q)
4:     $l, u, m \leftarrow$ findPointInversionInitValues(γ, Q)
5:     $t_0 \leftarrow m$
6:     **for** $k = 1, 2, ..., M$ **do**
7:         $t_1 \leftarrow t_0 + \epsilon$
8:         $\phi_0 \leftarrow D(\gamma(t_0), Q)$ and $\phi_1 \leftarrow D(\gamma(t_1), Q)$
9:         $\phi' \leftarrow \frac{\phi_1 - \phi_0}{\epsilon}$
10:        $t_0 \leftarrow t_0 - \frac{\phi_0}{\phi'}$
11:        **if** $t_0 < l$ **then** $t_0 \leftarrow l$
12:        **if** $t_0 > u$ **then** $t_0 \leftarrow u$
13:    **return** t_0

If the target distance is not equal to zero, the algorithm can be used to project points onto the curve, as can be seen in 2.6. If the curve is furthermore not injective, the algorithm still proves effective to find the distance $D(Q, \gamma)$, since the minimum distance is the same for all $t^* \in T^*$.

Given a surface $\beta(u, v)$ with $u, v \in [0, 1]$ and a point $Q \in \mathbb{R}^d$, we can also devise a point inversion algorithm by the same principle. We let $u_i = \frac{i}{n_u}, v_j = \frac{j}{n_v}$ for $i \in \{0, ..., n_u\}, j \in \{0, ..., n_v\}$ and $n_u, n_v \in \mathbb{N}$. Then we seek

$$m_u, m_v = \underset{(u,v) \in \{u_0,...,u_n\} \times \{v_0,...,v_n\}}{\arg\min} \phi(u, v),$$

where $\phi(u, v) := D(\beta(u, v), Q)$.

Then we apply Newton's method on $[l_u, u_u] \times [l_v, u_v] = [m_u - \frac{1}{n_u}, m_u + \frac{1}{n_u}] \times [m_v - \frac{1}{n_v}, m_v + \frac{1}{n_v}]$ with the start parameters m_u, m_v.

If the target distance is zero and γ is a NURBS curve (or β a NURBS surface), we can observe that the devised scheme is the inversion of de Boor's algorithm (Algorithm 2), that will return the input parameter that fits the point Q. This justifies the name *point inversion algorithm*.

2.3.2 Intersection of a Ray and a Curve in 2D

Definition 2.3.3. A *ray* with support vector $A \in \mathbb{R}^d$ and direction vector $B \in \mathbb{R}^d$ is given by the set of points

$$\hat{R}_{A,B} = \{A + tB \ : \ t \in \mathbb{R}, \ t \geq 0\}.$$

The dependence of a point on the ray on the real parameter t motivates the description of this set as a map

$$R_{A,B} : \mathbb{R} \to \mathbb{R}^d, \ \ t \mapsto A + tB.$$

which yields the equation $\hat{R}_{A,B} = R_{A,B}([0, \infty))$.

In this section, we want to find an algorithm that intersects a curve $\gamma(t)$ with $t \in [0, 1]$ with a ray $R_{A,B}(s)$ with $s \in [0, \infty)$. Generally, the intersection of these two sets can be written as

$$I = \gamma([0, 1]) \cap R_{A,B}([0, \infty)).$$

The algorithm presented will return only up to one element in that set, specifically the one corresponding to the lowest value of the ray parameter s. If however $I = \emptyset$, then no element will be returned.

Definition 2.3.4. Let $R_{A,B}$ a ray and $\gamma(t)$ a curve. Then the ray-curve-distance w.r.t $R_{A,B}$ and γ is defined as

$$D(R_{A,B}, \gamma) := D(\gamma, R_{A,B}) := \min_{s \in [0,\infty)} D(\gamma, R_{A,B}(s))$$

Definition 2.3.5. Let $R_{A,B}(s)$ a ray and $\gamma(t)$ a curve. If a solution to

$$\min_{s \in [0,\infty)} s \quad \text{subject to} \quad D(\gamma, R_{A,B}(s)) = 0$$

exists, then it is called *collision parameter* of $R_{A,B}$ w.r.t. γ.

We define the return value of our algorithm as the one element set given by

$$I_{\min} := \begin{cases} \{R_{A,B}(s^*)\} & \text{if } D(R_{A,B}(s^*), \gamma) \leq \epsilon, \\ \emptyset & \text{otherwise,} \end{cases}$$

where the absolute tolerance $\epsilon > 0$ is close to 0 and s^* is an approximation of the collision parameter of $R_{A,B}$ w.r.t. γ. If $I_{\min} \neq \emptyset$, then we refer to the element in $I_{\min}$ as *collision point*.

Remark. Why is the notion of the collision point of interest? To exemplify the prospect of our algorithm, imagine the following scenario: Let there be a reflective interface represented by a curve γ and a beam of light represented by a ray $R_{A,B}$. Then our model suggests the equivalence of the physical point of reflection and the collision point of the ray with respect to the curve.

We can find the approximation s^* of the collision parameter by using a common CAD scheme called *ray marching*, in which we traverse the ray $R_{A,B}$ by a small distance increments s until we achieve collision with the curve γ. How do we choose the optimal value for s? The idea is the following: Using the point inversion algorithm, we can calculate the *safe distance s* of the point A on the ray to the curve γ. Then we can easily construct a point P that fulfills $D(A, P) = s$ and lies on the ray $R_{A,B}$ by

$$P := A + s\frac{B}{||B||}.$$

Now there are only two possibilities: Either P lies within the ϵ-ball of the collision point, or the line segment $\overline{AP} \subset R_{A,B}([0, \infty))$ does not intersect with γ. In the first case, we can return $\{P\}$. In the second case, we can repeat the procedure on the set

$$R_{A,B}([0, \infty)) \setminus \overline{AP} = R_{A,B}([s, \infty)) = R_{P,B}([0, \infty)).$$

If after a certain amount of iterations N the algorithm does not converge to a point which lies within the ϵ-ball of the collision point, we return $\emptyset$.
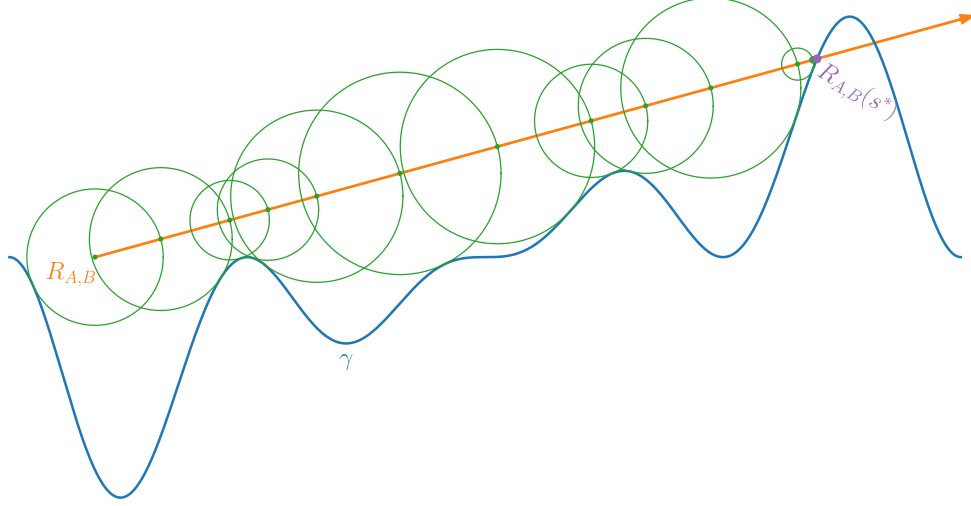

Figure 2.7: Ray marching.

Figure 2.7 describes ray marching visually. At each iteration, a new safe distance s (depicted as green circle radii) along the ray is calculated. The ray is traversed using s as step size (to achieve the points depicted in green) until the safe distance falls below the absolute tolerance ϵ. The resulting point, depicted in purple, is close to the collision point. The implementation of ray marching algorithm given a point inversion algorithm proves to be relatively simple.

Algorithm 6 Ray Marching

1: **procedure** INTERSECTCURVERAY(γ, A, B)
2:     $B \leftarrow \frac{B}{||B||}, s \leftarrow 0, P \leftarrow A$
3:     **for** $k = 1, 2, ..., N$ **do**
4:         $s \leftarrow D(\gamma(\text{pointInversion}(\gamma, P)), P)$
5:         $P \leftarrow P + sB$
6:         **if** $s < \epsilon$ **then**
7:             **return** $\{P\}$
8:     **return** $\emptyset$

2.3.3 Intersecting Two Curves in 2D

In order to trim curves at intersection points, we require the pair of parameters at which two curves intersect. Let $\gamma_1(s)$ and $\gamma_2(t)$ be two continuous curves in $\mathbb{R}^2$ with $s, t \in [0, 1]$ which instersect at finitely many points at most. In this section, we seek for the set of parameters at which these curves intersect.

Definition 2.3.6. The distance between two curves γ_1, γ_2 is defined as

$$D(\gamma_1, \gamma_2) := \min_{(s,t) \in [0,1]^2} D(\gamma_1(s), \gamma_2(t)).$$

Similarly to the prior sections, our goal is to minimize a distance function $D(\gamma_1(s), \gamma_2(t))$. In this case, we will employ a pragmatic scheme that uses a piecewise linear approximation of the curve, in which finding intersections is comparably simple and involves finding the intersection of a number of line segments.

Definition 2.3.7. The intersection parameter set of two continuous curves γ_1 and γ_2 is defined as

$$I(\gamma_1, \gamma_2) := \{(s, t) \in [0, 1]^2 : \gamma_1(s) = \gamma_2(t)\}.$$

Notice that $\gamma_1([0, 1]) \cap \gamma_2([0, 1]) = \emptyset$ if and only if $I(\gamma_1, \gamma_2) = \emptyset$.
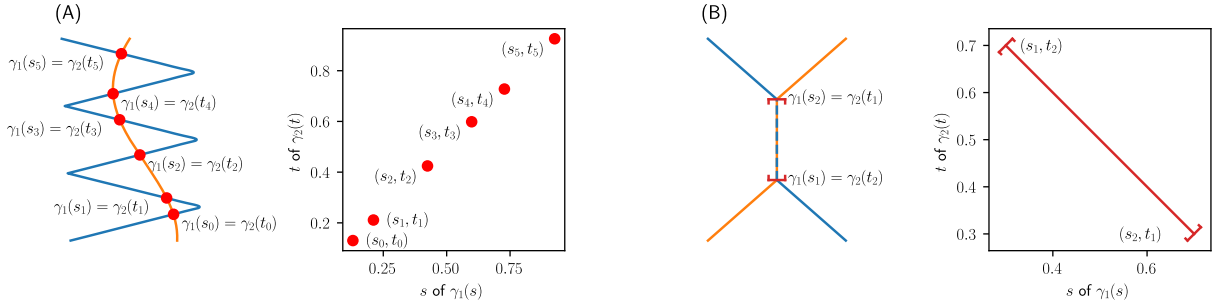

Figure 2.8: In (A) we have $|I(\gamma_1, \gamma_2)| < \infty$, whereas in (B) we have $|I(\gamma_1, \gamma_2)| = \infty$.

For the use with CoolingGen, our goal is to find the set $I(\gamma_1, \gamma_2)$ in case of $|I(\gamma_1, \gamma_2)| < \infty$ (see Figure 2.8).

Definition 2.3.8. The line segment between the points A_s and A_e is defined as the set

$$\overline{A_s A_e} := \{(1 - t)A_s + tA_e : t \in [0, 1]\}.$$

The dependence of a point on the line segment on the real parameter t motivates the description of this set as a map

$$L_A : \mathbb{R} \to \mathbb{R}^d, \quad t \mapsto (1 - t)A_s + tA_e,$$

which yields the equation $\overline{A_s A_e} = L_A([0, 1])$. Notice that given the definition of the direction vector $A_d := A_e - A_s$, we can write

$$L_A(t) = A_s + tA_d$$

The key idea of our algorithm is described by the following theorem.

Theorem 2.3.9. Let γ_1 and γ_2 be two continuous curves and let $(s^*, t^*) \in I(\gamma_1, \gamma_2) \cap (0, 1)^2$. If the curve derivatives yield $\nabla \gamma_1(s^*) \neq \nabla \gamma_2(t^*)$, then there exist neighborhoods

$$[s^* - \epsilon, s^* + \epsilon] \quad \text{and} \quad [t^* - \epsilon, t^* + \epsilon]$$

18

around s^* and t^*, respectively, where $\epsilon > 0$. Then the line segments

$$\overline{\gamma_1(s^* - \epsilon)\gamma_1(s^* + \epsilon)} \quad \text{and} \quad \overline{\gamma_2(t^* - \epsilon)\gamma_2(t^* + \epsilon)}$$

intersect.

Remark. Suppose that the line segments $\overline{\gamma_1(s_1)\gamma_1(s_2)}$ and $\overline{\gamma_2(t_1)\gamma_2(t_2)}$ intersect. We cannot conclude that there is an intersection $(s, t) \in I(\gamma_1, \gamma_2)$ with $s \in [s_1, s_2]$ and $t \in [t_1, t_2]$. Using this theorem as core concept for our algorithm, we will need to ensure that

$$D(\gamma_1|_{[s_1,s_2]}, \gamma_2|_{[t_1,t_2]}) \leq \alpha$$

for a sufficiently small absolute tolerance $\alpha > 0$. If this is not the case, then no intersection lies inside of $[s_1, s_2] \times [t_1, t_2]$ and every line segment intersection found within should be discarded.

If for any intersection parameter pair $(s^*, t^*) \in I(\gamma_1, \gamma_2)$ we have $\nabla\gamma_1(s^*) = \nabla\gamma_2(t^*)$, then it is likely that the intersection is not detected by the described line segment intersection scheme.

Theorem 2.3.10. Let $L_A([0,1])$ and $L_B([0,1])$ be two line segments in $\mathbb{R}^2$. If the lines $L_A((-\infty, \infty))$ and $L_B((-\infty, \infty))$ are not parallel, their single intersection pointt is given by $L_A(t_A) = L_B(t_B)$, where

$$t_A = \frac{\det\begin{pmatrix} D_y & D_x \\ B_{d_y} & B_{d_x} \end{pmatrix}}{\det\begin{pmatrix} B_{d_x} & B_{d_y} \\ A_{d_x} & A_{d_y} \end{pmatrix}} \quad \text{and} \quad t_B = \frac{\det\begin{pmatrix} D_y & D_x \\ A_{d_y} & A_{d_x} \end{pmatrix}}{\det\begin{pmatrix} B_{d_x} & B_{d_y} \\ A_{d_x} & A_{d_y} \end{pmatrix}},$$

where $D = B_s - A_s$ and $t_A, t_B \in \mathbb{R}$. If $t_A \in [0,1] \wedge t_B \in [0,1]$, the line segments intersect in a single point.

In our algorithm we sample the curves γ_1 and γ_2 at $t_i = \frac{i}{N}$, where $i \in \{0, ..., N\}$. In the next step we check for an intersection of

$$\overline{\gamma_1(t_i)\gamma(t_{i+1})} \quad \text{and} \quad \overline{\gamma_2(t_j)\gamma_2(t_{j+1})}$$

for $i, j \in \{0, ..., N-1\}$. For all intersection pairs (i^*, j^*), we calculate the interval midpoint distance

$$D\left(\gamma_1\left(\frac{t_{i^*} + t_{i^*+1}}{2}\right), \gamma_2\left(\frac{t_{j^*} + t_{j^*+1}}{2}\right)\right)$$

and recursively repeat this procedure on the curves $\gamma_1([t_i, t_{i+1}])$ and $\gamma_2([t_j, t_{j+1}])$. If after a given recursion depth, the interval midpoint distance of some pair (i^*, j^*) is greater than a given absolute tolerance α, we discard (i^*, j^*).

The sampling into a piecewise linear interpolation of any curve will be handled by the following algorithm.

Algorithm 7 Calculating the piecewise linear interpolation

1: **Input**

2:      γ curve on $[0,1]$

3:      l, u lower and upper bound inside of $[0,1]$

4:      N number of line segments that approximate the curve

5: **procedure** PIECEWISELININTERP(γ, l, u, N)

6:      $P \leftarrow$ empty vector with $N + 1$ entries

7:      **for** $i = 0, ..., N$ **do**

8:          $P_i \leftarrow \gamma\left((u-l)\frac{i}{N} + l\right)$

9:      **return** P

Calculating whether two line segments intersect is a constant time operation. For each recursion depth, this operation is executed N^2 times, granting the total performance of $O(N^2)$.
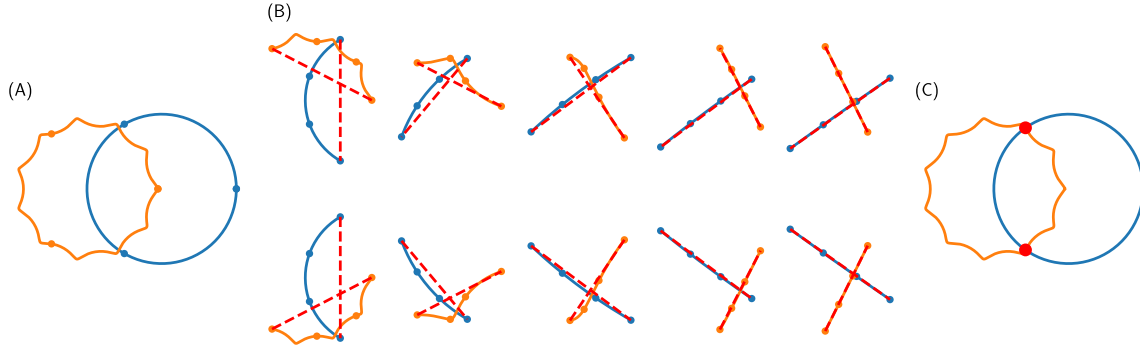

Figure 2.9: Demonstration of the curve intersection algorithm. Figure (A) shows the input curves, Figure (B) the different steps and Figure (C) the result. The dots on the curve represent the samples on the curve. The red lines represent the intersection of two line segments.

The algorithm in Figure 2.9 first calculates estimates of the intersection points and then refines those estimates until the target distance falls below α, in which case it returns the point. If a maximum recursion depth $d_{\max}$ is reached before falling below target distance, no point is returned instead. Using Algorithm 7 and writing the procedure from Theorem 2.3.10 as function `lineSegmentsIntersect`, which returns `true` if and only if the input line segments intersect, we can write the curve intersection algorithm as follows.

Algorithm 8 Curve Intersection

1: **Input**
2:     γ_1, γ_2 curves on $[0, 1]$
3:     $d_{\max}$ maximum recursion depth
4:     α absolute tolerance value
5: **Output**
6:     $I(\gamma_1, \gamma_2)$ intersection parameter set
7: **procedure** INTERSECTCURVESRECURSION$(I, \gamma_1, l_1, u_1, \gamma_2, l_2, u_2, d)$
8:     $m_1 \leftarrow \frac{l_1+u_1}{2}$ and $m_2 \leftarrow \frac{l_2+u_2}{2}$
9:     **if** $D(\gamma_1(m_1), \gamma_2(m_2)) \leq \alpha$ **then** append (m_1, m_2) to I and **return**
10:    **if** $d \geq d_{\max}$ **then** do nothing and **return**
11:    $P^{(1)} \leftarrow$ piecewiseLinInterp(γ_1, l_1, u_1, N) and $P^{(2)} \leftarrow$ piecewiseLinInterp(γ_2, l_2, u_2, N)
12:    **for** $i = 0, ..., N - 1$ **do**
13:        **for** $j = 0, ..., N - 1$ **do**
14:            **if** lineSegmentsIntersect$(P_i^{(1)}, P_{i+1}^{(1)}, P_j^{(2)}, P_{j+1}^{(2)})$ **then**
15:                $s_1 \leftarrow (l_1 - u_1)\frac{i}{N} + l_1$ and $s_2 \leftarrow (l_1 - u_1)\frac{i+1}{N} + l_1$
16:                $t_1 \leftarrow (l_2 - u_2)\frac{j}{N} + l_2$ and $t_2 \leftarrow (l_2 - u_2)\frac{j+1}{N} + l_2$
17:                intersectCurvesRecursion$(I, \gamma_1, s_1, s_2, \gamma_2, t_1, t_2, d + 1)$
18:    **return** I
19: **procedure** INTERSECTCURVES(γ_1, γ_2)
20:    $I \leftarrow \emptyset$
21:    intersectCurvesRecursion$(I, \gamma_1, 0, 1, \gamma_2, 0, 1, 0)$
22:    **return** I

Using slight modifications, one can also make use of this algorithm in self-intersection detection. The details of self-intersection are worked out in the next section.

As discussed before, this intersection algorithm might not identify an intersection parameter pair (s, t) where $\nabla \gamma_1(s) = \nabla \gamma_2(t)$. It does however prove fast and robust in the case of CoolingGen, where such intersections are currently not of interest.

2.3.4   Offset Curves and Self-Intersections in 2D

Offset curves are an important CAD tool and can be used to model contours of a certain thickness, which is why they are often referred to as parallel curves. Offset curves are paramount in the creation of fillets, which we will elaborate later. Among the variety of methods in CoolingGen, the creation of offset curves proves to be the most useful one, which perhaps lies in the very nature of cooling geometries, most of which are comprised of offset surfaces inside a given turbine blade surface.

Definition 2.3.11. Let $\gamma(t) = (x(t), y(t)) \in \mathbb{R}^2$ for $t \in [0, 1]$ be a differentiable curve. Then $O_d^\gamma(t)$ is called the d-offset curve and is defined as

$$O_d^\gamma(t) := \gamma(t) + dN^\gamma(t),$$

where $N^\gamma(t)$ is called the normal of $\gamma(t)$ and defined as

$$N^\gamma(t) := \frac{\nabla\gamma(t)^\perp}{||\nabla\gamma(t)||}$$

and

$$\nabla\gamma(t)^\perp = \left(\frac{\mathrm{d}x}{\mathrm{d}t}(t), \frac{\mathrm{d}y}{\mathrm{d}t}(t)\right)^\perp = \left(-\frac{\mathrm{d}y}{\mathrm{d}t}(t), \frac{\mathrm{d}x}{\mathrm{d}t}(t)\right)$$
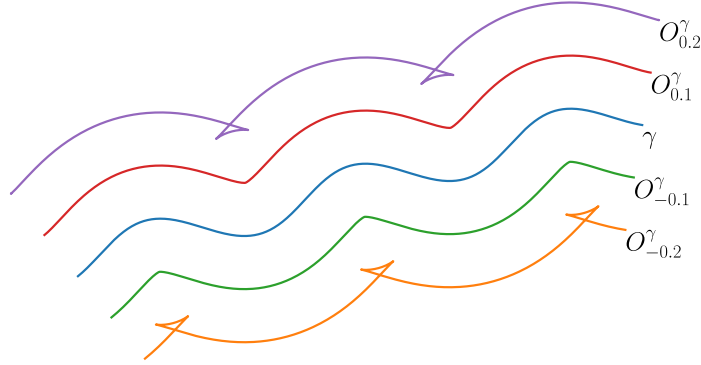
is orthogonal to the gradient of $\gamma(t)$.

Figure 2.10: Offset curves for a given curve γ and for different values of d.

As can be observed in Figure 2.10, some O_d^γ tend to self-intersect even though γ does not self-intersect. We previously established that the non-existence of any self-intersection of a curve is equivalent to its injectivity. In CoolingGen, we are often interested in modelling parallel contours. However, self-intersections do not represent meaningful objects in this context. Specifying the offset value d, a user of CoolingGen would expect to find a curve $\overline{O_d^\gamma}$ that at least satisfies the property

$$\min_s D(\gamma(s), \overline{O_d^\gamma}) = d. \tag{2.9}$$

Informally, if we imagine a ball of radius d to roll along one side of the curve γ, then $O_d^\gamma(t)$ is injective as long as the ball only touches one point at a time.

Remark. Formally, we are able to define the *curvature* $\kappa^\gamma(t)$ of a curve at any given point, which is equal to the reciprocal of the radius of the tangential sphere of the curve at that point. This notion allows us to make the following observation: If there exists some t such that $\kappa^\gamma(t) > \frac{1}{d}$, then $O_d^\gamma(t)$ is not injective.

If we force injectivity of O_d^γ in a certain way, we will be able to guarantee the property in Equation 2.9. To do this, we need to find the self-intersections of O_d^γ.

Definition 2.3.12. The parameter set of self-intersections of a curve $\gamma(t)$ is defined as

$$I(\gamma) := \{(s,t) \in [0,1]^2 : \gamma(s) = \gamma(t) \ \wedge \ s < t\}.$$

To find these self-intersections, we can use a slightly modified version of Algorithm 8. In the first recursion step of intersectCurvesRecursion, instead of iterating j from 0 to $N-1$, we are

only interested in j from $i+2$ to $N-1$, since for all $(s,t) \in I(O_d^\gamma)$, we have $s < t$. Because $s < t$ each such parameter pair naturally represents an interval subset $[s,t]$ of the parameter space $[0,1]$.

Definition 2.3.13. A pair of self-intersections $(s_1, t_1), (s_2, t_2) \in I(\gamma)$ is called nested if $[s_1, t_1] \cap [s_2, t_2] \neq \emptyset$. We call $I(\gamma)$ untangled if $I(\gamma)$ does not contain a nested pair of self-intersections.

To meaningfully trim the curve, we need to ensure that the self-intersection parameter set is untangled. We can do this by iterating over the set of intersections $I(O_d^\gamma) = \{(s_i, t_i) : i \in \{1, ..., m\}\}$ returned by Algorithm 8 and checking for disjointness of pairs $[s_i, t_i]$ and $[s_j, t_j]$ for $i \neq j$, where $i, j \in \{1, ..., m\}$. In case these two sets are not disjoint, we can replace them with their union $[s_i, t_i] \cup [s_j, t_j]$. Using this procedure, we can calculate the untangled intersection set $\overline{I}(O_d^\gamma)$.

Definition 2.3.14. For an untangled self-intersection set $\overline{I}(\gamma)$, we call the set

$$T(\gamma) := \bigcup_{(s,t) \in \overline{I}(\gamma)} [s,t]$$

the trim range of γ.

We can now choose to only further use and display the curve on $\overline{[0,1] \setminus T(O_d^\gamma)}$ or on $T(O_d^\gamma)$.
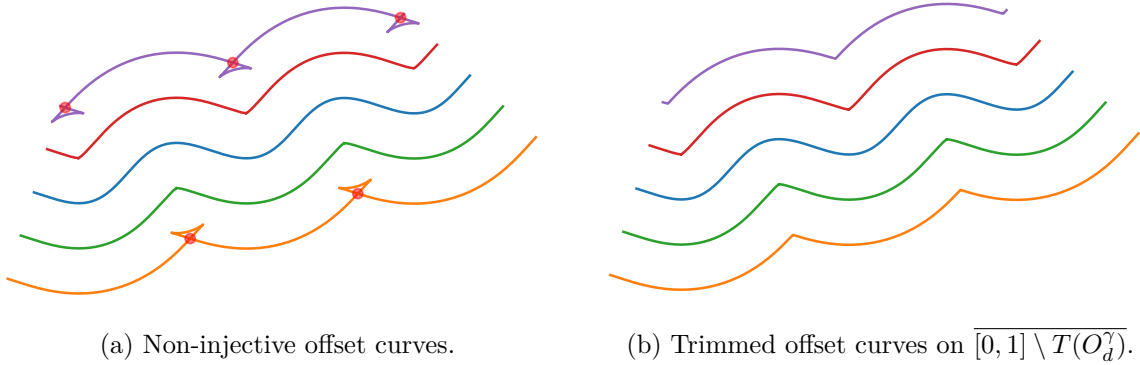

(a) Non-injective offset curves.　　　　　(b) Trimmed offset curves on $\overline{[0,1] \setminus T(O_d^\gamma)}$.

Figure 2.11: Trimming two offset curves at intervals of self intersections for a given curve γ and for different values of d.

Now, $O_d^\gamma|_{T(O_d^\gamma)}$ is not defined on all of $[0,1]$ if there are any self-intersections in O_d^γ. However, we can define a domain scaling map ξ^M, such that

$$O_d^\gamma(\xi^M([0,1])) = O_d^\gamma(M)$$

for any finite union of closed intervals M. We write the elements of M as $[s_i, t_i]$ for $i \in \{1, ..., m\}$. By setting

$$\tilde{s}_1 := 0 \quad \text{and} \quad \tilde{t}_m := 1 \quad \text{and} \quad \tilde{s}_{j+1} := \tilde{t}_j := \frac{s_{j+1} + t_j}{2}$$

for $j \in \{1, ..., m-1\}$, we can define the maps

$$\xi_i^M(t) = \begin{cases} \frac{t_i - s_i}{\tilde{t}_i - \tilde{s}_i} t & \text{if } t \in [\tilde{s}_i, \tilde{t}_i], \\ 0 & \text{else,} \end{cases}$$

23

that map $[\tilde{s}_i, \tilde{t}_i]$ onto $[s_i, t_i]$ and any other value onto 0. Notice that

$$\bigcup_{i=1}^{m} [\tilde{s}_i, \tilde{t}_i] = [0, 1].$$

This way, the domain scaling map

$$\xi^M(t) = \sum_{i=1}^{m} \xi_i^M(t)$$

maps $[0, 1]$ onto M. Since both $\overline{[0,1] \setminus T(O_d^\gamma)}$ and $T(O_d^\gamma)$ are unions of closed intervals, we can use this procedure to define the trimmed offset curve as

$$\overline{O_d^\gamma}(t) = O_d^\gamma \circ \xi^{\overline{[0,1] \setminus T(O_d^\gamma)}}(t)$$

or

$$\overline{O_d^\gamma}(t) = O_d^\gamma \circ \xi^{T(O_d^\gamma)}(t)$$

respectively. This curve now satisfies Equation 2.9.

As has been shown, the construction of meaningful offset curves is in no way trivial and requires a multitude of tools. The simple definition of an offset curve (Definition 2.3.11) is only seemingly adequate. Nonetheless, larger offsets, that would lead to self-intersection, are required by the industry. But since self-intersecting curves do no represent sensible objects, we sought for a far more convoluted process.

In fact, the creation of fillets also plays a role in the creation of offset curves, since the procedure presented leaves behind non-differentiable places on the trimmed offset curves, which are undesirable for CoolingGen's purposes.

2.3.5 The Creation of Fillets in 2D

Given two curves γ_1 and $\gamma_2 \in \mathbb{R}^2$ defined on $t \in [0, 1]$ we can sometimes construct a circle of a given radius that shares one tangential intersection point with each curve. A circle like this is called a fillet circle. Segments of these circles can replace non-differentiable segments from a curve. More formally, we can make the following definition.

Definition 2.3.15. Let γ_1 and γ_2 be two differentiable curves. If a curve $\phi_r^{\gamma_1,\gamma_2}$ satisfies the implicit definition

$$\phi_r^{\gamma_1,\gamma_2}([0, 1]) = \{(x, y) : (x - x_0)^2 + (y - y_0)^2 = r^2\}$$

for a center point (x_0, y_0) and a radius r, then it is a circle. If furthermore there exist intersection points

$$\gamma_1(s_1) = \phi_r^{\gamma_1,\gamma_2}(\sigma_1) \quad \text{and} \quad \gamma_2(s_2) = \phi_r^{\gamma_1,\gamma_2}(\sigma_2)$$

for some $s_1, s_2, \sigma_1, \sigma_2 \in [0, 1]$ and these intersection points are tangential in the sense that

$$\frac{\nabla \gamma_1(s_1)}{||\nabla \gamma_1(s_1)||} = \frac{\nabla \phi_r^{\gamma_1,\gamma_2}(\sigma_1)}{||\nabla \phi_r^{\gamma_1,\gamma_2}(\sigma_1)||} \quad \text{and} \quad \frac{\nabla \gamma_2(s_2)}{||\nabla \gamma_2(s_2)||} = \frac{\nabla \phi_r^{\gamma_1,\gamma_2}(\sigma_2)}{||\nabla \phi_r^{\gamma_1,\gamma_2}(\sigma_2)||},$$

then $\phi_r^{\gamma_1,\gamma_2}$ is a fillet circle of radius r of γ_1 and γ_2.

Remark. A fillet circle $\phi_r^{\gamma_1,\gamma_2}$ does not necessarily exist for two given curves γ_1, γ_2. If a fillet curve $\phi_{r^*}^{\gamma_1,\gamma_2}$ exists for some radius r^*, it does not exist for all radii $r \in \mathbb{R}$.

Figure 2.12: A fillet curve of radius 1 and the respective curves γ_1 and γ_2.

We will find a procedure that yields a fillet circle for a given radius r and a pair of curves γ_1, γ_2 if it exists and returns nothing otherwise. We only need to find the center point (x_0, y_0). Then we can use the parametric definition of a circle and write

$$\phi_r^{\gamma_1,\gamma_2}(t) = (r\cos(2\pi t) + x_0, r\sin(2\pi t) + y_0).$$

For example, as shown in Figure 2.12, given the curves $\gamma_1(t) = (2t - 1, 1)$ and $\gamma_2 = (1, 2t - 1)$ and a radius $r = 1$, the center point (x_0, y_0) of the fillet circle is equal to $(0, 0)$. Therefore, in this case,

$$\phi_r^{\gamma_1,\gamma_2}(t) = (\cos(2\pi t), \sin(2\pi t)),$$

which is the unit circle.

Theorem 2.3.16. Let γ_1, γ_2 and r such that a fillet circle $\phi_r^{\gamma_1,\gamma_2}$ exists. Then the midpoint $M = (x_0, y_0)$ of a fillet circle is given by

$$M = O_r^{\gamma_1}(s_1) = O_r^{\gamma_2}(s_2)$$

for $(s_1, s_2) \in I(O_r^{\gamma_1}, O_r^{\gamma_2})$.

Proof. Let $\tilde{\phi}(t) = r(\sin 2\pi t, \cos 2\pi t) + O_r^{\gamma_1}(s_1)$. Then we can calculate

$$\tilde{\phi}(t) = r(\sin 2\pi t, \cos 2\pi t) + \gamma(s_1) + rN^\gamma(s_1)$$
$$= r(\sin 2\pi t, \cos 2\pi t) + \gamma(s_1) + r\frac{\nabla\gamma(s_1)^\perp}{||\nabla\gamma(s_1)||}.$$

Notice that $(\sin 2\pi t, \cos 2\pi t)$ is equal to an arbitrary unit vector, so for some fixed $\sigma_1 \in [0, 1]$ the equation

$$(\sin 2\pi \sigma_1, \cos 2\pi \sigma_1) = \frac{\nabla\gamma(s_1)^\perp}{||\nabla\gamma(s_1)||}$$

will be satisfied, since $\frac{\nabla\gamma(s_1)^\perp}{||\nabla\gamma(s_1)||}$ is a fixed unit vector. In the same manner, we can construct σ_2 for the equivalent curve definition $\tilde{\phi}(t) = r(\sin 2\pi t, \cos 2\pi t) + O_r^{\gamma_2}(s_2)$. Notice that σ_1 and σ_2 also satisfy

$$\tilde{\phi}(\sigma_1) = \gamma_1(s_1) \quad \text{and} \quad \tilde{\phi}(\sigma_2) = \gamma_2(s_2).$$

By calculating $\nabla\tilde{\phi}(t)$, we find

$$\nabla\tilde{\phi}(t) = 2\pi(\cos 2\pi t, -\sin 2\pi t),$$

which after normalization yields the equalities

$$\frac{\nabla\gamma_1(s_1)}{||\nabla\gamma_1(s_1)||} = \frac{\nabla\tilde{\phi}_r^{\gamma_1,\gamma_2}(\sigma_1)}{||\nabla\tilde{\phi}_r^{\gamma_1,\gamma_2}(\sigma_1)||} \quad \text{and} \quad \frac{\nabla\gamma_2(s_2)}{||\nabla\gamma_2(s_2)||} = \frac{\nabla\tilde{\phi}_r^{\gamma_1,\gamma_2}(\sigma_2)}{||\nabla\tilde{\phi}_r^{\gamma_1,\gamma_2}(\sigma_2)||}.$$

Therefore, $\tilde{\phi}$ is in fact a fillet circle. $\qquad\square$

Theorem 2.3.16 tells us we can use offset curve and intersection methods to find the center point (x_0, y_0) in the general case using the following steps given a radius r and two curves γ_1 and γ_2.

1. Calculate the two offset curves $O_r^{\gamma_1}$ and $O_r^{\gamma_2}$.

2. Find their intersection parameter set $I(O_r^{\gamma_1}, O_r^{\gamma_2})$.

3. For $(s, t) \in I(O_r^{\gamma_1}, O_r^{\gamma_2})$, set $(x_0, y_0) := O_r^{\gamma_1}(s) = O_r^{\gamma_2}(t)$.
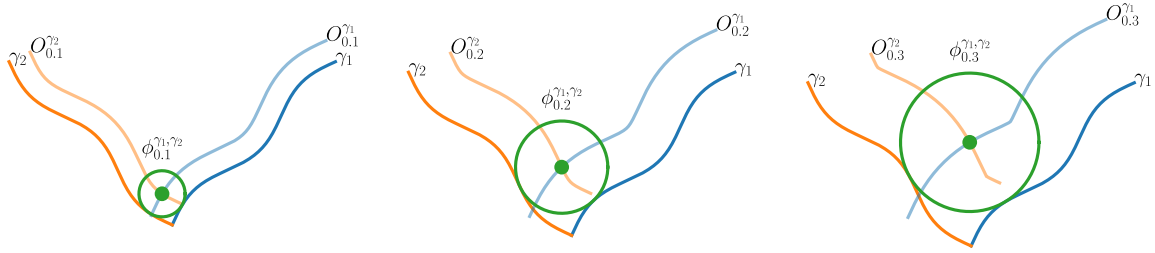

Figure 2.13: Construction of the fillet circle of different radii.

As can be seen in Figure 2.13, the curve $\phi_r^{\gamma_1,\gamma_2}$ constructed this way fulfills the requirements of Definition 2.3.15 and therefore is a fillet circle. Given the fillet circle, we now only need to trim the curves γ_1 and γ_2 and $\phi_r^{\gamma_1,\gamma_2}$.
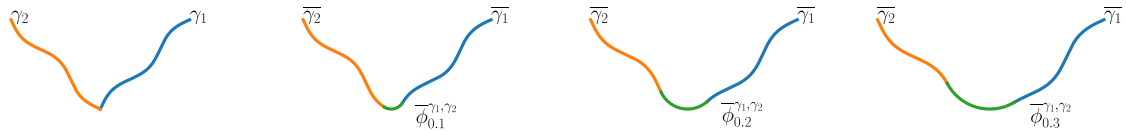

Figure 2.14: Trimmed curves and fillets

In CoolingGen, the curves which we want to connect by a fillet are always connected at their boundary points. Without loss of generality, we let $\gamma_1(0) = \gamma_2(0)$. The trimmed input curves are then given by

$$\overline{\gamma_1}(s) = \gamma_1|_{[s^*,1]}\left(\frac{s - s^*}{1 - s^*}\right) \quad \text{and} \quad \overline{\gamma_2}(t) = \gamma_2|_{[t^*,1]}\left(\frac{t - t^*}{1 - t^*}\right)$$

for $(s^*, t^*) \in I(O_r^{\gamma_1}, O_r^{\gamma_2})$. The parameters s and t are scaled such that the domains of the trimmed curves $\overline{\gamma_1}$ and $\overline{\gamma_2}$ remain equal to $[0,1]$.

Now, instead of actually trimming $\phi_r^{\gamma_1,\gamma_2}$, we can construct a circular arc between the end points $D_i := \overline{\gamma_i}(0)$ of the trimmed curves for $i \in \{1,2\}$. Let $M = (x_0, y_0)$ the fillet circle center. By sweeping the line segment $\overline{M_1 D_1}$ by a certain angle Θ, we can retrieve $\overline{\phi}_r^{\gamma_1,\gamma_2}$. This angle can be calculated by

$$\Theta = \arccos \frac{(D_1 - M) \cdot (D_2 - M)}{||D_1 - M||\ ||D_2 - M||},$$

where $(\cdot)$ is the standard dot product. We can now write the trimmed fillet curve as

$$\overline{\phi}_r^{\gamma_1,\gamma_2}(t) = R_{+t\Theta}(D_1 - M) + M = R_{-t\Theta}(D_2 - M) + M,$$

for $t \in [0,1]$, where R_Θ is the rotation matrix given by

$$R_{t\Theta} := \begin{pmatrix} \cos t\Theta & -\sin t\Theta \\ \sin t\Theta & \cos t\Theta \end{pmatrix}.$$

We are now left with the two trimmed input curves $\overline{\gamma_1}$ and $\overline{\gamma_2}$ and the fillet curve $\overline{\phi}_r^{\gamma_1,\gamma_2}(t)$.

3 Jet Engine Specific Methods

3.1 Fundamental Terms

- figure of (part of) turbine

- leading edge/trailing edge

- ss / ps

(sauce: books on cooling) The creation of cooling geometries inside of turbine blades is not only vital for the enhancement of the thermodynamic efficiency and power output of turbine engines. The materials melting temperature is often exceeded by that of the turbine inlet. To withstand this extreme condition, cooling is required. The blade geometries that we are concerned with in the development of CoolingGen are the ones that succeed the inlet in axial direction.

CoolingGen creates geometries which lie inside of the blade surface $B(u, v)$, which is an output of BladeGen, a tool used by the DLR for the design of blade surfaces. The surface $B(u, v)$ is closed in u-direction. For a given u, increasing v yields a further distance from the turbines hub. Because of rotational symmetry, it is sometimes convenient to describe these geometries in cylindrical coordinates. The transformation from Cartesian coordinates to cylindrical coordinates is given by the map

$$Z : (x, y, z) \mapsto (x, \sqrt{y^2 + z^2}).$$

Given the associated circumferential angle $\theta = \text{arctan2}(y, z)$, the transformation to cylindrical coordinates is invertible.

We also make the distinction between two kinds of blades, rotor and stator blades. While the rotor blades rotate around the hub, the stator blades have fixed positions. This was taken into account when designing CoolingGen, so both kinds are currently supported.

3.2 The S2 Stream Surface and Stream Surface Coordinates

(source: Wu, 1952 at NACA) A stream line is a line that at every point is tangential to the velocity vector field of the flow of the fluid. Its generalization, the stream surface, describes a surface with the same property. The flow in a turbine can be described by a generalization of the stream surface. When designing turbine blades, it is common practice to describe the flow in two families of stream surfaces. These surfaces are called S_1 and S_2. The S_1 surfaces, also known as *blade-to-blade* surfaces, describe the flow behavior between individual blade sections, whereas their counterpart, the S_2 surfaces, which are also known as *meridional* surfaces, describe the flow through the turbine.
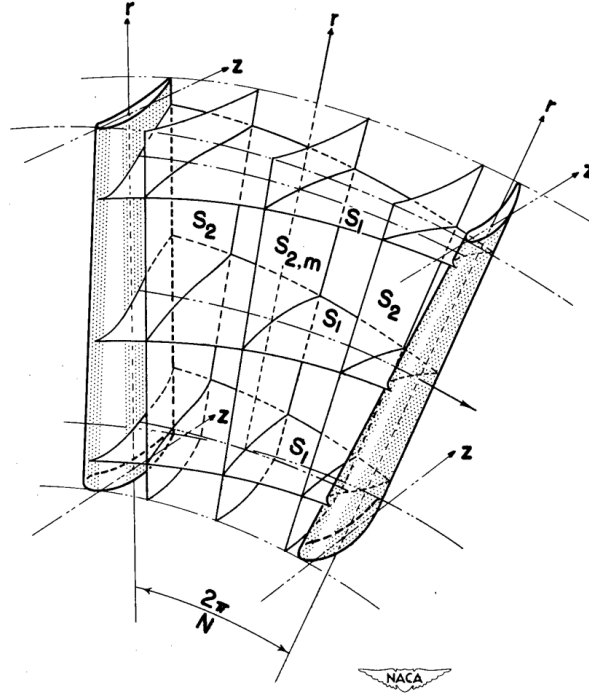
Figure 3.1: Example S_1 and S_2 surfaces of a turbomachine. The z coordinate in the figure is x.

Each S_2 surface is a parametric surface and therefore a map

$$s(u, v) : [0, 1]^2 \to \mathbb{R}^3, \quad (u, v) \mapsto (x, r, m),$$

where x is the axial coordinate, $r = \sqrt{y^2 + z^2}$ the distance from the turbine hub and m is the arc length.

To design the blades for turbomachinery, BladeGen and CoolingGen make use of a certain S_2 surface, the so called $S_{2,m}$ surface. This surface lies midway between two blades. Each stream line described by $S_{2,m}$ can then be written as $S_{2,m}(\cdot, v)$. By intersecting the cylindrically transformed u-isoparametric curves $Z(B(u, \cdot))$ of the blade with each stream line $S_{2,m}(\cdot, v)$, we can construct a curve $P_{\text{stream}}^{(v)}(u)$ from the intersection points $P_{u,v}$, given by

$$P_{\text{stream}}^{(v)}(u) = (m, r\theta, v),$$

where m is the first argument of $P_{u,v}$, the radius r is equal to the second argument of $P_{u,v}$ and θ is the circumferential angle and v is constant for each $P_{\text{stream}}^{(v)}$, making the curve planar. This coordinate system with respect to arc length m and radius-angle product $r\theta$ is a so called *stream surface coordinate system*. Even though the input blade surface $B(u, v)$ lies in $\mathbb{R}^3$, the most important methods of CoolingGen are operations on objects in this stream surface coordinate system.

4 Results

4.1 Chambers

- what are chambers

- what are they good for

- how do we construct them

Channels are hollow sections inside a turbine blade which allow for the coolant to pass through. For the construction of channels, we distinguish between straight and curved sections of the channel. The straight sections represent hollow bodies that let the coolant pass in v-direction of the turbine blade. These sections are called *chambers*. The curved sections let the coolant pass in u-direction of the turbine blade. We cal the latter sections *turns*. Inside these turns, the coolant flows between chambers. In this section, we present how chambers are constructed, whereas turn construction is throughly explained in the next section.
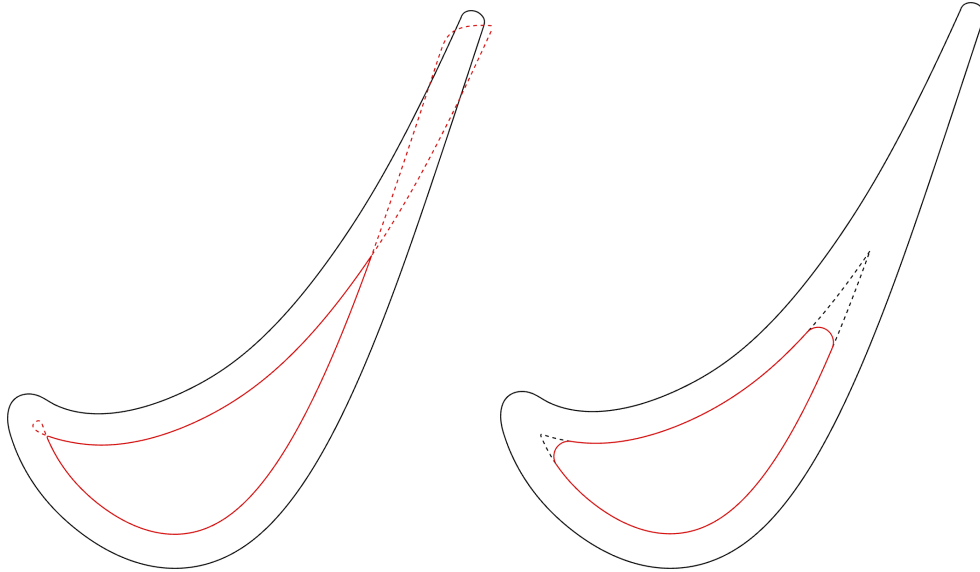

Figure 4.1: Offsetting and trimming a profile, then adding fillets where necessary.

First, we apply the stream surface coordinate transformation to a number of v-isoparametric curves of the blade to calculate a fixed number of profiles $P_{\text{stream}}^{(v_i)}(u)$ for $i \in \{0, ..., N\}$. These profiles are then offset by an input parameter. The profile is automatically trimmed adequately and fillets are added, the radius of which are declared once again as an input. We refer to the resulting profile as *shrunk profile* and declare it $S^{(v_i)}(t)$.

(a) Subdivision of profile along camber.   (b) Offsetting, trimming and adding fillets.
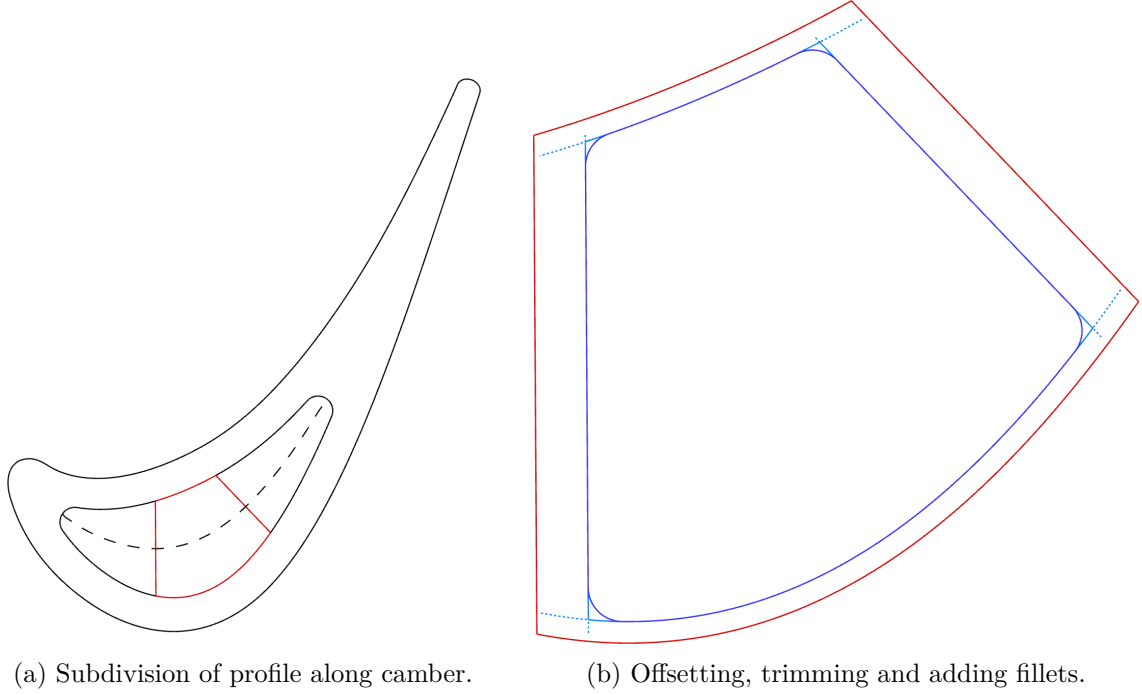
Figure 4.2: Construction of a chamber profile.

We calculate the camber curve of each shrunk profile $S^{(v_i)}$. The camber curve $c^{(v_i)}(t)$ is a design aid which is defined by the following property. A point x lies on the camber curve $c^{(v_i)}$ of $S^{(v_i)}$ if and only if for some d its offset curve $O_d^{Sv_i}$ has a self intersection at x. Along the camber curve, we define the wall input, which is given by a set of parameters w_i representing the positions of each wall relative to the camber curve, $i \in \{1, ..., N_C - 1\}$, where N_C is the number of chambers that shall be created. For each position, we also define an angle ω_i. Each position-angle pair represents two rays

$$c(w_i) + sR_{\omega_i}\nabla c(w_i) \quad \text{and} \quad c(w_i) - sR_{\omega_i}\nabla c(w_i)$$

for $s \in [0, \infty)$, where R is a rotation matrix like the one presented in ???. Using the ray marching algorithm, we can find the intersection p_i^+ and p_i^- of the rays and the profiles. The line segment $\overline{p_i^+ p_i^-}$ now represents the i-th wall.

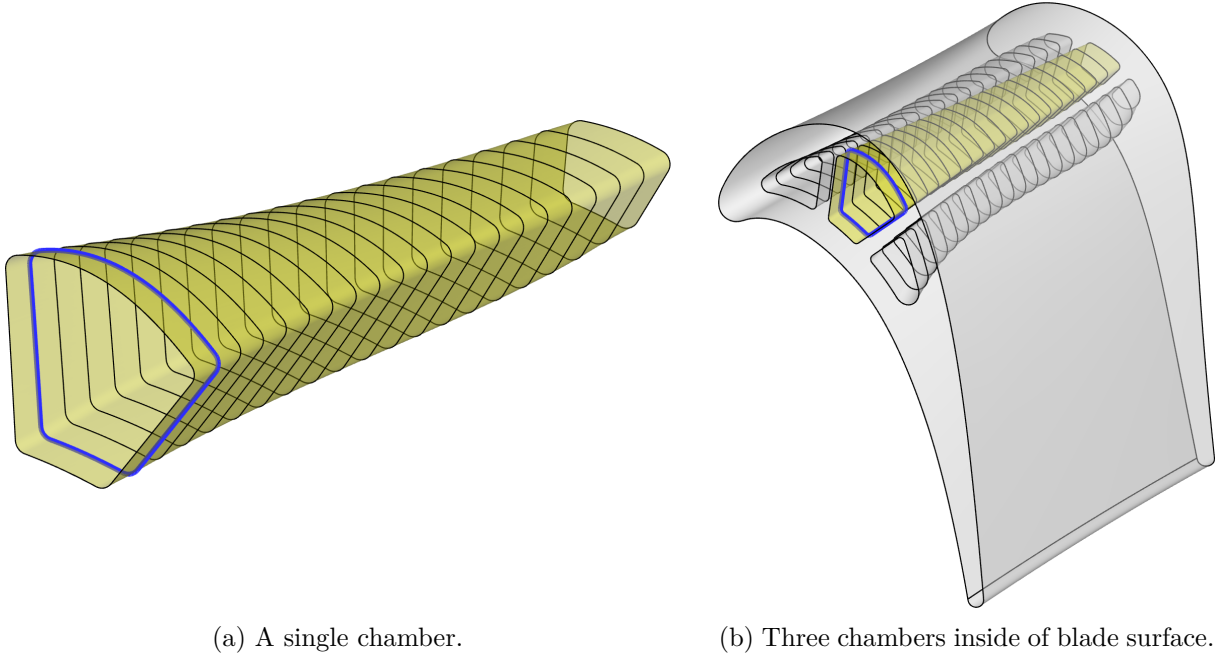The blade is then partitioned at these intersection points.

(a) A single chamber.

(b) Three chambers inside of blade surface.

Figure 4.3: Lifted chamber surfaces.

4.2 Turns

(a) Combining the chambers. The axis of rotation is marked in red.

(b) Intersecting the combined surface with affine planes that contain the axis of rotation.
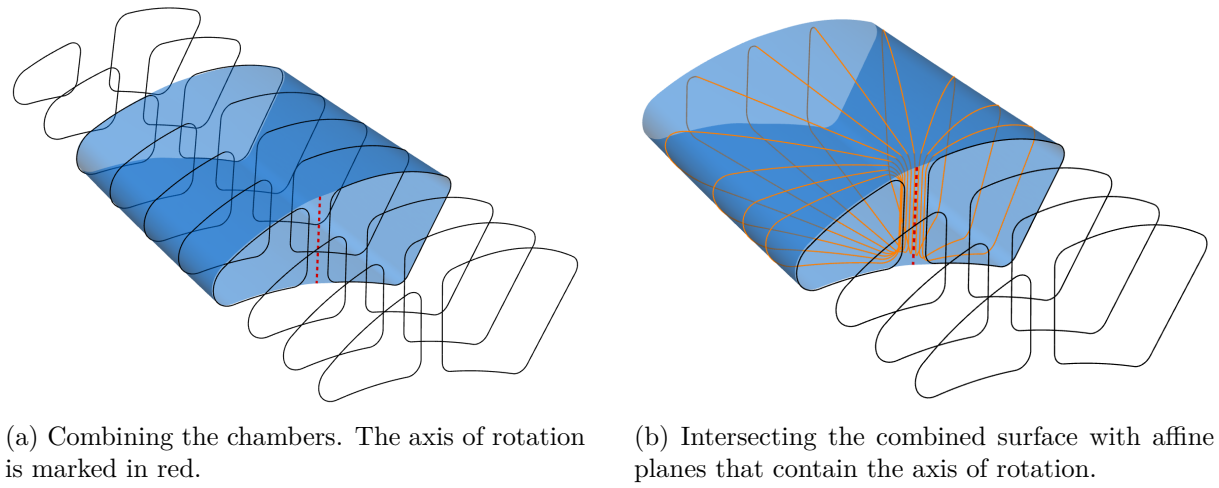
Figure 4.4: Construction of a turnaround.

(a) Channel profiles.

(b) Channel surface.
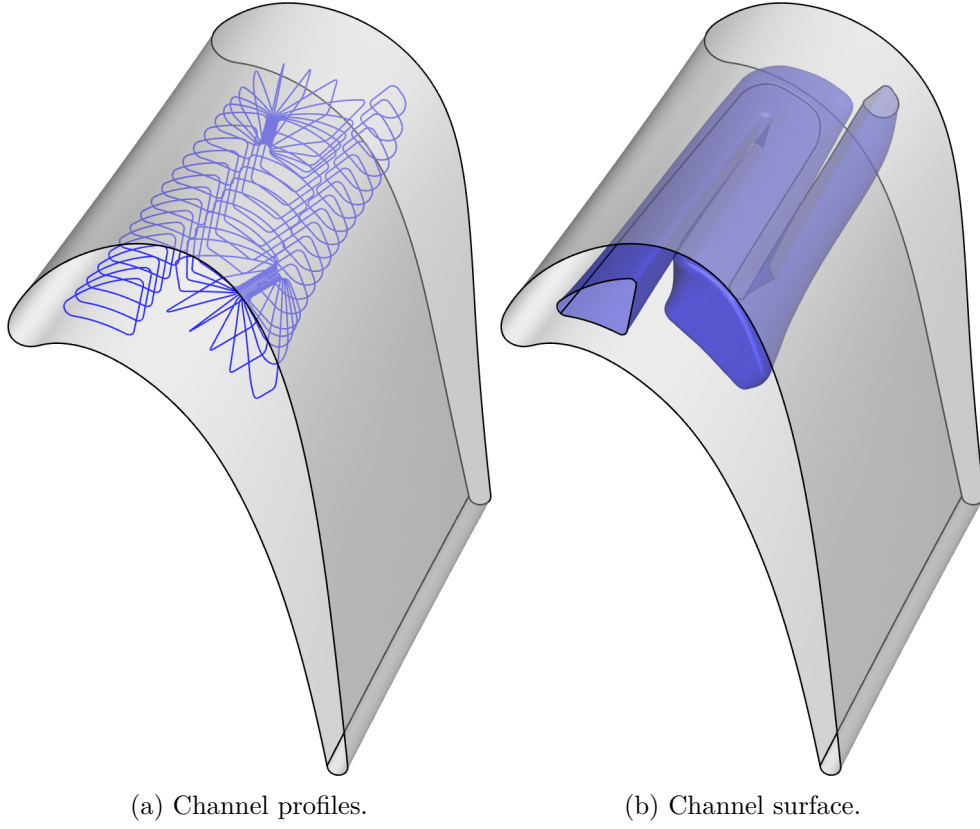
Figure 4.5: Cooling channel with three chambers and two turnarounds.

4.3 Film Cooling Holes

(a) Cylindrical.

(b) Fan shaped.
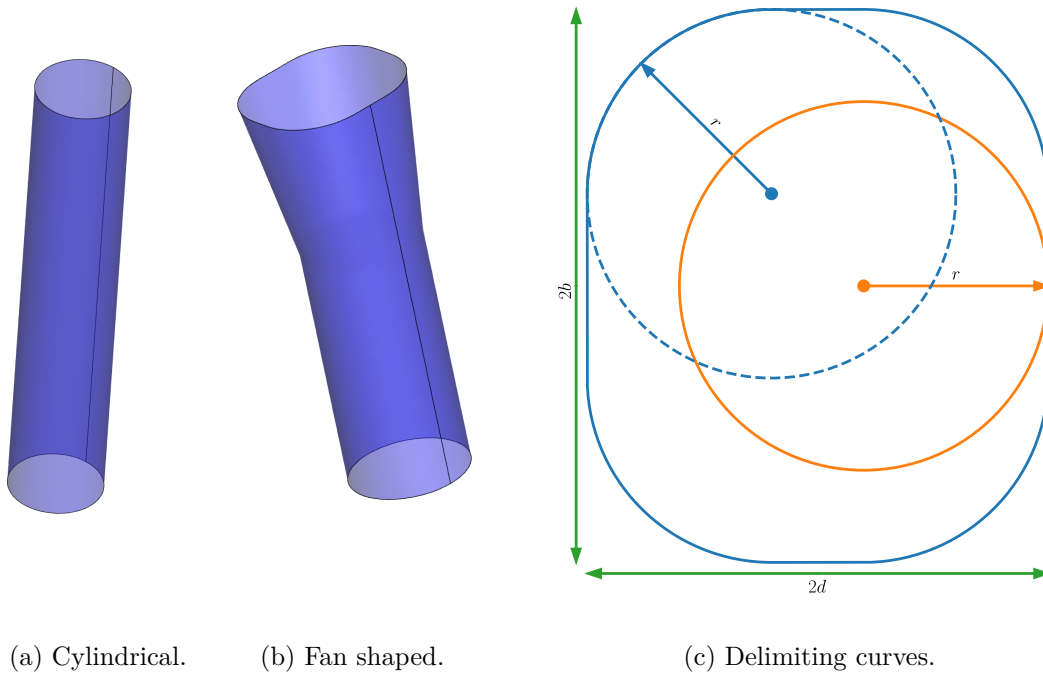
(c) Delimiting curves.

Figure 4.6: Film cooling holes and their delimiting curves

4.4   Impingement Inserts

4.5   Slots

4.6   Export for CENTAUR

4.7   Export for Open CASCADE

5 Discussion

5.1 Future Work

5.2 Conclusion

[Pie97]

6 References

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