

# Mathematical Preliminaries

Introductory Course on Multiphysics Modelling

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## 1 Vectors, tensors, and index notation

### 1.1 Generalization of the concept of vector

- A **vector** is a quantity that possesses both a **magnitude** and a **direction** and obeys certain laws (of **vector algebra**): the vector addition and the commutative and associative laws, the associative and distributive laws for the multiplication with scalars.
- The vectors are suited to describe physical phenomena, since they are **independent of any system of reference**.

The **concept of a vector** that is independent of any coordinate system **can be generalised** to higher-order quantities, which are called **tensors**. Consequently, vectors and scalars can be treated as lower-rank tensors.

**Scalars** have a magnitude but no direction. They are tensors of order 0. *Example:* the mass density.

**Vectors** are characterised by their magnitude and direction. They are tensors of order 1.  
*Example:* the velocity vector.

**Tensors of second order** are quantities which multiplied by a vector give as the result another vector. *Example:* the stress tensor.

**Higher-order tensors** are often encountered in constitutive relations between second-order tensor quantities. *Example:* the fourth-order elasticity tensor.

## 1.2 Summation convention and index notation

### *Einstein's summation convention*

A summation is carried out over repeated indices in an expression. (The summation sign is skipped.)

*Example 1.*

$$\begin{aligned}
 a_i b_i &\equiv \sum_{i=1}^3 a_i b_i = a_1 b_1 + a_2 b_2 + a_3 b_3 \\
 A_{ii} &\equiv \sum_{i=1}^3 A_{ii} = A_{11} + A_{22} + A_{33} \\
 A_{ij} b_j &\equiv \sum_{j=1}^3 A_{ij} b_j = A_{i1} b_1 + A_{i2} b_2 + A_{i3} b_3 \quad (i = 1, 2, 3) \quad [3 \text{ expressions}] \\
 T_{ij} S_{ij} &\equiv \sum_{i=1}^3 \sum_{j=1}^3 T_{ij} S_{ij} = T_{11} S_{11} + T_{12} S_{12} + T_{13} S_{13} \\
 &\quad + T_{21} S_{21} + T_{22} S_{22} + T_{23} S_{23} \\
 &\quad + T_{31} S_{31} + T_{32} S_{32} + T_{33} S_{33}
 \end{aligned}$$

*The principles of index notation:*

- **An index cannot appear more than twice in one term!** If necessary, the normal summation symbol must be used. A repeated index is called a **bound** or **dummy index**.

*Example 2.*

$$\begin{aligned}
 A_{ii}, \quad C_{ijkl} S_{kl}, \quad A_{ij} b_i c_j &\leftarrow \text{Correct} \\
 A_{ij} b_j c_j &\leftarrow \text{Wrong!} \\
 \sum_j A_{ij} b_j c_j &\leftarrow \text{Correct}
 \end{aligned}$$

A term with more than two-times-repeated index is correct if:

- the summation sign is used, e.g.:  $\sum_i a_i b_i c_i = a_1 b_1 c_1 + a_2 b_2 c_2 + a_3 b_3 c_3$ , or
- the dummy index is underlined, e.g.:  $a_{\underline{i}} b_{\underline{i}} c_{\underline{i}} = a_1 b_1 c_1 + a_2 b_2 c_2 + a_3 b_3 c_3$ .
- If the index appears once, it is called a **free index**. The number of free indices determines the order of a tensor.

Example 3.

$$\begin{aligned} A_{ii}, \quad a_i b_i, \quad T_{ij} S_{ij} &\leftarrow \text{scalars (no free indices)} \\ A_{ij} b_j &\leftarrow \text{a vector (one free index: } i) \\ C_{ijkl} S_{kl} &\leftarrow \text{a second-order tensor (two free indices: } i, j) \end{aligned}$$

- The denomination of a dummy index (in a term) is arbitrary since it vanishes after the summation, thus,  $a_i b_i \equiv a_j b_j$ .

Example 4.

$$\begin{aligned} a_i b_i &= a_1 b_1 + a_2 b_2 + a_3 b_3 = a_j b_j \\ A_{ii} &\equiv A_{jj}, \quad T_{ij} S_{ij} \equiv T_{kl} S_{kl}, \quad T_{ij} + C_{ijkl} S_{kl} \equiv T_{ij} + C_{ijmn} S_{mn} \end{aligned}$$

### 1.3 Kronecker delta and permutation symbol

**Definition 5** (Kronecker delta).

$$\delta_{ij} = \begin{cases} 1 & \text{for } i = j \\ 0 & \text{for } i \neq j \end{cases}$$

- The Kronecker delta can be used to substitute one index by another, for example:  
 $a_i \delta_{ij} = a_1 \delta_{1j} + a_2 \delta_{2j} + a_3 \delta_{3j} = a_j$ .
- When Cartesian coordinates are used (with orthonormal base vectors  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$ ) the Kronecker delta  $\delta_{ij}$  is the **(matrix) representation** of the **unity tensor**  $\mathbf{I} = \delta_{ij} \mathbf{e}_i \otimes \mathbf{e}_j = \mathbf{e}_1 \otimes \mathbf{e}_1 + \mathbf{e}_2 \otimes \mathbf{e}_2 + \mathbf{e}_3 \otimes \mathbf{e}_3$ .
- $\mathbf{A} \cdot \mathbf{I} = A_{ij} \delta_{ij} = A_{ii}$  which is the **trace** of the matrix (tensor)  $\mathbf{A}$ .

**Definition 6** (Permutation symbol).

$$\epsilon_{ijk} = \begin{cases} 1 & \text{for even permutations: 123, 231, 312} \\ -1 & \text{for odd permutations: 132, 321, 213} \\ 0 & \text{if an index is repeated} \end{cases}$$

The permutation symbol (or tensor) is widely used in index notation to express the **vector** or **cross product** of two vectors:

$$\mathbf{c} = \mathbf{a} \times \mathbf{b} = \begin{vmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix} \rightarrow c_i = \epsilon_{ijk} a_j b_k \rightarrow \begin{cases} c_1 = a_2 b_3 - a_3 b_2 \\ c_2 = a_3 b_1 - a_1 b_3 \\ c_3 = a_1 b_2 - a_2 b_1 \end{cases}$$

## 1.4 Tensors and their representations

### Informal definition of tensor

A **tensor** is a generalized **linear ‘quantity’** that can be expressed as a **multi-dimensional array** relative to a choice of basis of the particular space on which it is defined. Thus,

- a tensor is independent of any chosen frame of reference,
- its representation behaves in a specific way under coordinate transformations.

### Cartesian system of reference

Let  $\mathcal{E}^3$  be the three-dimensional **Euclidean space** with a **Cartesian coordinate system** with three **orthonormal base vectors**  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$ , so that

$$\mathbf{e}_i \cdot \mathbf{e}_j = \delta_{ij} \quad (i, j = 1, 2, 3).$$

- A **second-order tensor**  $\mathbf{T} \in \mathcal{E}^3 \otimes \mathcal{E}^3$  is defined by

$$\begin{aligned} \mathbf{T} := T_{ij} \mathbf{e}_i \otimes \mathbf{e}_j &= T_{11} \mathbf{e}_1 \otimes \mathbf{e}_1 + T_{12} \mathbf{e}_1 \otimes \mathbf{e}_2 + T_{13} \mathbf{e}_1 \otimes \mathbf{e}_3 \\ &\quad + T_{21} \mathbf{e}_2 \otimes \mathbf{e}_1 + T_{22} \mathbf{e}_2 \otimes \mathbf{e}_2 + T_{23} \mathbf{e}_2 \otimes \mathbf{e}_3 \\ &\quad + T_{31} \mathbf{e}_3 \otimes \mathbf{e}_1 + T_{32} \mathbf{e}_3 \otimes \mathbf{e}_2 + T_{33} \mathbf{e}_3 \otimes \mathbf{e}_3 \end{aligned}$$

where  $\otimes$  denotes the tensorial (or dyadic) product, and  $T_{ij}$  is the **(matrix) representation** of  $\mathbf{T}$  in the given frame of reference defined by the base vectors  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$ .

- The second-order tensor  $\mathbf{T} \in \mathcal{E}^3 \otimes \mathcal{E}^3$  can be viewed as a **linear transformation** from  $\mathcal{E}^3$  onto  $\mathcal{E}^3$ , meaning that it transforms every vector  $\mathbf{v} \in \mathcal{E}^3$  into another vector from  $\mathcal{E}^3$  as follows

$$\begin{aligned} \mathbf{T} \cdot \mathbf{v} &= (T_{ij} \mathbf{e}_i \otimes \mathbf{e}_j) \cdot (v_k \mathbf{e}_k) = T_{ij} v_k \overbrace{(\mathbf{e}_j \cdot \mathbf{e}_k)}^{\delta_{jk}} \mathbf{e}_i \\ &= T_{ij} v_k \delta_{jk} \mathbf{e}_i = T_{ij} v_j \mathbf{e}_i = w_i \mathbf{e}_i = \mathbf{w} \in \mathcal{E}^3 \quad \text{where} \quad w_i = T_{ij} v_j \end{aligned}$$

- A **general tensor of order  $n$**  is defined by

$$\mathbf{T}_n := T_{ijk\dots} \underbrace{\mathbf{e}_i \otimes \mathbf{e}_j \otimes \mathbf{e}_k \otimes \dots}_{n \text{ terms}},$$

$n \text{ indices}$

where  $T_{ijk\dots}$  is its **( $n$ -dimensional array) representation** in the given frame of reference.

*Example 7.* Let  $\mathbf{C} \in \mathcal{E}^3 \otimes \mathcal{E}^3 \otimes \mathcal{E}^3 \otimes \mathcal{E}^3$  and  $\mathbf{S} \in \mathcal{E}^3 \otimes \mathcal{E}^3$ . The fourth-order tensor  $\mathbf{C}$  describes a linear transformation in  $\mathcal{E}^3 \otimes \mathcal{E}^3$ :

$$\begin{aligned} \mathbf{C} \bullet \mathbf{S} &= \mathbf{C} : \mathbf{S} = (C_{ijkl} \mathbf{e}_i \otimes \mathbf{e}_j \otimes \mathbf{e}_k \otimes \mathbf{e}_l) : (S_{mn} \mathbf{e}_m \otimes \mathbf{e}_n) \\ &= C_{ijkl} S_{mn} (\mathbf{e}_k \cdot \mathbf{e}_m) (\mathbf{e}_l \cdot \mathbf{e}_n) \mathbf{e}_i \otimes \mathbf{e}_j \\ &= C_{ijkl} S_{mn} \delta_{km} \delta_{ln} \mathbf{e}_i \otimes \mathbf{e}_j = C_{ijkl} S_{kl} \mathbf{e}_i \otimes \mathbf{e}_j \\ &= T_{ij} \mathbf{e}_i \otimes \mathbf{e}_j = \mathbf{T} \in \mathcal{E}^3 \otimes \mathcal{E}^3 \quad \text{where} \quad T_{ij} = C_{ijkl} S_{kl} \end{aligned}$$

## 1.5 Multiplication of vectors and tensors

*Example 8.* Let:  $s$  be a scalar (a zero-order tensor),  $\mathbf{v}, \mathbf{w}$  be vectors (first-order tensors),  $\mathbf{R}, \mathbf{S}, \mathbf{T}$  be second-order tensors,  $\mathbf{D}$  be a third-order tensor, and  $\mathbf{C}$  be a fourth-order tensor. The order of tensors is shown explicitly in the expressions below.

$$\begin{aligned}
 s &= \underset{0}{\mathbf{v}} \bullet \underset{1}{\mathbf{w}} = \underset{1}{\mathbf{v}} \underset{1}{\mathbf{w}} = \underset{1}{\mathbf{v}} \cdot \underset{1}{\mathbf{w}} \rightarrow v_i w_i = s \\
 \underset{1}{\mathbf{v}} &= \underset{2}{\mathbf{T}} \underset{1}{\mathbf{w}} = \underset{2}{\mathbf{T}} \cdot \underset{1}{\mathbf{w}} \rightarrow T_{ij} w_j = v_i \\
 \underset{2}{\mathbf{R}} &= \underset{2}{\mathbf{T}} \underset{2}{\mathbf{S}} = \underset{2}{\mathbf{T}} \cdot \underset{2}{\mathbf{S}} \rightarrow T_{ij} S_{jk} = R_{ik} \\
 s &= \underset{0}{\mathbf{T}} \bullet \underset{2}{\mathbf{S}} = \underset{2}{\mathbf{T}} : \underset{2}{\mathbf{S}} \rightarrow T_{ij} S_{ij} = s \\
 \underset{2}{\mathbf{T}} &= \underset{4}{\mathbf{C}} \bullet \underset{2}{\mathbf{S}} = \underset{4}{\mathbf{C}} : \underset{2}{\mathbf{S}} \rightarrow C_{ijkl} S_{kl} = T_{ij} \\
 \underset{2}{\mathbf{T}} &= \underset{1}{\mathbf{v}} \underset{3}{\mathbf{D}} = \underset{1}{\mathbf{v}} \cdot \underset{3}{\mathbf{D}} \rightarrow v_k D_{kij} = T_{ij}
 \end{aligned}$$

*Remark:* Notice a vital difference between the two dot-operators ‘ $\bullet$ ’ and ‘ $\cdot$ ’. To avoid ambiguity, usually, the operators ‘ $:$ ’ and ‘ $\cdot$ ’ are not used, and the dot-operator has the meaning of the (full) dot-product, so that  $C_{ijkl} S_{kl} \rightarrow \mathbf{C} \bullet \mathbf{S}$ ,  $T_{ij} S_{ij} \rightarrow \mathbf{T} \bullet \mathbf{S}$ , and  $T_{ij} S_{jk} \rightarrow \mathbf{T} \mathbf{S}$ .

## 1.6 Vertical-bar convention and Nabla-operator

### Vertical-bar convention

The **vertical-bar (or comma) convention** is used to facilitate the denomination of partial derivatives with respect to the Cartesian position vectors  $\mathbf{x} \sim x_i$ , for example,

$$\frac{\partial \mathbf{u}}{\partial \mathbf{x}} \rightarrow \frac{\partial u_i}{\partial x_j} =: u_{i|j}$$

**Definition 9** (Nabla-operator).

$$\nabla \equiv (\cdot)_{|i} \mathbf{e}_i = (\cdot)_{|1} \mathbf{e}_1 + (\cdot)_{|2} \mathbf{e}_2 + (\cdot)_{|3} \mathbf{e}_3$$

The **gradient**, **divergence**, **curl (rotation)**, and **Laplacian** operations can be written using the **Nabla-operator**:

$$\begin{aligned}
 \mathbf{v} &= \text{grad } s \equiv \nabla s \rightarrow v_i = s_{|i} \\
 \mathbf{T} &= \text{grad } \mathbf{v} \equiv \nabla \otimes \mathbf{v} \rightarrow T_{ij} = v_{i|j} \\
 s &= \text{div } \mathbf{v} \equiv \nabla \cdot \mathbf{v} \rightarrow s = v_{i|i} \\
 \mathbf{v} &= \text{div } \mathbf{T} \equiv \nabla \cdot \mathbf{T} \rightarrow v_i = T_{ji|i} \\
 \mathbf{w} &= \text{curl } \mathbf{v} \equiv \nabla \times \mathbf{v} \rightarrow w_i = \epsilon_{ijk} v_{k|j} \\
 \text{lapl}(\cdot) &\equiv \Delta(\cdot) \equiv \nabla^2(\cdot) \rightarrow (\cdot)_{|ii}
 \end{aligned}$$

*Some vector calculus identities:*

$$\bullet \quad \boxed{\nabla \times (\nabla s) = \mathbf{0}} \quad (\text{curl grad} = \mathbf{0})$$

*Proof.*

$$\nabla \times (\nabla s) = \epsilon_{ijk} (s_{|k})_{|j} = \epsilon_{ijk} s_{|kj} = \begin{cases} \text{for } i = 1: s_{|23} - s_{|32} = 0 \\ \text{for } i = 2: s_{|31} - s_{|13} = 0 \\ \text{for } i = 3: s_{|12} - s_{|21} = 0 \end{cases}$$

□

- $\boxed{\nabla \cdot (\nabla \times \mathbf{v}) = 0}$  (div curl = 0)

*Proof.*

$$\nabla \cdot (\nabla \times \mathbf{v}) = (\epsilon_{ijk} v_{k|j})_{|i} = \epsilon_{ijk} v_{k|ji} = (v_{3|21} - v_{3|12}) + (v_{1|32} - v_{1|23}) + (v_{2|13} - v_{2|31}) = 0$$

□

- $\boxed{\nabla \times (\nabla \times \mathbf{v}) = \nabla(\nabla \cdot \mathbf{v}) - \nabla^2 \mathbf{v}}$  (curl curl = grad div – lapl)

*Proof.*

$$\begin{aligned} \nabla \times (\nabla \times \mathbf{v}) &\rightarrow \epsilon_{mni} (\epsilon_{ijk} v_{k|j})_{|n} = \epsilon_{mni} \epsilon_{ijk} v_{k|jn} \\ \text{for } m = 1: \epsilon_{1ni} \epsilon_{ijk} v_{k|jn} &= \epsilon_{123} (\epsilon_{312} v_{2|12} + \epsilon_{321} v_{1|22}) + \epsilon_{132} (\epsilon_{213} v_{3|13} + \epsilon_{231} v_{1|33}) \\ &= (v_{2|2} + v_{3|3})_{|1} - (v_{1|22} + v_{1|33}) \\ &= (v_{1|1} + v_{2|2} + v_{3|3})_{|1} - (v_{1|11} + v_{1|22} + v_{1|33}) \\ &= (v_{i|i})_{|1} - v_{1|ii} = (\nabla \cdot \mathbf{v})_{|1} - \nabla^2 v_1 \\ \text{for } m = 2: \epsilon_{2ni} \epsilon_{ijk} v_{k|jn} &= (v_{i|i})_{|2} - v_{2|ii} = (\nabla \cdot \mathbf{v})_{|2} - \nabla^2 v_2 \\ \text{for } m = 3: \epsilon_{3ni} \epsilon_{ijk} v_{k|jn} &= (v_{i|i})_{|3} - v_{3|ii} = (\nabla \cdot \mathbf{v})_{|3} - \nabla^2 v_3 \end{aligned}$$

□

## 2 Integral theorems

### 2.1 General idea

**Integral theorems** of vector calculus,

- the **classical (Kelvin-)Stokes' theorem** (the curl theorem),
- **Green's theorem**,
- **Gauss theorem** (the Gauss-Ostrogradsky divergence theorem),

are special cases of the **general Stokes' theorem**, which generalizes the **fundamental theorem of calculus**.

**Fundamental theorem of calculus** relates scalar integral to boundary points:

$$\int_a^b f'(x) dx = f(b) - f(a)$$

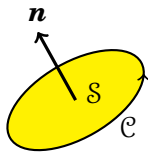
**Stokes's (curl) theorem** relates surface integrals to line integrals. *Applications:* e.g. conservative forces.

**Green's theorem** is a two-dimensional special case of Stokes' theorem.

**Gauss (divergence) theorem** relates volume integrals to surface integrals. *Applications:* analysis of flux, pressure.

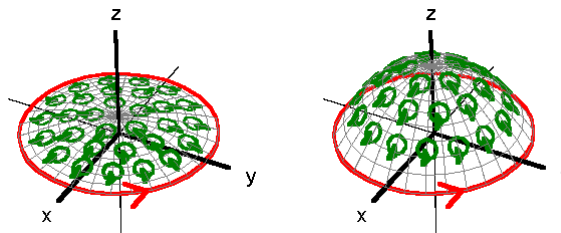
## 2.2 Stokes' theorem

**Theorem 10** (Stokes' curl theorem). *Let  $\mathcal{C}$  be a simple closed curve spanned by a surface  $\mathcal{S}$  with unit normal  $\mathbf{n}$ . Then, for a continuously differentiable vector field  $\mathbf{f}$ :*



$$\int_{\mathcal{S}} (\nabla \times \mathbf{f}) \cdot \underbrace{\mathbf{n}}_{d\mathbf{S}} dS = \int_{\mathcal{C}} \mathbf{f} \cdot d\mathbf{r}$$

- *Formal requirements:* the surface  $\mathcal{S}$  must be open, orientable and piecewise smooth with correspondingly orientated, simple, piecewise smooth boundary (curve)  $\mathcal{C}$ .
- Stokes' theorem implies that **the flux** of  $\nabla \times \mathbf{f}$  **through a surface  $\mathcal{S}$**  depends only on the boundary  $\mathcal{C}$  of  $\mathcal{S}$  and is therefore **independent of the surface's shape**.



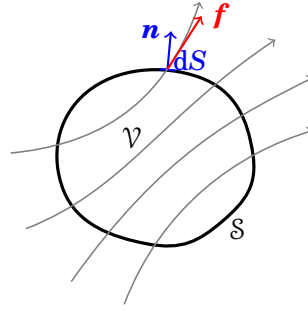
- **Green's theorem in the plane** may be viewed as a special case of Stokes' theorem (with  $\mathbf{f} = [u(x, y), v(x, y), 0]$ ):

$$\int_{\mathcal{S}} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) dx dy = \int_{\mathcal{C}} u dx + v dy$$

## 2.3 Gauss-Ostrogradsky theorem

**Theorem 11** (Gauss divergence theorem). *Let the region  $\mathcal{V}$  be bounded by a simple surface  $\mathcal{S}$  with unit outward normal  $\mathbf{n}$ . Then, for a continuously differentiable vector field  $\mathbf{f}$ :*

$$\int_{\mathcal{V}} \nabla \cdot \mathbf{f} dV = \int_{\mathcal{S}} \mathbf{f} \cdot \underbrace{\mathbf{n}}_{d\mathbf{S}} dS; \quad \text{in particular} \quad \int_{\mathcal{V}} \nabla f dV = \int_{\mathcal{S}} f \mathbf{n} dS.$$



- The divergence theorem is a result that relates the flow (that is, flux) of a vector field through a surface to the behavior of the vector field inside the surface.
- Intuitively, it states that the sum of all sources minus the sum of all sinks gives the net flow out of a region.

### 3 Time-harmonic approach

**Dynamic problems.** In dynamic problems, the field variables depend upon position  $\mathbf{x}$  and time  $t$ , for example,  $u = u(\mathbf{x}, t)$ .

**Separation of variables.** In many cases, the governing PDEs can be solved by expressing  $u$  as a product of functions that each depend only on one of the independent variables:  $u(\mathbf{x}, t) = \hat{u}(\mathbf{x})\check{u}(t)$ .

**Steady state.** A system is in steady state if its recently observed behaviour will continue into the future. An opposite situation is called the transient state which is often a start-up in many steady state systems. An important case of steady state is the time-harmonic behaviour.

**Time-harmonic solution.** If the time-dependent function  $\check{u}(t)$  is a time-harmonic function (with the frequency  $f$ ), the solution can be written as

$$u(\mathbf{x}, t) = \hat{u}(\mathbf{x}) \cos(\omega t + \alpha(\mathbf{x}))$$

where  $\omega = 2\pi f$  is called the **circular** (or **angular**) **frequency**,  $\alpha(\mathbf{x})$  is the **phase-angle shift**, and  $\hat{u}(\mathbf{x})$  can be interpreted as a **spatial amplitude**.

#### Complex notation of time-harmonic problems

A convenient way to handle time-harmonic problems is in **complex notation** with the real-part as a physically meaningful solution:

$$\begin{aligned} u(\mathbf{x}, t) &= \hat{u}(\mathbf{x}) \cos(\omega t + \alpha(\mathbf{x})) = \hat{u} \Re \left\{ \overbrace{\cos(\omega t + \alpha) + i \sin(\omega t + \alpha)}^{\exp[i(\omega t + \alpha)]} \right\} \\ &= \hat{u} \Re \{ \exp[i(\omega t + \alpha)] \} = \Re \left\{ \underbrace{\hat{u} \exp(i\alpha)}_{\tilde{u}} \exp(i\omega t) \right\} = \Re \{ \tilde{u} \exp(i\omega t) \} \end{aligned}$$

where the so-called **complex amplitude** (or **phasor**) is introduced:

$$\tilde{u} = \tilde{u}(\mathbf{x}) = \hat{u}(\mathbf{x}) \exp(i\alpha(\mathbf{x})) = \hat{u}(\mathbf{x}) (\cos \alpha(\mathbf{x}) + i \sin \alpha(\mathbf{x}))$$



**Example 12.** Consider a **linear dynamic system** characterized by the matrices of stiffness  $K$ , damping  $C$ , and mass  $M$ :

$$K q(t) + C \dot{q}(t) + M \ddot{q}(t) = Q(t)$$

where  $Q(t)$  is the dynamic excitation (a time-varying force) and  $q(t)$  is the system's response (displacement).

- Let the driving force  $Q(t)$  be harmonic with the angular frequency  $\omega$  and the (real) amplitude  $\hat{Q}$ :

$$Q(t) = \hat{Q} \cos(\omega t) = \hat{Q} \Re\{\cos(\omega t) + i \sin(\omega t)\} = \Re\{\hat{Q} \exp(i\omega t)\}$$

- Since the system is linear the response  $q(t)$  will also be harmonic with the same angular frequency but (in general) shifted by the phase angle  $\alpha$ :

$$\begin{aligned} q(t) &= \hat{q} \cos(\omega t + \alpha) = \hat{q} \Re\{\cos(\omega t + \alpha) + i \sin(\omega t + \alpha)\} \\ &= \hat{q} \Re\{\exp[i(\omega t + \alpha)]\} = \Re\{\underbrace{\hat{q} \exp(i\alpha)}_{\tilde{q}} \exp(i\omega t)\} = \Re\{\tilde{q} \exp(i\omega t)\} \end{aligned}$$

Here,  $\hat{q}$  and  $\tilde{q}$  are the real and complex amplitudes, respectively. The real amplitude  $\hat{q}$  and the phase angle  $\alpha$  are unknowns; thus, unknown is the complex amplitude  $\tilde{q} = \hat{q}(\cos \alpha + i \sin \alpha)$ .

- Now, one can substitute into the system's equation

$$\begin{aligned} Q(t) &\leftarrow \hat{Q} \exp(i\omega t), \\ q(t) &\leftarrow \tilde{q} \exp(i\omega t), \quad \text{so that} \quad \dot{q}(t) = \tilde{q} i\omega \exp(i\omega t), \quad \ddot{q}(t) = -\tilde{q} \omega^2 \exp(i\omega t) \end{aligned}$$

to easily obtain the following algebraic equation for the unknown complex amplitude  $\tilde{q}$ :

$$[K + i\omega C - \omega^2 M] \tilde{q} = \hat{Q}$$

- For the Rayleigh damping model, where  $C = \beta_K K + \beta_M M$  ( $\beta_K$  and  $\beta_M$  are real constants), this equation can be presented as follows:

$$[\tilde{K} - \omega^2 \tilde{M}] \tilde{q} = \hat{Q}, \quad \text{where} \quad \tilde{K} = K(1 + i\omega \beta_K), \quad \tilde{M} = M\left(1 + \frac{\beta_M}{i\omega}\right)$$

are complex matrices.

- Having computed the complex amplitude  $\tilde{q}$  for the given frequency  $\omega$ , one can finally find the time-harmonic response as the real-part of the complex solution:

$$q(t) = \Re\{\tilde{q} \exp(i\omega t)\} = \hat{q} \cos(\omega t + \alpha), \quad \text{where} \quad \begin{cases} \hat{q} = |\tilde{q}| \\ \alpha = \arg(\tilde{q}) \end{cases}$$

Here,  $|\tilde{q}| = \sqrt{\Re\{\tilde{q}\}^2 + \Im\{\tilde{q}\}^2}$  is the absolute value or modulus of the complex number  $\tilde{q}$ , and  $\arg(\tilde{q}) = \arctan\left(\frac{\Im\{\tilde{q}\}}{\Re\{\tilde{q}\}}\right)$  is called the argument or angle of  $\tilde{q}$ .