

# Design Project #2

ELECENG 2EI4

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L03

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March 5, 2023

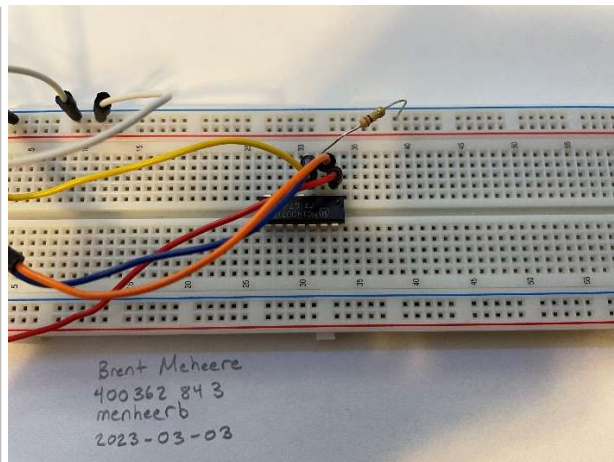
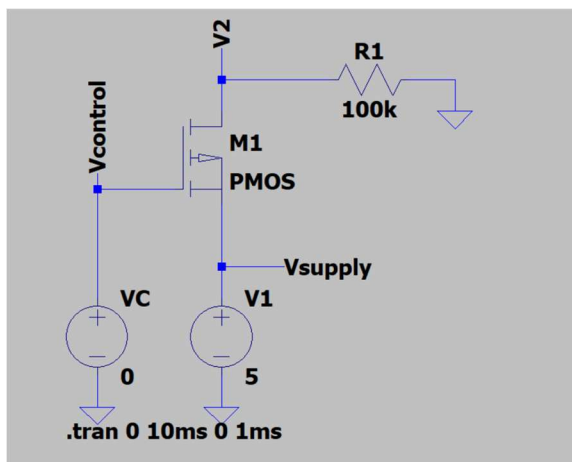
As a future member of the engineering profession, the student is responsible for performing the required work in an honest manner, without plagiarism and cheating. Submitting this work with my name and student number is a statement and understanding that this work is my own and adheres to the Academic Integrity Policy of McMaster University and the Code of Conduct of the Professional Engineers of Ontario. Submitted by [**Brent Menheere, menheerb, 400362843**]

## Test Plan:

In order to test the functionality of the circuits involved in this project and measure the non-idealities associated with switches a test plan needs to be put in place. To test the functionality of the first switch, the OFF state will be tested first. To test the OFF state, the following values need to be set;  $V_{\text{control}} = 5 \text{ V}$  and  $V_{\text{supply}} = 5 \text{ V}$ . The value of  $V_1$  can be measured from  $V_{\text{supply}}$ , which will be  $5 \text{ V}$ , and  $V_2$  will be measured from the output side of the MOSFET connected to the  $100 \text{ k}\Omega$  resistor. The expected measurement of  $V_2$  is  $0 \text{ V}$ . From this state we can test the leakage current by taking the measured value of  $V_2$  over  $100 \text{ k}\Omega$ . To test the ON,  $V_{\text{control}}$  must be changed to  $0 \text{ V}$ . Again,  $V_1$  will be measured from  $V_{\text{supply}}$  and  $V_2$  will be measured from the output side of the MOSFET connected to the  $100 \text{ k}\Omega$  resistor. The expected value of  $V_2$  is  $5 \text{ V}$ . The non-ideality we can measure in this state is  $R_{\text{on}}$ . This can be measured by taking the difference between  $V_1$  and  $V_2$ . If there is a difference between the two that means that there is some sort of resistance within the MOSFET. In this state the function of  $V_2$  following  $V_1$  can be tested by varying the voltage of  $V_1$  and seeing how  $V_2$  responds. A similar testing process can be used when testing the second switch. To measure the functionality of this switch, measurements must be taken at  $V_1$  (supply),  $V_A$ , and  $V_B$ . The first state is  $V_A$  ON. To test this state the following values are set;  $V_{\text{control}} = 0 \text{ V}$  and  $V_{\text{supply}} = 5 \text{ V}$ .  $V_A$  must be around  $5 \text{ V}$  and  $V_B$   $0 \text{ V}$ . To measure the functionality of  $V_B$  ON,  $V_{\text{control}}$  must now be  $5 \text{ V}$ . The expected values of  $V_A$  and  $V_B$  are  $0 \text{ V}$  and  $5 \text{ V}$  respectively. The same non-idealities apply in terms of this switch.

## Switch Type 1:

Circuit Schematic:



Measurements:

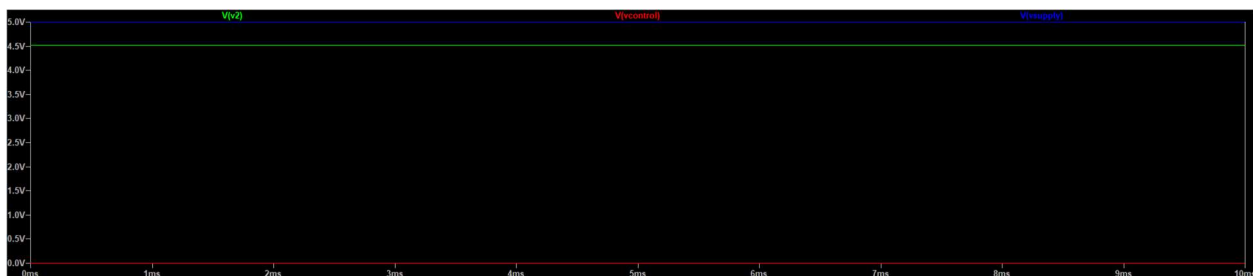


Figure 1  $V_{\text{control}} = 0$ , switch ON

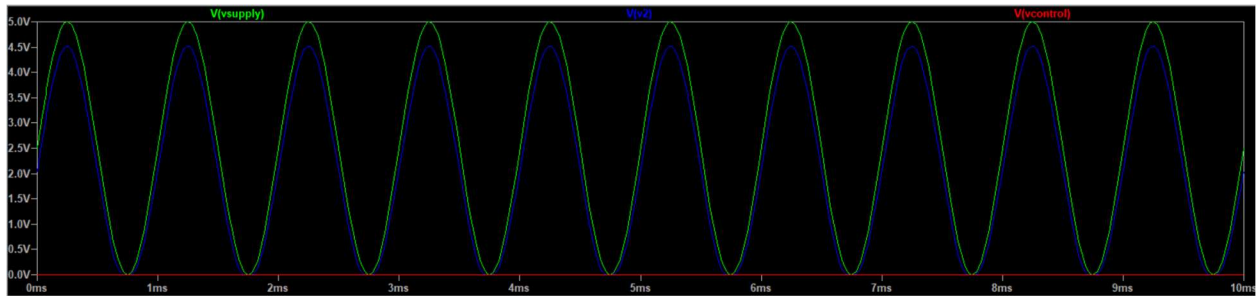


Figure 2 Verifies that V2 follows V1 when ON

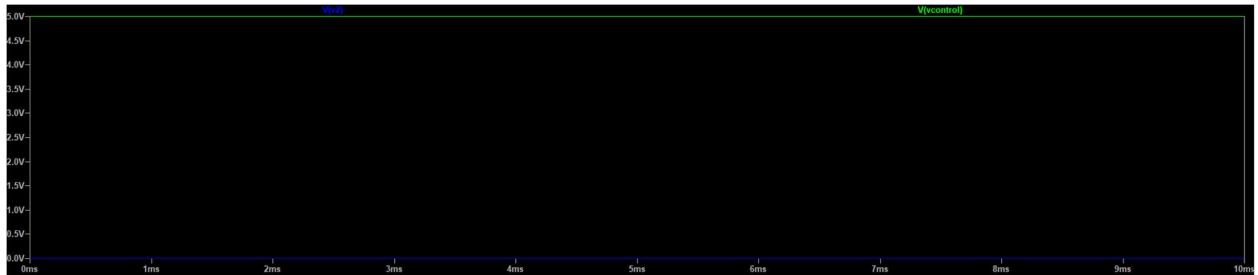


Figure 3 Vcontrol = 5, V2 = 0, switch OFF, Vsupply not shown since it got covered by Vcontrol

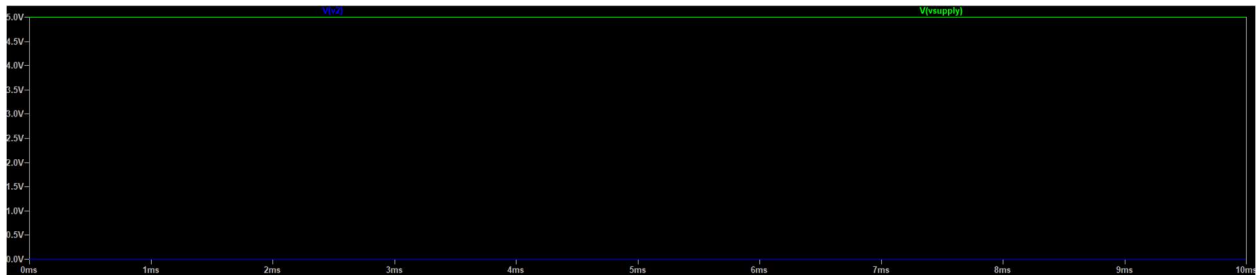


Figure 4 Vsupply = 5, V2 = 0, switch OFF, , Vcontrol not shown since it got covered by Vsupply

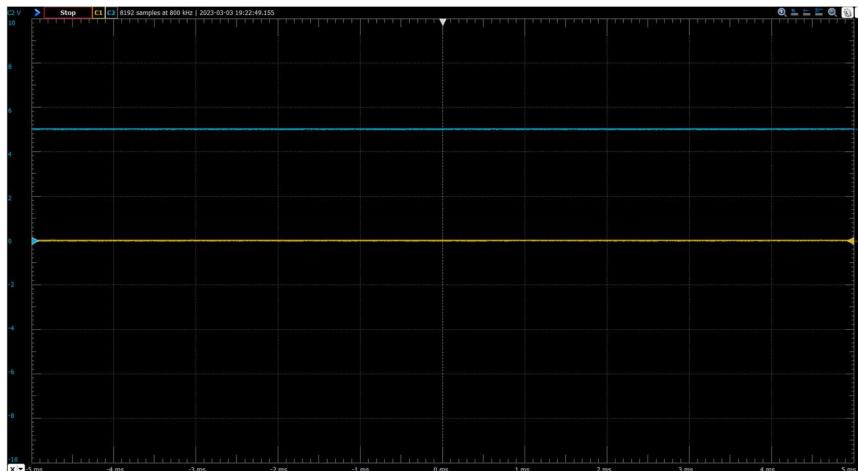


Figure 5 Switch OFF, C1 = V1, C2 = Vcontrol

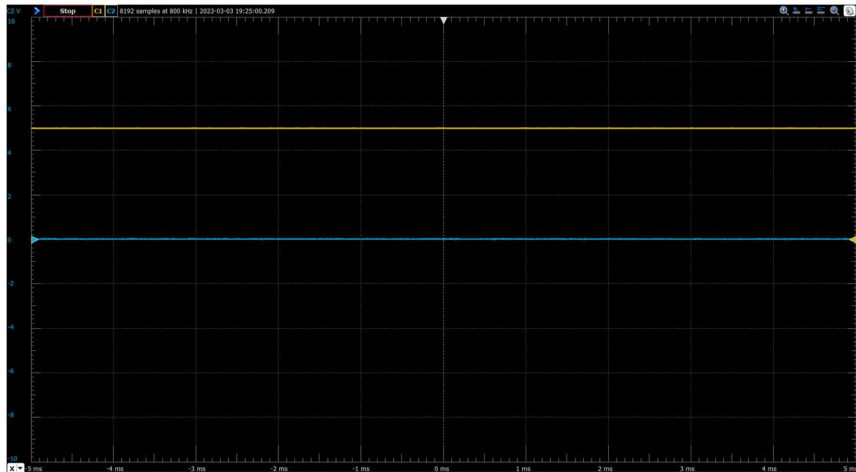


Figure 6 Switch ON,  $C1 = V1$ ,  $C2 = Vcontrol$

OFF:

$$I(\text{leakage}) = V2/R = 0 \text{ A}$$

ON:

$$V1 - V2 = 0.5 \text{ V}$$

Explanation:

The results of the LTSpice simulation are shown in Figures 1 through 4. Figure 1 and 2 show measurements associated with the ON state. From Figure 1 it's evident that  $V_{control}$  was set to zero and  $V_{supply}/V1$  was set to 5 V. In Figure 2,  $V_{supply}/V1$  was set to a varying AC source to test the effects that  $V1$  have on  $V2$ . These two figures verify the functionality of the switch. However, some non-idealities are shown as well. It's clear in both figures that  $V2$  is capped at 4.5 V, which represents that the max voltage this switch can operate at is 4.5 V. Along with this, it is visible in Figure 2 that  $V2$  doesn't exactly follow  $V1$  at all times. This can be related to an internal resistance in the MOSFET or simply a time delay between changes. Figures 3 and 4 show measurements associated with the OFF state. Both figures show the same state and inputs,  $V_{control}$  and  $V_{supply} = 5 \text{ V}$ , however I split them up so that  $V_{control}$  and  $V_{supply}$  would not cover each other. From the figures, when  $V_{control}$  is 5 V the switch is OFF and  $V2$  is measured to be 0 V. From this state, the leakage current can be calculated. Since  $V2$  is zero, there is no leakage current. Finally, in figures 5 and 6, the OFF and ON states are tested on the physical circuit. Unexpectedly, there is no capped output voltage seen, and  $V2$  exactly reflects  $V1$ . This could be because the MOSFET used in the simulation is not the exact MOSFET used in the physical circuit.

NOTE: All non-idealities were calculated with simulated results, I could not produce results for non-idealities on AD2.

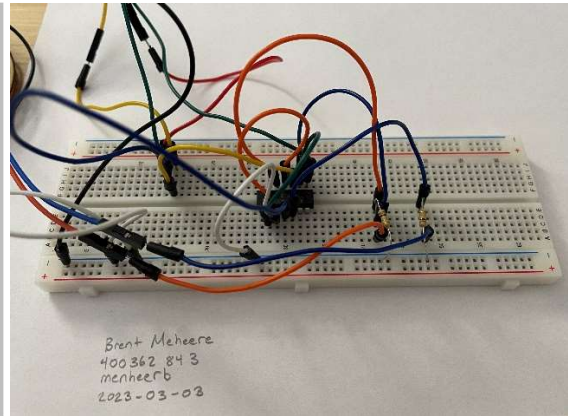
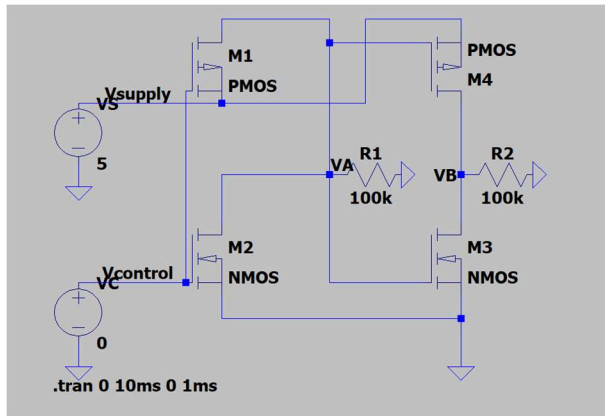
Design Trade-offs:

The design used in switch 1 utilizes the most basic function of a MOSFET. Since MOSFETs have 3 inputs and this switch uses a total of 3 inputs/outputs, there were no trade-offs since it cannot be simpler.

than this. This design is most likely the cheapest and least complex voltage-controlled switch that can be made to meet our needs.

## Switch Type 2:

Circuit Schematic:



Measurements:

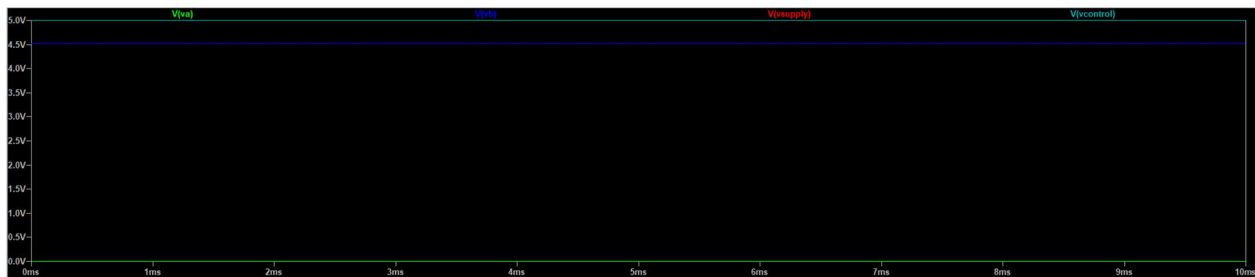


Figure 7 V<sub>control</sub> = 5, V<sub>B</sub> = ON, V<sub>A</sub> = OFF

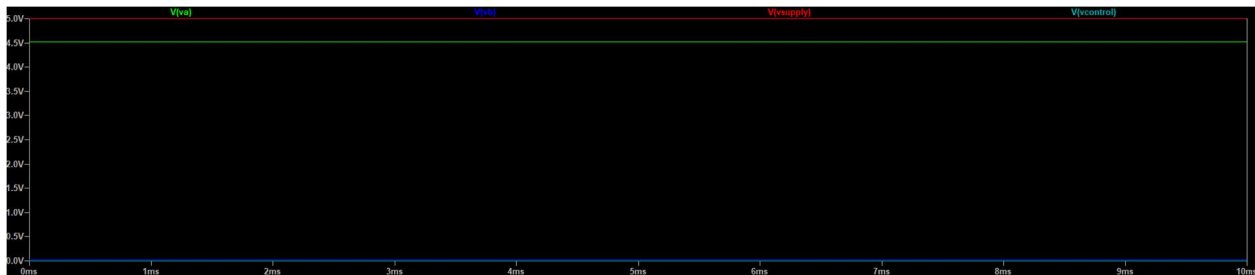


Figure 8 V<sub>control</sub> = 0, V<sub>B</sub> = OFF, V<sub>A</sub> = ON

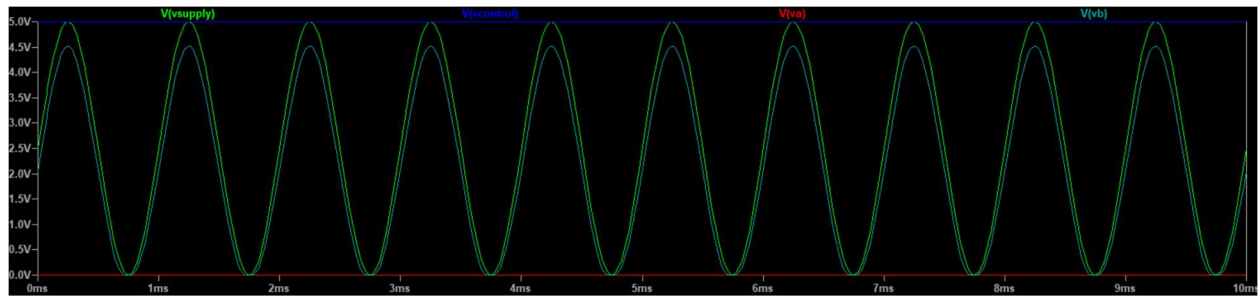


Figure 9 VB ON, VA OFF, Varying V1

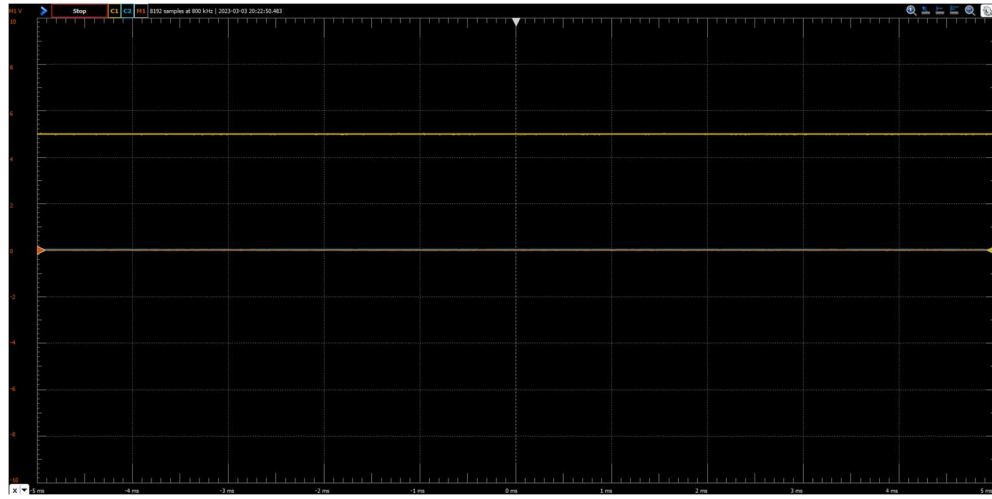


Figure 10 Vcontrol = 0, VB = OFF, VA = ON, C1 = VA, C2 = VB, MATH = Vcontrol

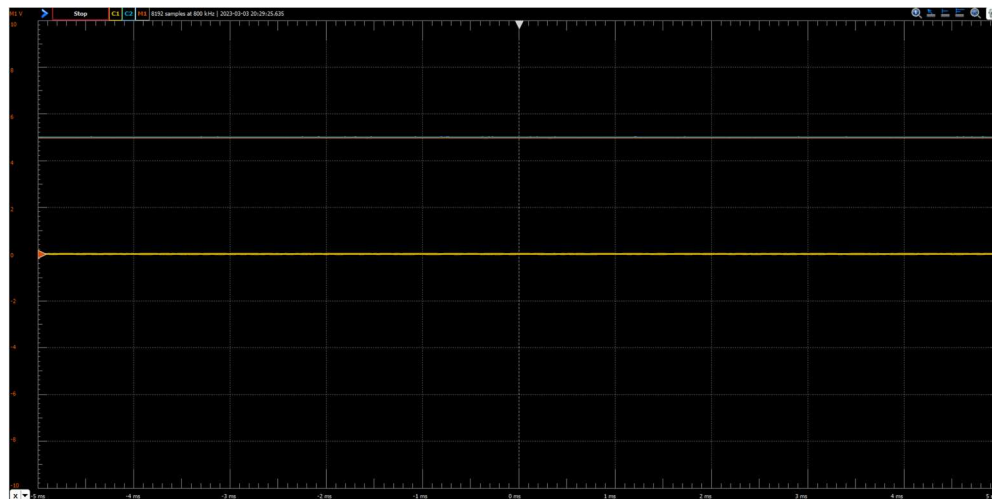


Figure 11 Vcontrol = 5, VB = ON, VA = OFF, C1 = VA, C2 = VB, MATH = Vcontrol

$$I_A(\text{leakage}) = V_A/R_1 = 0 \text{ A}$$

$$I_B(\text{leakage}) = V_B/R_2 = 0 \text{ A}$$

VA ON:

$$V_1 - V_A = 0.5 \text{ V}$$

$V_B = 0 \text{ V}$

VB ON:

$V_1 - V_B = 0.5 \text{ V}$

$V_A = 0$ :

#### Explanation:

Figures 7 and 8 verify the basic functionality of switch 2. When  $V_{\text{control}} = 0$ ,  $V_A$  should reflect  $V_1$ , when  $V_{\text{control}} = 5 \text{ V}$ ,  $V_B$  should reflect  $V_1$ . In both cases,  $V_{\text{supply}}/V_1$  was set to 5 V. Similar to switch 1, to test how the output voltage reflects the input voltage, in Figure 9 I set  $V_{\text{supply}}/V_1$  to a varying AC source and measured how  $V_B$  reacted. Again, the output voltage was capped at 4.5, showing that the max operating voltage is 4.5 V. It is also evident again that either an internal resistance or time delay causes the output voltage to not strictly follow the input voltage. Figures 10 and 11 show the outputs of VA ON, and VB ON implemented onto a physical circuit and measured on the AD2. Again, the expected capped voltage from the simulation was not seen when physically implemented.

NOTE: All non-idealities were calculated with simulated results, I could not produce results for non-idealities on AD2.

#### Design Trade-offs:

The most prevalent design decision for switch 2 was to make it as simple as possible. This design utilizes a total of 4 MOSFETS, 2 voltage sources, and 2 output terminals for measurement. When working with more complex circuits involving many connections and components, keeping things organized is essential for debugging and building purposes. The biggest step to make this circuit as simple as it can be, was to create a clean schematic to minimize error and confusion. To make the schematic easy to follow, the amount of wire and nodes were minimized. Along with this, the components used were minimized as well. The least amount of MOSFETS I could use while maintaining functionality was 4 (2 PMOS and 2 NMOS). If put into production, minimizing the amount of wire and components needed would reduce cost.