

Heat pumps I – Thermodynamic processes

Dr. Herena Torio



Agenda

- Heat pump overview
- Re-visiting thermodynamics
- Components and cycles



The heat pump cycle

Principle

Refrigerant - Pressure dependent phase change compressor points 3 evaporator condenser **Tcold** Thot Tevap **Tcond** Tc Th expansion valve **High pressure** Low pressure ca.10 bar ca. 2 bar Function of temperature! Function of temperature!





The heat pump cycle

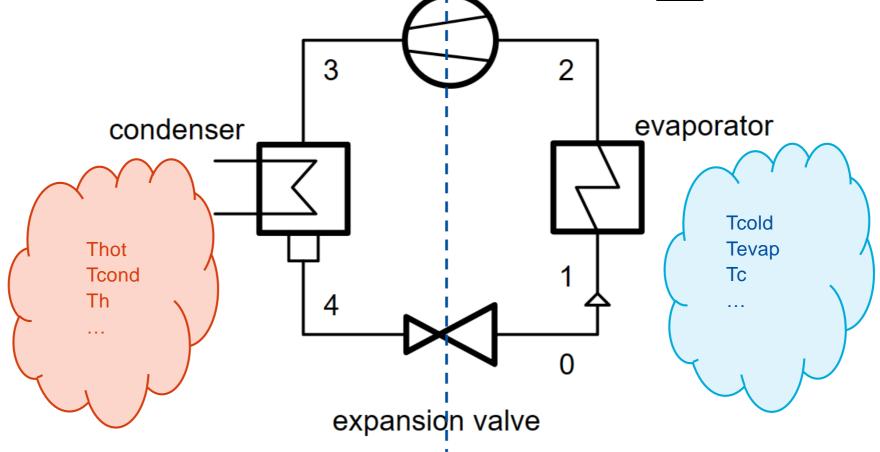
Principle

Refrigerant - Pressure dependent phase change points



Source: Grassi, 2018

Indoor unit



compressor

High pressure

ca.10 bar Function of temperature!

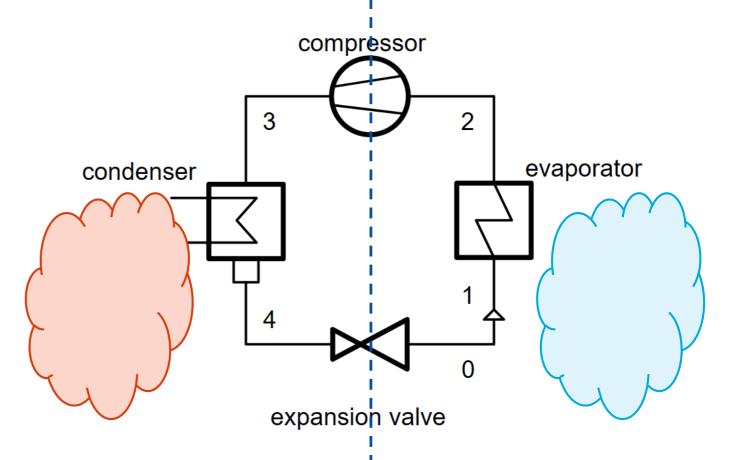
Low pressure

ca. 2 bar Function of temperature!

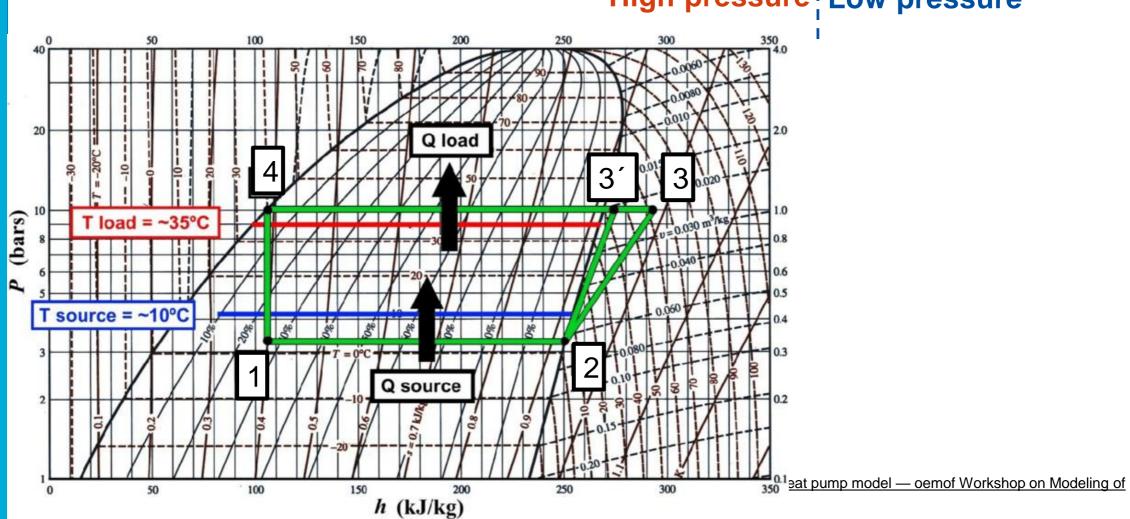




The heat pump cycle



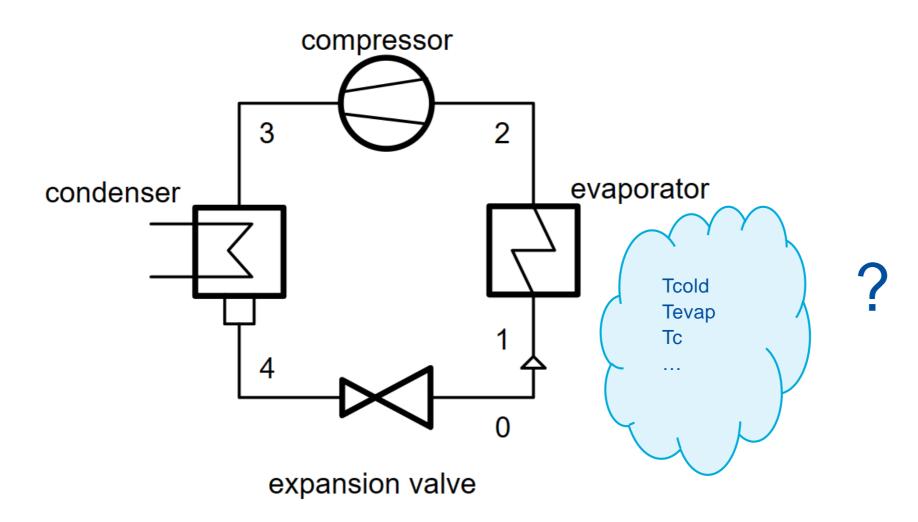
High pressure Low pressure





The heat pump cycle

Typical sources and sinks



High pressure

ca.10 bar

Function of temperature!

Low pressure

ca. 2 bar

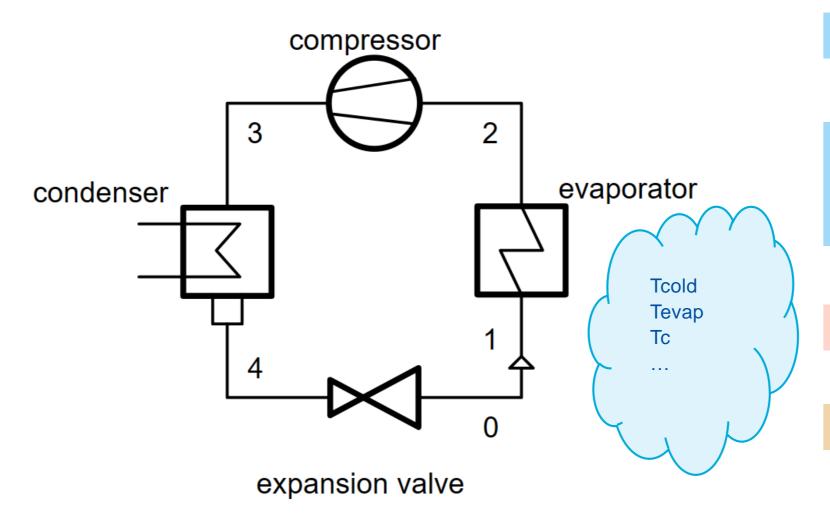
Function of temperature!





The heat pump cycle

Typical sources and sinks



Ambient air

Groundwater (or any other water source)

Waste heat

Solar thermal! ©

High pressure

ca.10 bar

Function of temperature!

Low pressure

ca. 2 bar

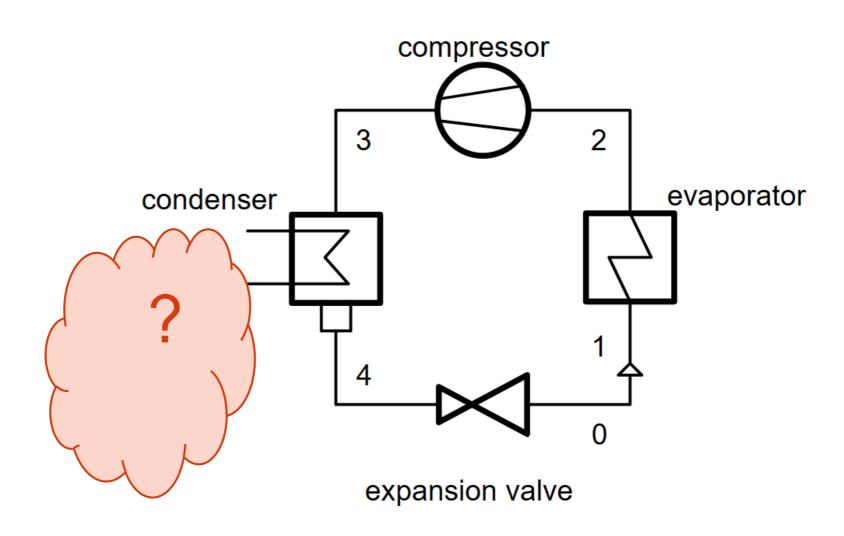
Function of temperature!





The heat pump cycle

Typical sources and sinks



High pressure

Low pressure

ca.10 bar

ca. 2 bar

Function of temperature!

Function of temperature!





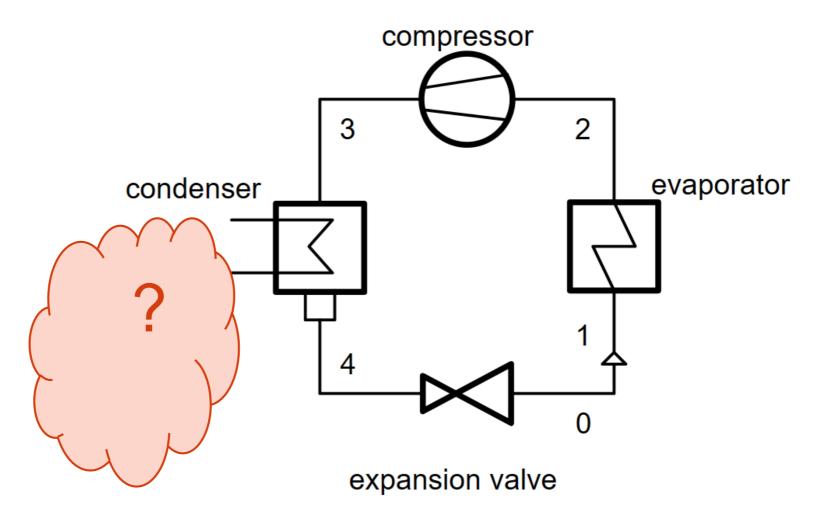
The heat pump cycle

Typical sources and sinks

Space heating

DHW

Industrial heat



High pressure

ca.10 bar ca. 2 bar

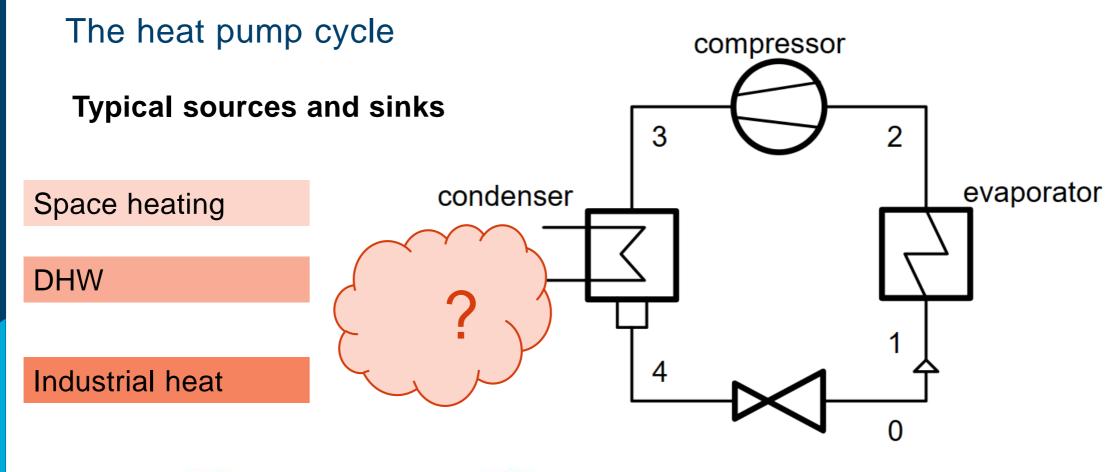
Function of temperature!

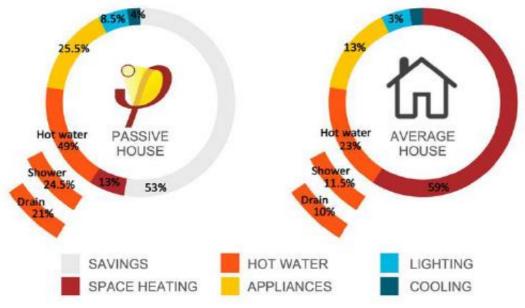
Function of temperature!



Low pressure







expansion valve

Small Excurs:

DHW demands on the rise, in share and importance

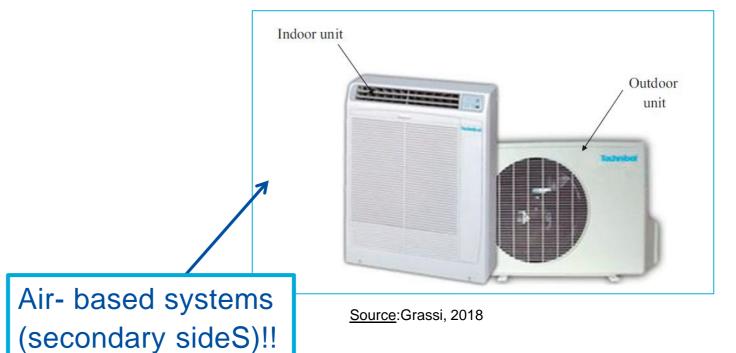
Source: Hervas, 2020





The heat pump cycle

Typical sources and sinks



Space heating

Condenser

Physical Physical Revaporator

Condenser

Physical Revaporator

Condenser

Physical Revaporator

Physical Revaporator

Condenser

Physical Revaporator

Condenser

Physical Revaporator

Condenser

Physical Revaporator

Condenser

compressor

expansion valve

Ambient air

Source: Grassi, 2018

Groundwater (or any other water source)

Waste heat

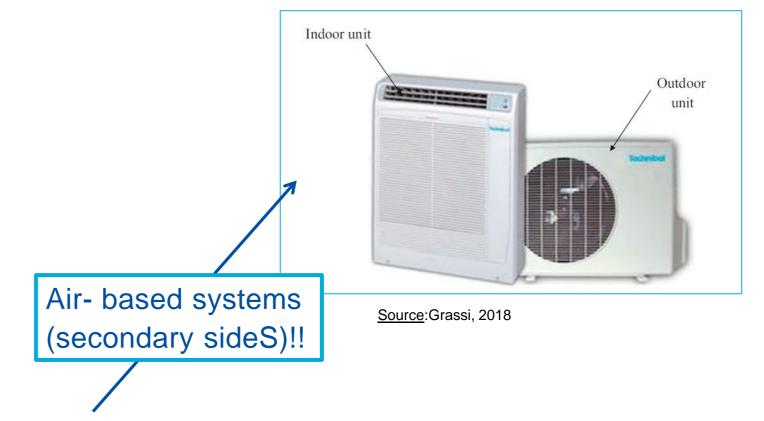
Solar thermal! ©

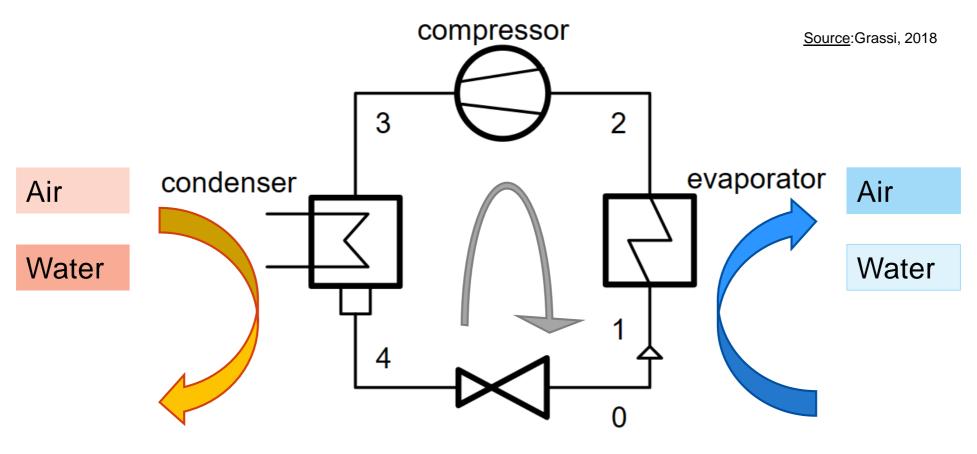




The heat pump cycle

Typical sources and sinks

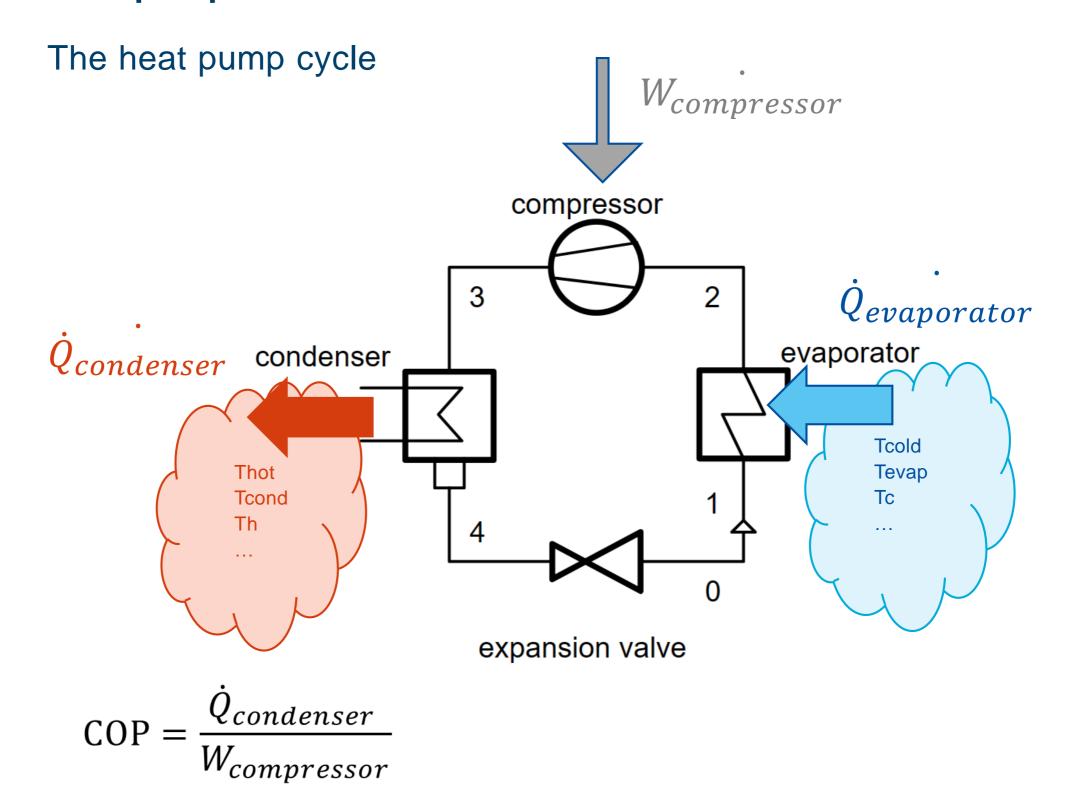




expansion valve











Agenda

- Heat pump overview
- Re-visiting thermodynamics
- Components and cycles

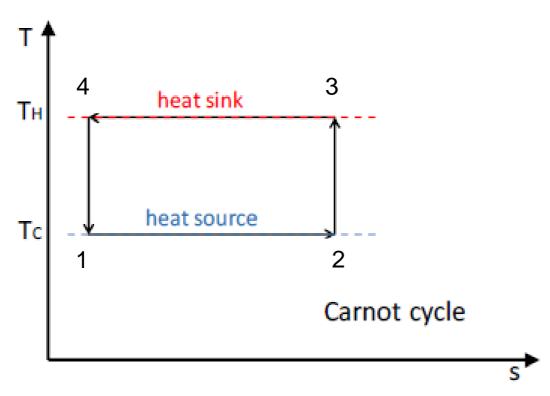


The heat pump cycle

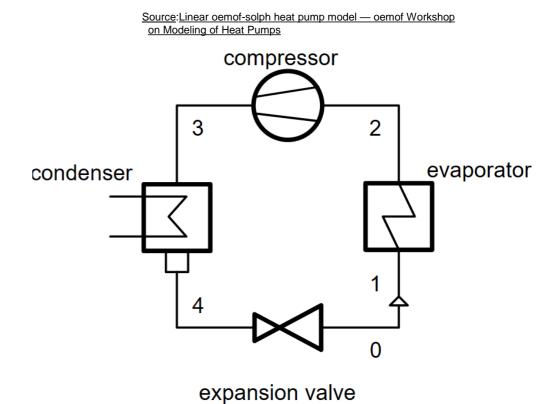
Carnot approximation

Assumptions: → isothermal heat transfer at both source and sink

→ infinite sink and reservoir (source)



$$COP = \frac{\dot{Q}_{condenser}}{W_{compressor}}$$





The heat pump cycle

Carnot (ideal) COP

The ideal performance of a heat pump

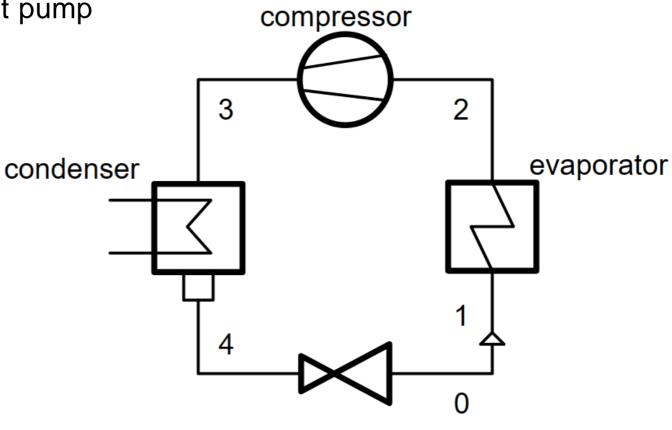
$$\mathrm{COP} = \frac{\dot{Q}_{condenser}}{W_{compressor}}$$

Energy balance

$$\dot{Q}_{cond.} = W_{compr.} + \dot{Q}_{evap.}$$

$$COP = \frac{\dot{Q}_{cond.}}{\dot{Q}_{cond.} - \dot{Q}_{evap.}}$$

<u>Source:Linear oemof-solph heat pump model — oemof Workshop on Modeling of Heat Pumps</u>



expansion valve

Assumption: ideal heat transfer (isothermal),

Temperatures are considered at the "secondary side" of the cond/evap

$$COP_{Carnot} = \frac{T_{cond}}{T_{cond} - T_{evap}} = \frac{T_h}{T_h - T_c} = \frac{T_4}{T_4 - T_2}$$

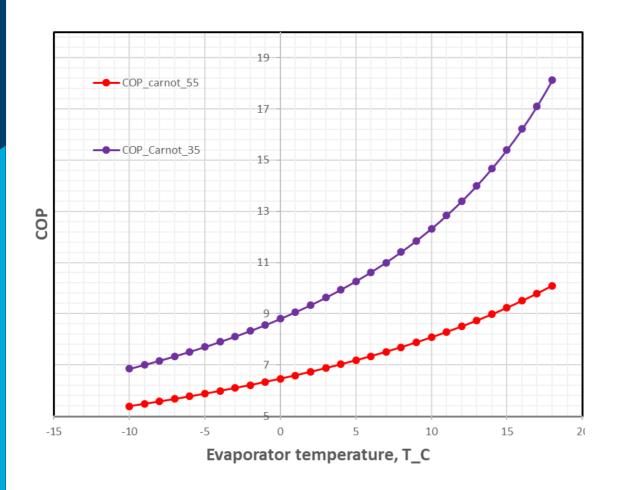




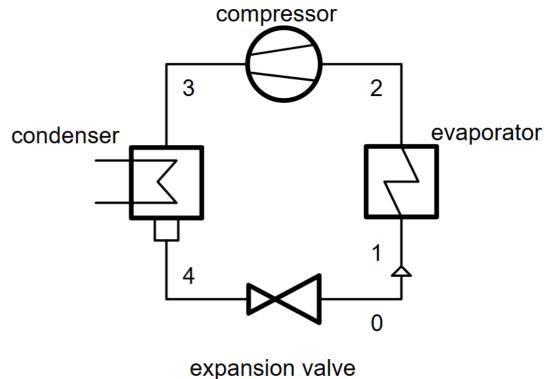
The heat pump cycle

Carnot (ideal) COP

The ideal performance of a heat pump



<u>Source:Linear oemof-solph heat pump model — oemof Workshop</u> on Modeling of Heat Pumps



$$COP_{Carnot} = \frac{T_{cond}}{T_{cond} - T_{evap}} = \frac{T_h}{T_h - T_c} = \frac{T_4}{T_4 - T_2}$$



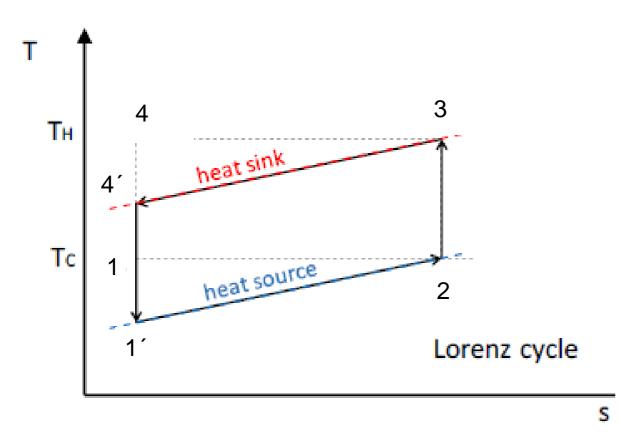


The heat pump cycle

Lorenz approximation

Assumptions: → non-isothermal heat transfer at both source and sink

→ temperature gradients at sink and reservoir (source)



condenser 2 evaporator T_c

Source:Linear oemof-solph heat pump model —

$$COP = \frac{\dot{Q}_{cond}}{W_{compr}} = \frac{\dot{Q}_{3-4}}{W_{3-2}}$$

expansion valve

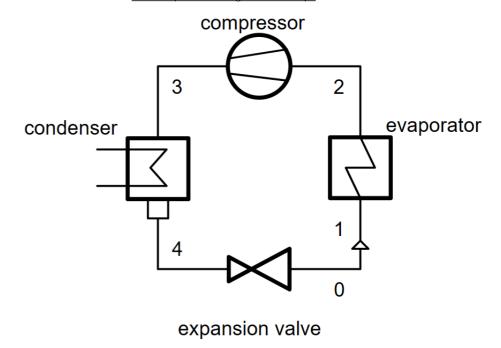


The heat pump cycle

Lorenz COP

The ideal performance of a heat pump

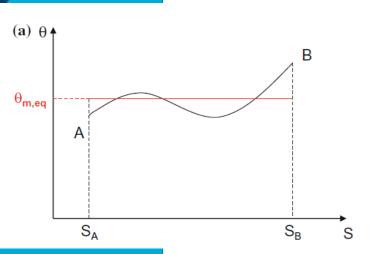
$$COP = \frac{\dot{Q}_{cond}}{W_{compr}} = \frac{\dot{Q}_{3-4}}{W_{3-2}} = \frac{\overline{T}_{H} (s_{2} - s_{1})}{\overline{(T}_{H} - \overline{T}_{C}) (s_{2} - s_{1})}$$



 \bar{T}_H, \bar{T}_C Entropy-averaged temperatures = avg. Temperature in T-S diagramm representing avg. Temperature difference

Assumptions:

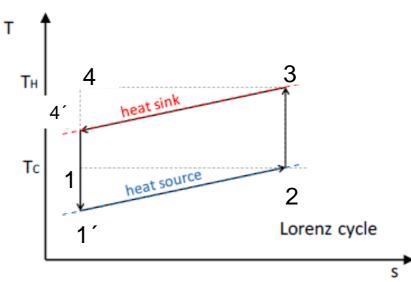
$$\dot{m}c_p$$
 =constant
pressure, p_H , p_C = constant



$$\bar{T}_H = \frac{h_3 - h_{4\prime}}{s_3 - s_{4\prime}} = \frac{T_3 - T_{4\prime}}{\ln(\frac{T_3}{T_{4\prime}})}$$

$$\overline{T}_C = \frac{h_2 - h_{1\prime}}{s_2 - s_{1\prime}} = \frac{T_2 - T_{1\prime}}{\ln(\frac{T_2}{T_{1\prime}})}$$

$$COP_{Lorenz} = \frac{\dot{Q}_{cond}}{W_{compr}} = \frac{\overline{T}_{H}\left(s_{2} - s_{1}\right)}{\overline{\left(\overline{T}_{H} - \overline{T}_{C}\right)\left(s_{2} - s_{1}\right)}} = \frac{1}{1 - \frac{\overline{T}_{C}}{\overline{T}_{H}}}$$



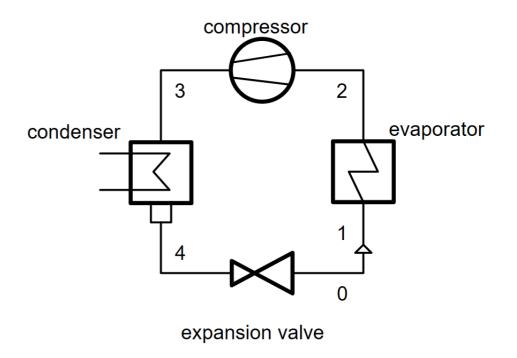


The heat pump cycle

Lorenz + Carnot COP

The ideal performance of a heat pump

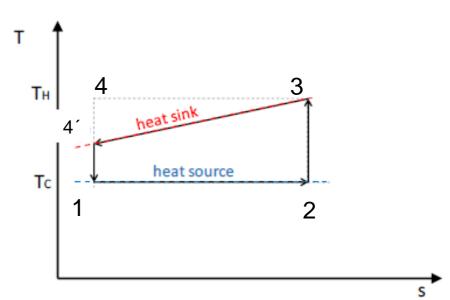
$$COP = \frac{\dot{Q}_{cond}}{W_{compr}} = \frac{\dot{Q}_{3-4}}{W_{1-2}} = \frac{\overline{T}_{H} (s_{2} - s_{1})}{\overline{(T}_{H} - \overline{T}_{C}) (s_{2} - s_{1})}$$



 $\overline{T}_H, \overline{T}_C$ Entropy-averaged temperatures = avg. Temperature in T-S diagramm representing avg. Temperature difference

Assumptions: $\dot{m}c_p = constant$ $pressure, p_H, p_C = constant$

$$\bar{T}_H = \frac{h_3 - h_{4\prime}}{s_3 - s_{4\prime}} = \frac{T_3 - T_{4\prime}}{\ln(\frac{T_3}{T_{4\prime}})}$$



 $\bar{T}_C = T_C$, infinite sink/source, constant temperature

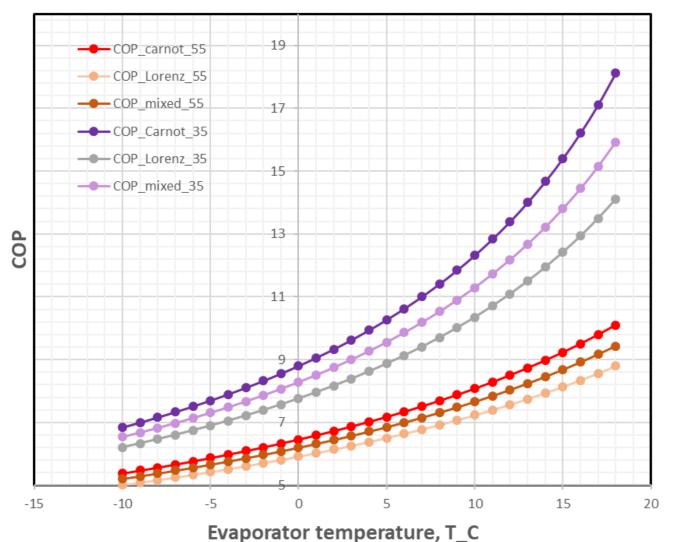
$$COP_{mixed} = \frac{\dot{Q}_{cond}}{W_{compr}} = \frac{\overline{T}_H (s_2 - s_1)}{\overline{(T}_H - \overline{T}_C) (s_2 - s_1)} = \frac{1}{1 - \frac{\overline{T}_C}{\overline{T}_H}}$$

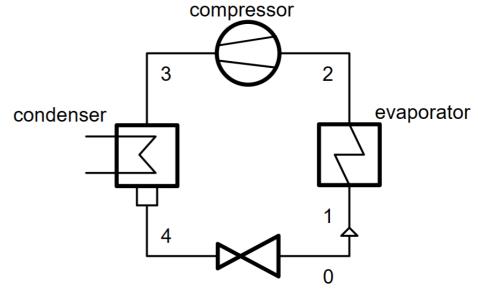


The heat pump cycle

Lorenz + Carnot COP

The ideal performance of a heat pump





expansion valve





The heat pump cycle

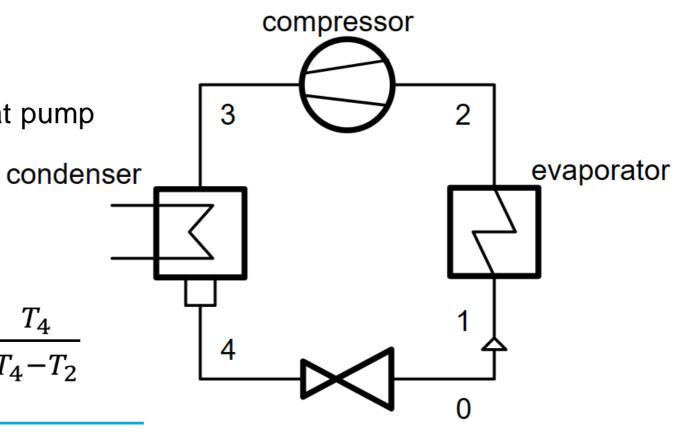
Real (and ideal) COP

The ideal performance of a heat pump

$$COP = \frac{\dot{Q}_{condenser}}{W_{compressor}}$$

$$COP_{Carnot} = \frac{T_h}{T_h - T_c} = \frac{T_4}{T_4 - T_2}$$

<u>Source:Linear oemof-solph heat pump model — oemof Workshop on Modeling of Heat Pumps</u>



expansion valve

$$\eta_{hp} = \frac{COP}{COP_{carnot}}$$

Characterizes how far the **real performance** deviates from an ideal one. Calibration parameter





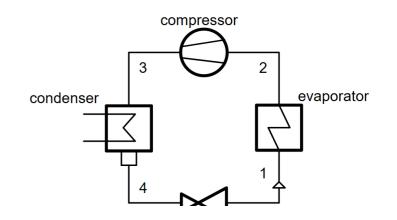
The heat pump cycle

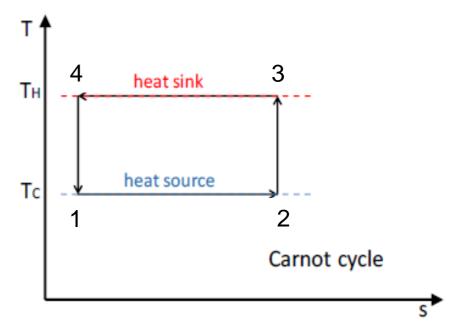
Real (and ideal) COP

The real performance of a heat pump

$$COP = \frac{\dot{Q}_{condenser}}{W_{compressor}}$$

$$COP_{Carnot} = \frac{T_h}{T_h - T_c} = \frac{T_4}{T_4 - T_2}$$

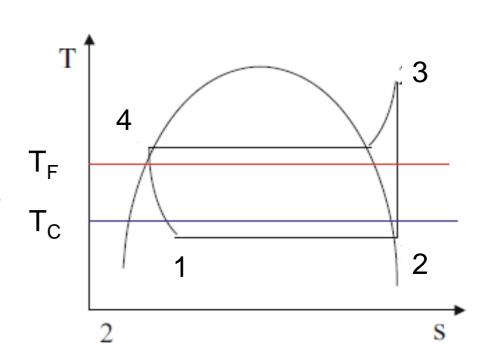




$$\eta_{hp} = \frac{COP}{COP_{Carnot}}$$

Characterizes how far the **real performance** deviates from an ideal one.

Calibration parameter





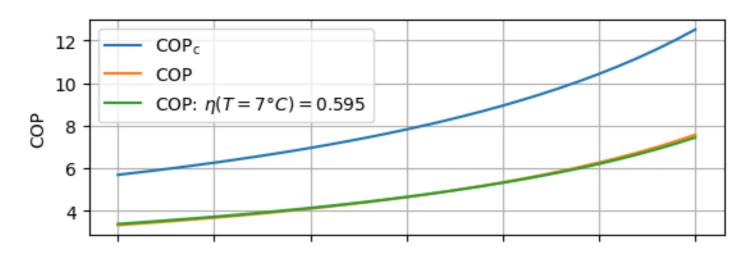
The heat pump cycle

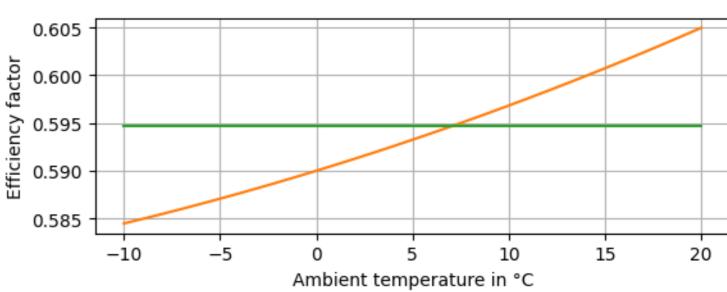
Real (and ideal) COP

The real performance of a heat pump

$$\eta_{hp} = \frac{COP}{COP_{carnot}}$$

- Characterizes how far the real performance deviates from an ideal one.
- Calibration parameter; assumed to be constant often!





Assuming constant compressor efficiency



The heat pump cycle

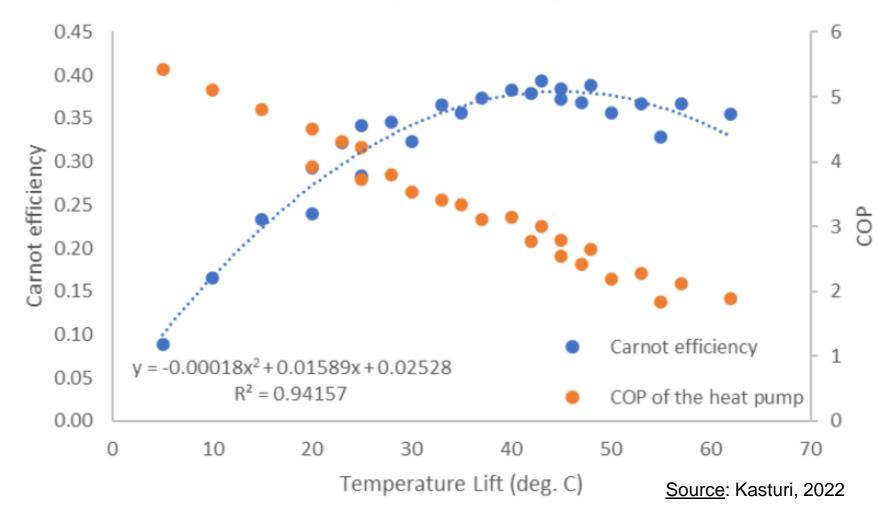
Real (and ideal) COP

The real performance of a heat pump

$$\eta_{hp} = \frac{COP}{COP_{Carnot}}$$

- Carnot efficiencies are rather low
- Lower carnot efficiencies at lower temperature lifts, T_H-T_C

Carnot Efficiency/COP vs. Temperature lift







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The heat pump cycle

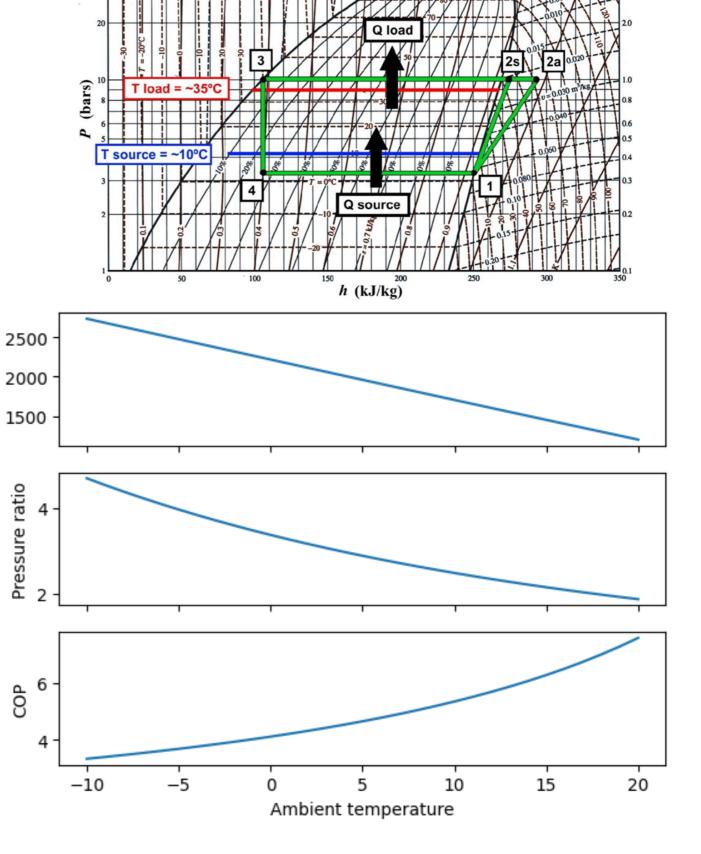
Full load

Compressor efficiency can be considered as constant (calibration point)

 \dot{W}_{cp} in W

Pressure ratio and electrical input decline with increasing source temperature

COP dependent on Temperatures







The heat pump cycle

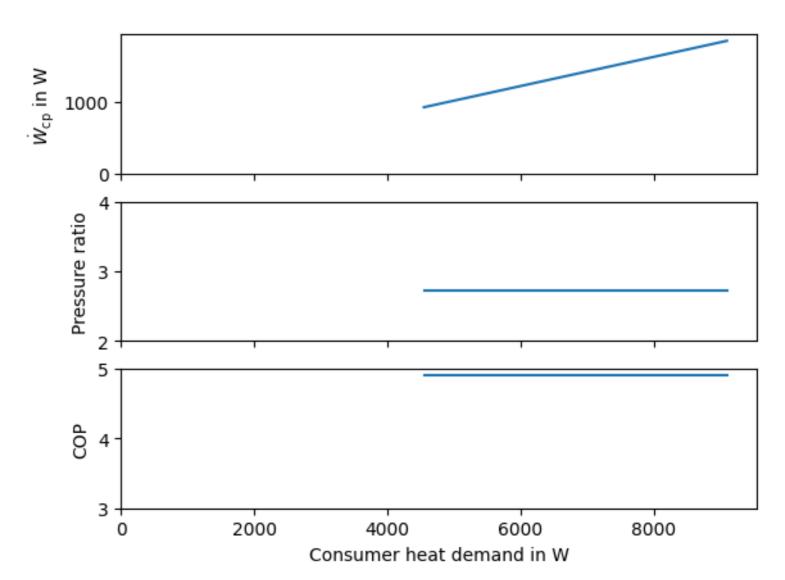
Full load

Compressor efficiency can be considered as constant (calibration point)

Electrical input is a linear function of the heat supplied (constant compr. eff.)

Pressure ratio independent of load to be supplied

COP **IN**dependent on heat supplied (Qcond)







The heat pump cycle

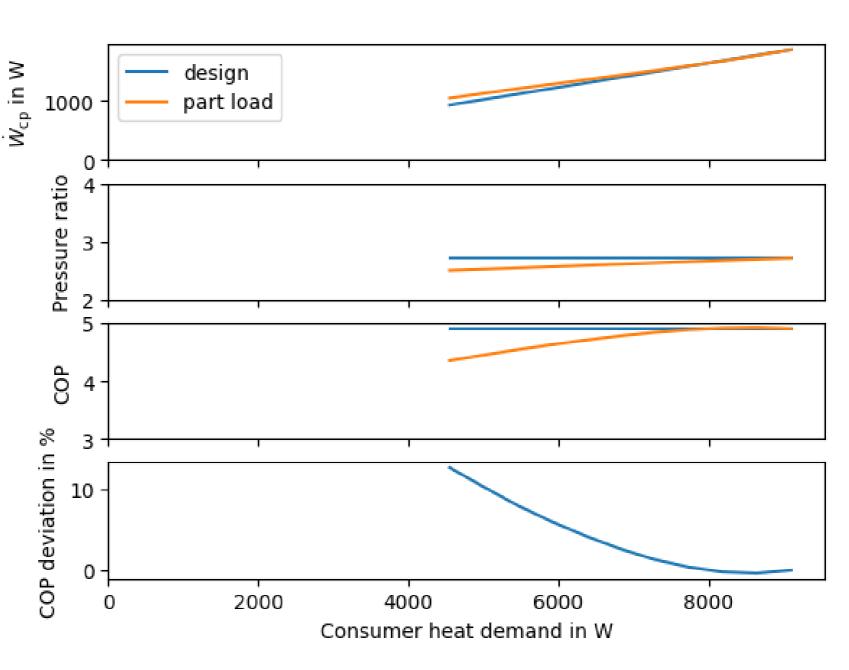
Partial load

Compressor efficiency can be considered as state-dependent (non constant)

For loads lower than 75-50% of max.power higher deviations of the power ratio

Leading to higher differences in the COP

COP is dependent of the partial load behaviour





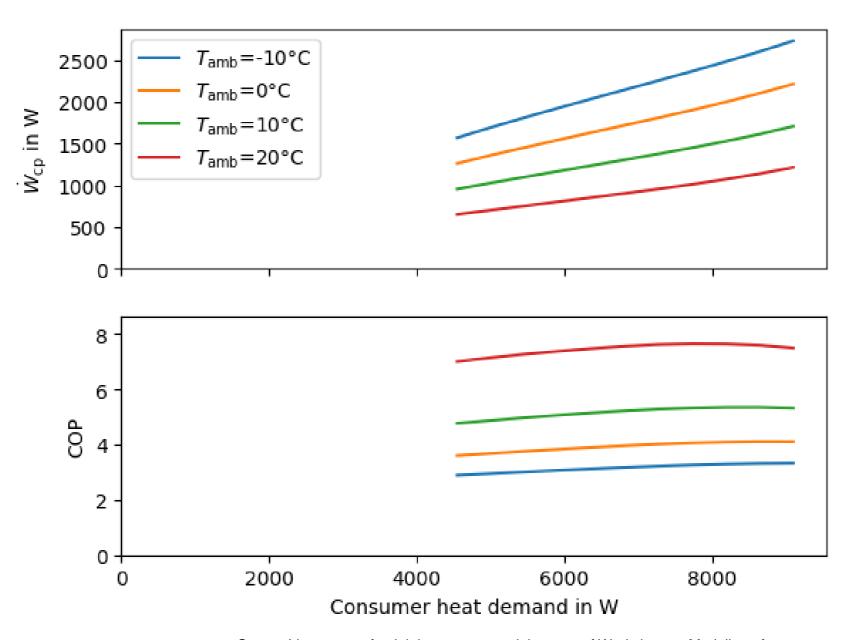


The heat pump cycle

Partial load

Compressor efficiency can be considered as state-dependent (non constant)

- At part load COP decreases
- For loads lower than 75-50% of max.power compressor power is not a linear function of the load anymore
- COP is not fully constant for lower loads





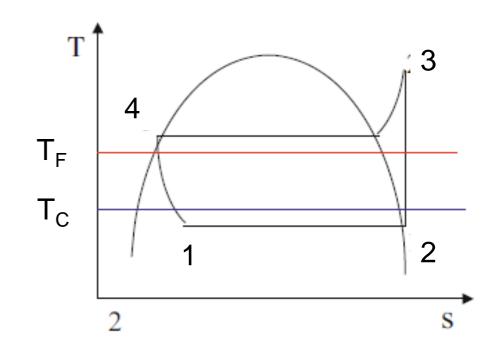


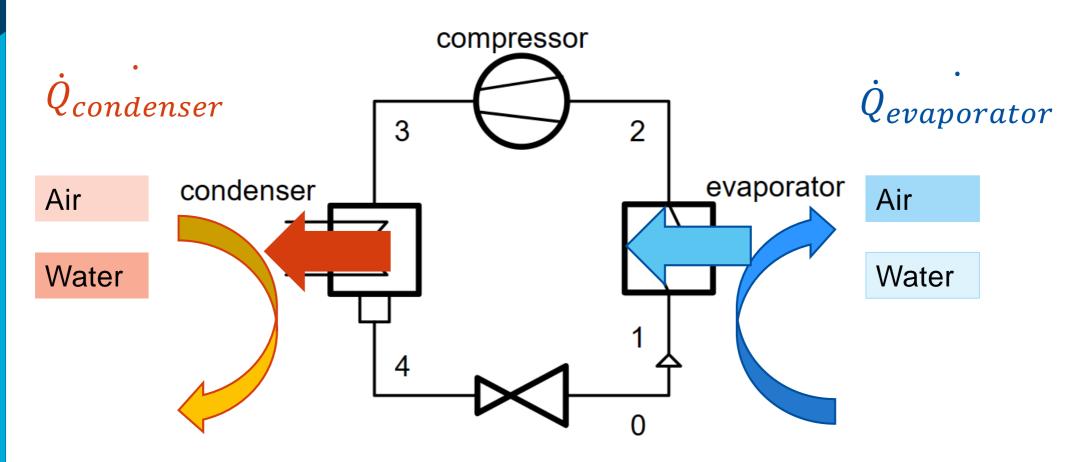
The heat pump cycle

Operation - Real behaviour (simluated)

Constant mass flow vs. Constant temperature difference

(in the secondary sides of both evaporator and condenser)





expansion valve

RE Heat

Dr. Herena Torio, Institute of Physics,

 $\dot{Q}_{evaporator} = \dot{m}c_p \Delta T$

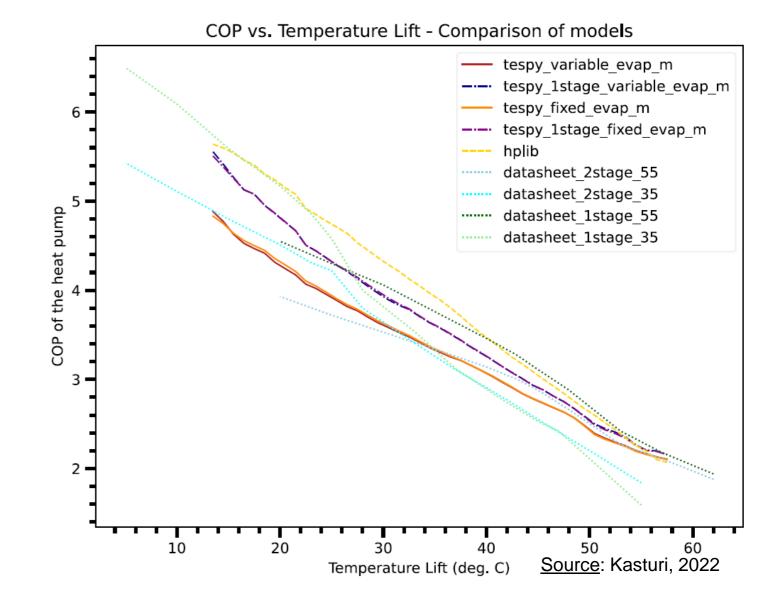


The heat pump cycle

Operation

Constant mass flow vs. Constant temperature difference (in the secondary sides of both evaporator and condenser)

- Very similar COP - performance for both operation strategies





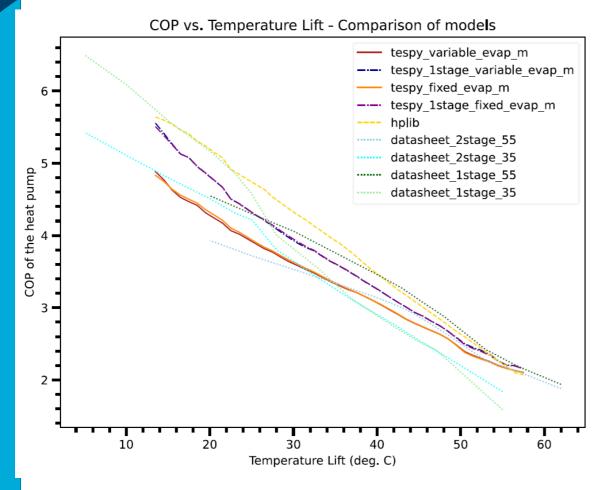


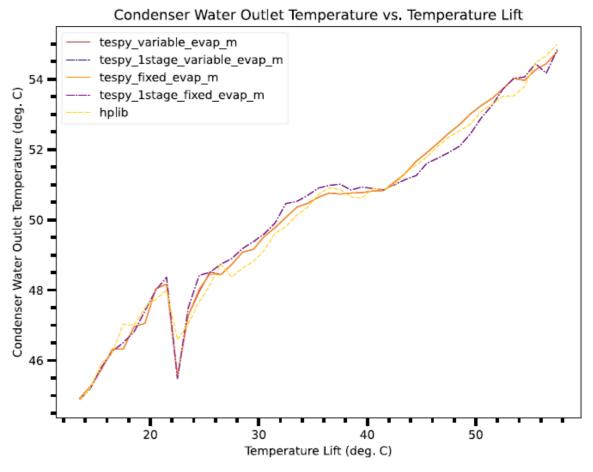
The heat pump cycle

Operation

Constant mass flow vs. Constant temperature difference (in the secondary sides of both evaporator and condenser)

- Very similar COP performance for both operation strategies
- Very similar condenser outlet temperatures







Source: Kasturi, 2022



References

Grassi 2018. Heat pump fundamentals and applications. Green Energy and Technology, Springer Ed. Link: https://link.springer.com/book/10.1007/978-3-319-62199-9, Last accessed: Oct. 2023

Kasturi 2023. Simulation of photovoltaic-thermal (PV-T) solar assisted heat pump (SAHP) systems for building thermal demands. Master thesis at the UOL.

Hervas Blanco. 2020. Low temperature waste water heat recovery for Domestic Hot Water production based on heat pumps. PhD Thesis. Instituto Ingenieria Energetica. Universidad Politecnica de Valencia. Link: Aprovechamiento del calor residual a baja temperatura mediante bombas de calor para la producción de agua caliente (upv.es), Last accessed: 03.11.2023