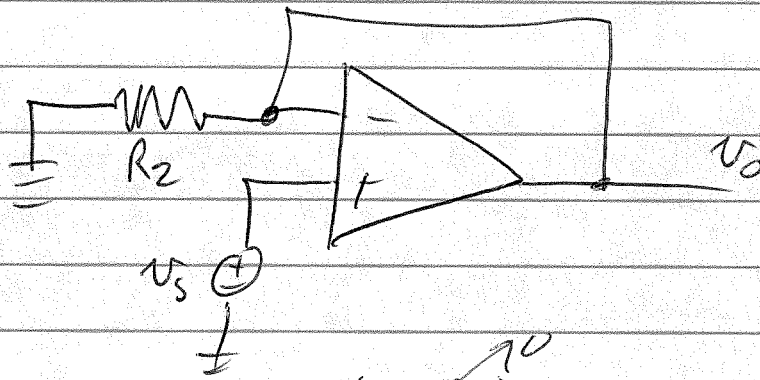


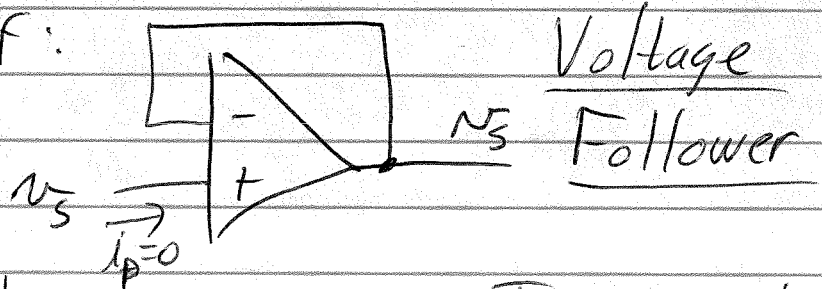
In important special case of the
NonInverting Configuration is for $R_1 = 0$:



$$v_o = \left(1 + \frac{R_1}{R_2}\right) v_s = (1) v_s = v_s$$

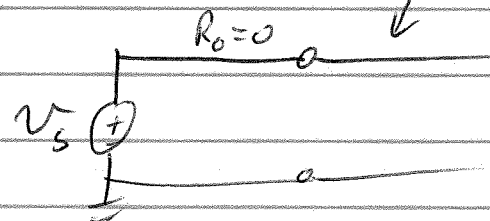
$$v_o = v_s \quad (\text{Voltage Follower})$$

We do not need R_2 to determine gain, so
leave it off:

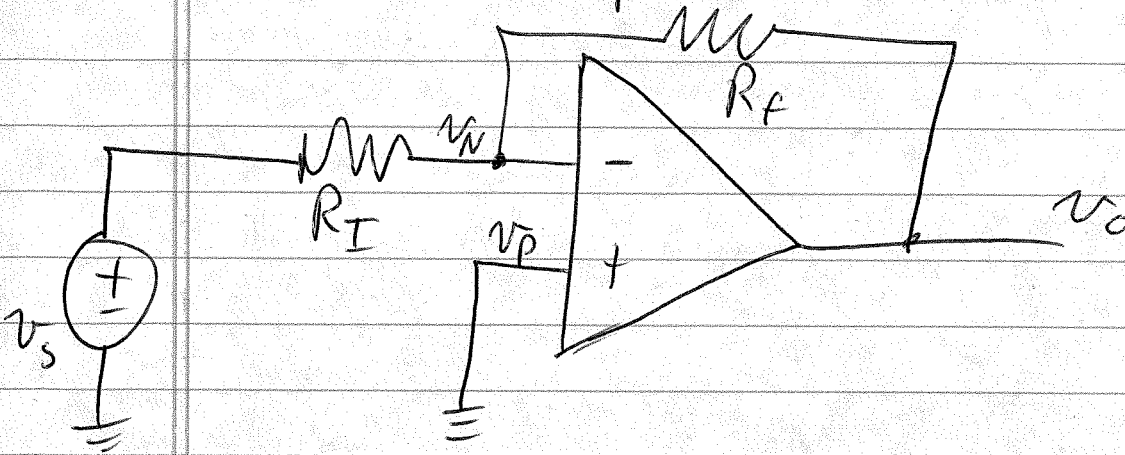


Takes a
voltage
with no
current
 $i_p = 0$

Turns it into
a voltage with
(possibly) huge
current.



Another example:



- 1.) Resistor between $v_o + v_N$, so GR 1 applies.
 $v_N = v_P$
 but $v_P = 0$, so $v_N = 0$.

- 2.) Apply KCL at Inverting Input:

$$\frac{v_N - v_s}{R_I} + \frac{v_N - v_o}{R_F} = 0$$

but $v_N = 0$, so $-\frac{v_s}{R_I} - \frac{v_o}{R_F} = 0$

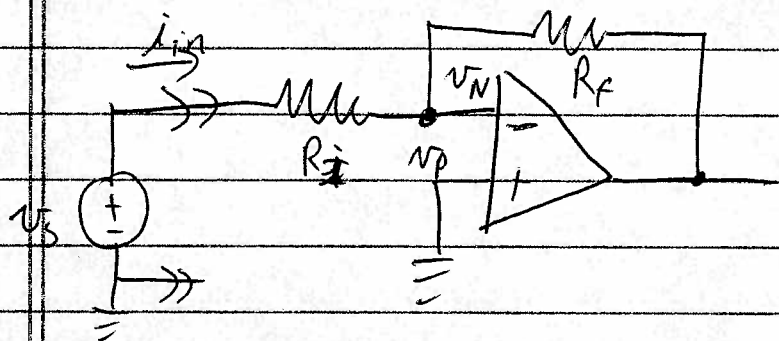
$$\frac{v_o}{R_F} = -\frac{v_s}{R_I}$$

$$v_o = -\frac{R_F}{R_I} v_s = G v_s$$

$$G = -\frac{R_F}{R_I}$$

Inverting
Amplifier

Input R?

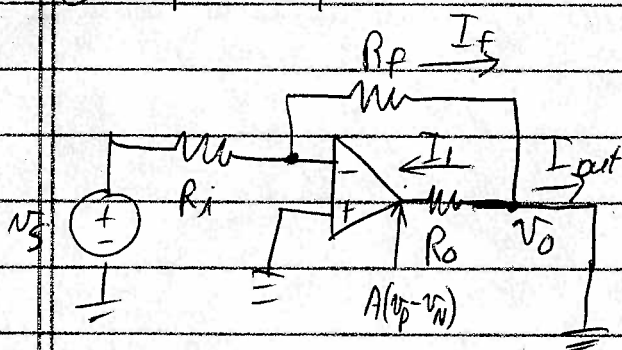


~~Output is same as before, R_s to op~~

$$i_{in} = \frac{v_s - v_N}{R_i} = \frac{v_s}{R_i}$$

$$\text{So } R_{in} = \frac{v_s}{i_{in}} = \frac{v_s}{v_s/R_i} = R_i$$

Output Equiv?



~~Dependent Src will be negative, "pulling" all the current from R_f in through R_o through the VCVS, to ground. v_N will not be zero, although the Op Amp tries.~~

$$\begin{aligned} \frac{v_N - v_s}{R_i} + \frac{v_N - v_o}{R_f} &= 0 \\ \frac{v_N}{R_i} + \frac{v_N}{R_f} &= \frac{v_s}{R_i} + \frac{v_o}{R_f} \\ v_N &= \frac{R_f v_s + R_i v_o}{R_i + R_f} \end{aligned}$$

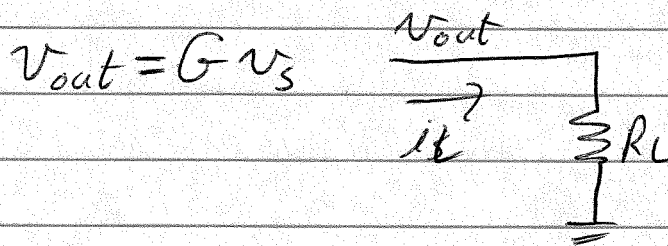
$$\begin{aligned} \frac{v_N - v_s}{R_i} + \frac{v_N - 0}{R_f} &= 0 \\ (R_i + R_f) v_N &= R_i v_s \\ v_N &= \frac{R_i}{R_i + R_f} v_s \end{aligned}$$

$$I_T = \frac{v_N}{R_f} = \frac{R_i}{R_i + R_f} \frac{v_s}{R_f} \text{ must be taken in by dependent Src.}$$

$$\begin{aligned} \frac{A(v_p - v_N)}{R_o} &= \frac{v_s}{R_i + R_f} \\ \frac{A v_N}{R_o} &= \frac{v_s}{R_i + R_f} \\ v_N &= \frac{R_o}{R_i + R_f} \frac{v_s}{A} \end{aligned}$$

Several contradictory things: $v_N = 0 + v_{out} = 0$ (165)
No current thru R_f .

Put on load + calculate ~~i_{out}~~ :



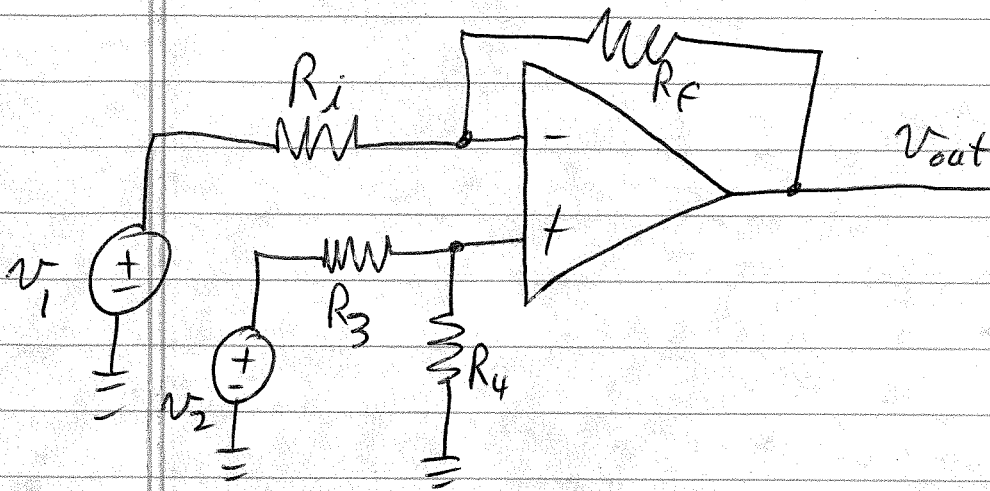
No way to
calculate i_{sc} .

$$i_L = \frac{v_{out}}{R_L}$$

Find i_{sc} : $\lim_{R_L \rightarrow 0} i_L = \infty = i_{sc}$

$$R_T = \frac{v_{oc}}{i_{sc}} = \frac{G v_s}{\infty} = 0$$

Let's analyze the most general case we can:



Could use ~~nodal analysis~~ my general technique:

- 1) Resistive Negative Feedback? ✓ Yes
 $v_N = v_P$

$$v_P \text{ by Voltage Division: } v_P = \frac{R_4}{R_3 + R_4} v_2 = v_N$$

- 2) KCL @ inverting input:

$$\frac{v_N - v_1}{R_i} + \frac{v_N - v_{out}}{R_f} = 0$$

$$\left(\frac{1}{R_i} + \frac{1}{R_f}\right) v_N - \frac{1}{R_i} v_1 - \frac{1}{R_f} v_{out} = 0$$

$$v_{out} = \frac{R_f + R_i}{R_i} v_N - \frac{R_f}{R_i} v_1$$

$$v_{out} = \left(\frac{R_f + R_i}{R_i}\right) \left(\frac{R_4}{R_3 + R_4}\right) v_2 - \frac{R_f}{R_i} v_1 \quad \left(\text{Differential Amp}\right)$$

Special Case: Let $R_3 = R_i$, $R_4 = R_F$,

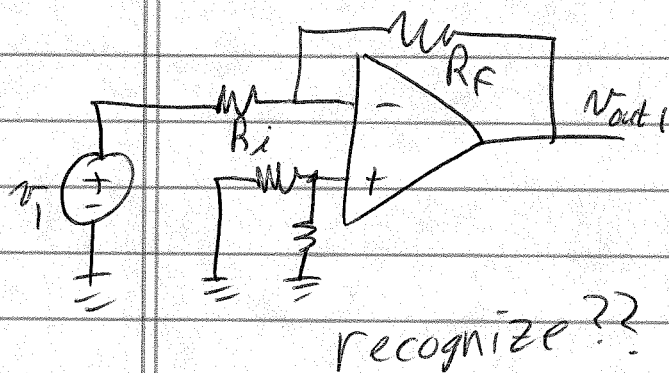
$$\text{then } v_{out} = \left(\frac{R_F + R_i}{R_i} \right) \left(\frac{R_F}{R_F + R_i} \right) v_2 - \frac{R_F}{R_i} v_1$$

$$v_{out} = \frac{R_F}{R_i} (v_2 - v_1) \quad \left(\text{called a True Differential Configuration} \right)$$

Go back to original ckt + think "2 Indep. Sres."

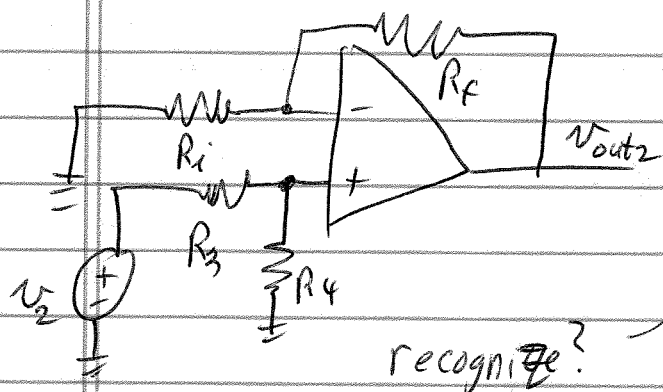
Superposition & ϕ

Turn off 2:



$$v_{out1} = - \frac{R_F}{R_i} v_1$$

Turn off 1:



$$v_{out2} = \left(1 + \frac{R_F}{R_i} \right) v_p$$

Voltage Div. $v_p = \frac{R_4}{R_3 + R_4} v_2$

$$\text{so } v_{out2} = \left(1 + \frac{R_F}{R_i} \right) \left(\frac{R_4}{R_3 + R_4} \right) v_2$$

