

# Final practice problems - solutions

29. The direction of fastest change is  $\nabla f(x, y) = (2x - 2)\mathbf{i} + (2y - 4)\mathbf{j}$ , so we need to find all points  $(x, y)$  where  $\nabla f(x, y)$  is parallel to  $\mathbf{i} + \mathbf{j} \Leftrightarrow (2x - 2)\mathbf{i} + (2y - 4)\mathbf{j} = k(\mathbf{i} + \mathbf{j}) \Leftrightarrow k = 2x - 2$  and  $k = 2y - 4$ . Then  $2x - 2 = 2y - 4 \Rightarrow y = x + 1$ , so the direction of fastest change is  $\mathbf{i} + \mathbf{j}$  at all points on the line  $y = x + 1$ .

67. Let  $\mathbf{u} = \langle a, b \rangle$  and  $\mathbf{v} = \langle c, d \rangle$ . Then we know that at the given point,  $D_{\mathbf{u}}f = \nabla f \cdot \mathbf{u} = af_x + bf_y$  and  $D_{\mathbf{v}}f = \nabla f \cdot \mathbf{v} = cf_x + df_y$ . But these are just two linear equations in the two unknowns  $f_x$  and  $f_y$ , and since  $\mathbf{u}$  and  $\mathbf{v}$  are not parallel, we can solve the equations to find  $\nabla f = \langle f_x, f_y \rangle$  at the given point. In fact,

$$\nabla f = \left\langle \frac{dD_{\mathbf{u}}f - bD_{\mathbf{v}}f}{ad - bc}, \frac{aD_{\mathbf{v}}f - cD_{\mathbf{u}}f}{ad - bc} \right\rangle.$$

51. Let the dimensions be  $x$ ,  $y$  and  $z$ , then minimize  $xy + 2(xz + yz)$  if  $xyz = 32,000 \text{ cm}^3$ . Then

$$f(x, y) = xy + [64,000(x + y)/xy] = xy + 64,000(x^{-1} + y^{-1}), \quad f_x = y - 64,000x^{-2}, \quad f_y = x - 64,000y^{-2}.$$

And  $f_x = 0$  implies  $y = 64,000/x^2$ ; substituting into  $f_y = 0$  implies  $x^3 = 64,000$  or  $x = 40$  and then  $y = 40$ . Now

$D(x, y) = [(2)(64,000)]^2 x^{-3} y^{-3} - 1 > 0$  for  $(40, 40)$  and  $f_{xx}(40, 40) > 0$  so this is indeed a minimum. Thus the dimensions of the box are  $x = y = 40 \text{ cm}$ ,  $z = 20 \text{ cm}$ .

We are given  $Y(N, P) = kNP e^{-N-P}$  where nitrogen level is  $N$  and phosphorus level is  $P$  in the soil (measured in appropriate units) and  $k$  is a constant. We need to find levels of nitrogen and phosphorus which shall result in the best yield. Hence we shall find the partial derivatives and then equate them to 0 to find the critical points.

$$Y_N(N, P) = kP(Ne^{-N-P}(-1) + e^{-N-P}) = kPe^{-N-P}(1 - N)$$

$$Y_P(N, P) = kN(Pe^{-N-P}(-1) + e^{-N-P}) = kNe^{-N-P}(1 - P)$$

When we equate them to 0, we get the critical points  $(1, 1)$  as we can not have the level of  $P$  and  $N$  to be 0.

Using second derivatives test, we get:

$$Y_{NN} = kP(e^{-N-P}(-1) + (1 - N)e^{-N-P}(-1)); Y_{NN}(1, 1) = -ke^{-2}$$

$$Y_{PP} = kN(e^{-N-P}(-1) + (1 - P)e^{-N-P}(-1)); Y_{PP}(1, 1) = -ke^{-2}$$

$$Y_{NP} = k(1 - N)(1 - P)e^{-N-P}; Y_{NP}(1, 1) = 0$$

We know that  $D(x, y) = f_{xx}f_{yy} - f_{xy}^2$

$$D(1, 1) = k^2 e^{-4} > 0; Y_{NN} < 0$$

Hence the point  $(1, 1)$  is a point of maxima.

21. In cylindrical coordinates,  $E$  is bounded by the cylinder  $r = 1$ , the plane  $z = 0$ , and the cone  $z = 2r$ . So

$$E = \{(r, \theta, z) \mid 0 \leq \theta \leq 2\pi, 0 \leq r \leq 1, 0 \leq z \leq 2r\} \text{ and}$$

$$\begin{aligned} \iiint_E x^2 dV &= \int_0^{2\pi} \int_0^1 \int_0^{2r} r^2 \cos^2 \theta r dz dr d\theta = \int_0^{2\pi} \int_0^1 [r^3 \cos^2 \theta z]_{z=0}^{z=2r} dr d\theta = \int_0^{2\pi} \int_0^1 2r^4 \cos^2 \theta dr d\theta \\ &= \int_0^{2\pi} \left[ \frac{2}{5} r^5 \cos^2 \theta \right]_{r=0}^{r=1} d\theta = \frac{2}{5} \int_0^{2\pi} \cos^2 \theta d\theta = \frac{2}{5} \int_0^{2\pi} \frac{1}{2} (1 + \cos 2\theta) d\theta = \frac{1}{5} [\theta + \frac{1}{2} \sin 2\theta]_0^{2\pi} = \frac{2\pi}{5} \end{aligned}$$

25. In spherical coordinates,  $E$  is represented by  $\{(\rho, \theta, \phi) \mid 0 \leq \rho \leq 1, 0 \leq \theta \leq \frac{\pi}{2}, 0 \leq \phi \leq \frac{\pi}{2}\}$ . Thus

$$\begin{aligned} \iiint_E x e^{x^2+y^2+z^2} dV &= \int_0^{\pi/2} \int_0^{\pi/2} \int_0^1 (\rho \sin \phi \cos \theta) e^{\rho^2} \rho^2 \sin \phi d\rho d\theta d\phi = \int_0^{\pi/2} \sin^2 \phi d\phi \int_0^{\pi/2} \cos \theta d\theta \int_0^1 \rho^3 e^{\rho^2} d\rho \\ &= \int_0^{\pi/2} \frac{1}{2} (1 - \cos 2\phi) d\phi \int_0^{\pi/2} \cos \theta d\theta \left( \left[ \frac{1}{2} \rho^2 e^{\rho^2} \right]_0^1 - \int_0^1 \rho e^{\rho^2} d\rho \right) \\ &\quad \left[ \text{integrate by parts with } u = \rho^2, dv = \rho e^{\rho^2} d\rho \right] \\ &= \left[ \frac{1}{2} \phi - \frac{1}{4} \sin 2\phi \right]_0^{\pi/2} [\sin \theta]_0^{\pi/2} \left[ \frac{1}{2} \rho^2 e^{\rho^2} - \frac{1}{2} e^{\rho^2} \right]_0^1 = \left( \frac{\pi}{4} - 0 \right) (1 - 0) \left( 0 + \frac{1}{2} \right) = \frac{\pi}{8} \end{aligned}$$

39.  $W = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_0^{2\pi} \langle t - \sin t, 3 - \cos t \rangle \cdot \langle 1 - \cos t, \sin t \rangle dt$

$$= \int_0^{2\pi} (t - t \cos t - \sin t + \sin t \cos t + 3 \sin t - \sin t \cos t) dt$$

$$= \int_0^{2\pi} (t - t \cos t + 2 \sin t) dt = \left[ \frac{1}{2} t^2 - (t \sin t + \cos t) - 2 \cos t \right]_0^{2\pi} \quad \left[ \begin{array}{l} \text{integrate by parts} \\ \text{in the second term} \end{array} \right]$$

$$= 2\pi^2$$

28.  $\nabla f(x, y) = \cos(x - 2y) \mathbf{i} - 2 \cos(x - 2y) \mathbf{j}$

(a) We use Theorem 2:  $\int_{C_1} \mathbf{F} \cdot d\mathbf{r} = \int_{C_1} \nabla f \cdot d\mathbf{r} = f(\mathbf{r}(b)) - f(\mathbf{r}(a))$  where  $C_1$  starts at  $t = a$  and ends at  $t = b$ . So

because  $f(0, 0) = \sin 0 = 0$  and  $f(\pi, \pi) = \sin(\pi - 2\pi) = 0$ , one possible curve  $C_1$  is the straight line from  $(0, 0)$  to  $(\pi, \pi)$ ; that is,  $\mathbf{r}(t) = \pi t \mathbf{i} + \pi t \mathbf{j}$ ,  $0 \leq t \leq 1$ .

(b) From (a),  $\int_{C_2} \mathbf{F} \cdot d\mathbf{r} = f(\mathbf{r}(b)) - f(\mathbf{r}(a))$ . So because  $f(0, 0) = \sin 0 = 0$  and  $f(\frac{\pi}{2}, 0) = 1$ , one possible curve  $C_2$  is

$\mathbf{r}(t) = \frac{\pi}{2} t \mathbf{i}$ ,  $0 \leq t \leq 1$ , the straight line from  $(0, 0)$  to  $(\frac{\pi}{2}, 0)$ .

44. A parametric representation for the hemisphere  $S$  is  $\mathbf{r}(\phi, \theta) = 3 \sin \phi \cos \theta \mathbf{i} + 3 \sin \phi \sin \theta \mathbf{j} + 3 \cos \phi \mathbf{k}$ ,  $0 \leq \phi \leq \pi/2$ ,

$0 \leq \theta \leq 2\pi$ . Then  $\mathbf{r}_\phi = 3 \cos \phi \cos \theta \mathbf{i} + 3 \cos \phi \sin \theta \mathbf{j} - 3 \sin \phi \mathbf{k}$ ,  $\mathbf{r}_\theta = -3 \sin \phi \sin \theta \mathbf{i} + 3 \sin \phi \cos \theta \mathbf{j}$ , and the outward orientation is given by  $\mathbf{r}_\phi \times \mathbf{r}_\theta = 9 \sin^2 \phi \cos \theta \mathbf{i} + 9 \sin^2 \phi \sin \theta \mathbf{j} + 9 \sin \phi \cos \phi \mathbf{k}$ . The rate of flow through  $S$  is

$$\begin{aligned} \iint_S \rho \mathbf{v} \cdot d\mathbf{S} &= \rho \int_0^{\pi/2} \int_0^{2\pi} (3 \sin \phi \sin \theta \mathbf{i} + 3 \sin \phi \cos \theta \mathbf{j}) \cdot (9 \sin^2 \phi \cos \theta \mathbf{i} + 9 \sin^2 \phi \sin \theta \mathbf{j} + 9 \sin \phi \cos \phi \mathbf{k}) d\theta d\phi \\ &= 27\rho \int_0^{\pi/2} \int_0^{2\pi} (\sin^3 \phi \sin \theta \cos \theta + \sin^3 \phi \sin \theta \cos \theta) d\theta d\phi = 54\rho \int_0^{\pi/2} \sin^3 \phi d\phi \int_0^{2\pi} \sin \theta \cos \theta d\theta \\ &= 54\rho \left[ -\frac{1}{3} (2 + \sin^2 \phi) \cos \phi \right]_0^{\pi/2} \left[ \frac{1}{2} \sin^2 \theta \right]_0^{2\pi} = 0 \text{ kg/s} \end{aligned}$$

5.  $C$  is the square in the plane  $z = -1$ . Rather than evaluating a line integral around  $C$  we can use Equation 3:

$\iint_{S_1} \text{curl } \mathbf{F} \cdot d\mathbf{S} = \oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_{S_2} \text{curl } \mathbf{F} \cdot d\mathbf{S}$  where  $S_1$  is the original cube without the bottom and  $S_2$  is the bottom face of the cube.  $\text{curl } \mathbf{F} = x^2z \mathbf{i} + (xy - 2xyz) \mathbf{j} + (y - xz) \mathbf{k}$ . For  $S_2$ , we choose  $\mathbf{n} = \mathbf{k}$  so that  $C$  has the same orientation for both surfaces. Then  $\text{curl } \mathbf{F} \cdot \mathbf{n} = y - xz = x + y$  on  $S_2$ , where  $z = -1$ . Thus  $\iint_{S_2} \text{curl } \mathbf{F} \cdot d\mathbf{S} = \int_{-1}^1 \int_{-1}^1 (x + y) dx dy = 0$  so  $\iint_{S_1} \text{curl } \mathbf{F} \cdot d\mathbf{S} = 0$ .

16. Let  $S$  be the surface in the plane  $x + y + z = 1$  with upward orientation enclosed by  $C$ . Then an upward unit normal vector for  $S$  is  $\mathbf{n} = \frac{1}{\sqrt{3}} (\mathbf{i} + \mathbf{j} + \mathbf{k})$ . Orient  $C$  in the counterclockwise direction, as viewed from above.  $\int_C z dx - 2x dy + 3y dz$  is equivalent to  $\int_C \mathbf{F} \cdot d\mathbf{r}$  for  $\mathbf{F}(x, y, z) = z \mathbf{i} - 2x \mathbf{j} + 3y \mathbf{k}$ , and the components of  $\mathbf{F}$  are polynomials, which have continuous partial derivatives throughout  $\mathbb{R}^3$ . We have  $\text{curl } \mathbf{F} = 3 \mathbf{i} + \mathbf{j} - 2 \mathbf{k}$ , so by Stokes' Theorem,

$$\begin{aligned} \int_C z dx - 2x dy + 3y dz &= \int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \text{curl } \mathbf{F} \cdot \mathbf{n} dS = \iint_S (3 \mathbf{i} + \mathbf{j} - 2 \mathbf{k}) \cdot \frac{1}{\sqrt{3}} (\mathbf{i} + \mathbf{j} + \mathbf{k}) dS \\ &= \frac{2}{\sqrt{3}} \iint_S dS = \frac{2}{\sqrt{3}} (\text{surface area of } S) \end{aligned}$$

Thus the value of  $\int_C z dx - 2x dy + 3y dz$  is always  $\frac{2}{\sqrt{3}}$  times the area of the region enclosed by  $C$ , regardless of its shape or location. [Notice that because  $\mathbf{n}$  is normal to a plane, it is constant. But  $\text{curl } \mathbf{F}$  is also constant, so the dot product  $\text{curl } \mathbf{F} \cdot \mathbf{n}$  is constant and we could have simply argued that  $\iint_S \text{curl } \mathbf{F} \cdot \mathbf{n} dS$  is a constant multiple of  $\iint_S dS$ , the surface area of  $S$ .]

7.  $\text{div } \mathbf{F} = 3y^2 + 0 + 3z^2$ , so using cylindrical coordinates with  $y = r \cos \theta$ ,  $z = r \sin \theta$ ,  $x = x$  we have

$$\begin{aligned} \iint_S \mathbf{F} \cdot d\mathbf{S} &= \iiint_E (3y^2 + 3z^2) dV = \int_0^{2\pi} \int_0^1 \int_{-1}^2 (3r^2 \cos^2 \theta + 3r^2 \sin^2 \theta) r dx dr d\theta \\ &= 3 \int_0^{2\pi} d\theta \int_0^1 r^3 dr \int_{-1}^2 dx = 3(2\pi) \left(\frac{1}{4}\right) (3) = \frac{9\pi}{2} \end{aligned}$$

24. We first need to find  $\mathbf{F}$  so that  $\iint_S \mathbf{F} \cdot \mathbf{n} dS = \iint_S (2x + 2y + z^2) dS$ , so  $\mathbf{F} \cdot \mathbf{n} = 2x + 2y + z^2$ . But for  $S$ ,

$$\mathbf{n} = \frac{x \mathbf{i} + y \mathbf{j} + z \mathbf{k}}{\sqrt{x^2 + y^2 + z^2}} = x \mathbf{i} + y \mathbf{j} + z \mathbf{k}. \text{ Thus } \mathbf{F} = 2 \mathbf{i} + 2 \mathbf{j} + z \mathbf{k} \text{ and } \text{div } \mathbf{F} = 1.$$

If  $B = \{(x, y, z) \mid x^2 + y^2 + z^2 \leq 1\}$ , then  $\iint_S (2x + 2y + z^2) dS = \iiint_B dV = V(B) = \frac{4}{3}\pi(1)^3 = \frac{4}{3}\pi$ .