

1.

We have

$$X(s) = \frac{\beta}{s+1}, \operatorname{Re}\{s\} > -1.$$

Also,

$$G(s) = X(s) + \alpha X(-s), -1 < \operatorname{Re}\{s\} < 1$$

Therefore.

$$G(s) = \beta \left[ \frac{1-s+\alpha s+\alpha}{1-s^2} \right]$$

Comparing with the given equation for  $G(s)$ 

$$\alpha = -1 \quad \beta = \frac{1}{2}$$

2.

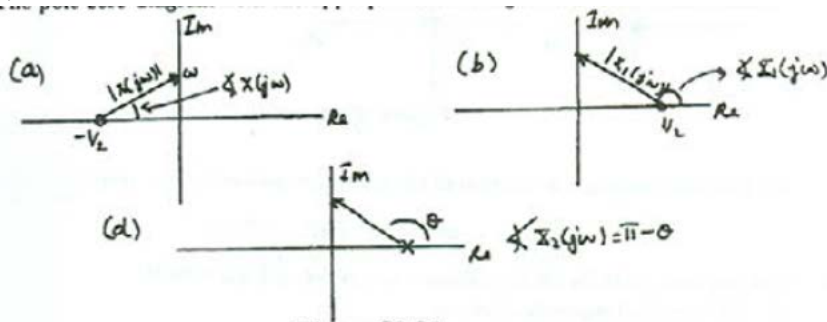


Figure S9.24

(a) The pole-zero diagram with the appropriate markings is shown in Figure S9.24

(b) By inspecting the pole-zero diagram of part (a), it is clear that the pole zero diagram shown in Figure S9.24 will also result in the same  $|X(j\omega)|$ . This would correspond to the Laplace transform

$$X_1(s) = s - \frac{1}{2} \quad \operatorname{Re}\{s\} < \frac{1}{2}$$

(c)

$$\angle X(j\omega) = \pi - \angle X_1(j\omega)$$

(d)  $X_2(s)$  with the pole-zero diagram shown below in Figure 9.24 would have the property that  $\angle X_2(j\omega) = \angle X(j\omega)$ . Here,  $X_2(s) = \frac{-1}{s-1/2}$ (e)  $|X_2(j\omega)| = 1/|X(j\omega)|$ (f) From the result of part (b), it is clear that  $X_1(s)$  may be obtained by reflecting the poles and zeros in the right-half of the s-plane to the left-half of the s-plane. Therefore,

$$X_1(s) = \frac{s+1/2}{s+2}$$

From part (d), it is clear that  $X_2(s)$  may be obtained by reflecting the poles (zeros) in the right-half of the s-plane to the left-half and simultaneously changing them to zeros (poles). Therefore,

$$X_2(s) = \frac{(s+1)^2}{(s+1/2)(s+2)}$$

3.

(a) Consider the signal  $y(t) = x(t - t_0)$ . Now,

$$Y(s) = \int_{-\infty}^{\infty} x(t - t_0) e^{-st} dt$$

Replacing  $t - t_0$  by  $r$ , we get

$$\begin{aligned} Y(s) &= \int_{-\infty}^{\infty} x(r) e^{-s(r+t_0)} dr \\ &= e^{-st_0} \int_{-\infty}^{\infty} x(r) e^{-sr} dr \\ &= e^{-st_0} X(s) \end{aligned}$$

This obviously converges when  $X(s)$  converges because  $e^{-st_0}$  has no poles.

Therefore, the ROC of  $Y(s)$  is the same as the ROC of  $X(s)$ .

(b) Consider the signal  $y(t) = e^{s_0 t} x(t)$ . Now,

$$\begin{aligned} y(t) &= e^{s_0 t} x(t) \\ Y(s) &= \int_{-\infty}^{\infty} x(t) e^{s_0 t} e^{-st} dt \\ &= \int_{-\infty}^{\infty} x(t) e^{-(s-s_0)t} dt \\ &= X(s - s_0) \end{aligned}$$

If  $X(s)$  converges in the range  $a < \text{Re}\{s\} < b$ , then  $X(s - s_0)$  converges in the range  $a + s_0 < s < b + s_0$ . This is the ROC of  $Y(s)$ .

(c) Consider the signal  $y(t) = x(at)$ . Now,

$$Y(s) = \int_{-\infty}^{\infty} x(at) e^{-st} dt$$

Replacing  $at$  by  $r$  and assuming that  $a > 1$ , we get

$$\begin{aligned} Y(s) &= (1/a) \int_{-\infty}^{\infty} x(r) e^{-s(r/a)} dr \\ &= (1/a) X(s/a) \end{aligned}$$

If  $a < 0$ , then

$$\begin{aligned} Y(s) &= -(1/a) \int_{-\infty}^{\infty} x(r) e^{-s(r/a)} dr \\ &= -(1/a) X(s/a) \end{aligned}$$

Therefore,

$$Y(s) = \frac{1}{|a|} X\left(\frac{s}{a}\right)$$

If  $X(s)$  converges in the range  $\alpha < \text{Re}\{s\} < \beta$ , then  $X(s/a)$  converges in the range  $\alpha/a < s < \beta/a$  when  $a > 0$ . When  $a < 0$ , then  $X(s/a)$  converges in the range  $\beta/a < s < \alpha/a$ .

(d) Consider the signal  $y(t) = x(t) \cdot h(t)$ . Now,

$$\begin{aligned} Y(s) &= \int_{-\infty}^{\infty} [x(t) \cdot h(t)] e^{-st} dt \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x(r) h(t-r) dr e^{-st} dt \\ &= \int_{-\infty}^{\infty} x(r) \left[ \int_{-\infty}^{\infty} h(t-r) e^{-st} dt \right] dr \end{aligned}$$

Using the time-shifting property, we get

$$\begin{aligned} Y(s) &= \int_{-\infty}^{\infty} x(r)H(s)e^{-sr} dr \\ &= H(s) \int_{-\infty}^{\infty} x(r)e^{-sr} dr \\ &= H(s)X(s) \end{aligned}$$

4.

According to the clues given, we can get the following analysis:

$h(t)$  is real value function, we get that the poles and zeros occur in conjugate pairs, so the known poles are  $-1 \pm j$ , and the known zeros are  $3 \pm j$ .

As there are two infinite zeros, we know that there are at least two finite poles.

As  $h(t)$  is stable and causal, we know all poles must lie in the left half  $s$  plane and the ROC must include  $j\omega$  axis and cover the right half plane.

True for (a). We get  $e^{-3t}h(t) \Leftrightarrow X(s+3)$ , as ROC of  $X(s)$  includes the  $j\omega$  axis and is right half plane, we know the ROC of  $X(s+3)$  must include  $j\omega$  axis, and (a) is true.

Insufficient information for (b). According to the analysis above, there may be other poles which lie in right side of  $\text{Re}\{s\} = -1$ , we cannot determine whether the ROC is  $\text{Re}\{s\} > -1$

True for (c). Since  $H(s)$  is rational,  $H(s)$  can be expressed as a ratio of two polynomials in  $s$ . We get:

$$H(s) = \frac{Y(s)}{X(s)} = \frac{P(s)}{Q(s)}$$

where  $P(s)$ ,  $Q(s)$  are the polynomials in  $s$ . We can get  $Y(s)Q(s) = P(s)X(s)$ , the differential equation can be derived from this. Since  $h(t)$  is real, we know that the coefficients of the polynomials are also real, so the coefficients of the differential equation are real.

False for (d). Since  $H(s)$  has infinite zeros. we know  $\lim_{s \rightarrow \infty} H(s) = 0$ .

True for (e). According to the above analysis, we know that  $H(s)$  has at least 4 poles.

False for (f). We know that  $e^{st}$  is the eigen function of LTI system, so output of input  $x(t) = e^{st}$  is  $H(s)e^{st}$ .  $e^{3t}\sin(t)$  can be decomposed into  $\frac{1}{2j}(e^{(3+j)t} - e^{(3-j)t})$ . The  $s$  value  $3 \pm j$  are the zeros of  $H(s)$ , so we know that the output is zero.

5.

Taking the Laplace transform of both sides of the equation, we get:

$$(s^3Y(s) + 6s^2 + 11s + 6)Y(s) - (s^2 + 6s + 11)y(0^-) - (s + 6)y'(0^-) - y''(0^-) = X(s)$$

Set  $y(0^-)$ ,  $y'(0^-)$ ,  $y''(0^-)$  all to zeros, we get:

$$Y(s) = \frac{1}{6} \left( \frac{1}{s+1} - 3\frac{1}{s+2} + 3\frac{1}{s+3} - \frac{1}{s+4} \right)$$

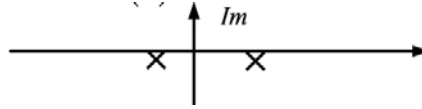
Then take the inverse transform, we get the zero state response:

$$y(t) = \frac{1}{6}(e^{-t} - 3e^{-2t} + 3e^{-3t} - e^{-4t})u(t)$$

6. (a) Taking the Laplace transform of both sides of the given differential equation and simplifying, we obtain

$$H(s) = \frac{Y(s)}{X(s)} = \frac{1}{s^2 - s - 2} = \frac{1}{(s - 2)(s + 1)}$$

The pole-zero plot for  $H(s)$  is as shown below



(b) The partial fraction expansion of  $H(s)$  is

$$H(s) = \frac{1}{(s - 2)(s + 1)} = \frac{1}{3(s - 2)} - \frac{1}{3(s + 1)}$$

1. If the system is stable, the ROC for  $H(s)$  has to be  $-1 < \Re\{s\} < 2$ . Therefore

$$h(t) = -\frac{e^{2t}u(-t)}{3} - \frac{e^{-t}u(t)}{3}$$

2. If the system is causal, the ROC for  $H(s)$  has to be  $\Re\{s\} > 2$ . Therefore

$$h(t) = \frac{e^{2t}u(t)}{3} - \frac{e^{-t}u(t)}{3}$$

3. If the system is neither stable nor causal, the ROC for  $H(s)$  has to be  $\Re\{s\} < -1$ . Therefore

$$h(t) = -\frac{e^{2t}u(-t)}{3} + \frac{e^{-t}u(-t)}{3}$$

7. (a)

$$\begin{aligned} v_i(t) &= RC \frac{dv_0(t)}{dt} + L \frac{d\{C \frac{dv_0(t)}{dt}\}}{dt} + v_0(t) \\ v_i(t) &= RC \frac{dv_0(t)}{dt} + LC \frac{d^2v_0(t)}{dt^2} + v_0(t) \\ v_i(t) &= \frac{3dv_0(t)}{2dt} + \frac{d^2v_0(t)}{2dt^2} + v_0(t) \end{aligned}$$

(b)

$$\begin{aligned} V_i(s) &= RC(sV_0(s) - V_0(0_+)) + LC(s^2V_0(s) - sV_0(0_+) - \frac{dv_0(0_+)}{dt}) + V_0(s) \\ V_i(s) &= \frac{3}{2}(sV_0(s) - 1) + \frac{1}{2}(s^2V_0(s) - s - 2) + V_0(s) \\ \frac{1}{s+3} &= (\frac{1}{2}s^2 + \frac{3}{2}s + 1)V_0(s) - \frac{1}{2}s - \frac{5}{2} \\ V_0(s) &= \frac{s^2+8s+17}{(s+1)(s+2)(s+3)} = \frac{5}{s+1} - \frac{5}{s+2} + \frac{1}{s+3} \end{aligned}$$

Therefore,

$$v_0(t) = (5e^{-t} - 5e^{-2t} + e^{-3t})u(t)$$