

1 Zeta Analysis - Comparison of Callahan's MathCad script to Lampe's analysis in R

1.1 Load

```
source("DoAll.R")

## Warning: package 'pracma' was built under R version 3.1.1
## Loading required package: wavethresh
## Loading required package: MASS
## WaveThresh: R wavelet software, release 4.6.6, installed
##
## Copyright Guy Nason and others 1993-2013
##
## Note: nlevels has been renamed to nlevelsWT
##
## Loading required package: adlift
## Loading required package: EbayesThresh
##
## *****
## adlift: a package to perform wavelet lifting schemes
##
## --- Written by Matt Nunes and Marina Knight ---
## Current package version: 1.3-2 ( 01/11/2012 )
##
##      +- packaged by MAN +-
## *****
##
## adlift 1.3-2 loaded
##
##
## Attaching package: 'adlift'
##
## The following object is masked from 'package:EbayesThresh':
##
## postmean.cauchy
##
## *****
## binhf: Haar-Fisz functions for binomial data
##
## --- Written by Matt Nunes ---
## Current package version: 1.0-1 ( 24/04/2014 )
##
## *****
##
## binhf 1.0-1 loaded
##
##
## Attaching package: 'binhf'
##
## The following objects are masked from 'package:EbayesThresh':
```

```

##
##     ebayesthresh.wavelet.wd, negloglik.laplace, wandafromx
##
## The following object is masked from 'package:wavethresh':
##
##     madmad
##
## The following object is masked from 'package:base':
##
##     norm
##
##
## Attaching package: 'deSolve'
##
## The following object is masked from 'package:pracma':
##
##     rk4
##
## Loading required package: rootSolve
##
## Attaching package: 'rootSolve'
##
## The following objects are masked from 'package:pracma':
##
##     gradient, hessian
##
## Loading required package: coda
## Loading required package: lattice
##
## Attaching package: 'FME'
##
## The following object is masked from 'package:pracma':
##
##     Norm
##
## Loading required package: timeDate
## Loading required package: timeSeries
##
## Attaching package: 'fBasics'
##
## The following object is masked from 'package:deSolve':
##
##     rk
##
## The following object is masked from 'package:binhf':
##
##     norm
##
## The following objects are masked from 'package:pracma':
##
##     akimaInterp, inv, kron, pascal
##
## The following object is masked from 'package:base':

```

```
##
```

```
## norm
```

se/CSV_M_SC/1

```
## 10  2.34 -1.487e-05 0.000e+00 -7.015e-06 0.000e+00
## 11  2.25 -1.119e-05 0.000e+00 -6.524e-06 0.000e+00
## 12  2.21 -1.406e-05 0.000e+00 -9.305e-06 0.000e+00
## 13  2.27 -2.178e-05 2.778e-09 -1.050e-05 1.389e-09
## 14  2.52 -1.354e-05 0.000e+00 -7.716e-06 0.000e+00
## 15  2.19 -1.220e-05 0.000e+00 -1.060e-05 0.000e+00
## 16  2.33 -1.509e-05 2.556e-08 -8.127e-06 0.000e+00
## 17  2.29 -1.355e-05 6.805e-09 -9.277e-06 0.000e+00
## 18  2.33 -1.649e-05 5.556e-09 -1.308e-05 0.000e+00
```

1.2 function to evaluate zeta

```
# ===== DIFFERENTIAL EQUATION =====
ZETA.01 <- function(Time, State, Parm){

# # ---- EFFECTIVE STRESS PARAMETERS FOR CRUSHED SALT FORMULATION OF MODEL ----
# KAP0 <- 10.119
# KAP1 <- 1.005
# DDT <- 0.896
# NK <- 1.331
# KAP2 <- 1
# ETA0 <- 0.102854
# ETA1 <- 3.9387
# ETA2 <- 1
# NF <- 3.5122

# ---- EFFECTIVE STRESS PARAMETERS FOR CRUSHED SALT FORMULATION OF MODEL ----
# # ---- VALUES FOR MATHCAD CHECK
KAP0 <- 10.119
KAP1 <- 1.005
NK <- 1.331
#-----
DDT <- 0.8854
KAP2 <- 1
ETA0 <- 0.015
ETA1 <- 1
ETA2 <- 0.7
NF <- 8.40075

# # ---- Munson-Dawson Creep Parameters (17) ---- FOR CLEAN SALT
# A1 <- 8.386e22
# A2 <- 9.672e12
# Q1R <- 12581
# Q2R <- 5033
# N1 <- 5.5
# N2 <- 5.0
# B1 <- 6.0856e6
# B2 <- 3.034e-2
# Q <- 5335
# S0 <- 20.57
# M <- 3
# K0 <- 6.275e5
# C <- 9.198e-3
# ALPHA <- -17.37
# BETA <- -7.738
# DELTA <- 0.58
# MU <- 12400

# ---- Munson-Dawson Creep Parameters (17) ---- FOR ARGILLACEOUS SALT
A1 <- 1.407e23
A2 <- 1.314e13
Q1R <- 12581
Q2R <- 5033
```

```

N1          <- 5.5
N2          <- 5.0
B1          <- 8.988e6
B2          <- 4.289e-2
Q           <- 5335
S0          <- 20.57
M           <- 3
K0          <- 2.47e6
C           <- 9.198e-3
ALPHA <- -14.96
BETA  <- -7.738
DELTA <- 0.58
MU     <- 12400

#---- DATA INTERPRETED FROM TEST DATA
# TEMP <- temp.interp(Time)
# AS   <- as.interp(Time)
# LS   <- ls.interp(Time)
# D    <- d.interp(Time)

#---- constant data values for comparison to Callahan's analysis
TEMP <- 300
AS   <- (-6/300.8)*Time
LS   <- (-2/300.8)*Time
D    <- 0.9

# ---- calculate variables ----
# browser()
MS <- (2.0 * LS + AS) / 3 # MEAN STRESS
DS <- LS - AS             # STRESS DIFFERENCE
DEN <- D                  # CURRENT FRACTIONAL DENSITY

Z3 <- State[1] # internal variable "zeta" for the transient function (FU)

VAR <- ifelse(DEN <= DDT, DDT, DEN)

# ---- Equivalent Stress ----
OMEGAA <- ((1 - DEN) * NF / (1 - (1 - DEN)^(1/NF)))^NF^(2/(NF + 1))
ETA    <- ETA0 * OMEGAA^ETA1
TERMA  <- ((2 - DEN)/DEN)^((2 * NF)/(NF + 1))

# ---- Eqn. 2-3 (SAND97-2601) ----
# Equivalent stress measure for Disl. Creep
SEQF <- sqrt(ETA * MS^2 + ETA2 * TERMA * DS^2)

# ==== START: equivalent inelastic strain rate form for dislocation creep ====
# ---- Steady State Strain Rate Calc ----
ES1 <- A1 * (SEQF / MU)^N1 * exp(-Q1R/TEMP) # Dislocation climb - Eqn. 2-30
ES2 <- A2 * (SEQF / MU)^N2 * exp(-Q2R/TEMP) # Undefined Mechanism - Eqn. 2-31

# Slip - Eqn. 2-32 (SAND98-2601)
# browser()
ARG <- Q * ((SEQF - S0) / MU)

```

```

ES3 <- (B1 * exp(-Q1R / TEMP) + B2 * exp(-Q2R / TEMP)) *
      sinh(ARG) * Heaviside(SEQF - S0)

ESS = ES1 + ES2 + ES3 # Steady-state strain rate, Eqn. 2-29 (SAND97-2601)

# ---- EVALUATE TRANSIENT FUNCTION, 3 branches: work hardening, equilibrium, recovery
# browser()
EFT <- K0 * exp(C * TEMP) * (SEQF / MU) ^ M # Transient Strain Limit, Eqn. 2-28
BIGD <- ALPHA + BETA * log10(SEQF / MU)      # Work-Hardening parameter, Eqn 2-28

FU <- ifelse(Z3 == EFT, 1, ifelse(Z3 < EFT, exp(BIGD * (1 - Z3 / EFT) ^ 2),
                                   exp(-DELTA * (1 - Z3 / EFT) ^ 2)))

MD <- FU * ESS # equivalent inelastic strain rate form for dislocation creep, Eqn 2-23

DZ3 <- (FU - 1) * ESS # derivative of internal variable "ZETA"
DZ <- list(c(DZ3), MD, FU, ESS, ES1, ES2, ES3,
           DZ3, EFT, SEQF, BIGD, AS, LS, ETA, OMEGAA)

return(DZ)
}

```

1.3 load settings for zeta function

```

# =====
PAR.TEST <- DATA.INP[which(DATA.INP$ITEST == "SC1B"),] # SUBSET OF DATA FOR ANALYSIS
# PAR.TEST <- PAR.TEST[1:28,]

# ---- linear interpolation functions to be called in "ZETA.01" ----
temp.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$TEMP)
as.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$AS)
ls.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$LS)
d.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$D)

# ---- intial values for state variables ----
Z3 <- 1e-12 # internal variable "ZETA" for the transient function (FU)
# integral of Eqn 2-27, (initial values)

IC <- (c(Z3 = Z3)) # array of initial values

# TIME <- PAR.TEST$TIME
TIME <- c(0, 50, 52.5, 65, 91.61, 126.101, 174.21, 240.386, 300) #for comparison

# ---- function for Predicting the Creep Strain(E) Rates ----
ZETA.ODE <- ode(func = ZETA.01, y = IC, times = TIME, verbose = TRUE,
               maxsteps = 1000000, rtol = 1e-14, atol = 1e-14, hmax = 1 )

##
## -----
## Time settings
## -----
##

```

```

## Normal computation of output values of y(t) at t = TOUT
##
## -----
## Integration settings
## -----
##
## Model function an R-function:
## Jacobian not specified
##
##
## -----
## lsoda return code
## -----
##
## return code (idid) = 2
## Integration was successful.
##
## -----
## INTEGER values
## -----
##
## 1 The return code : 2
## 2 The number of steps taken for the problem so far: 330
## 3 The number of function evaluations for the problem so far: 567
## 5 The method order last used (successfully): 5
## 6 The order of the method to be attempted on the next step: 5
## 7 If return flag =-4,-5: the largest component in error vector 0
## 8 The length of the real work array actually required: 36
## 9 The length of the integer work array actually required: 21
## 14 The number of Jacobian evaluations and LU decompositions so far: 0
## 15 The method indicator for the last succesful step,
##     1=adams (nonstiff), 2= bdf (stiff): 1
## 16 The current method indicator to be attempted on the next step,
##     1=adams (nonstiff), 2= bdf (stiff): 1
##
## -----
## RSTATE values
## -----
##
## 1 The step size in t last used (successfully): 1
## 2 The step size to be attempted on the next step: 1
## 3 The current value of the independent variable which the solver has reached: 300.6
## 4 Tolerance scale factor > 1.0 computed when requesting too much accuracy: 0
## 5 The value of t at the time of the last method switch, if any: 0
##

```