

A Linear Technique to Predict Non-Normal Turbulence Applied to a Magnetized Plasma

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In nonlinear dynamical systems with highly nonorthogonal linear eigenvectors, linear non-modal analysis is more useful than normal mode analysis in predicting turbulent properties. However, the non-trivial time evolution of non-modal structures makes quantitative prediction difficult. We present a technique to overcome this difficulty by modelling the effect that the advective nonlinearities have on spatial turbulent structures. The nonlinearities are taken as a periodic randomizing force with period consistent with critical balance arguments. We apply this technique to a model of drift wave turbulence in the Large Plasma Device (LAPD) [W. Geikelman *et al.*, Rev. Sci. Instr. **62**, 2875 (1991)], where non-modal effects dominate the turbulence. We compare the resulting growth rate spectrum to that obtained from a nonlinear simulation, showing good quantitative agreement.

Keywords:

Normal mode analysis – the calculation of eigenvalues and eigenvectors of a linearized dynamical system – has long been used to solve a number of problems ranging from heat conduction along a solid bar to quantum mechanical energy states of atoms. Despite its wide-ranging success, normal mode analysis has failed in important instances, particularly in predicting the onset of subcritical turbulence in hydrodynamic flows. The reason for this failure was not explained until the early 1990’s when Trefethen and others attributed the pitfalls of normal mode analysis to the non-normality of linear operators of dynamical systems [1–3]. A non-normal operator has eigenvectors that are nonorthogonal to one another. One consequence of eigenvector nonorthogonality is that even when all eigenvectors are stable and decay exponentially under linear evolution, superpositions of eigenvectors can grow, albeit transiently. Physically, this means that certain types of fluctuations of the laminar state can access free energy from background gradients even though normal mode fluctuations cannot. When combined with nonlinear effects, this allows for sustained subcritical turbulence. Such behavior is obscured by traditional normal mode analysis, which only effectively describes the long time asymptotic behavior of fluctuations under the action of the linear operator. Transient growth events, which can dominate nonlinear evolution, require initial-value (non-modal) calculations rather than normal mode calculations.

Non-modal analysis has been embraced by the hydrodynamics community over the past two decades in the attempt to explain and predict subcritical turbulence. But the plasma community still heavily relies on normal mode analysis to inform turbulent predictions and observations, with a few notable exceptions [4–6]. Furthermore, non-modal treatments have generally been explanatory rather than predictive and have centered around the transition to turbulence in subcritical systems rather than on properties of fully-developed turbulence. This paper takes up the task of developing a quantitative approach to

predicting turbulent properties using only non-modal linear calculations. Our approach is to evolve the linear solution from an ensemble of random initial conditions and calculate the average growth rate of the solutions over a specified timescale. Optimally this time scale would be the nonlinear decorrelation time of the turbulent system, but in order to enable predictive capability, we employ critical balance arguments to use a characteristic *linear* time. This procedure produces an effective growth rate spectrum that can be used to predict turbulent properties such as saturation levels. While the concepts behind this technique are general enough to be applied to many nonlinear dynamical systems, the details vary for each case, so we restrict our treatment to one particular turbulence model. The technique reproduces the turbulent growth rate spectrum of the direct nonlinear simulation fairly well, especially in comparison to the linear spectrum, which has little bearing on the turbulence.

The model describes pressure-gradient-driven turbulence in the uniformly magnetized, cylindrical plasma produced by the Large Plasma Device (LAPD) [7]. Due to LAPD’s large size and high collisionality, a fluid model is appropriate to describe the turbulence [8–10]. We use a reduced Braginskii [11] 2-fluid model:

$$\partial_t N = -\mathbf{v}_E \cdot \nabla N_0 - N_0 \nabla_{\parallel} v_{\parallel e} + \mu_N \nabla_{\perp}^2 N + S_N + \{\phi, N\}, \quad (1)$$

$$\begin{aligned} \partial_t v_{\parallel e} = & -\frac{m_i}{m_e} \frac{T_{e0}}{N_0} \nabla_{\parallel} N - 1.71 \frac{m_i}{m_e} \nabla_{\parallel} T_e \\ & + \frac{m_i}{m_e} \nabla_{\parallel} \phi - \nu_e v_{\parallel e} + \{\phi, v_{\parallel e}\}, \quad (2) \end{aligned}$$

$$\partial_t \varpi = -N_0 \nabla_{\parallel} v_{\parallel e} - \nu_{in} \varpi + \mu_{\phi} \nabla_{\perp}^2 \varpi + \{\phi, \varpi\}, \quad (3)$$

$$\begin{aligned} \partial_t T_e = & -\mathbf{v}_E \cdot \nabla T_{e0} - 1.71 \frac{2}{3} T_{e0} \nabla_{\parallel} v_{\parallel e} + \frac{2}{3 N_0} \kappa_{\parallel e} \nabla_{\parallel}^2 T_e \\ & - \frac{2 m_e}{m_i} \nu_e T_e + \mu_T \nabla_{\perp}^2 T_e + S_T + \{\phi, T_e\}, \quad (4) \end{aligned}$$

where N is the density, $v_{\parallel e}$ the parallel electron velocity, $\varpi \equiv \nabla_{\perp} \cdot (N_0 \nabla_{\perp} \phi)$ is potential vorticity, and T_e

the electron temperature. The equations employ Bohm normalizations: lengths are normalized to the ion sound gyroradius ρ_s , times to the ion cyclotron time ω_{ci}^{-1} , velocities to the sound speed c_s , densities to the equilibrium peak density, and electron temperatures and potentials to the equilibrium peak electron temperature. The profiles N_0 and T_{e0} and other parameters are all taken from experimental measurements. ϕ_0 does not appear in the equations because we model one particular experiment in which the equilibrium radial electric field and therefore azimuthal flow was reduced to near zero value using a limiter biasing technique [12].

The equations are global and partially linearized. The only nonlinearities retained are the advective nonlinearities, which are written with Poisson brackets. We add artificial diffusion and viscosity terms with small numerical coefficients ($\mu_N, \mu_\phi, \mu_T = 10^{-3}$) to ensure numerical stability in nonlinear simulations, which are performed with the BOUT++ code [13]. We use periodic axial and zero value radial boundary conditions. Further details of the model, including validation studies, may be found in the references [8–10, 14, 15], though we mention here that the model does very well in reproducing the statistical properties of the experimentally-observed turbulence.

The nonlinear simulation reveals a fascinating property of the turbulence – it is dominated by a nonlinear instability process despite being linearly unstable to drift waves [14, 15]. This nonlinear instability process, which was discovered by Drake et al. [16] in a similar plasma model, works as follows: magnetic-field-aligned ($k_{\parallel} = 0$) convective filaments transport density across the equilibrium density gradient, setting up $k_{\parallel} = 0$ density filaments (the same applies to the temperature). These filaments are unstable to a secondary drift wave instability, which grows on the periphery of the filaments. These drift waves, which have finite k_{\parallel} and propagate primarily radially, nonlinearly couple to one another and reinforce the original convective filaments.

Although the instability is called a nonlinear instability, the first part of the mechanism – the transport of background density by the convective filaments – is a linear one. In fact, the other parts of the mechanism are driven by energetically conservative nonlinear interactions, meaning that the convective transport is the only step responsible for energy injection into the fluctuations from the laminar state. Deriving an equation for the evolution of the energy from Eqs. 1-4 [14, 15], we may symbolically write

$$\frac{dE(m, n)}{dt} = Q(m, n) + D(m, n) + \sum_{m', n'} T(m, m', n, n'). \quad (5)$$

In this equation, m and n represent the azimuthal and axial Fourier mode numbers, respectively. Since Eqs. 1-4 are not explicitly dependent on θ and z , the energy

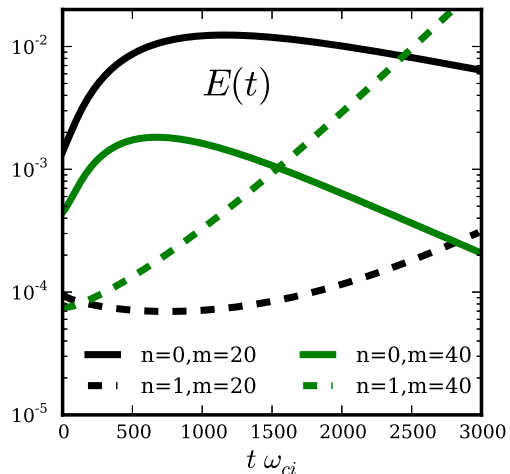


FIG. 1: Linear evolution of energy starting from a turbulent initial state. The $n = 0$ curves have an initial period of transient growth before exponentially decaying.

equation is separable for every m and n . Further, Q represents the linear energy exchange with the equilibrium (convective transport), D the dissipation from irreversible processes like collisions, and T the nonlinear triad wave transfer. Since $\int f\{g, f\}dV = 0$, or equivalently $\sum_{m, m', n, n'} T(m, m', n, n') = 0$, the Poisson bracketed advective nonlinearities in the model are energetically conservative and therefore do not inject or dissipate energy on the whole. Consequently, the fluctuation energy originates completely from Q , the linear convective transport mechanism.

This convective transport of density filaments is akin to the paradigmatic “lift-up” mechanism in hydrodynamic shear flows whereby streamwise vortices drive streamwise streaks [17]. Both are transient growth processes. We see this in our simulations by following the evolution of the energy of several Fourier m, n modes after turning off the nonlinearities in an already turbulent simulation. A few representative m, n modes are shown in Fig. 1. The linear transient growth of the filamentary structures is seen in the $n = 0$ modes, which grow transiently before decaying exponentially at the rate of their least stable eigenmode. This kind of behavior is rather unintuitive to some because all $n = 0$ linear eigenmodes are stable, and the normal mode paradigm has conditioned us to believe that a linear superposition of such eigenmodes should decay. But as the hydrodynamics community discovered, linear superpositions of nonorthogonal vectors may behave unintuitively. Notice now that the $n = 1, m = 20$ mode decays transiently before growing exponentially with growth rate of the most unstable eigenmode at $n = 1, m = 20$. This isn’t quite as interesting as the $n = 0$ behavior, and it can occur in normal

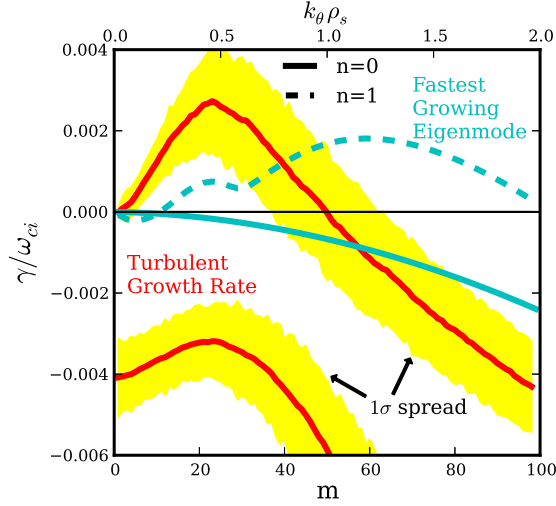


FIG. 2: Linear and turbulent growth rate m spectra for $n = 0$ (solid lines) and $n = 1$ (dashed lines) Fourier components. The linear growth rates are those of the least stable eigenmodes at each m, n , while the turbulent growth rates represent $\frac{\partial E}{\partial t}|_{\text{lin}}/2E$ from the nonlinear simulation. The shaded region marks the 1σ spread in the turbulent growth rate spectrum, obtained from the distribution of growth rates calculated from the nonlinear simulation over a long time range.

systems. Furthermore, it has no parallel in truly subcritical turbulence, but it can be helpful for interpreting later results.

We stress that Fig. 1 is obtained by *linear* evolution from an initial turbulent state. Since the transient growth, which is behind subcritical turbulence, is a purely linear phenomenon, it has long been a goal of researchers to predict the onset of subcritical turbulence using only linear, non-modal calculations. It is our goal, however, to go a step further and use linear calculations to understand and even predict turbulent properties. Such calculations would be much faster and easier to interpret than direct simulations of nonlinear equations. Perhaps one of the most useful statistical properties that we can use to describe the turbulence – and one that is conveniently amenable to linear analysis – is the turbulent growth rate spectrum.

To obtain the turbulent growth rate spectrum from the nonlinear simulation, we begin with the expression $\frac{dE(m,n)}{dt}|_{\text{lin}} = Q(m,n) + D(m,n)$, which accounts for the total net energy injection at each m, n into the fluctuations. An effective instantaneous growth rate $\gamma_{\text{eff}}(m, n, t) = \frac{dE(m,n,t)}{dt}|_{\text{lin}}/2E(m, n, t)$ can then be defined. This effective growth rate is calculated from the spatial structure of the fluctuations, so it is well-defined for both turbulent fluctuations and eigenmode fluctuations. If calculated from a linear simulation run for a sufficiently long time, $\gamma_{\text{eff}}(m, n)$ is the same as the eigenmode growth rate of the least stable linear eigenmode for each m, n . For turbulence, $\gamma_{\text{eff}}(m, n)$ is generally not

equal to an eigenmode growth rate, especially in the case where the system is non-normal. We plot this growth rate in Fig. 2 for $n = 0$ and $n = 1$ components. The turbulent growth rate curves are calculated from this formula, averaged over a time of about $3 \times 10^4 \omega_{ci}^{-1}$ during the saturated turbulent phase of the nonlinear simulation: $\gamma_{\text{Turb}}(m, n) = \int \gamma_{\text{eff}}(m, n, t) dt$. We show this turbulent growth rate along with the 1σ contour, which indicates how greatly $\gamma_{\text{eff}}(m, n, t)$ varies over time. Along with these, the growth rates of the least stable (or most unstable) linear eigenmodes are shown.

As already stated, one sees from Fig. 2 that the linear eigenmodes are unstable for $n = 1$ and stable for $n = 0$ as expected for drift waves. However, the turbulent growth rates are positive for $n = 0, m < 50$ (subcritical-like behavior), but negative for $n = 1$ at all m . There was already a hint of this from the initial behavior of the curves in Fig. 1, but this figure represents quantitative confirmation. Again, the $n = 0$ energy injection is a manifestation of the convective filaments drawing energy from the equilibrium density gradient and depositing this energy into the density fluctuations.

Our goal now is to reproduce the turbulent growth rate curves in Fig. 2 without performing nonlinear simulations. This is difficult because the growth rates depend on turbulent structures, which for non-normal systems, may be very different from eigenmode structures, and which change in time due to transient evolution. It is clear, however, that the turbulent structures at any given time are a result of both linear evolution and nonlinear energy transfer. If we imagine that the nonlinearities randomize the turbulent structures at each wavenumber while the linearities evolve the structures deterministically, we can develop a procedure for choosing proper spatial structures that may be used in calculating effective growth rates.

To elucidate this procedure, we begin by taking Eqs. 1-4 and Fourier decomposing in the azimuthal and axial directions. Then, we discretize in the radial direction ($r \rightarrow r_0, r_1, \dots, r_N$), and approximate radial derivatives with finite differences. The resulting system of equations may be written in matrix form:

$$\mathbf{B}_{m,n} \frac{d\mathbf{v}_{m,n}(t)}{dt} = \mathbf{C}_{m,n} \mathbf{v}_{m,n}(t) - \sum_{m',n'} \mathbf{v}_{E,m-m',n-n'} \cdot \nabla_{\perp} (\mathbf{B}_{m',n'} \mathbf{v}_{m',n'}(t)), \quad (6)$$

where $\mathbf{v}_{m,n} = (N(r), v_{\parallel e}(r), \phi(r), T_e(r))^T_{m,n}$ is the state of the system, and $\mathbf{B}_{m,n}$ and $\mathbf{C}_{m,n}$ are coefficient matrices that include the equilibrium information and finite difference coefficients. The first term on the RHS represents the linearities, and the second term the nonlinearities. The equations for different m and n are separated, although the nonlinearity couples the different m 's and

n 's. In other words, eigenmodes with different m and n are orthogonal and linearly non-interacting. Note that for each m, n , there exist $4 \times N_r$ linearly independent, but nonorthogonal eigenvectors. Hence forth, we drop the m, n subscripts.

In order to use non-modal analysis to calculate growth rates and other measures, one must choose a norm and inner product with which to work. While any choice of inner product is possible, including that which orthogonalizes all eigenvectors, a physically relevant one is generally preferred [3–5]. The most commonly used is an energy inner product. Recall that the inner product of two vectors may be written $\langle \mathbf{x}, \mathbf{y} \rangle = \mathbf{y}^* \mathbf{M} \mathbf{x}$, where $*$ stands for the conjugate transpose, and \mathbf{M} is a positive-definite matrix. \mathbf{M} should be chosen such that $\|\mathbf{v}\| = \sqrt{\langle \mathbf{v}, \mathbf{v} \rangle} = \sqrt{E}$. That is, the norm of the state vector is the square root of the energy. Furthermore, it is often convenient in computations to use the L_2 -norm, $\|\mathbf{u}\|_2 = \sqrt{\sum_i |u_i|^2}$. These requirements can be accomplished through the change of variables $\mathbf{u} = \mathbf{M}^{\frac{1}{2}} \mathbf{v}$. Then the linear portion of Eq. 6 becomes

$$\frac{d\mathbf{u}}{dt} = \mathbf{A} \mathbf{u}, \quad \text{where } \mathbf{A} = \mathbf{M}^{\frac{1}{2}} \mathbf{B}^{-1} \mathbf{C} \mathbf{M}^{-\frac{1}{2}}. \quad (7)$$

The eigenvalues of \mathbf{A} are the same as those of $\mathbf{B}^{-1} \mathbf{C}$ because $\mathbf{M}^{\frac{1}{2}} \mathbf{B}^{-1} \mathbf{C} \mathbf{M}^{-\frac{1}{2}}$ is a similarity transformation.

The solution of Eq. 7 is

$$\mathbf{u}(t) = e^{\mathbf{A}t} \mathbf{u}(0). \quad (8)$$

This solution depends on the initial condition $\mathbf{u}(0)$ in addition to the spectral properties of \mathbf{A} . For purposes of turbulent growth rate prediction, we are interested in the behavior of $\|\mathbf{u}(t)\|$. Therefore, we introduce the growth ratio $G(t)$, which measures the amplification or reduction in the square root of the energy from an initial state:

$$G(t) = \frac{\|\mathbf{u}(t)\|}{\|\mathbf{u}(0)\|} = \frac{\|e^{\mathbf{A}t} \mathbf{u}(0)\|}{\|\mathbf{u}(0)\|}. \quad (9)$$

It can be shown that this growth ratio is bounded from above by $G_{\max}(t) = \|e^{\mathbf{A}t}\|$. Furthermore, $G_{\max}(t) = e^{\gamma_s t}$, where γ_s is the spectral growth rate (the real part of the eigenvalue with largest real part), if and only if \mathbf{A} is normal [3]. Otherwise, $G_{\max}(t) > e^{\gamma_s t}$.

It is common practice in normal mode analysis to look for the least stable eigenmode, the idea being that eventually the fastest growing structure will overcome the others. For the non-modal case, it is common to study the properties of $G_{\max}(t)$, because if $G_{\max}(t) > 1$ at any time, there is a possibility of amplification, even if it is only transient. This allows for the possibility of exciting subcritical turbulence, which is where non-modal analysis is most often applied. However, it can be misleading

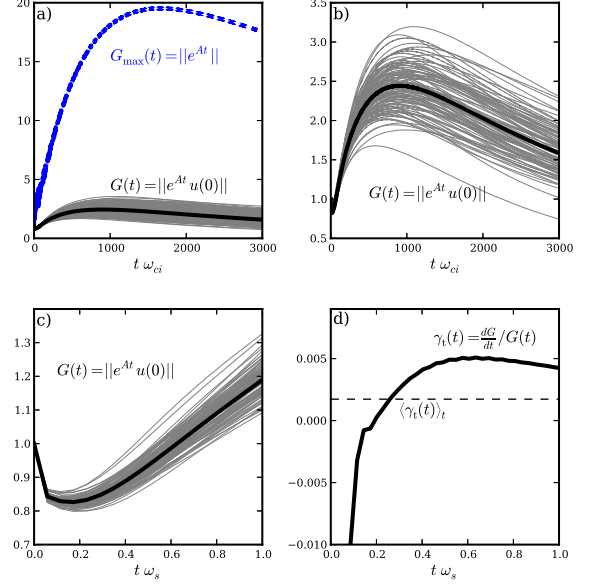


FIG. 3: a) The maximum growth ratio curve $G_{\max}(t)$ (dashed line) for $n = 0, m = 20$, and an ensemble of growth ratio curves (solid gray lines, with the solid black line the ensemble average) that start with a random initial condition $u(0)$ and evolve under the linear operator. b) The ensemble of growth ratio curves alone, and c) cut off at $t = \omega_s^{-1}$, the drift wave eigenmode time scale. d) The instantaneous growth rate of the ensemble averaged growth ratio along with the average value.

to study only $G_{\max}(t)$ when predicting specific properties of turbulence because $G_{\max}(t)$ is only the upper envelope of all possible $G(t)$ curves. No one particular initial condition $\mathbf{u}(0)$ evolves along $G_{\max}(t)$. Furthermore, it isn't obvious what kind of spatial structure or structures will come to dominate a turbulent system. In non-normal systems, unlike in the normal systems, optimal structures don't amplify themselves, rather, they evolve while increasing the total fluctuating energy.

We illustrate $G_{\max}(t)$ along with $G(t)$ for several random initial conditions in Fig. 3 a), all at $n = 0$ and $m = 20$. Despite the fact that all eigenmodes at this wavenumber are stable, there is the possibility for transient amplification by a factor of 20. Furthermore, a sample of randomly initialized vectors are all transiently amplified, but none display optimal growth as compared to $G_{\max}(t)$. We show a zoomed-in view of these randomly initialized curves in Fig. 3 b). It appears extremely unlikely to choose a random initial vector that either optimally amplifies the energy at any time or one that monotonically decays, which would be the case if the initial vector were one of the linear eigenvectors.

Non-modal analysis has likely remained a qualitative endeavor due to the time-dependent growth properties of

initial-value analysis as well as its intrinsic dependence on initial conditions. The key to quantifying non-modal analysis and making it predictive is to successfully model the effect that the nonlinearities have on the transient linear processes. To this effect, we first note that the advective nonlinearity in Eq. 6 has the form of the state vector divided by a time $\tau_{nl} \sim (v_E k_\perp)^{-1}$. This nonlinear time scale is generally associated with the eddy turnover time or the time in which eddies become decorrelated. In light of this, we present a heuristical model of the nonlinearities as a randomizing force that acts on this characteristic nonlinear time scale. Specifically, we start with a random initial condition, let it evolve linearly for a time τ_{nl} , and then re-randomized the system. While the nonlinearities obviously do not affect the system in discrete time steps, this simplification provides a way to use linear non-modal analysis in a predictive manner. In other words, there are certain spatial structures associated with the curves in Fig. 3 b) that change as a function of time. We consider only those structures from $t = 0$ (where the structures are completely random) to $t = \tau_{nl}$, and associate those structures with turbulent structures. These provide us with all we need to characterize the turbulence.

Now, since we do not know *a priori* at what level the turbulence will saturate, we cannot calculate the relative magnitude of τ_{nl} from $(v_E k_\perp)^{-1}$ directly. Thus, we invoke the conjecture of *critical balance*, which posits that the nonlinear time scale equals the linear time scale at all spatial scales [6]. We can then estimate the nonlinear time scale as $\tau_{nl} = \omega_s^{-1}$ – the inverse of the linear frequency (at each m, n). However, $\omega_s = 0$ for $n = 0$ eigenmodes, so we are forced to use ω_s for the fastest growing $n = 1$ eigenmode at each m to get a meaningful time scale. This is not wholly unjustified, however, due to the inherent nonlinear coupling of different modes, which is evident in Eq. 6.

To illustrate our procedure further, we show in Fig. 3 c) the randomly initialized linear evolution curves from start up until a time of ω_s^{-1} . The transient growth is cut off well before optimal amplification occurs, but as reflected by our procedure, there is no guarantee that the nonlinearities will allow complete non-modal amplification. Then, in Fig. 3 d), we calculate the instantaneous growth rate as a function of time of the ensemble averaged curve over that time period. The average of this instantaneous growth rate curve (the dashed line) gives a “Transient Growth Rate.” In Fig. 4, we compare the Transient Growth Rate Spectra (labeled “Trans. ω_s^{-1} ”) to the Turbulent Growth Rate Spectra. The $n = 0$ curves in Fig. 4 a) are fairly similar, especially when compared to the eigenmode spectra. The $n = 1$ curves in Fig. 4 b), on the other hand, are not very similar, although they trend with m in the same way, which is very different from the linear eigenmode trend. The difference between the $n = 1$ transient and turbulent growth rate spectra is

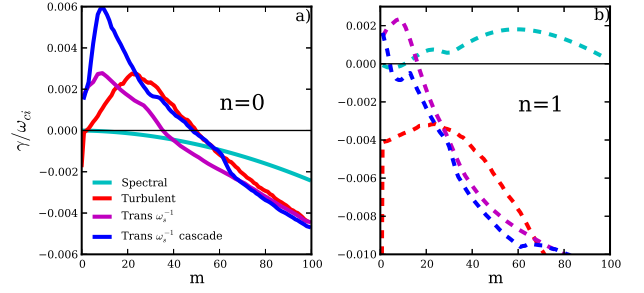


FIG. 4: The linear, turbulent, and transient growth rate spectra. The transient growth rate spectra are calculated by the average growth rate over a time $\omega_s^{-1}(m, n = 1)$ for the ensemble average growth ratio curves with the cascade curve using ω_s^{-1} at $m/2$ rather than m .

due to nonlinear effects not captured by the simple transient calculation procedure. In particular, the nonlinear simulation has a strong energy transfer from $n = 0$ to $n = 1$ Fourier components which is then dissipated by electron-ion collisions as the electrons stream along the field lines [14].

There is one more growth rate curve in Fig. 4, labelled “Trans ω_s^{-1} cascade.” We include this to address the apparent downshift (in m) of the “Trans ω_s^{-1} ” curve in comparison to the turbulent curve. The downshift is another consequence of our oversimplification of the nonlinearity. Specifically, we used ω_s^{-1} at each m for the nonlinear time scale at that same m . As seen in Eq. 6, $v_{m,n}$ is affected by every $\mathbf{v}_{E,m-m',n-n'}k'_\perp$, not by only $\mathbf{v}_{E,m,n}k_\perp$. Since we do not want to overcomplicate matters, we address this by posing a simple forward cascade model for the nonlinearity. That is, $v_{m,n}$ should be most affected by the term with $m' = m/2 \rightarrow m - m' = m/2$, corresponding to eddy mitosis. Then, $\mathbf{v}_{E,m-m',n-n'}k'_\perp \sim \mathbf{v}_{E,m/2}k'_\perp/2 \sim \omega_{s,m/2}^{-1}$, so we use ω_s^{-1} at $m/2$ for the randomizing time scale at m in deriving the “Trans ω_s^{-1} cascade” curves in Fig. 4. The $n = 0$ curve matches well with the $n = 0$ Turbulent Growth Rate curve at $m > 20$, but poorly for $m < 20$, which is expected because the cascade applies only at high m . *A priori*, we cannot determine the minimum m for which the cascade should apply, so this method is simply explanatory.

Nevertheless, our randomizing transient method, which requires only linear calculations, reproduces energetic growth properties of the turbulence that are not captured by eigenmode analysis. Clearly, when the linear systems are highly non-normal, transient growth rate analyses should be performed in place of (or in addition to) linear eigenmode analyses. Furthermore, the transient growth rates should be used in the kinds of predictions that are currently made with eigenmode growth rates. For instance, quasilinear theory uses the most unstable eigenmode growth rate $\gamma_{s,max}$ to predict the tur-

bulent saturation levels through the mixing length formula γ/k_{\perp}^2 . Using this formula with $\gamma_{s,\max} = 0.002$ and $m = 60$, one would predict a turbulent saturation level on the order of 0.1%. On the other hand, using this formula with the transient values $\gamma_{t,\max} = 0.003$, $m = 10$, we predict the saturation level on the order of 10%, which matches the saturation level in the nonlinear simulation.

In summary, non-modal linear calculations are more informative than normal mode calculations when the linear system under consideration is highly non-normal. In the specific case of a low-flow LAPD experiment, a nonlinear instability with linear $k_{\parallel} = 0$ drive dominates the energy dynamics of the turbulence. While this is a surprising result in light of normal mode analysis, it is not at all surprising given the system's non-modal behavior, which we show with a technique that takes into account the effect of the nonlinearities. In general, non-modal initial-value analysis is difficult to quantify and make predictive, but using some simple nonlinear modelling, we have shown that it is possible. Future studies will attempt to improve on the nonlinear modelling and expand the use of this non-modal technique to other non-normal turbulence models.

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