

Collector Field and Energy Demands

Learning outcomes

- Understand the main parameters for characterizing energy demands and their influence on the collector field performance/design
- Understand the influence of different variables (e.g. orientation, tilt mass flow,...) on the collector field performance/outcome
- Understand the main differences of different flow regimes in the collector field
- Get to know basic control strategies for the solar loop in solar thermal systems
- Understand main hydraulic “tools” promoting correct system behaviour

Outline

- **Energy demands: characterization**
- **Performance of collector field:**
 - Incident Radiation
 - Collector temperature
 - Operation strategies: mass flow
 - Control strategies
 - Pressure losses
 - Stagnation behaviour

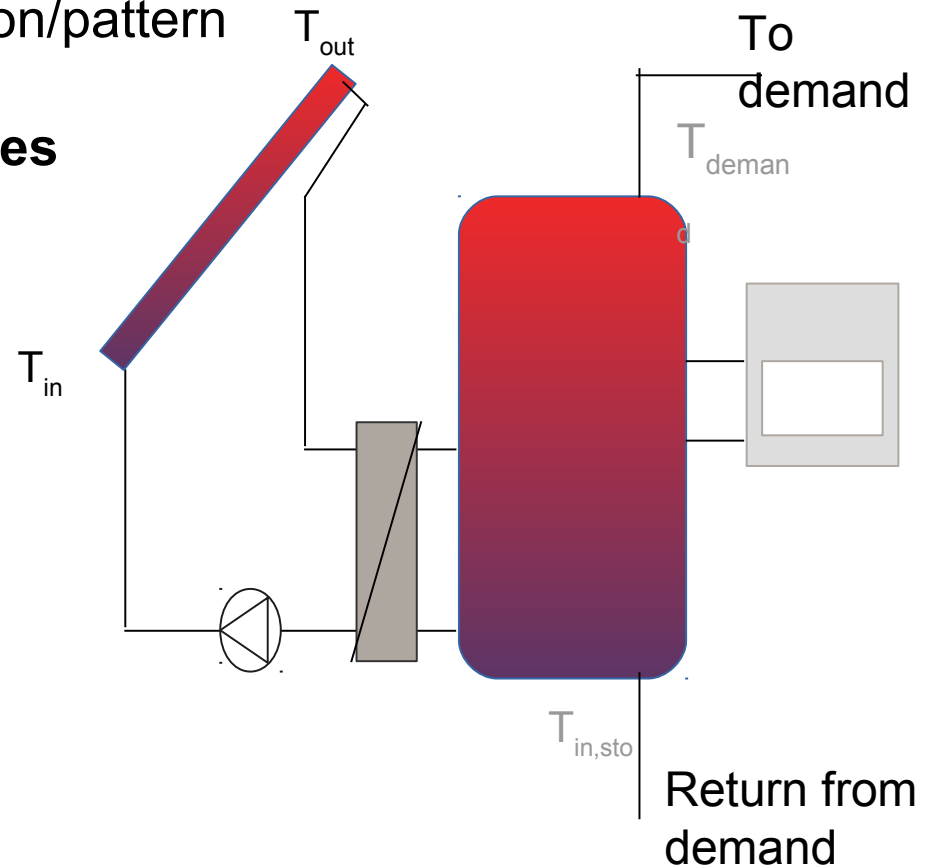
Characterizing energy demands

Example: DHW + SH demands

- **Seasonal (and daily!) variation/pattern**

- **Supply (desired) temperatures**
(T_{demand})

- **Return temperatures**
(from demand, $T_{\text{in,sto}}$)



Characterizing energy demands

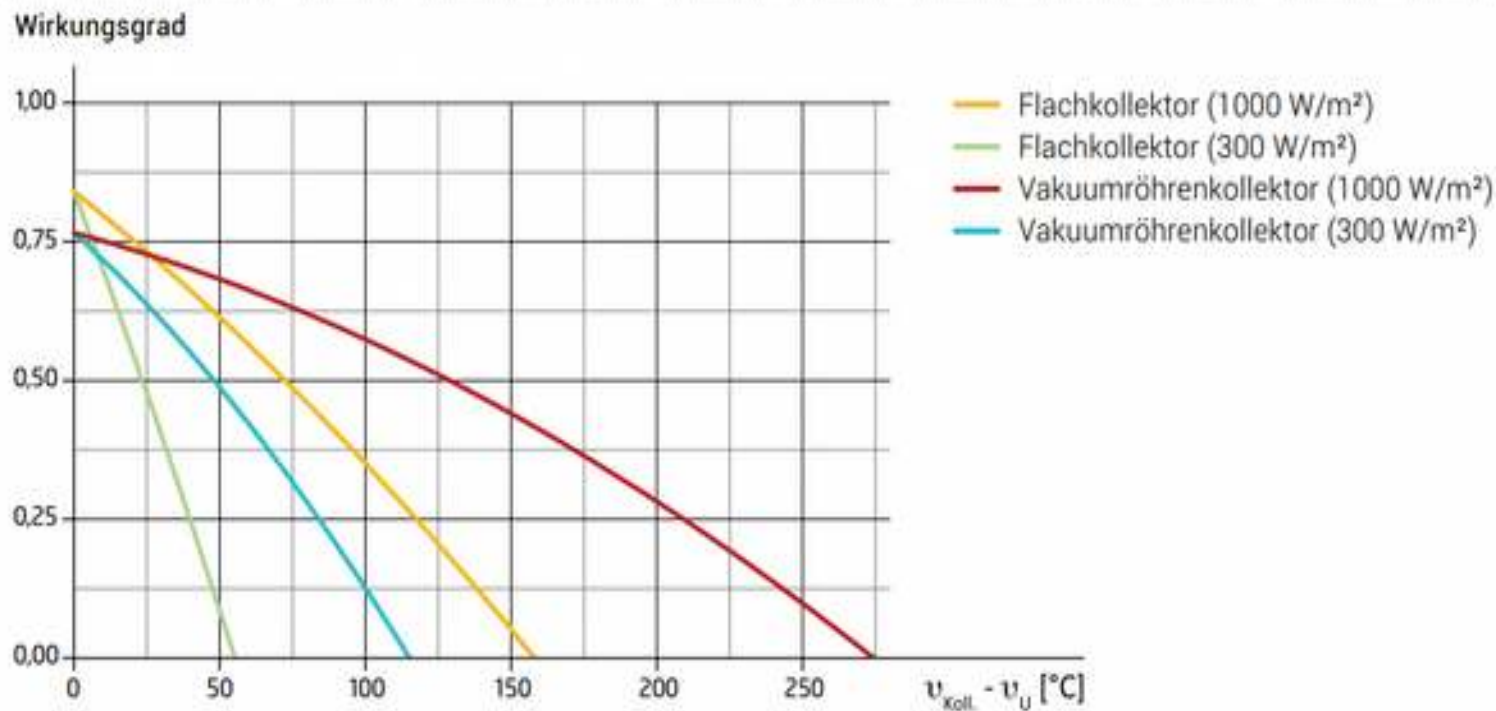
Example: DHW + SH demands

Space heating (SH)	Domestic hot water (DHW)
Large seasonal variation	All year round constant, small seasonal variation
Continuous daily profile	Daily profile with short high-power peaks
Low temperature applications (30-50°C) depending on emission system	High delivery temperature (45-60°C)
High return temperatures (25-35°C)	Low return temperatures (4-20°C)

Outline

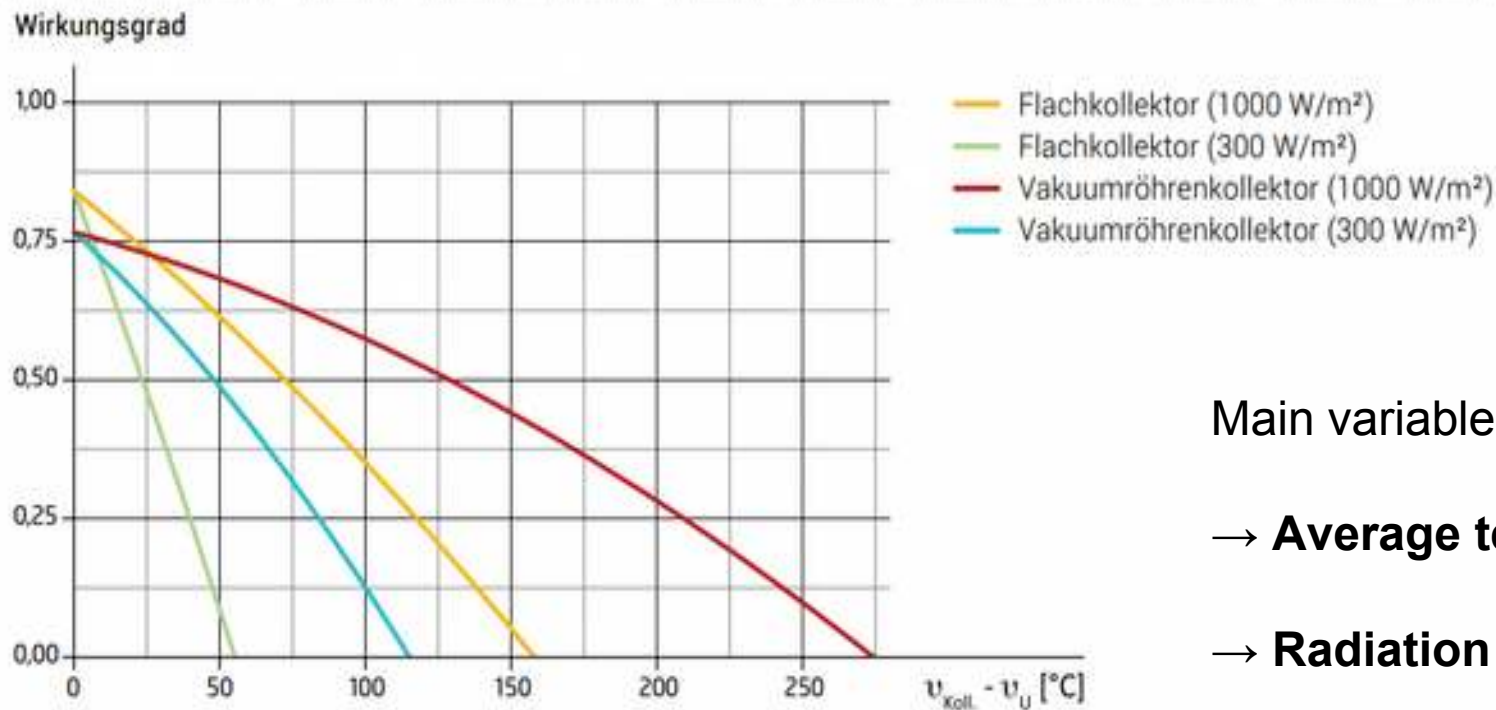
- **Energy demands: characterization**
- **Performance of collector field:**
 - Incident Radiation
 - Collector temperature
 - Operation strategies: mass flow
 - Control strategies
 - Pressure losses
 - Stagnation behaviour

Collector loop Performance



Source: Corradini et al., 2014

Collector loop Performance



Source: Corradini et al., 2014

Main variables:

→ **Average temperature**

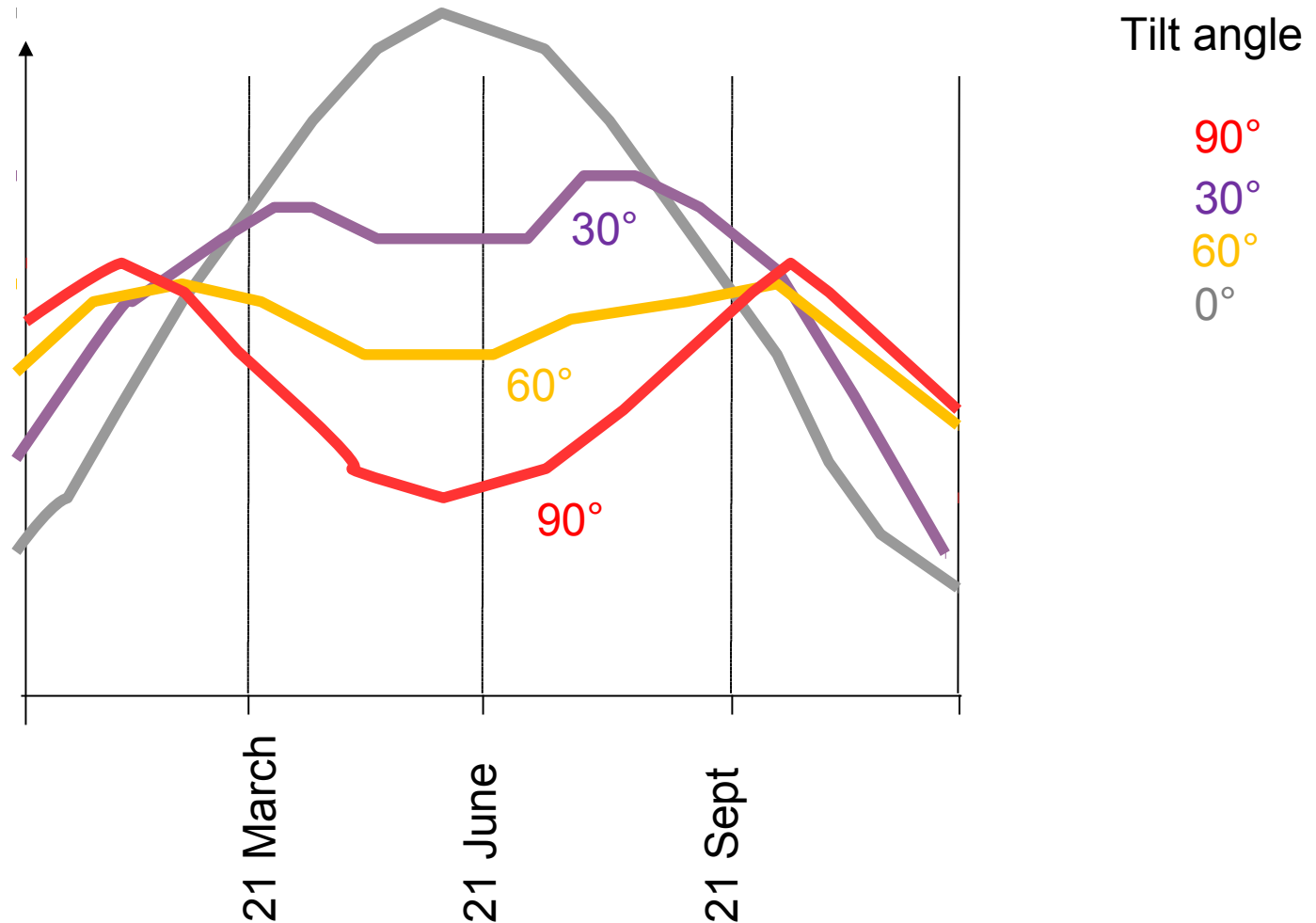
→ **Radiation**

→ **Ambient temperature**

Incident radiation

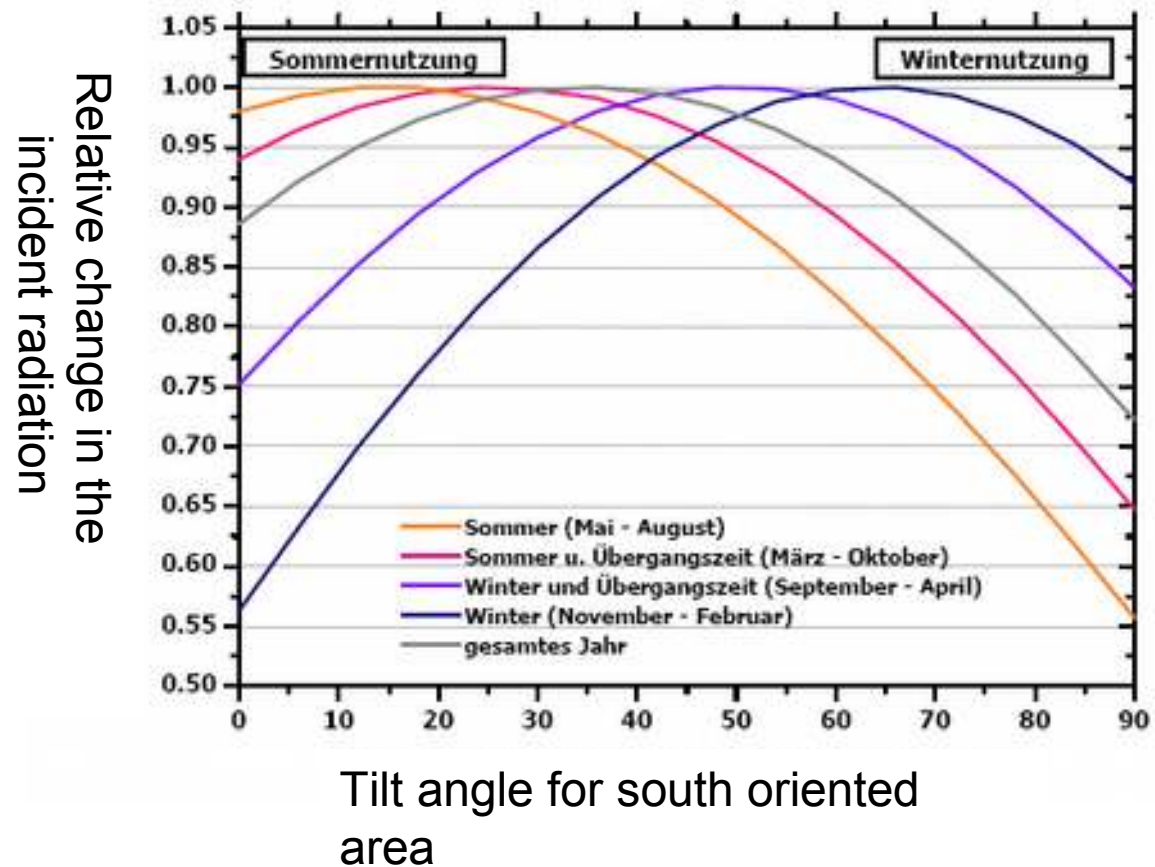
Tilt of the collector field

Incident
radiation
tilted plane



Incident radiation

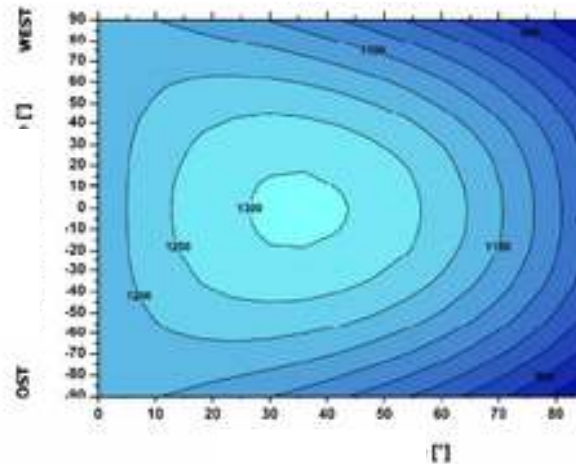
Tilt of the collector field



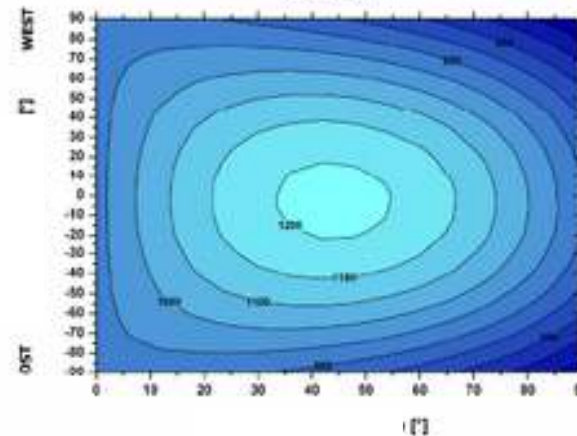
Incident radiation

Orientation and tilt of the collector field

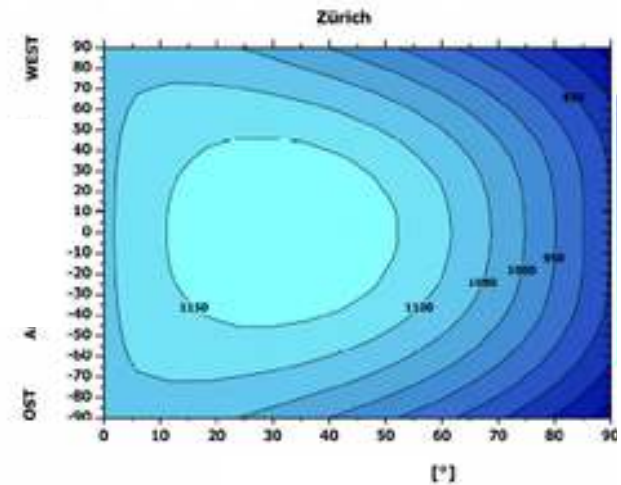
Solar resource
[kWhm⁻²a⁻¹]



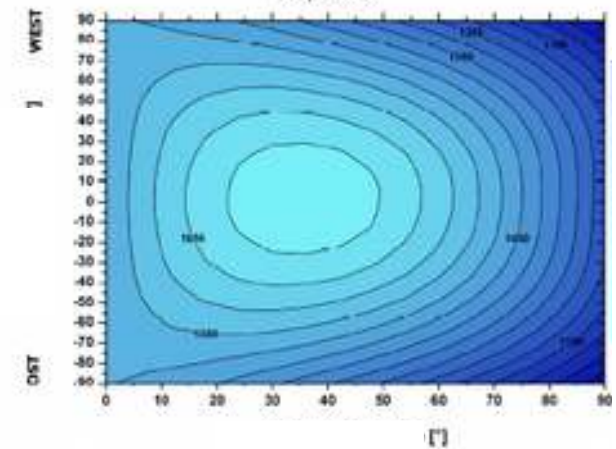
a Graz



c Stockholm



b Zürich



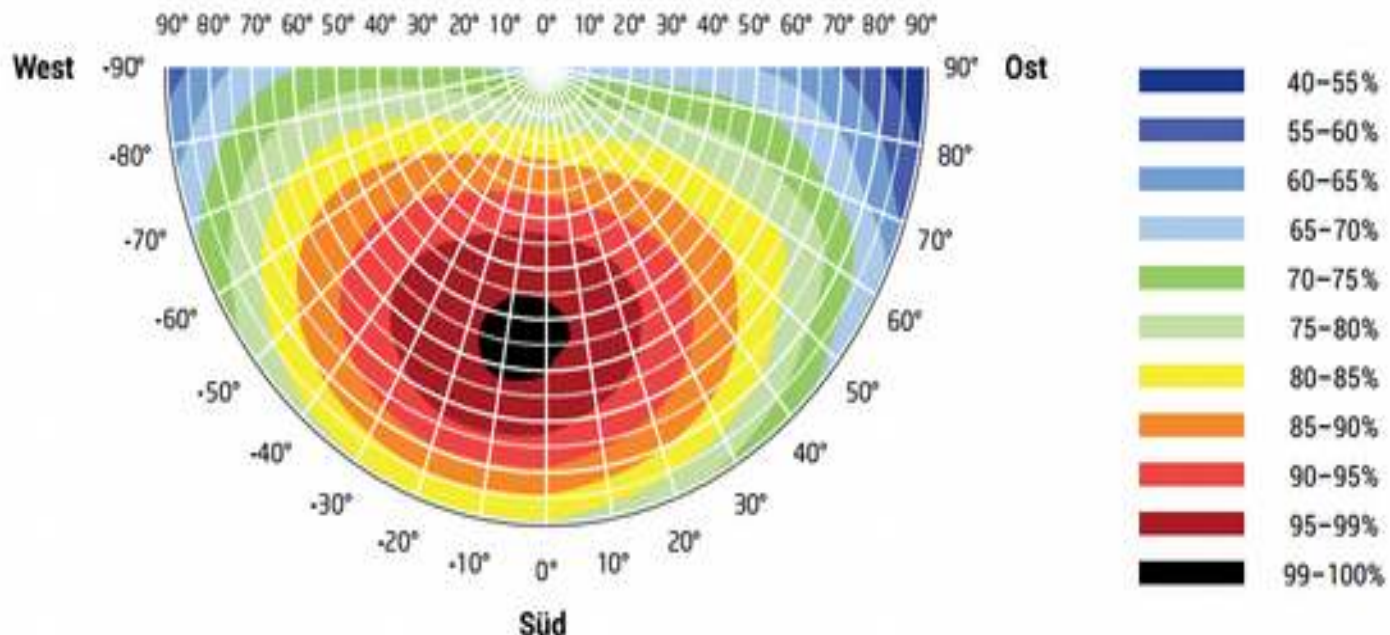
d Carpentras

Incident radiation

Orientation and tilt of the collector field

Maximizing collector energy yield: **demand specific!!**

Example: Combi-system (DHW+SH) in Würzburg (GER)



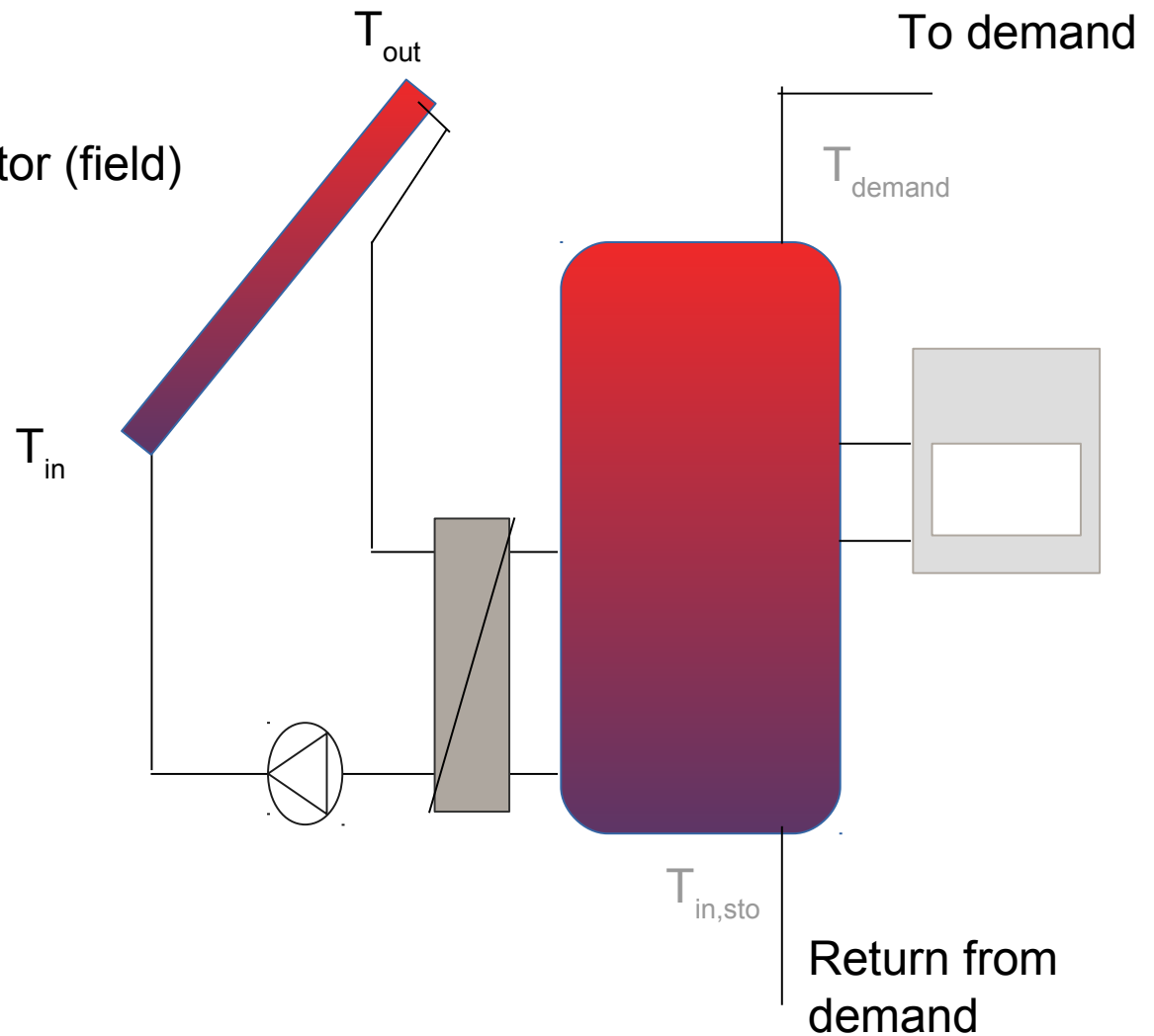
Outline

- **Energy demands: characterization**
- **Performance of collector field:**
 - Incident Radiation
 - Collector temperature
 - Operation strategies: mass flow
 - Control strategies
 - Pressure losses
 - Stagnation behaviour

Operation strategies

Collector loop

Average temperature collector (field)
= f (inlet, outlet, mass flow)



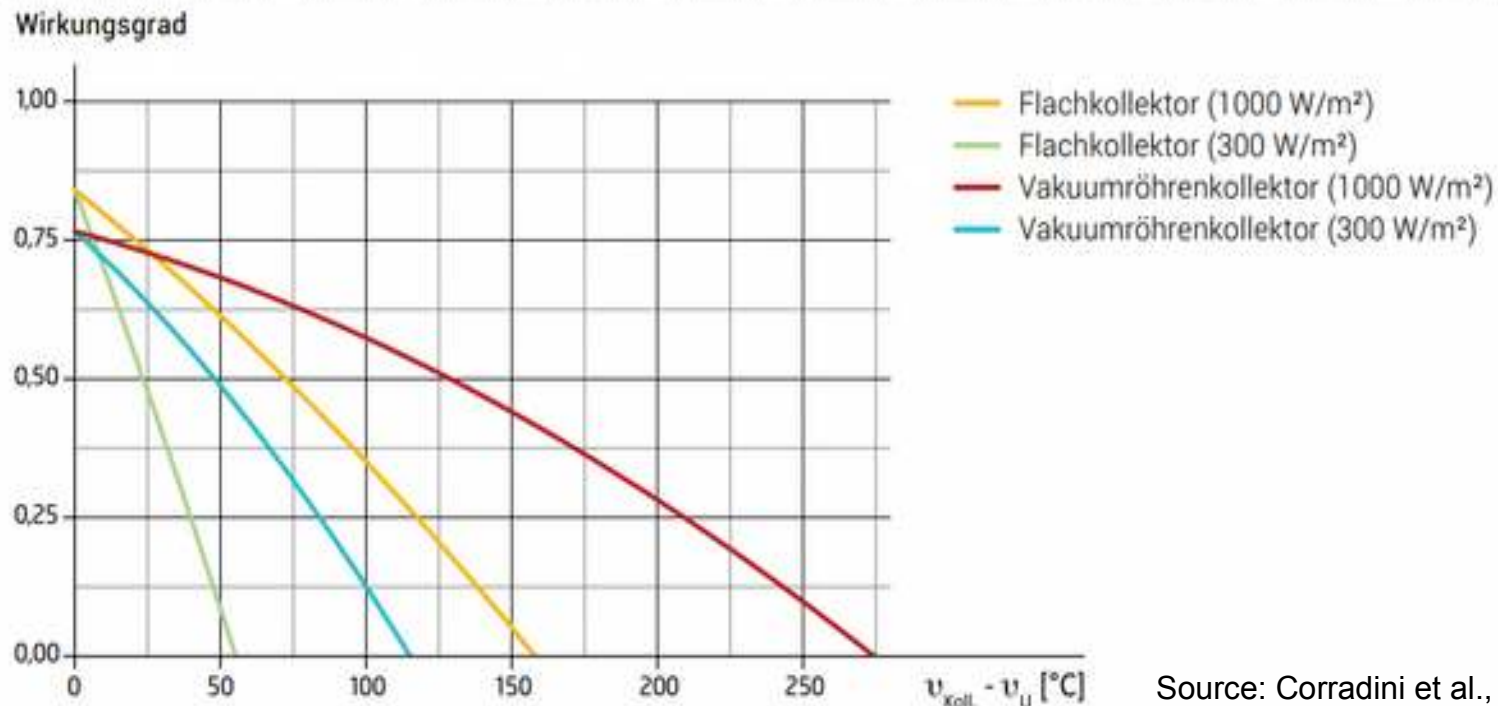
Operation strategies

Collector loop

High flow systems: $30 - 70 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 8-15 \text{ K}$

Low flow systems: $8 - 18 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 40-55 \text{ K}$

\dot{V}_{coll}



Source: Corradini et al., 2014

Operation strategies

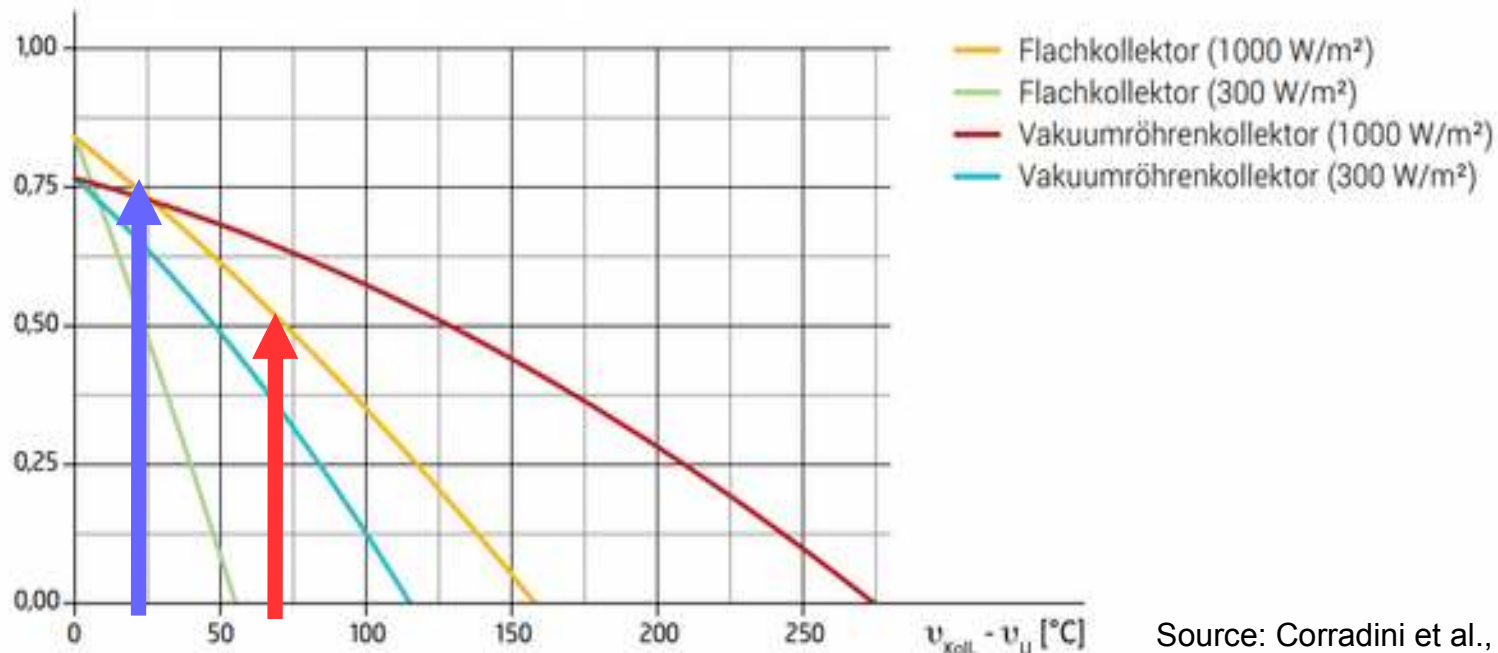
Collector loop

$$\dot{V}_{\text{coll}} = \frac{P_{\text{coll}}}{\rho \cdot c_p \cdot \Delta T_{\text{coll}}}$$

High flow systems: $30 - 70 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 8-15 \text{ K}$

Low flow systems: $8 - 18 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 40-55 \text{ K}$

Wirkungsgrad



Source: Corradini et al., 2014

Operation strategies

Collector loop

\dot{V}_{coll} p_{coll}

High flow systems: 30 -70 lh⁻¹m⁻²; $\Delta T_{coll} \approx 8-15$ K

Typically used for DHW production in small systems (single family houses)

High efficiency of collector field (low ΔT_{coll})

Slow warming up of storage (pre-heating)

Low flow systems: 8 -18 lh⁻¹m⁻², $\Delta T_{coll} \approx 40-55$ K

Worst collector efficiency (high ΔT_{coll})

End-use temperature given by solar loop (not pre-heating) -> less auxiliary energy required

Operation strategies

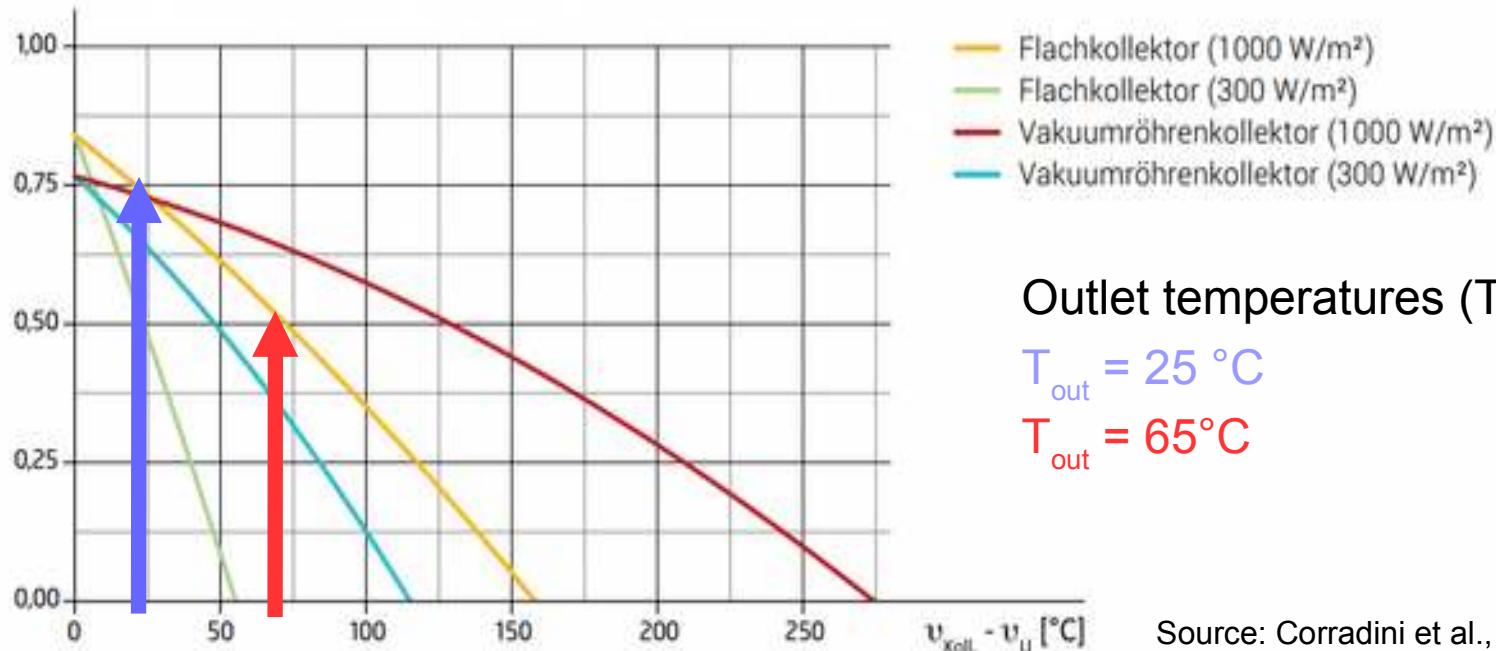
Collector loop

\dot{V}_{coll} p_{flui}

High flow systems: $30 - 70 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 8-15 \text{ K}$

Low flow systems: $8 - 18 \text{ lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 40-55 \text{ K}$

Wirkungsgrad



Outlet temperatures ($T_{\text{in}} = 15^\circ\text{C}$):

$T_{\text{out}} = 25^\circ\text{C}$

$T_{\text{out}} = 65^\circ\text{C}$

Operation strategies

Collector loop

High flow systems: 30 -70 $\text{lh}^{-1}\text{m}^{-2}$; $\Delta T_{\text{coll}} \approx 8-15 \text{ K}$

Typically used for DHW production in small systems (single family houses)

High efficiency of collector field (low ΔT_{coll})

Slow warming up of storage (pre-heating)

Low flow systems: 8 -18 $\text{lh}^{-1}\text{m}^{-2}$, $\Delta T_{\text{coll}} \approx 40-55 \text{ K}$

Worst collector efficiency (high ΔT_{coll})

End-use temperature given by solar loop (not pre-heating) -> less auxiliary energy required

Matched flow systems: variable 8-70 $\text{lh}^{-1}\text{m}^{-2}$, $\Delta T_{\text{coll}} \approx 8 - 55 \text{ K}$

constant $T_{\text{out, coll}}$ as a function of G , T_{storage} , Q_{demand}

High/Low flow operation

Operation strategies

Collector loop

Matched flow systems: variable $8\text{-}70 \text{ lh}^{-1}\text{m}^{-2}$, $\Delta T_{\text{coll}} \approx 8 - 55 \text{ K}$

constant T_{outl} as a function of G , T_{storage} , Q_{demand}

High/Low flow operation

$$\Delta T_{\text{coll-sto}} = T_{\text{out}} - T_{\text{sto}}$$

Pump turned on:

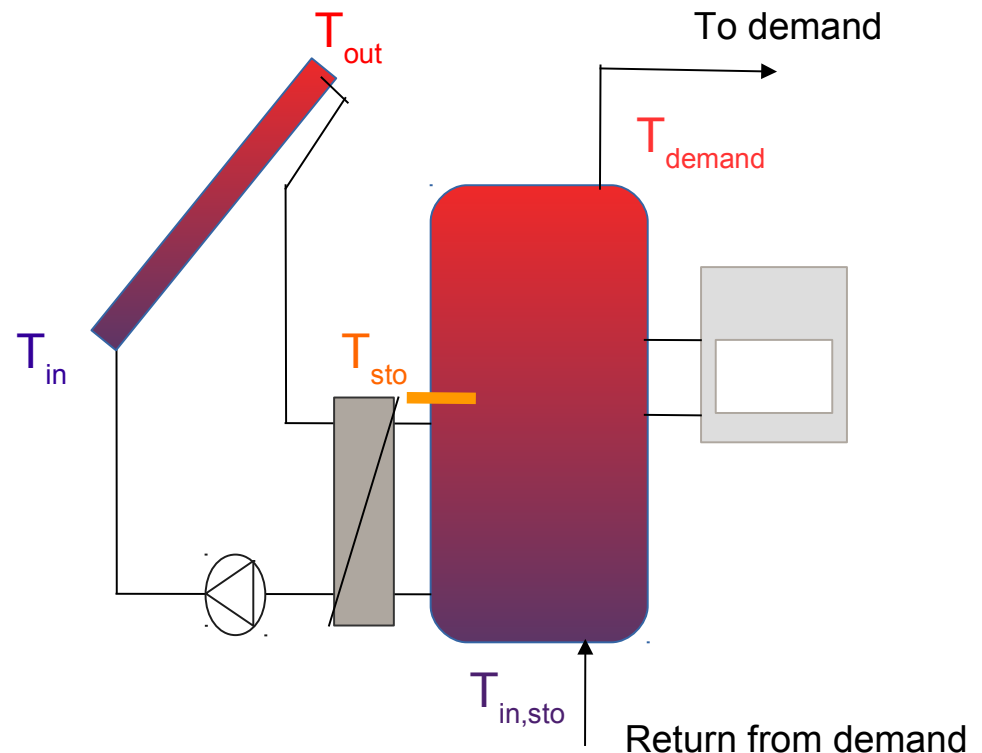
$$\Delta T_{\text{coll-sto}} > \Delta T_{\text{ON}}$$

$$\Delta T_{\text{ON}} = 10 \text{ K}$$

Pump turned off:

$$\Delta T_{\text{coll-sto}} < \Delta T_{\text{OFF}}$$

$$\Delta T_{\text{OFF}} = 3 \text{ K}$$

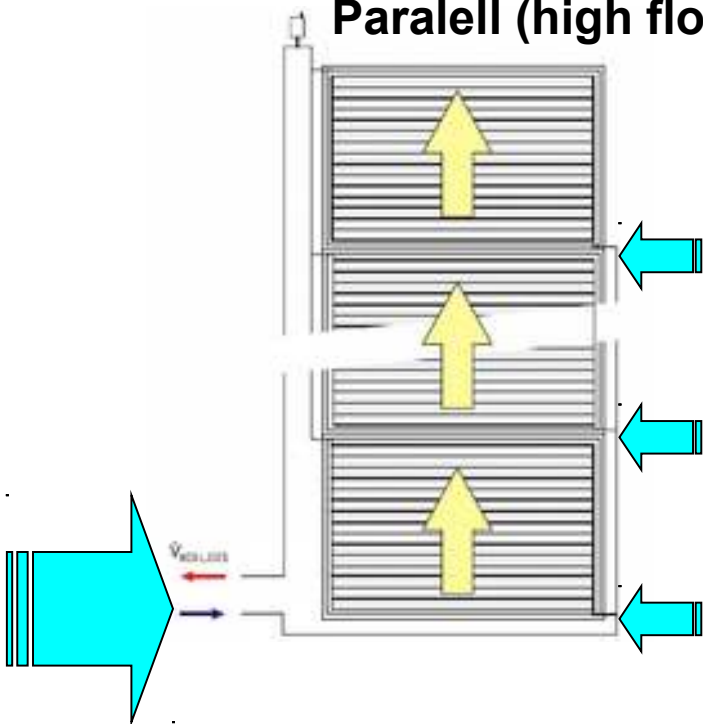


Operation strategies

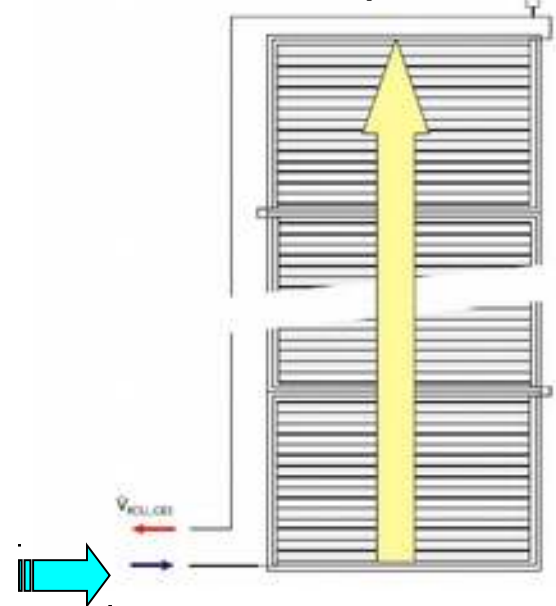
DESIGN: depending on required ΔT_{demand} :

- DHW (+SH): low flow, $\Delta T_{\text{demand}} > 30\text{K}$
- Only SH: high flow, $\Delta T_{\text{demand}} < 10\text{K}$

Paralell (high flow)



Series (low flow)

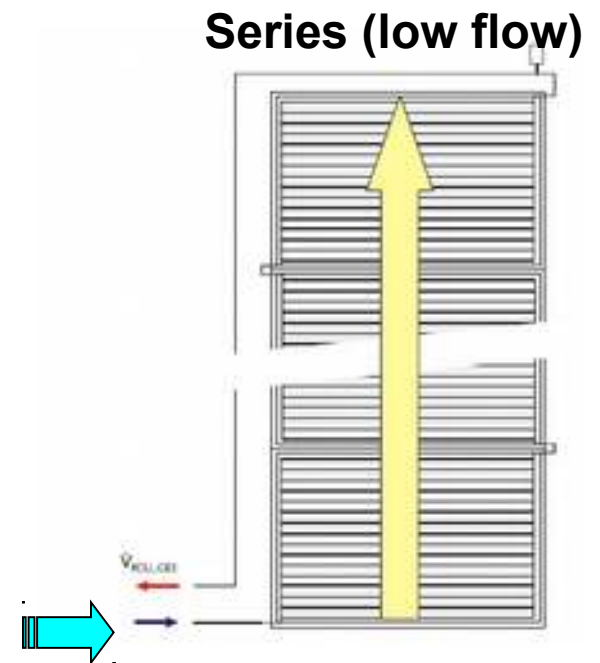
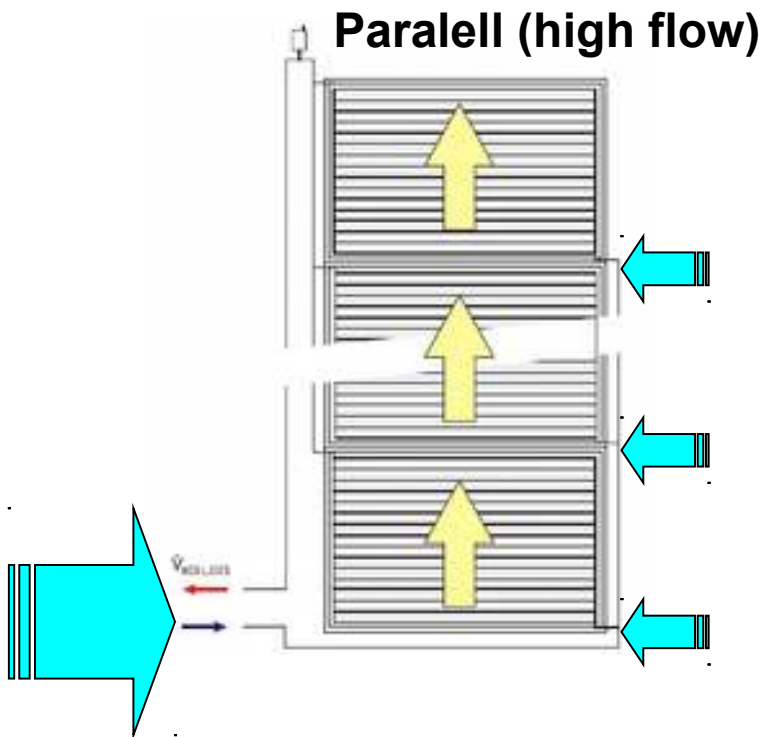


Operation strategies

Example: $A_{\text{coll}} = 6 \text{ m}^2$; $G = 800 \text{ W/m}^2$;

- Series: $m = 10 \text{ l/hm}^2$; $\eta_{\text{coll}} = 0.6$

- Parallel: $m = 30 \text{ l/hm}^2$; $\eta_{\text{coll}} = 0.75$

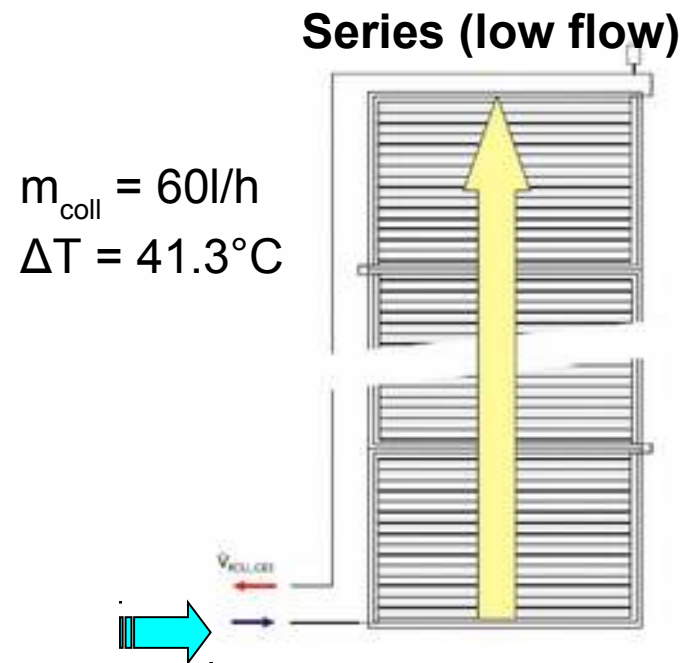
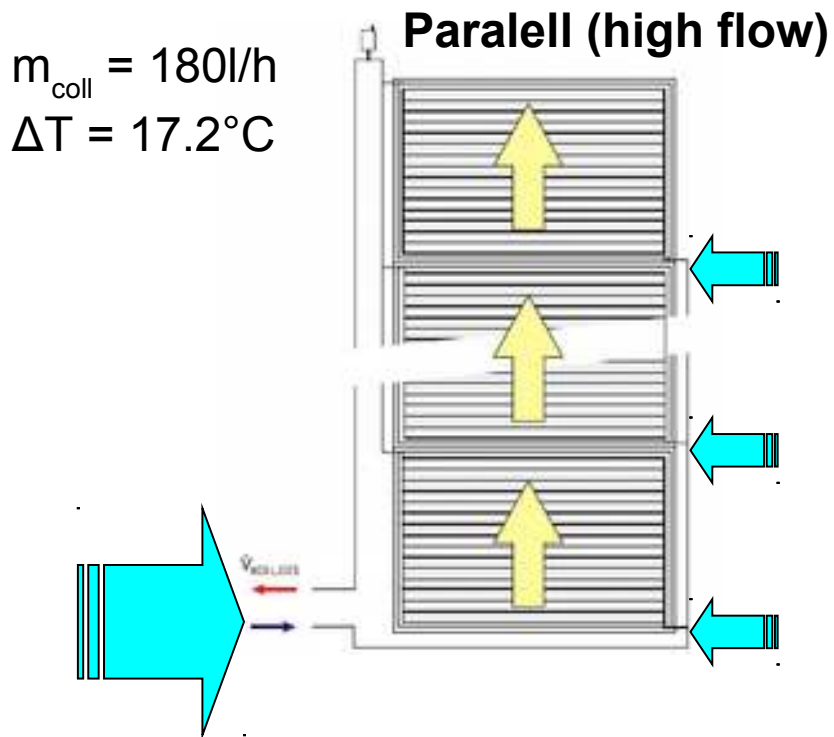


Operation strategies

Example: $A_{\text{coll}} = 6 \text{ m}^2$; $G = 800 \text{ W/m}^2$;

- Series: $m = 10 \text{ l/hm}^2$; $\eta_{\text{coll}} = 0.6$

- Parallel: $m = 30 \text{ l/hm}^2$; $\eta_{\text{coll}} = 0.75$



Outline

- **Energy demands: characterization**
- **Performance of collector field:**
 - Incident Radiation
 - Collector temperature
 - Operation strategies: mass flow
 - Control strategies
 - Pressure losses
 - Stagnation behaviour

Operation strategies

Pressure losses: hydraulic balance

$$\Delta p = R_{\text{pipes}} \cdot \frac{\lambda \rho V^2}{2 A}$$

R_{pipe} , hydraulic resistance [Pa/m]

λ , pipe friction factor (function of the flow type – turbulent, laminar)

V , volumetric flow rate [m³/s]

D , pipe diameter [m]

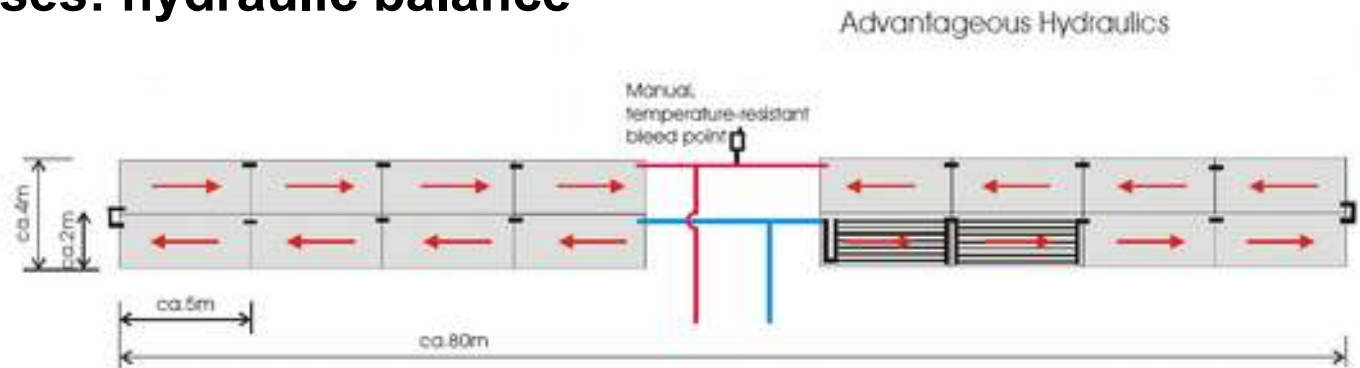
A , pipe cross section [m²],

Collector area [m ²]	Max pressure losses [mbar]
< 50	300
<200	600
500	800

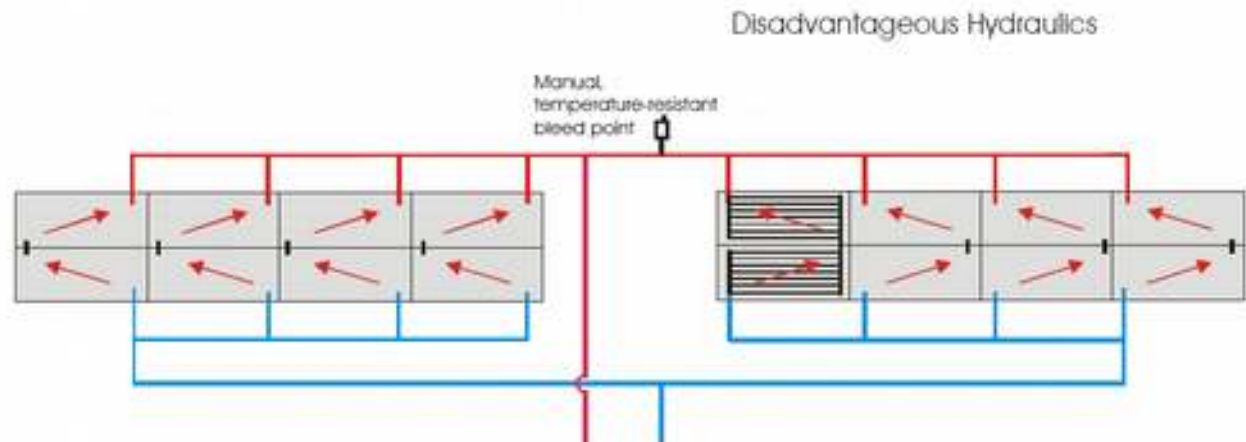
Operation strategies

Pressure losses: hydraulic balance

Series (low flow)



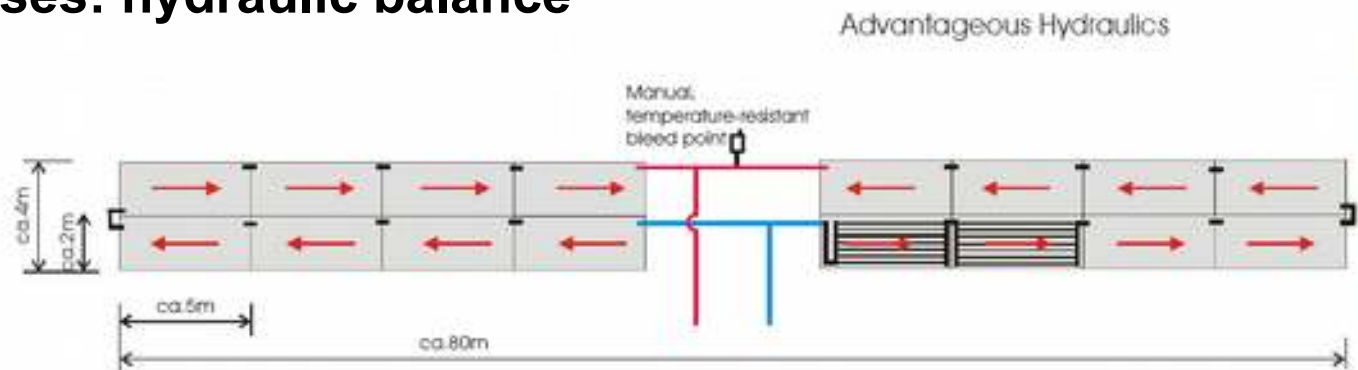
Parallel (high flow)



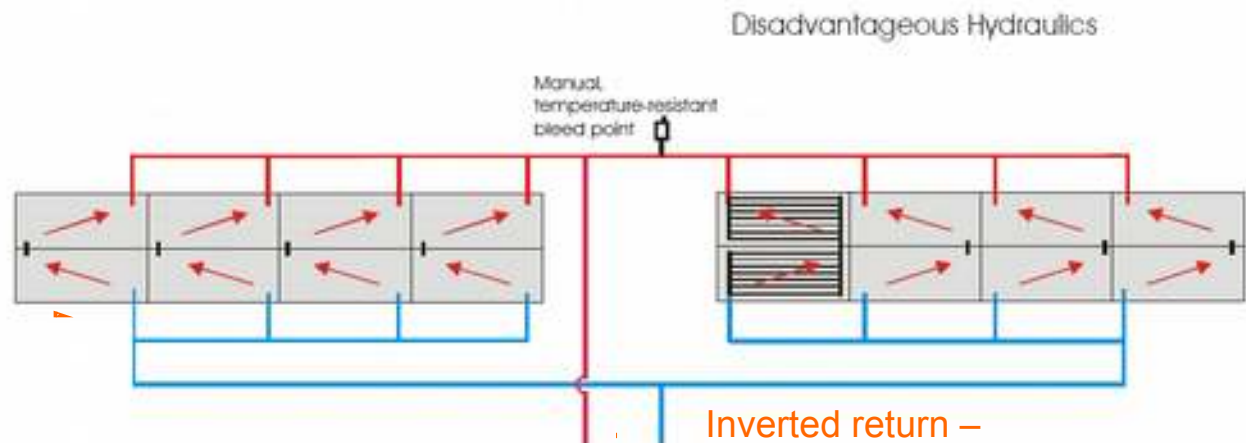
Operation strategies

Pressure losses: hydraulic balance

Series (low flow)



Parallel (high flow)



Inverted return –
compensate Δp in all
parallel connections!

Outline

- **Energy demands: characterization**
- **Performance of collector field:**
 - Incident Radiation
 - Collector temperature
 - Operation strategies: mass flow
 - Control strategies
 - Pressure losses
 - Stagnation behaviour

Stagnation behaviour

Critical system temperatures

- Maximum fluid temperature allowable for circulation pump: 110°C
- Max. hot water temperature (storage): 95°C
- Max. temperature for propylene glycol/water mixture (degradation): 105-140°C

Stagnation behaviour

Low flow systems

Advantages

- Increased solar fractions (energy savings), 10-25%
- Reduced lime deposits in storage
- Cost reduction:
 - Smaller pipes
 - Smaller pumps
 - Reduced solar collector fluid volume

Disadvantages

- Too high temperatures
- Thermosyphoning during summer nights in collector field

Stagnation behaviour

Low flow systems

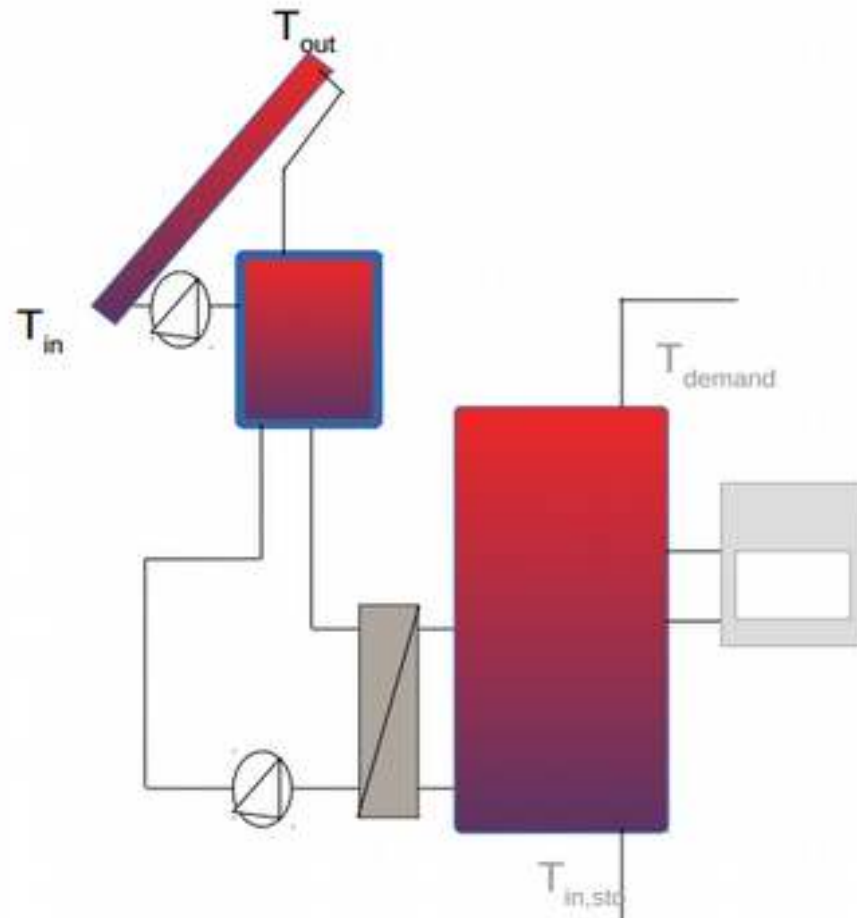
Possible Solutions to avoid overheating

- Increase collector flow in hot (summer) periods
- Collector flow at nighttime (cooling down) in hot periods
- Drain back systems
- Stop pump in hot periods -> Evaporation of solar collector fluid and expanded volume kept in expansion vessel (Stagnation).

Stagnation behaviour

Drain back systems

- No pressurized circuit: no safety valves, expansion vessel....
- Water as heat transfer medium
- Additional **volume** for drain back is needed
- Additional control system

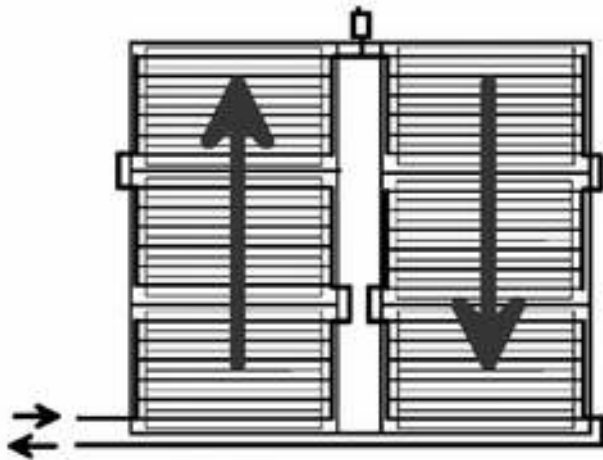


Stagnation behaviour

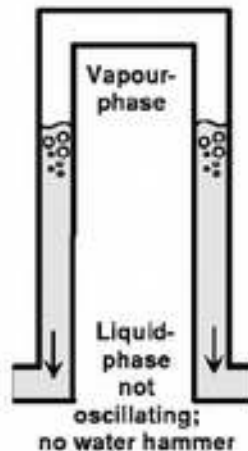
At least one manifold at the bottom to allow liquid (not yet vaporized)
be evacuated!

→ Otherwise more liquid needs to be evaporated (500 times volume increase)

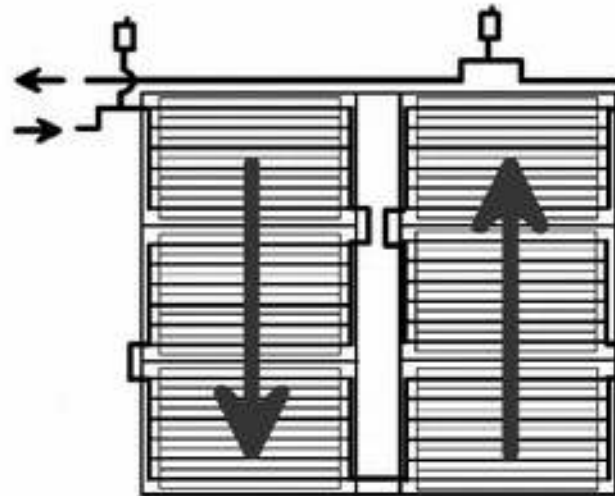
Normal operation



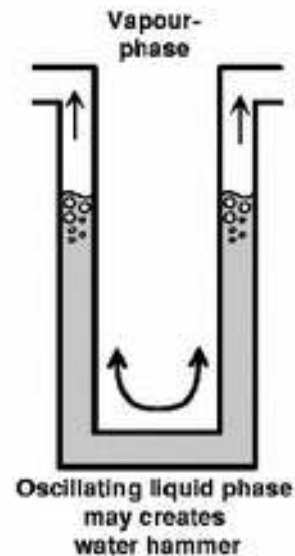
Start of stagnation



Normal operation



Start of stagnation



References

- Weselak, Schabbach. 2009. Regenerative Energietechnik. Springer Ed.
- AEE. Fink and Riva, 2004. Solar-supported heating networks in multi-storey residential buildings. Arbeitsgemeinschaft ERNEUERBARE ENERGIE GMBH, Austria
- Heimrath. 2004. Simulation, Optimierung und Vergleich solar-thermischer Anlagen zur Raumwärmeversorgung für Mehr-familienhäuser. PhD Thesis. TU Graz, Austria.
- Corradini et al. 2014. Solarthermie: Technik, Potenziale, Wirtschaftlichkeit und Ökobilanz für solarthermische Systeme in Einfamilienhäusern. Wüstenroth Stiftung (Ed.). 2014.