

```
## Warning: package 'pracma' was built under R version 3.1.1
```

```
## Loading required package: wavethresh
## Loading required package: MASS
## WaveThresh: R wavelet software, release 4.6.6, installed
##
## Copyright Guy Nason and others 1993-2013
##
## Note: nlevels has been renamed to nlevelsWT
##
## Loading required package: adlift
## Loading required package: EbayesThresh
##
## *****
## adlift: a package to perform wavelet lifting schemes
##
## --- Written by Matt Nunes and Marina Knight ---
## Current package version: 1.3-2 ( 01/11/2012 )
##
##      +- packaged by MAN +-
## *****
## adlift 1.3-2 loaded
##
##
## Attaching package: 'adlift'
##
## The following object is masked from 'package:EbayesThresh':
##
##   postmean.cauchy
##
## *****
## binhf: Haar-Fisz functions for binomial data
##
## --- Written by Matt Nunes ---
## Current package version: 1.0-1 ( 24/04/2014 )
##
## *****
## binhf 1.0-1 loaded
##
##
## Attaching package: 'binhf'
##
## The following objects are masked from 'package:EbayesThresh':
##
##   ebayesthresh.wavelet.wd, negloglik.laplace, wandafromx
##
## The following object is masked from 'package:wavethresh':
##
##   madmad
##
## The following object is masked from 'package:base':
##
##   norm
##
## Attaching package: 'deSolve'
```

```

##
## The following object is masked from 'package:pracma':
##
##      rk4
##
## Loading required package:  rootSolve
##
## Attaching package:  'rootSolve'
##
## The following objects are masked from 'package:pracma':
##
##      gradient, hessian
##
## Loading required package:  coda
## Loading required package:  lattice
##
## Attaching package:  'FME'
##
## The following object is masked from 'package:pracma':
##
##      Norm
##
## Loading required package:  timeDate
## Loading required package:  timeSeries
##
## Attaching package:  'fBasics'
##
## The following object is masked from 'package:deSolve':
##
##      rk
##
## The following object is masked from 'package:binhf':
##
##      norm
##
## The following objects are masked from 'package:pracma':
##
##      akimaInterp, inv, kron, pascal
##
## The following object is masked from 'package:base':
##
##      norm

```

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## 14	SC5A	2	61.339	-9.078	-8.651	-8.970	-6.938	-6.8880	
## 15	SC6A	2	67.914	-10.397	-9.534	-10.329	-6.971	-6.8860	
## 16	SC7A	2	65.968	-6.645	-6.447	-6.536	-5.203	-5.1440	
## 17	SC8A	2	60.767	-9.449	-7.590	-7.952	-5.188	-5.1480	
## 18	SC9B	2	60.937	-9.384	-8.139	-9.311	-5.203	-5.1370	
##	S.L.AVG	S.D.AVG	E.V.MIN	E.V.MAX	E.A.MIN	E.A.MAX	T.AVG	FD.MIN	FD.MAX
## 1	-3.256	0.4457	-0.174330	0	-0.08441		0 293.0	0.7018	0.8354
## 2	-1.014	3.9473	-0.017568	0	-0.15550		0 297.5	0.9258	0.9422
## 3	-4.999	4.0097	-0.068824	0	-0.09518		0 294.7	0.9170	0.9823
## 4	-1.008	4.0019	-0.033969	0	-0.15064		0 297.9	0.9073	0.9387
## 5	-2.000	3.9803	-0.060718	0	-0.14177		0 297.1	0.9092	0.9661
## 6	-3.003	3.9901	-0.061275	0	-0.13528		0 296.7	0.9312	0.9900
## 7	-4.000	3.9895	-0.069213	0	-0.14917		0 294.8	0.9043	0.9691
## 8	-1.003	4.9916	-0.006195	0	-0.01482		0 298.0	0.8373	0.8425
## 9	-1.025	4.9693	-0.021617	0	-0.04677		0 298.0	0.7813	0.7983
## 10	-3.439	0.6925	-0.243860	0	-0.09874		0 298.0	0.7286	0.9298
## 11	-3.459	1.3683	-0.225030	0	-0.11139		0 298.0	0.7445	0.9324
## 12	-3.454	2.0623	-0.241510	0	-0.13777		0 298.0	0.7291	0.9283
## 13	-6.894	0.6944	-0.222610	0	-0.09474		0 298.0	0.7439	0.9294
## 14	-6.916	2.0549	-0.190630	0	-0.09817		0 298.0	0.8167	0.9883
## 15	-6.912	3.4164	-0.188180	0	-0.12228		0 298.0	0.7874	0.9504
## 16	-5.173	1.3636	-0.227880	0	-0.10278		0 298.0	0.7706	0.9678
## 17	-5.167	2.7848	-0.216170	0	-0.13914		0 298.0	0.7461	0.9261
## 18	-5.165	4.1463	-0.212080	0	-0.16152		0 298.0	0.7791	0.9631
##	W.AVG	ER.V.MIN	ER.V.MAX	ER.A.MIN	ER.A.MAX				
## 1	2.40	-1.064e-06	0.000e+00	-5.177e-07	0.000e+00				
## 2	1.66	-1.208e-06	4.225e-09	-1.131e-05	0.000e+00				
## 3	1.49	-4.494e-06	7.194e-09	-4.622e-06	7.000e-06				
## 4	1.77	-7.282e-06	1.038e-09	-1.510e-05	0.000e+00				
## 5	1.63	-2.617e-06	0.000e+00	-3.613e-06	0.000e+00				
## 6	1.59	-1.827e-06	5.523e-08	-2.597e-06	0.000e+00				
## 7	1.55	-2.395e-06	3.822e-09	-2.329e-06	0.000e+00				
## 8	0.00	-1.986e-08	0.000e+00	-6.720e-08	0.000e+00				
## 9	0.00	-4.492e-06	0.000e+00	-1.512e-05	0.000e+00				
## 10	2.34	-1.487e-05	0.000e+00	-7.015e-06	0.000e+00				
## 11	2.25	-1.119e-05	0.000e+00	-6.524e-06	0.000e+00				
## 12	2.21	-1.406e-05	0.000e+00	-9.305e-06	0.000e+00				
## 13	2.27	-2.178e-05	2.778e-09	-1.050e-05	1.389e-09				
## 14	2.52	-1.354e-05	0.000e+00	-7.716e-06	0.000e+00				
## 15	2.19	-1.220e-05	0.000e+00	-1.060e-05	0.000e+00				
## 16	2.33	-1.509e-05	2.556e-08	-8.127e-06	0.000e+00				
## 17	2.29	-1.355e-05	6.805e-09	-9.277e-06	0.000e+00				
## 18	2.33	-1.649e-05	5.556e-09	-1.308e-05	0.000e+00				

```
#####
# SOLVE FOR THE STRAINS USING CALLAHAN'S MODEL
# TEST SC1B
#####

# ==== "events" function, for specifying step functions ====
# ---- SETS STRAINS AND RATES = 0 AT TIME == 0 ----
eventfun <- function(Time, State, Parm){
  with (as.list(State),{

    # ---- if time == 0, derivative = 0 ----
    DZ <- ifelse(c(Time == 0, Time == 0, Time == 0), {c(0, 0, 0)}, {DZ})

    return(DZ)
  })
}

# ==== DIFFERENTIAL EQUATION ====
STRAINS.02 <- function(Time, State, Parm){
  with(as.list(c(State, Parm)),{
    # function for calculating axial and lateral strain rates
    # Input must be in vector or matrix form, no data frames
    # Eqns. referenced from: SAND97-2601
    # CPar: EAT0, ETA1, ETA2, NF, AA1, PP, NSP, R1, R3, R4, QSR
    # FPar: KAP0, KAP1, KAP2, NK, DDT
    # TestData:

    # ===== parameters hard coded into function directly =====
    # browser()
    KAP0 <- 10.119
    KAP1 <- 1.005
    DDT <- 0.896
    NK <- 1.331
    KAP2 <- 1

    ETA0 <- 0.102854      # -
    ETA1 <- 3.9387        # -
    ETA2 <- 1             # constant -
    NF <- 3.5122          # -
    AA1 <- 0.3147          # -
    PP <- 1.6332           # -
    NSP <- 0.557621       # -
    R1 <- 1.041 * 10 ^ -6 # [K/(MPa-sec)]
    R3 <- 15.1281         # -
    R4 <- 0.1677765       # -
    QSR <- 1077.46        # [K]

    # ---- Munson-Dawson Creep Parameters (17) ----
    A1 <- 8.386e22
    A2 <- 9.672e12
    Q1R <- 12581
    Q2R <- 5033
    N1 <- 5.5
    N2 <- 5.0
    B1 <- 6.0856e6
    B2 <- 3.034e-2
    Q <- 5335
    S0 <- 20.57
    M <- 3
  })
}
```

```

KO          <- 6.275e5
C           <- 9.198e-3
ALPHA <- -17.37
BETA        <- -7.738
DELTA <- 0.58
MU          <- 12400

# ---- fitting assumptions ----
RHOIS <- 2160.0 # ASSUMED IN SITU SALT DENSITY

# ---- interpolated input variables ----
TIME <- time.interp(Time)
# browser()
TEMP <- temp.interp(Time)
AS   <- as.interp(Time)
LS   <- ls.interp(Time)
D    <- d.interp(Time)

# ---- calculate variables ----
MS <- (2.0 * LS + AS) / 3 # MEAN STRESS
DS <- LS - AS             # STRESS DIFFERENCE
# ELC <- (EVC - EAC) / 2 # CREEP TRUE LATERAL STRAIN
DO <- 1382.4 / RHOIS      # EMPLACED FRACTIONAL DENSITY (0.64 FRAC DENSITY)
DI <- RHOI / RHOIS        # FRACTIONAL DENSITY at the start of creep

# ==== this portion has been moved to lambda <- function() ====
#WT1 <- DT / NTIME # WEIGHTING FUNCTION FOR CREEP CONSOLIDATION PARAMETERS
#WT  <- 1 # WEIGHTING FUNCTION FOR FLOW PARAMETERS
# =====
# integral of Eqn 2-27, (initial values)

# ==== define the differential equation ====
# browser()
VOL      <- Z1 + 2*Z2 # TRUE VOLUMETRIC STRAIN
VOLT     <- VOL + log(DO/DI) # VOLUMETRIC STRAIN + INITIAL TRUE STRAIN ESTIMATE
DEN      <- DI/exp(VOL) # CURRENT FRACTIONAL DENSITY

# ifelse(D >= 1,{
#   MD <- 0 # if fractional density is 1, dislocation creep = 0
#   SP <- 0},# if fractional density is 1, pressure solutioning = 0
# {VAR <- ifelse(DEN <= DDT, DDT, DEN) # DEFINE DENSITY CEILING ISH

VAR <- ifelse(DEN <= DDT, DDT, DEN) # DEFINE DENSITY floor ISH
# ==== DEBUG ====
DEBUG.VAR <- ifelse(DEN <= DDT, 1, -1)

# ---- Equivalent Stress ----
OMEGAA <- ((1 - DEN) * NF / (1 - (1 - DEN)^(1/NF)))^NF^(2/(NF + 1))
OMEGAK <- ((1 - VAR) * NK / (1 - (1 - VAR)^(1/NK)))^NK^(2/(NK + 1))
ETA     <- ETA0 * OMEGAA^ETA1
KAP     <- KAP0 * OMEGAK^KAP1
TERMA   <- ((2 - DEN)/DEN)^((2 * NF)/(NF + 1))
TERMK   <- ((2 - DEN)/DEN)^((2 * NK)/(NK + 1))

# ---- Eqn. 2-3 (SAND97-2601) ----
# Equivalent stress measure for Disl. Creep and Press Sol'ing
SEQF <- sqrt(ETA * MS^2 + ETA2 * TERMA * DS^2)
# Equivalent stress measure for Flow Potential
SEQ  <- sqrt(KAP * MS^2 + KAP2 * TERMK * DS^2)

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# ---- Eqn. 2-17 (SAND97-2601) ----
ALPHA2 <- KAP * MS / 3
BETA2 <- KAP2 * TERMK * DS

# ---- Eqn. 2-20, WithOUT dislocation creep and pressure solutioning ----
F2A <- (ALPHA2 - BETA2)/SEQ # fit to axial strains
F2L <- (ALPHA2 + 0.5 * BETA2)/SEQ # fit to lateral strains
F2V <- 3 * ALPHA2 / SEQ # fit to volumetric strains

# ==== START: equivalent inelastic strain rate form for dislocation creep ====

# ---- Steady State Strain Rate Calc ----
ES1 <- A1 * (SEQF / MU)^N1 * exp(-Q1R/TEMP) # Dislocation climb - Eqn. 2-30
ES2 <- A2 * (SEQF / MU)^N2 * exp(-Q2R/TEMP) # Undefined Mechanism - Eqn. 2-31

# Slip - Eqn. 2-32 (SAND98-2601)
H <- SEQF - S0 # HEAVISIDE FUNCTION
ARG <- Q * (SEQF - S0) / MU
ES3 <- ifelse(H >= 0, 0.5 * (B1 * exp(-Q1R / TEMP) + B2 * exp(-Q2R / TEMP)) *
              (exp(ARG) - exp(-ARG)),0)
# ==== DEBUG ====
DEBUG.ES3 <- ifelse(H >=0, 1, -1)

ESS = ES1 + ES2 + ES3 # Steady-state strain rate, Eqn. 2-29 (SAND97-2601)

# ---- EVALUATE TRANSIENT FUNCTION, 3 branches: work hardening, equilibrium, recovery
EFT <- K0 * exp(C * TEMP) * (SEQF / MU) ^ M # Transient Strain Limit, Eqn. 2-28
BIGD <- ALPHA + BETA * log10(SEQF / MU) # Work-Hardening parameter, Eqn 2-28

FU <- ifelse(Z3 == EFT, 1, ifelse(Z3 < EFT, exp(BIGD * (1 - Z3 / EFT) ^ 2),
                                exp(-DELTA * (1 - Z3 / EFT) ^ 2)))

# ==== DEBUG ====
DEBUG.FU <- ifelse(Z3 == EFT, 0, ifelse(Z3 < EFT, -1, 1))

MD <- FU * ESS # equivalent inelastic strain rate form for dislocation creep, Eqn 2-23

# ==== START: Equivalent Inelastic Strain Rate Form for Pressure Solutioning ====
# ---- Calculate initial volumetric strain - Based on spherical packing ----
CR <- abs(exp(VOLT) - 1) # USES THE DEFINITION OF ENGINEERING STRAIN

# ---- Determine functional form - either large or small strains, Eqn 2-34 ----
GAMMA <- ifelse(CR <= 0.15, 1, (abs((DO - exp(VOLT)) / ((1 - DO) * exp(VOLT)))) ^ NSP)
# Small Strains (Vol Strain > - 15%)
# Large Strains (Vol Strain < - 15%)
# ==== DEBUG ====
DEBUG.GAMMA <- ifelse(CR <= 0.15, 1,-1)

# ---- component of eqn 2-35 ---
X3 <- exp((R3 - 1) * VOLT) / (abs(1 - exp(VOLT))) ^ R4

# ---- determine value of moisture function (w) ----
M2 <- ifelse (W == 0, 0, W ^ AA1)

# ---- Equivalent Inelastic Strain Rate Form for Pressure Solutioning, Eqn 2-35
G2 <- 1 / DD ^ PP # calculate grain size function
T2 <- exp(-QSR / TEMP) / TEMP
SP <- R1 * M2 * G2 * T2 * X3 * GAMMA * SEQF #})

```

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DZ1 <- (MD + SP) * F2A # derivative: axial strain rate
DZ2 <- (MD + SP) * F2L # derivative: lateral strain rate
DZ3 <- (FU - 1) * ESS # derivative of internal variable "xi"
# browser()
DZ <- list(c(DZ1, DZ2, DZ3), MD, FU, ESS, ES1, ES2, ES3, SP, DZ1, DZ2,
           DZ3, F2A, F2L, EFT, SEQ, SEQF, BIGD, DEBUG.GAMMA,
           DEBUG.ES3, AS, LS, OMEGAA, OMEGAK, VAR, DEN)

return(DZ)
})
}

PAR.TEST <- DATA.INP[which(DATA.INP$ITEST == "SC1B"),] # SUBSET OF DATA FOR ANALYSIS
# debug.out <- paste(CurrentDirectory, "debug_SC1B.csv", sep = "/")
# write.table(ODE.DT, file = debug.out, sep = ",")

# ---- linear interpolation functions to be called in "strain_Rates.01" ----
time.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$TIME)
temp.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$TEMP)
# as.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$AS)
# ls.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$LS)
as.interp <- approxfun(x = DATA.BEAN$TIME, y = DATA.BEAN$STRESS_YY / 10^6)
ls.interp <- approxfun(x = DATA.BEAN$TIME, y = DATA.BEAN$STRESS_XX / 10^6)

d.interp <- approxfun(x = PAR.TEST$TIME, y = PAR.TEST$D)

RHOI <- as.numeric(PAR.TEST$RHOI[1]) # DENSITY AT THE START OF CREEP
DD <- as.numeric(PAR.TEST$DD[1]) # AVERAGE GRAIN SIZE [MM]
W <- as.numeric(PAR.TEST$W[1]) # WATER CONENT BY PERCENT WEIGHT

PARM <- c(RHOI = RHOI, DD = DD, W = W) # CONSTANT TEST SPECIFIC PARAMETERS

# ---- intial values for state variables ----
Z1 <- 0 # Predicted axial strain (initial values)
Z2 <- 0 # Predicted lateral strain (initial values)
Z3 <- 0 # internal variable "xi" for the transient function (FU)
# integral of Eqn 2-27, (initial values)

IC <- (c(Z1 = Z1, Z2 = Z2, Z3 = Z3)) # array of initial values

TIME <- DATA.BEAN$TIME

# ---- function for Predicting the Creep Strain(E) Rates ----
P.CER <- ode(func = STRAINS.02, parms = PARM, y = IC,
            times = TIME, verbose = TRUE)#, events = list(func = eventfun, time = 0),

##
## -----
## Time settings
## -----
##
## Normal computation of output values of y(t) at t = TOUT
##
## -----
## Integration settings
## -----
##
## Model function an R-function:
## Jacobian not specified

```

```

##
##
## -----
## lsoda return code
## -----
##
##   return code (idid) =  2
##   Integration was successful.
##
## -----
## INTEGER values
## -----
##
##   1 The return code : 2
##   2 The number of steps taken for the problem so far: 116
##   3 The number of function evaluations for the problem so far: 238
##   5 The method order last used (successfully): 4
##   6 The order of the method to be attempted on the next step: 4
##   7 If return flag =-4,-5: the largest component in error vector 0
##   8 The length of the real work array actually required: 68
##   9 The length of the integer work array actually required: 23
##  14 The number of Jacobian evaluations and LU decompositions so far: 0
##  15 The method indicator for the last succesful step,
##       1=adams (nonstiff), 2= bdf (stiff): 1
##  16 The current method indicator to be attempted on the next step,
##       1=adams (nonstiff), 2= bdf (stiff): 1
##
## -----
## RSTATE values
## -----
##
##   1 The step size in t last used (successfully): 252000
##   2 The step size to be attempted on the next step: 252000
##   3 The current value of the independent variable which the solver has reached: 5548000
##   4 Tolerance scale factor > 1.0 computed when requesting too much accuracy: 0
##   5 The value of t at the time of the last method switch, if any: 0
##

```